# DRAFT INTERSECTION CONTROL EVALUATION 

(UIHLEIN ROAD AT SR 70)

Florida Department of Transportation<br>District 1<br>SR 70<br>Limits of Project: from Lorraine Road to CR 675/Waterbury Road<br>Manatee County, Florida<br>Financial Management Number: 414506-2<br>ETDM Number: 14263<br>Date: JUNE 2019

The environmental review, consultation, and other actions required by applicable federal environmental laws for this project are being, or have been, carried out by FDOT pursuant to 23 U.S.C. § 327 and a Memorandum of Understanding dated December 14, 2016 and executed by FHWA and FDOT.

## Memorandum

Date: June 24, 2019

To: David C. Turley, PE
FDOT District 1

From: Christopher Benitez, PE, PTOE<br>Stantec Consulting Services, Inc.

Project: $\quad 414506-2$ : SR 70 between Lorraine Road and CR 675
Subject: Intersection Control Evaluation (ICE)
Uihlein Road at SR 70

## Reference: Intersection Control Evaluation (ICE): Uihlein Road at SR 70

The purpose of this memorandum is to document the Florida Department of Transportation (FDOT) Intersection Control Evaluation (ICE) for the intersection of SR 70 and Uihlein Road. This ICE has been completed as part of the FDOT District 1 project: 414506-2 - SR 70 between Lorraine Road to CR 675. The project proposes to increase capacity along SR 70 by widening from a two-lane undivided to a four-lane divided facility along with traffic operational improvements at the intersections. The ICE analysis was initiated during the Project Development \& Environment (PD\&E) phase of the project due to the failing traffic operations during future conditions. According to the project Design Traffic Technical Memorandum (dated October 2018), the intersection of Uihlein Road and SR 70 will operate at Level of Service (LOS) F as a twoway stop-controlled intersection.

An FDOT ICE for the intersection of Uihlein Road and SR 70 was completed for both Stage 1 and Stage 2 for several alternative intersection configurations. Based on an interpretation of the results of the ICE analysis, the roundabout is the recommended option. The analysis included an evaluation of the traffic operations, safety, cost, multimodal accommodations, and other impacts such as environmental, utility, and right of way. The evaluation focused on the SR 70 future build conditions as a four-lane divided facility with a design speed of 55 mph . The results are provided in the Stage 2 ICE Form in Attachment A. The memorandum is organized as follows:

- Attachment A: ICE Stage 2 Form and Results
- Attachment B: Conceptual Plans
- Attachment C: Traffic Operational Analysis
- Attachment D: Safety Performance for Intersection Control Evaluation (SPICE)
- Attachment E: Cost Estimates
- Attachment F: Delay Calculations
- Attachment G: Benefit/Cost Summary
- Attachment H: ICE Stage 1 Form, Capacity Analysis for Planning of Junctions (CAP-X), and Stage 1 SPICE


# ATTACHMENT A FDOT ICE Stage 2 Form and Results 

## Intersection Control Evaluation (ICE) Form

## Stage 2: Intial Control Strategy Assessment

To fulfill the requirements of Stage 2 (Intersection Control Strategy) of FDOT's ICE procedures, complete the following form and append all supporting documentation. Completed forms can be submitted to the District Traffic Operations Engineer (DTOE) and District Design Engineer (DDE) for the project's approval.

| Project Name | SR 70 from Lorraine Rd to CR 675 |  | FDOT Project \# | 414506-2-22-01 |  | Date | 06/25/19 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Submitted By | Nicole Harris, PE |  | ompany | Stantec | Email | nicole. | stantec.com |
| List all viable intersection control strategies identified in Stage 1 (Screening): |  |  |  |  |  |  |  |
| Signalized Control |  | Roundabout |  |  | Displaced Left-Turn |  |  |
| Continuous Green Tee |  |  |  |  |  |  |  |



FDOT ICE: Stage 2

| Safety Performance |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Enter the most recent five (5) years of crash data from the CAR System. |  |  |  | Most recent year of crash data available |  |  | 2018 |
| Crash Type |  | 2014 | 2015 | 2016 | 2017 | 2018 | Total |
| Combined | Total |  |  |  |  |  |  |
|  | Fatal/Injury |  |  |  |  |  |  |
|  | PDO |  |  |  |  |  |  |
| Single-Vehicle | Total | 0 | 1 | 1 | 0 | 2 | 4 |
|  | Fatal/Injury | 0 | 0 | 0 | 0 | 1 | 1 |
|  | PDO | 0 | 1 | 1 | 0 | 1 | 3 |
| Multi-Vehicle | Total | 0 | 0 | 1 | 1 | 2 | 4 |
|  | Fatal/Injury | 0 | 0 | 0 | 1 | 2 | 3 |
|  | PDO | 0 | 0 | 1 | 0 | 0 | 1 |
| Vehicle-Pedestrian | Fatal/Injury | 0 | 0 | 0 | 0 | 0 | 0 |
| Vehicle-Bicycle | Fatal/Injury | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | All | 0 | 1 | 2 | 1 | 4 | 8 |

Apply the FDOT SPICE Tool to model anticipated safety performance of each control strategy. For intersection types not accommodated in the tool, manually apply crash modification factors detailed in the ICE procedures document or qualitatively describe anticipated safety impacts.

| Control Strategy | Onticipated Impact on Safety Performance | Opening Year |  | Design Year |  |
| :--- | :--- | :---: | :---: | :---: | :---: |
|  | Predicted <br> Total <br> Crashes | Predicted <br> Fatal+Injury <br> Crashes | Predicted <br> Total <br> Crashes | Predicted <br> Fatal+Injury <br> Crashes |  |
| Signalized Control | This option is comparable to the Displaced Left-Turn and Continuous <br> Green Tee options. | 5.18 | 1.84 | 12.50 | 3.90 |
| Roundabout | This option has the lowest Predicted Fatal+Injury crashes during both <br> Opening and Design years | 7.00 | 1.23 | 14.82 | 2.98 |
| Displaced Left-Turn | This option is comparable to the Signalized and Continuous Green <br> Tee options. | 4.56 | 1.62 | 11.00 | 3.43 |
| Continuous Green Tee | This option is comparable to the Signalized and Displaced Left-Turn <br> options. | 4.97 | 1.56 | 12.00 | 3.31 |
|  |  |  |  |  |  |


| Costs and Benefit/Cost Ratios |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Remaining cognizant of the current level of detail of each control strategy's conceptual design, provide a cost estimate for each. You may want to include costs for preliminary engineering, required right-of-way acquisitions, construction, and a contingency. Apply the FDOT ICE Tool to determine the delay benefit-cost ratio (B/C), safety B/C, overall B/C, and net-present value for each control stratetgy. |  |  |  |  |  |  |
| Control Strategy | ROW Costs (\$) | Construction Costs (\$) | FDOT ICE Tool Outputs |  |  |  |
|  |  |  | Delay B/C | Safety B/C | Overall B/C | Net Present Value |
| Signalized Control | \$0 | \$2,090,000 | Base | Base | Base | Base |
| Roundabout | \$30,000 | \$1,750,000 | Preferred | Preferred | Preferred | \$11,947,931 |
| Displaced Left-Turn | \$1,820,000 | \$2,390,000 | 1.82 | 1.69 | 3.50 | \$2,012,798 |
| Continuous Green Tee | \$2,150,000 | \$2,150,000 | 50.79 | 26.98 | 77.77 | \$4,606,421 |
|  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |

FDOT ICE: Stage 2


Environmental, Utility, and Right-of-Way Impacts
Summarize any issues related to environmental, utility, or right-of-way (including relocation) impacts specific to each control strategy. Be sure to consider the NEPA requirements for each control type.

| Signalized Control | Improvements are within right-of-way and no new environmental impacts are anticipated. The overhead transmission lines <br> on the north side of the corridor are not expected to be impacted. |
| :--- | :--- |
| Roundabout | Minor right of way needs. No new environmental impacts are anticipated. The overhead transmission lines on the north side <br> of the corridor are not expected to be impacted. |
| Displaced Left-Turn | Right of way acquisition may be needed. There is also potential impacts to the overhead transmission lines on the north <br> side. A driveway/connection will also be impacted. |
| Continuous Green Tee | Improvements are within right-of-way and no new environmental impacts are anticipated. The overhead transmission lines <br> on the north side of the corridor are not expected to be impacted. |
|  |  |


| Public Input/Feedback (if appropriate) |
| :--- |
| Summarize any agency or public input regarding the control strategies: |
| None performed to date. |

FDOT ICE: Stage 2

Control Strategy Evaluation
Provide a brief justification as to why each of the following is either viable or not viable. If a single control strategy is recommended, select it as the only strategy to be advanced.

| Control Strategy | Strategy to be <br> Advanced? |  |
| :---: | :---: | :--- |
| Signalized Control | No | This option was analyzed as the base intersection control. Comparing the B/C, NPV, and traffic <br> operations to other options, this is not the recommended strategy. |
| Roundabout | Yes | 1) Preferred option based on B/C and NPV compared to base; 2) less severe crashes ; 3) traffic <br> operations at LOS C or better; 4) no right of way impacts; and, 5) enhances the livable communities <br> characteristic by lowering vehicle speeds. |
| Displaced Left-Turn | No | This option has the highest costs and potential impacts to utilities. Although, it does have a B/C <br> greater than 1 and a positive NPV which indicates that it is a better than the base option (signalized). |
| Continuous Green Tee | No | This option is the second best option from a B/C and NPV perspective. |
|  | No |  |
|  | No |  |


| Resolution |  |  |  |
| :---: | :---: | :---: | :---: |
| To be filled out by FDOT District Traffic Operations Engineer and District Design Engineer |  |  |  |
| Project Determination |  |  | \% |
| Comments |  |  |  |
| DTOE Name | Signature |  | Date |
| DDE Name | Signature |  | Date |

# ATTACHMENT B <br> Conceptual Plans 

SR 70 and Uihlein Road
Signalized Intersection


## SR 70 and Uihlein Road <br> Roundabout

## Key Features:

- New roundabout with an 2-lanes for both Eastbound and Westbound approachesalong SR 70
- 2-lane for the approach along Uihlein Road including a right-tum bypass la ne
- Inscribed Circle Dia meter (ICD) of a pproximately 190 feet
- Minor right-of-way acquisition
- No impacts anticipated to the overhead transmission lines on noth side of roadway

SR 70 and Uihlein Road Partial Displaced Left-Tum


## SR 70 and Uihlein Road Continuous Green-Tee



## ATTACHMENT C

## Traffic Operational Analysis



|  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |



|  | L | d | $\cdots$ | , | a | k | 4 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | SBL | SBR | SEL | SET | NWU | NWT | NWR |  |
| Lane Configurations | ${ }^{1}$ | 「' | ${ }^{7}$ | 44 | $\dagger$ | 44 | F゙ |  |
| Traffic Volume (veh/h) | 114 | 411 | 698 | 1256 | 0 | 781 | 120 |  |
| Future Volume (veh/h) | 114 | 411 | 698 | 1256 | 0 | 781 | 120 |  |
| Number | 7 | 14 | 1 | 6 |  | 2 | 12 |  |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 |  |  |  | 1.00 |  |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 |  |
| Adj Sat Flow, veh/h/ln | 1863 | 1863 | 1776 | 1776 |  | 1776 | 1776 |  |
| Adj Flow Rate, veh/h | 120 | 433 | 735 | 1322 |  | 822 | 126 |  |
| Adj No. of Lanes | 1 | 1 | 1 | 2 |  | 2 | 1 |  |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 |  | 0.95 | 0.95 |  |
| Percent Heavy Veh, \% | 2 | 2 | 7 | 7 |  | 7 | 7 |  |
| Cap, veh/h | 353 | 843 | 662 | 2253 |  | 904 | 704 |  |
| Arrive On Green | 0.20 | 0.20 | 0.33 | 0.67 |  | 0.27 | 0.27 |  |
| Sat Flow, veh/h | 1774 | 1583 | 1691 | 3463 |  | 3463 | 1509 |  |
| Grp Volume(v), veh/h | 120 | 433 | 735 | 1322 |  | 822 | 126 |  |
| Grp Sat Flow(s),veh/h/ln | 1774 | 1583 | 1691 | 1687 |  | 1687 | 1509 |  |
| Q Serve(g_s), s | 5.2 | 15.9 | 30.0 | 19.3 |  | 21.2 | 4.4 |  |
| Cycle Q Clear(g_c), s | 5.2 | 15.9 | 30.0 | 19.3 |  | 21.2 | 4.4 |  |
| Prop In Lane | 1.00 | 1.00 | 1.00 |  |  |  | 1.00 |  |
| Lane Grp Cap(c), veh/h | 353 | 843 | 662 | 2253 |  | 904 | 704 |  |
| V/C Ratio(X) | 0.34 | 0.51 | 1.11 | 0.59 |  | 0.91 | 0.18 |  |
| Avail Cap(c_a), veh/h | 355 | 844 | 662 | 2253 |  | 904 | 704 |  |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 |  |
| Upstream Filter(l) | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 |  |
| Uniform Delay (d), s/veh | 31.0 | 13.6 | 22.7 | 8.2 |  | 31.9 | 14.0 |  |
| Incr Delay (d2), s/veh | 0.6 | 0.5 | 69.4 | 1.1 |  | 14.7 | 0.6 |  |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| \%ile BackOfQ(50\%),veh/ln | 2.6 | 15.9 | 29.1 | 9.2 |  | 11.7 | 2.6 |  |
| LnGrp Delay(d),s/veh | 31.6 | 14.1 | 92.1 | 9.3 |  | 46.6 | 14.5 |  |
| LnGrp LOS | C | B | F | A |  | D | B |  |
| Approach Vol, veh/h | 553 |  |  | 2057 |  | 948 |  |  |
| Approach Delay, s/veh | 17.9 |  |  | 38.9 |  | 42.3 |  |  |
| Approach LOS | B |  |  | D |  | D |  |  |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| Assigned Phs | 1 | 2 |  | 4 |  | 6 |  |  |
| Phs Duration ( $G+Y+R c$ ), $s$ | 36.0 | 30.1 |  | 23.9 |  | 66.1 |  |  |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ), s | 6.0 | 6.0 |  | 6.0 |  | 6.0 |  |  |
| Max Green Setting (Gmax), s | 30.0 | 24.0 |  | 18.0 |  | 60.0 |  |  |
| Max Q Clear Time (g_c+11), s | 32.0 | 23.2 |  | 17.9 |  | 21.3 |  |  |
| Green Ext Time (p_c), s | 0.0 | 0.5 |  | 0.0 |  | 11.9 |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |
| HCM 2010 Ctrl Delay |  |  | 36.5 |  |  |  |  |  |
| HCM 2010 LOS |  |  | D |  |  |  |  |  |
| Notes |  |  |  |  |  |  |  |  |




Clearance Time (s)

| Vehicle Extension (s) |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: |
| Lane Grp Cap (vph) | 1654 | 795 | 3463 | 2205 |
| V/s Ratio Prot | 0.13 | 00.04 | 0.16 | $c 0.26$ |
| V/s Ratio Perm |  |  |  |  |
| V/c Ratio | 0.13 | 0.18 | 0.16 | 0.41 |
| Uniform Delay, d1 | 0.0 | 28.9 | 0.0 | 8.5 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 0.23 |
| Incremental Delay, d2 | 0.2 | 0.1 | 0.1 | 0.1 |
| Delay (s) | 0.2 | 29.0 | 0.1 | 2.1 |
| Level of Service |  | A | C | A |
| Approach Delay (s) | 0.2 |  |  | A |
| Approach LOS | A |  |  | A |
| (s) |  | A |  |  |


| Intersection Summary |  |  |  |
| :--- | ---: | :--- | ---: |
| HCM 2000 Control Delay | 3.3 | HCM 2000 Level of Service | A |
| HCM 2000 Volume to Capacity ratio | 0.42 |  | 24.0 |
| Actuated Cycle Length (s) | 95.0 | Sum of lost time (s) | A |
| Intersection Capacity Utilization | $37.5 \%$ | ICU Level of Service |  |
| Analysis Period (min) | 15 |  |  |
| ! Phase conflict between lane groups. |  |  |  |

c Critical Lane Group

c Critical Lane Group


Clearance Time (s)

| Vehicle Extension (s) |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: |
| Lane Grp Cap (vph) | 330 | 2092 | 2092 | 281 |
| v/s Ratio Prot | c 0.02 |  |  |  |
| v/s Ratio Perm |  |  |  |  |
| v/c Ratio | 0.11 | 0.42 | 0.28 | 0.03 |
| Uniform Delay, d1 | 30.9 | 7.1 | 6.3 | 30.4 |
| Progression Factor | 0.15 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 0.2 | 0.1 | 0.1 | 0.0 |
| Delay (s) | 4.9 | 7.3 | 6.4 | 30.5 |
| Level of Service | A | A | A | C |
| Approach Delay (s) | 4.9 | 7.3 | 7.9 |  |
| Approach LOS | A | A | A |  |


| Intersection Summary |  |  |  |
| :--- | ---: | :--- | ---: |
| HCM 2000 Control Delay | 7.5 | HCM 2000 Level of Service | A |
| HCM 2000 Volume to Capacity ratio | 0.41 |  | 24.0 |
| Actuated Cycle Length (s) | 95.0 | Sum of lost time (s) | A |
| Intersection Capacity Utilization | $39.0 \%$ | ICU Level of Service |  |
| Analysis Period (min) | 15 |  |  |
| C Critical Lane Group |  |  |  |


|  |  | $\pm$ | $\cdots$ | + | $k$ | 4 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | SBL | SBR | SEL | SET | NWT | NWR |  |
| Lane Configurations |  | F' | ${ }^{7} 1$ | 中4 | 44 |  |  |
| Traffic Volume (vph) | 0 | 128 | 217 | 830 | 549 | 0 |  |
| Future Volume (vph) | 0 | 128 | 217 | 830 | 549 | 0 |  |
| Ideal Flow (vphpl) | 1950 | 1950 | 1950 | 1950 | 1950 | 1950 |  |
| Total Lost time (s) |  | 4.0 | 6.0 | 4.0 | 6.0 |  |  |
| Lane Util. Factor |  | 1.00 | 0.97 | 0.95 | 0.95 |  |  |
| Frt |  | 0.86 | 1.00 | 1.00 | 1.00 |  |  |
| Flt Protected |  | 1.00 | 0.95 | 1.00 | 1.00 |  |  |
| Satd. Flow (prot) |  | 1654 | 3359 | 3463 | 3463 |  |  |
| Flt Permitted |  | 1.00 | 0.95 | 1.00 | 1.00 |  |  |
| Satd. Flow (perm) |  | 1654 | 3359 | 3463 | 3463 |  |  |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |  |
| Adj. Flow (vph) | 0 | 135 | 228 | 874 | 578 | 0 |  |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Lane Group Flow (vph) | 0 | 135 | 228 | 874 | 578 | 0 |  |
| Heavy Vehicles (\%) | 2\% | 2\% | 7\% | 7\% | 7\% | 7\% |  |
| Turn Type |  | custom | Prot | NA | NA |  |  |
| Protected Phases |  | Free! | 1 | Free | $2!$ |  |  |
| Permitted Phases |  |  |  |  |  |  |  |
| Actuated Green, G (s) |  | 95.0 | 25.2 | 95.0 | 32.6 |  |  |
| Effective Green, g (s) |  | 95.0 | 25.2 | 95.0 | 32.6 |  |  |
| Actuated g/C Ratio |  | 1.00 | 0.27 | 1.00 | 0.34 |  |  |
| Clearance Time (s) |  |  | 6.0 |  | 6.0 |  |  |
| Vehicle Extension (s) |  |  | 3.0 |  | 3.0 |  |  |
| Lane Grp Cap (vph) |  | 1654 | 891 | 3463 | 1188 |  |  |
| v/s Ratio Prot |  | 0.08 | 0.07 | 0.25 | c0.17 |  |  |
| v/s Ratio Perm |  |  |  |  |  |  |  |
| v/c Ratio |  | 0.08 | 0.26 | 0.25 | 0.49 |  |  |
| Uniform Delay, d1 |  | 0.0 | 27.5 | 0.0 | 24.6 |  |  |
| Progression Factor |  | 1.00 | 1.00 | 1.00 | 0.71 |  |  |
| Incremental Delay, d2 |  | 0.1 | 0.2 | 0.2 | 1.4 |  |  |
| Delay (s) |  | 0.1 | 27.7 | 0.2 | 18.9 |  |  |
| Level of Service |  | A | C | A | B |  |  |
| Approach Delay (s) | 0.1 |  |  | 5.9 | 18.9 |  |  |
| Approach LOS | A |  |  | A | B |  |  |
| Intersection Summary |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  |  | 9.6 |  | HCM 2000 | evel of Service | A |
| HCM 2000 Volume to Capacity ratio |  |  | 0.42 |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 95.0 |  | Sum of lost | ime (s) | 24.0 |
| Intersection Capacity Utilization |  |  | 30.8\% |  | CU Level o | Service | A |
| Analysis Period (min) |  |  | 15 |  |  |  |  |
| ! Phase conflict between lane groups. |  |  |  |  |  |  |  |
| c Critical Lane Group |  |  |  |  |  |  |  |


c Critical Lane Group


Clearance Time (s)

| Vehicle Extension (s) |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: |
| Lane Grp Cap (vph) | 473 | 1820 | 1820 | 403 |
| V/s Ratio Prot | c0.09 | 0.29 | $c 0.42$ | 0.04 |
| v/s Ratio Perm |  |  |  |  |
| V/c Ratio | 0.32 | 0.49 | 0.72 | 0.14 |
| Uniform Delay, d1 | 26.4 | 11.5 | 14.1 | 25.0 |
| Progression Factor | 0.16 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 0.4 | 0.2 | 1.4 | 0.2 |
| Delay (s) | 4.7 | B | 15.5 | 25.2 |
| Level of Service | A | B | C |  |
| Approach Delay (s) | 4.7 | 11.7 | 16.5 |  |
| Approach LOS | A | B | B |  |


| Intersection Summary |  |  |  |
| :--- | ---: | :--- | ---: |
| HCM 2000 Control Delay | 14.1 | HCM 2000 Level of Service | B |
| HCM 2000 Volume to Capacity ratio | 0.68 |  | 24.0 |
| Actuated Cycle Length (s) | 95.0 | Sum of lost time (s) | B |
| Intersection Capacity Utilization | $55.7 \%$ | ICU Level of Service |  |
| Analysis Period (min) | 15 |  |  |



c Critical Lane Group


Clearance Time (s)

| Vehicle Extension (s) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Lane Grp Cap (vph) | 595 | 1587 | 1587 | 507 |
| v/s Ratio Prot | c0.07 | c0.42 | 0.26 | 0.03 |
| v/s Ratio Perm |  |  |  |  |
| V/c Ratio | 0.20 | 0.83 | 0.52 | 0.09 |
| Uniform Delay, d1 | 20.7 | 19.9 | 15.5 | 19.9 |
| Progression Factor | 0.18 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 0.2 | 3.7 | 0.3 | 0.1 |
| Delay (s) | 3.9 | 23.6 | 15.8 | 19.9 |
| Level of Service | A | C | B | B |
| Approach Delay (s) | 3.9 | 23.6 | 16.4 |  |
| Approach LOS | A | C | B |  |


| Intersection Summary |  |  |  |
| :--- | ---: | :--- | ---: |
| HCM 2000 Control Delay | 19.7 | HCM 2000 Level of Service | B |
| HCM 2000 Volume to Capacity ratio | 0.67 |  | 24.0 |
| Actuated Cycle Length (s) | 95.0 | Sum of lost time (s) | A |
| Intersection Capacity Utilization | $54.4 \%$ | ICU Level of Service |  |
| Analysis Period (min) | 15 |  |  |
| C Critical Lane Group |  |  |  |



c Critical Lane Group

|  | $\downarrow$ | * | * | $\downarrow$ | $\uparrow$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | SBT | SBR2 | NWT | NWR | NEL |  |  |
| Lane Configurations | $\uparrow$ | 7 | $\uparrow \uparrow$ | 7 | 7\% |  |  |
| Traffic Volume (vph) | 44 | 206 | 865 | 43 | 133 |  |  |
| Future Volume (vph) | 44 | 206 | 865 | 43 | 133 |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 |  |  |
| Total Lost time (s) | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 0.95 | 1.00 | 0.97 |  |  |
| Fit | 1.00 | 0.85 | 1.00 | 0.85 | 1.00 |  |  |
| Flt Protected | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 |  |  |
| Satd. Flow (prot) | 1863 | 1583 | 3374 | 1509 | 3273 |  |  |
| Flt Permitted | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 |  |  |
| Satd. Flow (perm) | 1863 | 1583 | 3374 | 1509 | 3273 |  |  |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |  |  |
| Adj. Flow (vph) | 46 | 217 | 911 | 45 | 140 |  |  |
| RTOR Reduction (vph) | 0 | 35 | 0 | 11 | 0 |  |  |
| Lane Group Flow (vph) | 46 | 182 | 911 | 34 | 140 |  |  |
| Heavy Vehicles (\%) | 2\% | 2\% | 7\% | 7\% | 7\% |  |  |
| Turn Type | NA | custom | NA | custom | Prot |  |  |
| Protected Phases | 4 | 41 | 2 | 24 | 1 |  |  |
| Permitted Phases |  |  |  |  |  |  |  |
| Actuated Green, G (s) | 13.1 | 28.3 | 49.7 | 68.8 | 9.2 |  |  |
| Effective Green, g (s) | 13.1 | 28.3 | 49.7 | 68.8 | 9.2 |  |  |
| Actuated g/C Ratio | 0.15 | 0.31 | 0.55 | 0.76 | 0.10 |  |  |
| Clearance Time (s) | 6.0 |  | 6.0 |  | 6.0 |  |  |
| Vehicle Extension (s) | 3.0 |  | 3.0 |  | 3.0 |  |  |
| Lane Grp Cap (vph) | 271 | 497 | 1863 | 1153 | 334 |  |  |
| v/s Ratio Prot | 0.02 | c0.11 | c0.27 | 0.02 | 0.04 |  |  |
| v/s Ratio Perm |  |  |  |  |  |  |  |
| v/c Ratio | 0.17 | 0.37 | 0.49 | 0.03 | 0.42 |  |  |
| Uniform Delay, d1 | 33.7 | 23.9 | 12.4 | 2.6 | 37.9 |  |  |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |
| Incremental Delay, d2 | 0.3 | 0.5 | 0.9 | 0.0 | 0.9 |  |  |
| Delay (s) | 34.0 | 24.4 | 13.3 | 2.6 | 38.7 |  |  |
| Level of Service | C | C | B | A | D |  |  |
| Approach Delay (s) | 26.0 |  | 12.8 |  | 38.7 |  |  |
| Approach LOS | C |  | B |  | D |  |  |
| Intersection Summary |  |  |  |  |  |  |  |
| HCM 2000 Control DelayHCM 2000 Volume to Capacity ratio |  |  | 18.0 |  | HCM 2000 Level of Service | B |  |
|  |  |  | 0.48 |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 90.0 |  | Sum of lost time (s) | 18.0 |  |
| Intersection Capacity Utilization |  |  | 47.2\% |  | ICU Level of Service | A |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |
| C Critical Lane Group |  |  |  |  |  |  |  |


|  | $\downarrow$ | * | * | $\downarrow$ | $\uparrow$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | SBT | SBR2 | NWT | NWR | NEL |  |  |
| Lane Configurations | $\uparrow$ | 7 | $\uparrow \uparrow$ | 7 | 7\% |  |  |
| Traffic Volume (vph) | 35 | 128 | 549 | 37 | 217 |  |  |
| Future Volume (vph) | 35 | 128 | 549 | 37 | 217 |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 |  |  |
| Total Lost time (s) | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |  |  |
| Lane Utill. Factor | 1.00 | 1.00 | 0.95 | 1.00 | 0.97 |  |  |
| Frt | 1.00 | 0.85 | 1.00 | 0.85 | 1.00 |  |  |
| Flt Protected | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 |  |  |
| Satd. Flow (prot) | 1863 | 1583 | 3374 | 1509 | 3273 |  |  |
| Flt Permitted | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 |  |  |
| Satd. Flow (perm) | 1863 | 1583 | 3374 | 1509 | 3273 |  |  |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |  |  |
| Adj. Flow (vph) | 37 | 135 | 578 | 39 | 228 |  |  |
| RTOR Reduction (vph) | 0 | 86 |  | 10 | 0 |  |  |
| Lane Group Flow (vph) | 37 | 49 | 578 | 29 | 228 |  |  |
| Heavy Vehicles (\%) | 2\% | 2\% | 7\% | 7\% | 7\% |  |  |
| Turn Type | NA | custom | NA | custom | Prot |  |  |
| Protected Phases | 4 | 41 | 2 | 24 | 1 |  |  |
| Permitted Phases |  |  |  |  |  |  |  |
| Actuated Green, G (s) | 7.5 | 25.1 | 52.9 | 66.4 | 11.6 |  |  |
| Effective Green, g (s) | 7.5 | 25.1 | 52.9 | 66.4 | 11.6 |  |  |
| Actuated g/C Ratio | 0.08 | 0.28 | 0.59 | 0.74 | 0.13 |  |  |
| Clearance Time (s) | 6.0 |  | 6.0 |  | 6.0 |  |  |
| Vehicle Extension (s) | 3.0 |  | 3.0 |  | 3.0 |  |  |
| Lane Grp Cap (vph) | 155 | 441 | 1983 | 1113 | 421 |  |  |
| v/s Ratio Prot | c0.02 | 0.03 | c0.17 | 0.02 | c0.07 |  |  |
| v/s Ratio Perm |  |  |  |  |  |  |  |
| v/c Ratio | 0.24 | 0.11 | 0.29 | 0.03 | 0.54 |  |  |
| Uniform Delay, d1 | 38.6 | 24.2 | 9.2 | 3.2 | 36.7 |  |  |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |
| Incremental Delay, d2 | 0.8 | 0.1 | 0.4 | 0.0 | 1.4 |  |  |
| Delay (s) | 39.4 | 24.3 | 9.6 | 3.2 | 38.1 |  |  |
| Level of Service | D | C | A | A | D |  |  |
| Approach Delay (s) | 27.5 |  | 9.2 |  | 38.1 |  |  |
| Approach LOS | C |  | A |  | D |  |  |
| Intersection Summary |  |  |  |  |  |  |  |
| HCM 2000 Control DelayHCM 2000 Volume to Capacity ratio |  |  | 18.8 |  | HCM 2000 Level of Service | B |  |
|  |  |  | 0.33 |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 90.0 |  | Sum of lost time (s) | 18.0 |  |
| Intersection Capacity Utilization |  |  | 40.5\% |  | ICU Level of Service | A |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |
| C Critical Lane Group |  |  |  |  |  |  |  |


|  | $\downarrow$ | * | k | $\downarrow$ | $\uparrow$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | SBT | SBR2 | NWT | NWR | NEL |  |  |
| Lane Configurations | $\uparrow$ | 7 | $\uparrow \uparrow$ | 7 | 7\% |  |  |
| Traffic Volume (vph) | 142 | 663 | 1242 | 137 | 430 |  |  |
| Future Volume (vph) | 142 | 663 | 1242 | 137 | 430 |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 |  |  |
| Total Lost time (s) | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 0.95 | 1.00 | 0.97 |  |  |
| Fit | 1.00 | 0.85 | 1.00 | 0.85 | 1.00 |  |  |
| Flt Protected | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 |  |  |
| Satd. Flow (prot) | 1863 | 1583 | 3374 | 1509 | 3273 |  |  |
| Flt Permitted | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 |  |  |
| Satd. Flow (perm) | 1863 | 1583 | 3374 | 1509 | 3273 |  |  |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |  |  |
| Adj. Flow (vph) | 149 | 698 | 1307 | 144 | 453 |  |  |
| RTOR Reduction (vph) | 0 | 19 | 0 | 17 | 0 |  |  |
| Lane Group Flow (vph) | 149 | 679 | 1307 | 127 | 453 |  |  |
| Heavy Vehicles (\%) | 2\% | 2\% | 7\% | 7\% | 7\% |  |  |
| Turn Type | NA | custom | NA | custom | Prot |  |  |
| Protected Phases | 4 | 41 | 2 | 24 | 1 |  |  |
| Permitted Phases |  |  |  |  |  |  |  |
| Actuated Green, G (s) | 18.0 | 41.8 | 36.2 | 60.2 | 17.8 |  |  |
| Effective Green, g (s) | 18.0 | 41.8 | 36.2 | 60.2 | 17.8 |  |  |
| Actuated g/C Ratio | 0.20 | 0.46 | 0.40 | 0.67 | 0.20 |  |  |
| Clearance Time (s) | 6.0 |  | 6.0 |  | 6.0 |  |  |
| Vehicle Extension (s) | 3.0 |  | 3.0 |  | 3.0 |  |  |
| Lane Grp Cap (vph) | 372 | 735 | 1357 | 1009 | 647 |  |  |
| v/s Ratio Prot | 0.08 | c0.43 | c0.39 | 0.08 | 0.14 |  |  |
| v/s Ratio Perm |  |  |  |  |  |  |  |
| v/c Ratio | 0.40 | 0.92 | 0.96 | 0.13 | 0.70 |  |  |
| Uniform Delay, d1 | 31.3 | 22.6 | 26.2 | 5.4 | 33.6 |  |  |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |
| Incremental Delay, d2 | 0.7 | 17.2 | 17.1 | 0.1 | 3.4 |  |  |
| Delay (s) | 32.0 | 39.8 | 43.3 | 5.4 | 37.0 |  |  |
| Level of Service | C | D | D | A | D |  |  |
| Approach Delay (s) | 38.4 |  | 39.6 |  | 37.0 |  |  |
| Approach LOS | D |  | D |  | D |  |  |
| Intersection Summary |  |  |  |  |  |  |  |
| HCM 2000 Control DelayHCM 2000 Volume to Capacity ratio |  |  | 38.8 |  | HCM 2000 Level of Service | D |  |
|  |  |  | 1.02 |  |  |  |  |
| HCM 2000 Volume to Capacity ratio |  |  | 90.0 |  | Sum of lost time (s) | 18.0 |  |
| Intersection Capacity Utilization |  |  | 85.4\% |  | ICU Level of Service | E |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |
| C Critical Lane Group |  |  |  |  |  |  |  |


|  | $\downarrow$ | * | k | $\downarrow$ | $\uparrow$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | SBT | SBR2 | NWT | NWR | NEL |  |  |
| Lane Configurations | $\uparrow$ | 7 | $\uparrow \uparrow$ | 7 | 71 |  |  |
| Traffic Volume (vph) | 114 | 411 | 781 | 120 | 698 |  |  |
| Future Volume (vph) | 114 | 411 | 781 | 120 | 698 |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 |  |  |
| Total Lost time (s) | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 0.95 | 1.00 | 0.97 |  |  |
| Fit | 1.00 | 0.85 | 1.00 | 0.85 | 1.00 |  |  |
| Flt Protected | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 |  |  |
| Satd. Flow (prot) | 1863 | 1583 | 3374 | 1509 | 3273 |  |  |
| Flt Permitted | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 |  |  |
| Satd. Flow (perm) | 1863 | 1583 | 3374 | 1509 | 3273 |  |  |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |  |  |
| Adj. Flow (vph) | 120 | 433 | 822 | 126 | 735 |  |  |
| RTOR Reduction (vph) | 0 | 17 | 0 | 14 | 0 |  |  |
| Lane Group Flow (vph) | 120 | 416 | 822 | 112 | 735 |  |  |
| Heavy Vehicles (\%) | 2\% | 2\% | 7\% | 7\% | 7\% |  |  |
| Turn Type | NA | custom | NA | custom | Prot |  |  |
| Protected Phases | 4 | 41 | 2 | 24 | 1 |  |  |
| Permitted Phases |  |  |  |  |  |  |  |
| Actuated Green, G (s) | 17.3 | 47.3 | 30.7 | 54.0 | 24.0 |  |  |
| Effective Green, g (s) | 17.3 | 47.3 | 30.7 | 54.0 | 24.0 |  |  |
| Actuated g/C Ratio | 0.19 | 0.53 | 0.34 | 0.60 | 0.27 |  |  |
| Clearance Time (s) | 6.0 |  | 6.0 |  | 6.0 |  |  |
| Vehicle Extension (s) | 3.0 |  | 3.0 |  | 3.0 |  |  |
| Lane Grp Cap (vph) | 358 | 831 | 1150 | 905 | 872 |  |  |
| v/s Ratio Prot | 0.06 | c0.26 | c0.24 | 0.07 | c0.22 |  |  |
| v/s Ratio Perm |  |  |  |  |  |  |  |
| v/c Ratio | 0.34 | 0.50 | 0.71 | 0.12 | 0.84 |  |  |
| Uniform Delay, d1 | 31.4 | 13.7 | 25.8 | 7.8 | 31.2 |  |  |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |
| Incremental Delay, d2 | 0.6 | 0.5 | 3.8 | 0.1 | 7.5 |  |  |
| Delay (s) | 31.9 | 14.2 | 29.6 | 7.8 | 38.7 |  |  |
| Level of Service | C | B | C | A | D |  |  |
| Approach Delay (s) | 18.1 |  | 26.7 |  | 38.7 |  |  |
| Approach LOS | B |  | C |  | D |  |  |
| Intersection Summary |  |  |  |  |  |  |  |
| HCM 2000 Control DelayHCM 2000 Volume to Capacity ratio |  |  | 28.5 |  | HCM 2000 Level of Service | C |  |
|  |  |  | 0.73 |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 90.0 |  | Sum of lost time (s) | 18.0 |  |
| Intersection Capacity Utilization |  |  | 62.5\% |  | CU Level of Service | B |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |
| C Critical Lane Group |  |  |  |  |  |  |  |

SR 70 @ UIHLEIN RD ROUNDABOUT ANALYSIS

| 2025 OPENING YEAR (HCM 6th Edition) |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach | Delay (s) |  | Level of Service |  | v/c Ratio |  | 95th \% Queue (ft) |  |
|  | AM | PM | AM | PM | AM | PM | AM | PM |
| Overall | 5.8 | 6.2 | A | A |  |  |  |  |
| SR 70 EB | 5.3 | 7.1 | A | A | 0.28 | 0.43 | 35 | 65 |
| SR 70 WB | 7.3 | 6.2 | A | A | 0.41 | 0.29 | 60 | 35 |
| Uihlein Rd SB | 1.2 | 1.0 | A | A | 0.13 | 0.08 | 25 | 25 |


| 2025 OPENING YEAR (Sidra Standard) |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach | Delay (s) |  | Level of Service |  | v/c Ratio |  | 95th \% Queue (ft) |  |
|  | AM | PM | AM | PM | AM | PM | AM | PM |
| Overall | 4.6 | 4.8 | A | A |  |  |  |  |
| SR 70 EB | 4.7 | 4.8 | A | A | 0.25 | 0.38 | 45 | 75 |
| SR 70 WB | 4.4 | 4.7 | A | A | 0.36 | 0.25 | 65 | 40 |
| Uihlein Rd SB | 5.0 | 5.2 | A | A | 0.13 | 0.08 | 25 | 25 |


| 2045 DESIGN YEAR (HCM 6th Edition) |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach | Delay (s) |  | Level of Service |  | v/c Ratio |  | 95th \% Queue (ft) |  |  |  |
|  | AM | PM | AM | PM | AM | PM | AM | PM |  |  |
|  | $\mathbf{1 5 . 2}$ | $\mathbf{1 9 . 6}$ | C | C |  |  |  |  |  |  |
| SR 70 EB | 10.3 | 23.0 | B | C | 0.58 | 0.87 | 105 | 585 |  |  |
| SR 70 WB | 27.1 | 22.7 | D | C | 0.85 | 0.73 | 435 | 180 |  |  |
| Uihlein Rd SB | 2.7 | 1.7 | A | A | 0.43 | 0.26 | 35 | 25 |  |  |


| 2045 DESIGN YEAR (Sidra Standard) |  |  |  |  |  |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach | Delay (s) |  | Level of Service |  | v/c Ratio |  | 95th \% Queue (ft) |  |  |  |  |
|  | AM | PM | AM | PM | AM | PM | AM | PM |  |  |  |
| Overall | 7.9 | $\mathbf{8 . 9}$ | A | A |  |  |  |  |  |  |  |
| SR 70 EB | 6.5 | 7.1 | A | A | 0.52 | 0.76 | 125 | 280 |  |  |  |
| SR 70 WB | 10.6 | 14.8 | B | B | 0.72 | 0.67 | 255 | 230 |  |  |  |
| Uihlein Rd SB | 5.5 | 5.4 | A | A | 0.43 | 0.26 | 40 | 25 |  |  |  |

## SITE LAYOUT

- Site: [SR 70 \& Uihlein Rd]

Site Category: (None)
Roundabout


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Organisation: STANTEC | Created: Tuesday, June 11, 2019 8:51:38 AM
Project: C:IProjects\SR 70ISR70_uihlein_2025_2045_am_pm_hcm6.sip8

## MOVEMENT SUMMARY

## Site: [SR 70 \& Uihlein Rd]

2025 AM Peak-Hour
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | Turn | Deman Total veh/h | $\begin{aligned} & \text { lows } \\ & \text { HV } \\ & \% \end{aligned}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance ft | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed mph |
| East: SR 70 |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | T1 | 911 | 7.0 | 0.413 | 7.3 | LOS A | 2.2 | 58.2 | 0.38 | 0.24 | 0.38 | 34.5 |
| 12 | R2 | 45 | 7.0 | 0.413 | 7.3 | LOS A | 2.2 | 58.2 | 0.38 | 0.24 | 0.38 | 33.2 |
| Appro |  | 956 | 7.0 | 0.413 | 7.3 | LOS A | 2.2 | 58.2 | 0.38 | 0.24 | 0.38 | 34.4 |
| North: Uihlein Rd |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 46 | 2.0 | 0.076 | 6.8 | LOS A | 0.3 | 6.4 | 0.59 | 0.59 | 0.59 | 32.1 |
| 18 | R2 | 217 | 2.0 | 0.132 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 37.7 |
| Approach |  | 263 | 2.0 | 0.132 | 1.2 | LOS A | 0.3 | 6.4 | 0.10 | 0.10 | 0.10 | 36.5 |
| West: SR 70 |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 140 | 7.0 | 0.279 | 5.3 | LOS A | 1.3 | 35.3 | 0.17 | 0.07 | 0.17 | 34.4 |
|  | T1 | 571 | 7.0 | 0.279 | 5.3 | LOS A | 1.3 | 35.3 | 0.17 | 0.07 | 0.17 | 35.2 |
| Approach |  | 711 | 7.0 | 0.279 | 5.3 | LOS A | 1.3 | 35.3 | 0.17 | 0.07 | 0.17 | 35.0 |
| All Vehicles |  | 1929 | 6.3 | 0.413 | 5.8 | LOS A | 2.2 | 58.2 | 0.26 | 0.16 | 0.26 | 34.9 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: Same as Sign Control.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement. LOS F will result if v/c>1 irrespective of movement delay value (does not apply for approaches and intersection). Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010). Roundabout Capacity Model: US HCM 6.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: Traditional M1.
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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Organisation: STANTEC | Processed: Tuesday, June 11, 2019 7:58:37 AM
Project: C:IProjectsISR 70ISR70_uihlein_2025_2045_am_pm_hcm6.sip8

## MOVEMENT SUMMARY

## Site: [SR 70 \& Uihlein Rd]

2025 AM Peak-Hour
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \mathrm{Mov} \\ & \mathrm{ID} \end{aligned}$ |  | Deman Total veh/h | $\begin{gathered} \text { lows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | f Queue Distance ft | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed mph |
| East: SR 70 |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | T1 | 911 | 7.0 | 0.356 | 4.4 | LOS A | 2.4 | 62.8 | 0.39 | 0.43 | 0.39 | 37.2 |
| 12 | R2 | 45 | 7.0 | 0.356 | 4.6 | LOS A | 2.4 | 62.8 | 0.37 | 0.42 | 0.37 | 35.8 |
| Appr |  | 956 | 7.0 | 0.356 | 4.4 | LOS A | 2.4 | 62.8 | 0.39 | 0.43 | 0.39 | 37.1 |
| North: Uihlein Rd |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 46 | 2.0 | 0.063 | 12.8 | LOS B | 0.2 | 6.3 | 0.58 | 0.80 | 0.58 | 33.9 |
| 18 | R2 | 217 | 2.0 | 0.132 | 3.4 | LOS A | 0.0 | 0.0 | 0.00 | 0.41 | 0.00 | 37.7 |
| Approach |  | 263 | 2.0 | 0.132 | 5.0 | LOS A | 0.2 | 6.3 | 0.10 | 0.48 | 0.10 | 36.9 |
| West: SR 70 |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 140 | 7.0 | 0.245 | 10.3 | LOS B | 1.6 | 42.9 | 0.22 | 0.49 | 0.22 | 36.6 |
|  | T1 | 571 | 7.0 | 0.245 | 3.4 | LOS A | 1.7 | 43.9 | 0.21 | 0.38 | 0.21 | 37.6 |
| Approach |  | 711 | 7.0 | 0.245 | 4.7 | LOS A | 1.7 | 43.9 | 0.21 | 0.40 | 0.21 | 37.4 |
| All Vehicles |  | 1929 | 6.3 | 0.356 | 4.6 | LOS A | 2.4 | 62.8 | 0.28 | 0.43 | 0.28 | 37.2 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement. LOS F will result if v/c>1 irrespective of movement delay value (does not apply for approaches and intersection). Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010). Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

Site: [SR 70 \& Uihlein Rd]
2025 PM Peak-Hour
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ |  | Deman Total veh/h | $\begin{aligned} & \text { lows } \\ & \text { HV } \\ & \% \\ & \hline \end{aligned}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance ft | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed mph |
| East: SR 70 |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | T1 | 578 | 7.0 | 0.290 | 6.2 | LOS A | 1.3 | 34.3 | 0.42 | 0.30 | 0.42 | 35.1 |
| 12 | R2 | 39 | 7.0 | 0.290 | 6.2 | LOS A | 1.3 | 34.3 | 0.42 | 0.30 | 0.42 | 33.7 |
| Appr |  | 617 | 7.0 | 0.290 | 6.2 | LOS A | 1.3 | 34.3 | 0.42 | 0.30 | 0.42 | 35.0 |
| North: Uihlein Rd |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 37 | 2.0 | 0.045 | 4.8 | LOS A | 0.2 | 3.9 | 0.49 | 0.41 | 0.49 | 33.0 |
| 18 | R2 | 135 | 2.0 | 0.082 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 37.7 |
| Approach |  | 172 | 2.0 | 0.082 | 1.0 | LOS A | 0.2 | 3.9 | 0.11 | 0.09 | 0.11 | 36.5 |
| West: SR 70 |  |  |  |  |  |  |  |  |  |  |  |  |
| 18 | L2 | 228 | 7.0 | 0.430 | 7.1 | LOS A | 2.5 | 66.5 | 0.18 | 0.07 | 0.18 | 33.5 |
|  | T1 | 874 | 7.0 | 0.430 | 7.1 | LOS A | 2.5 | 66.5 | 0.18 | 0.07 | 0.18 | 34.2 |
| Approach |  | 1102 | 7.0 | 0.430 | 7.1 | LOS A | 2.5 | 66.5 | 0.18 | 0.07 | 0.18 | 34.1 |
| All Vehicles |  | 1891 | 6.5 | 0.430 | 6.2 | LOS A | 2.5 | 66.5 | 0.25 | 0.15 | 0.25 | 34.6 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: Same as Sign Control.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement. LOS F will result if v/c>1 irrespective of movement delay value (does not apply for approaches and intersection). Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010). Roundabout Capacity Model: US HCM 6.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: Traditional M1.
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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Project: C:IProjects\SR 70ISR70_uihlein_2025_2045_am_pm_hcm6.sip8

## MOVEMENT SUMMARY

Site: [SR 70 \& Uihlein Rd]
2025 PM Peak-Hour
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | Turn | Deman Total veh/h | $\begin{gathered} \text { lows } \\ \text { HV } \\ \% \\ \hline \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance ft | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed mph |
| East: SR 70 |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | T1 | 578 | 7.0 | 0.246 | 4.7 | LOS A | 1.5 | 39.2 | 0.44 | 0.47 | 0.44 | 37.0 |
| 12 | R2 | 39 | 7.0 | 0.246 | 4.9 | LOS A | 1.5 | 39.2 | 0.43 | 0.45 | 0.43 | 35.6 |
| Appro |  | 617 | 7.0 | 0.246 | 4.7 | LOS A | 1.5 | 39.2 | 0.44 | 0.46 | 0.44 | 36.9 |
| North: Uihlein Rd |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 37 | 2.0 | 0.043 | 11.9 | LOS B | 0.2 | 4.2 | 0.50 | 0.72 | 0.50 | 34.1 |
| 18 | R2 | 135 | 2.0 | 0.082 | 3.4 | LOS A | 0.0 | 0.0 | 0.00 | 0.41 | 0.00 | 37.7 |
| Approach |  | 172 | 2.0 | 0.082 | 5.2 | LOS A | 0.2 | 4.2 | 0.11 | 0.48 | 0.11 | 36.8 |
| West: SR 70 |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 228 | 7.0 | 0.376 | 10.3 | LOS B | 2.9 | 75.7 | 0.22 | 0.49 | 0.22 | 36.5 |
|  | T1 | 874 | 7.0 | 0.376 | 3.4 | LOS A | 2.9 | 76.6 | 0.21 | 0.38 | 0.21 | 37.5 |
| Approach |  | 1102 | 7.0 | 0.376 | 4.8 | LOS A | 2.9 | 76.6 | 0.21 | 0.40 | 0.21 | 37.3 |
| All Vehicles |  | 1891 | 6.5 | 0.376 | 4.8 | LOS A | 2.9 | 76.6 | 0.28 | 0.43 | 0.28 | 37.1 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement. LOS F will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

Site: [SR 70 \& Uihlein Rd]
2045 AM Peak-Hour
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ |  | Deman Total veh/h | $\begin{aligned} & \text { lows } \\ & \text { HV } \\ & \% \\ & \hline \end{aligned}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance ft | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed mph |
| East: SR 70 |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | T1 | 1307 | 7.0 | 0.850 | 27.1 | LOS D | 16.5 | 436.7 | 0.93 | 1.52 | 2.45 | 26.5 |
| 12 | R2 | 144 | 7.0 | 0.850 | 27.1 | LOS D | 16.5 | 436.7 | 0.93 | 1.52 | 2.45 | 25.7 |
| Appr |  | 1452 | 7.0 | 0.850 | 27.1 | LOS D | 16.5 | 436.7 | 0.93 | 1.52 | 2.45 | 26.5 |
| North: Uihlein Rd |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 149 | 2.0 | 0.353 | 14.8 | LOS B | 1.3 | 34.3 | 0.78 | 0.84 | 1.01 | 29.0 |
| 18 | R2 | 698 | 2.0 | 0.425 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 37.6 |
| Approach |  | 847 | 2.0 | 0.425 | 2.7 | LOS A | 1.3 | 34.3 | 0.14 | 0.15 | 0.18 | 35.6 |
| West: SR 70 lo |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 453 | 7.0 | 0.581 | 10.3 | LOS B | $3.9$ | 103.2 | 0.48 | 0.31 | 0.48 | 31.3 |
| $8 \quad$ T1 891 |  |  | 7.0 | 0.581 | 10.3 | LOS B | 3.9 | 103.2 | 0.48 | 0.31 | 0.48 | 32.6 |
| Approach |  | 1343 | 7.0 | 0.581 | 10.3 | LOS B | 3.9 | 103.2 | 0.48 | 0.31 | 0.48 | 32.2 |
| All Vehicles |  | 3642 | 5.8 | 0.850 | 15.2 | LOS C | 16.5 | 436.7 | 0.58 | 0.76 | 1.19 | 30.2 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: Same as Sign Control.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement. LOS F will result if v/c>1 irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010). Roundabout Capacity Model: US HCM 6.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: Traditional M1.
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

Site: [SR 70 \& Uihlein Rd]
2045 AM Peak-Hour
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ |  | Deman Total veh/h | $\begin{aligned} & \text { lows } \\ & \text { HV } \\ & \% \\ & \hline \end{aligned}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance ft | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed mph |
| East: SR 70 |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | T1 | 1307 | 7.0 | 0.723 | 10.6 | LOS B | 9.7 | 255.6 | 0.92 | 0.96 | 1.19 | 34.6 |
| 12 | R2 | 144 | 7.0 | 0.723 | 10.0 | LOS B | 9.7 | 255.6 | 0.91 | 0.92 | 1.15 | 33.7 |
| Appr |  | 1452 | 7.0 | 0.723 | 10.6 | LOS B | 9.7 | 255.6 | 0.92 | 0.96 | 1.19 | 34.5 |
| North: Uihlein Rd |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 149 | 2.0 | 0.324 | 15.0 | LOS B | 1.7 | 42.0 | 0.82 | 0.95 | 0.85 | 32.9 |
| 18 | R2 | 698 | 2.0 | 0.425 | 3.4 | LOS A | 0.0 | 0.0 | 0.00 | 0.41 | 0.00 | 37.6 |
| Approach |  | 847 | 2.0 | 0.425 | 5.5 | LOS A | 1.7 | 42.0 | 0.14 | 0.51 | 0.15 | 36.6 |
| West: SR 70 lol |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 453 | 7.0 | 0.515 | 11.2 | LOS B | $4.6$ | 121.4 | 0.55 | 0.61 | 0.55 | 34.7 |
| $8 \quad$ T1 891 |  |  | 7.0 | 0.515 | 4.1 | LOS A | 4.8 | 126.0 | 0.53 | 0.46 | 0.53 | 36.4 |
| Approach |  | 1343 | 7.0 | 0.515 | 6.5 | LOS A | 4.8 | 126.0 | 0.53 | 0.51 | 0.53 | 35.8 |
| All Vehicles |  | 3642 | 5.8 | 0.723 | 7.9 | LOS A | 9.7 | 255.6 | 0.60 | 0.69 | 0.71 | 35.5 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement. LOS F will result if v/c>1 irrespective of movement delay value (does not apply for approaches and intersection). Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010). Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

Site: [SR 70 \& Uihlein Rd]
2045 PM Peak-Hour
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | Turn | Deman Total veh/h | $\begin{gathered} \text { lows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance ft | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed mph |
| East: SR 70 |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | T1 | 822 | 7.0 | 0.731 | 22.7 | LOS C | 6.7 | 178.1 | 0.84 | 1.16 | 1.83 | 28.0 |
| 12 | R2 | 126 | 7.0 | 0.731 | 22.7 | LOS C | 6.7 | 178.1 | 0.84 | 1.16 | 1.83 | 27.1 |
| Appro |  | 948 | 7.0 | 0.731 | 22.7 | LOS C | 6.7 | 178.1 | 0.84 | 1.16 | 1.83 | 27.8 |
| North: Uihlein Rd |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 120 | 2.0 | 0.182 | 7.6 | LOS A | 0.6 | 16.4 | 0.61 | 0.61 | 0.61 | 31.8 |
| 18 | R2 | 433 | 2.0 | 0.264 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 0.00 | 37.6 |
| Approach |  | 553 | 2.0 | 0.264 | 1.7 | LOS A | 0.6 | 16.4 | 0.13 | 0.13 | 0.13 | 36.1 |
| West: SR 70 |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 735 | 7.0 | 0.866 | 23.0 | LOS C | 22.2 | 585.2 | 0.81 | 0.67 | 1.10 | 26.7 |
|  | T1 | 1322 | 7.0 | 0.866 | 23.0 | LOS C | 22.2 | 585.2 | 0.81 | 0.69 | 1.10 | 27.7 |
| Approach |  | 2057 | 7.0 | 0.866 | 23.0 | LOS C | 22.2 | 585.2 | 0.81 | 0.68 | 1.10 | 27.3 |
| All Vehicles |  | 3558 | 6.2 | 0.866 | 19.6 | LOS C | 22.2 | 585.2 | 0.71 | 0.73 | 1.15 | 28.5 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: Same as Sign Control.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement. LOS F will result if v/c>1 irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010). Roundabout Capacity Model: US HCM 6.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: Traditional M1.
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

Site: [SR 70 \& Uihlein Rd]
2045 PM Peak-Hour
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ |  | Deman Total veh/h | $\begin{aligned} & \text { lows } \\ & \text { HV } \\ & \% \\ & \hline \end{aligned}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance ft | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed mph |
| East: SR 70 |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | T1 | 822 | 7.0 | 0.673 | 14.9 | LOS B | 8.6 | 227.6 | 1.00 | 1.12 | 1.38 | 32.5 |
| 12 | R2 | 126 | 7.0 | 0.673 | 13.9 | LOS B | 8.6 | 227.6 | 1.00 | 1.09 | 1.36 | 31.9 |
| Appr |  | 948 | 7.0 | 0.673 | 14.8 | LOS B | 8.6 | 227.6 | 1.00 | 1.12 | 1.38 | 32.4 |
| North: Uihlein Rd |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 120 | 2.0 | 0.184 | 12.8 | LOS B | 0.9 | 22.1 | 0.68 | 0.85 | 0.68 | 33.6 |
| 18 | R2 | 433 | 2.0 | 0.264 | 3.4 | LOS A | 0.0 | 0.0 | 0.00 | 0.41 | 0.00 | 37.6 |
| Approach |  | 553 | 2.0 | 0.264 | 5.4 | LOS A | 0.9 | 22.1 | 0.15 | 0.51 | 0.15 | 36.6 |
| West: SR 70 |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 7351322 | 7.0 | 0.763 | 11.6 | LOS B | 10.5 | 276.4 | 0.74 | 0.60 | 0.74 | 34.1 |
| 8 | T1 |  | 7.0 | 0.763 | 4.5 | LOS A | 10.7 | 281.5 | 0.69 | 0.49 | 0.69 | 35.9 |
| Approach |  | 2057 | 7.0 | 0.763 | 7.1 | LOS A | 10.7 | 281.5 | 0.71 | 0.53 | 0.71 | 35.2 |
| All Vehicles |  | 3558 | 6.2 | 0.763 | 8.9 | LOS A | 10.7 | 281.5 | 0.70 | 0.68 | 0.80 | 34.6 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement. LOS F will result if v/c>1 irrespective of movement delay value (does not apply for approaches and intersection). Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010). Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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# ATTACHMENT D Safety Performance for Intersection Control Evaluation (SPICE) 

| Federal Highway Administration (FHWA)Safety Performance for Intersection Control Evaluation Tool |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Results |  |  |  |  |  |  |  |
| Summary of crash prediction results for each alternative |  |  |  |  |  |  |  |
| Project Information |  |  |  |  |  |  |  |
| Project Name: | SR 70 from Lorraine Rd to CR 675 |  |  | Intersection Type |  | At-Grade Intersections |  |
| Intersection: | SR 70 @ Uihlein |  |  | Opening Year |  |  |  |
| Agency: | D1 |  |  | Design Year |  |  |  |
| Project Reference: | 414506-2-22-01 |  |  | Facility Type |  | On Urban | urban Arterial |
| City: | Unincorporated Manatee County |  |  | Number of Legs |  |  |  |
| State: | FL |  |  | 1-Way/2-Way |  | 2-way | ting 2-way |
| Date: | 6/24/2019 |  |  | \# of Major Street Lanes (both directions) |  | 5 or fewer |  |
| Analyst: | Nicole Harris, PE |  |  | Major Street Approach Speed |  | Less than 55 mph |  |
| Crash Prediction Summary |  |  |  |  |  |  |  |
| Control Strategy | Crash Type | Opening Year | Design Year | Total Project Life Cycle | Rank | AADT Within Prediction Range? | Source of Prediction |
| Traffic Signal | Fatal \& Injury | $\begin{aligned} & \hline 5.18 \\ & 1.84 \\ & \hline \end{aligned}$ | $\begin{gathered} 12.50 \\ 3.90 \\ \hline \end{gathered}$ | $\begin{gathered} \hline 184.09 \\ 60.20 \\ \hline \end{gathered}$ | 4 | Yes | Calibrated SPF |
| 2-Iane Roundabout | Fatal \& Injury | $\begin{aligned} & 7.00 \\ & 1.23 \\ & \hline \end{aligned}$ | $\begin{gathered} 14.82 \\ 2.98 \\ \hline \end{gathered}$ | $\begin{gathered} 228.09 \\ 43.57 \\ \hline \end{gathered}$ | 1 | N/A | Uncalibrated SPF |
| Displaced Left Turn (DLT) | Fatal \& Injury | $\begin{aligned} & \hline 4.56 \\ & 1.62 \\ & \hline \end{aligned}$ | $\begin{gathered} 11.00 \\ 3.43 \\ \hline \end{gathered}$ | $\begin{gathered} \hline 162.00 \\ 52.98 \\ \hline \end{gathered}$ | 3 | N/A | CMF |
| Continuous Green-T Intersection | Fatal \& Injury | $\begin{aligned} & \hline 4.97 \\ & 1.56 \\ & \hline \end{aligned}$ | $\begin{gathered} 12.00 \\ 3.31 \\ \hline \end{gathered}$ | $\begin{gathered} \hline 176.72 \\ 51.17 \\ \hline \end{gathered}$ | 2 | N/A | CMF |

## SR 70 and Uihlein Signalized Intersection <br> Cost Estimate

| Pay Item | Description | Total Quantity | Unit | Weighted Avg. Unit Price |  | Amount | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ROADWAY: Area of influence of intersection is 1800-ft or 0.34 miles along SR 70 |  |  |  |  |  |  | This area area will be fully reconstructed |
| 101-1 | MOBILZATION | 10.00 | \% |  | \$ | 158,192.57 |  |
| 102-1 | MAINTENANCE OF TRAFFIC | 10.00 | \% |  | \$ | 158,192.57 |  |
| 110-1-1 | CLEARING \& GRUBBING | 8.27 | AC | \$ 11,000.00 | \$ | 90,970.00 | Clear area within the right of way in the 1800-ft limits: ( $1800 * 200$ <br> ft) $/ 43560=8.27 \mathrm{AC}$ |
| 120-1 | REGULAR EXCAVATION | 3,291.20 | CY | 5.10 | \$ | 16,785.12 | Cost per mile from model @ 0.34 miles |
| 160-4 | TYPE B STABIUZATION | 20,206.67 | SY | \$ 3.80 | \$ | 76,785.33 | Area to be constructed and stabilized including shoulders $-2 x$ $[1800 *(2.5+6.5+24+4+2.5)]+24(500)+30(750)+12 * 430 / 9$ |
| 285-709 | OPTIONAL BASE,BASE GROUP 09 | 18,206.67 | SY | \$ 17.00 | \$ | 309,513.33 | Paved area to be constructed:Use typical section $2 \times[1800 *(6.5+24+4)]$ $+24(500)+30(750)+12 * 430 / 9$ |
| 327-70-4 | MIШNG EXISTASPH PAVT, 3"AVG DEPTH | 270.78 | SY | \$ 2.40 | \$ | 649.87 | Area to be milled and resurfaced: Use typical section ( 8388 SF/9) for side street - shape |
| 334-1-24 | SUPERPAVE ASPH CONC, TRAF D, PG 76-22,PMA | 3,668.41 | TN | \$ 100.00 | \$ | 366,841.11 | Assume Traffic C: Area to be contructed +Area to be millied: (17000 $* 400) / 2000$ |
| 337-7-41 | ASPH CONC FC, TRAFFIC B,FC-12.5,PG 76-22 | 739.10 | TN | \$ 105.00 | \$ | 77,605.27 | Assume Traffic C: $(17000 * 80) / 2000$ |
| 430-175-112 | PIPE CULV, OPTMATL, ROUND, 12"S/CD | 658.24 | LF | \$ 91.00 | \$ | 59,899.84 | Cost per mile from model @ 0.34 miles |
| 520-1-10 | CONCREIE CURB \& GUITER, TYPE E | 3,590.40 | LF | \$ 20.00 | \$ | 71,808.00 | Cost per mile from model @ 0.34 miles |
| 522-2 | CONC REIE SIDEWALK AND DRIVEWAYS, 5 " | 1,994.44 | SY | \$ 38.00 | \$ | 75,788.72 | Cost per mile from model @ 0.34 miles |
| 570-1-2 | PERFORMANCE TURF, SOD | 4,438.13 | SY | \$ 2.60 | \$ | 11,539.14 | Cost per mile from model @ 0.34 miles |
| 715-511-140 | UGHTPOLECOMP,F\&I,SGLARM SM, AL, $40{ }^{\prime}$ | 11.90 | EA | \$ 14,600.00 | \$ | 173,740.00 | Cost per mile from model @ 0.34 miles |
|  | Signa lization | 1.00 | PI | \$ 250,000.00 | \$ | 250,000.00 | \$250,000 for SR 70 @ Uihlein |
|  | Partial Total |  |  |  | \$ | 1,581,925.73 |  |
|  | Roadway Total |  |  | - | \$ | 1,898,310.88 |  |
| 999-25 | INTIAL CONTINGENCY AMOUNT(DO NOTBID) | 10\% |  |  | \$ | 189,831.09 |  |
|  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |
| Intersection Grand Total |  |  |  |  | \$ | 2,088,142 |  |
| Notes: |  |  |  |  |  |  |  |
| PAY ITEM list was created based on FDOTLRE Cost per Mile: MODEL WUUA24-U-19-BB. Contingency covers all other items not shown in Table |  |  |  |  |  |  |  |
| Pavement design was assumed to be 4-in for travel lanes and 2-in for shoulders |  |  |  |  |  |  |  |
| MOTand MOBILZATION 10\%EACH |  |  |  |  |  |  |  |
| No right of way impacts. Potential minor utility impacts to be covered by contingency pay item |  |  |  |  |  |  |  |

## SR 70 and Uihlein Road Roundabout <br> Cost Estimate

| Pay Item | Desc niption | Total Q ua ntity | Unit |
| :--- | :---: | :---: | :---: |
| OADWAY: Area of influence of intersection is 1800-ft or 0.34 miles along SR 70 |  |  |  |



| ROADWAY: Area of influence of intersection is 1800-ft or 0.34 miles along SR 70 |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 101-1 | MOBILZATION | 10.00 | \% |  |  | \$ | 132,869.04 |
| 102-1 | MAINTENANCE OF TRAFFIC | 10.00 | \% |  |  | \$ | 132,869.04 |
| 110-1-1 | CLEARING \& GRUBBING | 8.27 | AC | \$ | 11,000.00 | \$ | 90,970.00 |
| 120-1 | REGULAR EXCAVATION | 3,291.20 | CY | \$ | 5.10 | \$ | 16,785.12 |
| 160-4 | TYPE B STABILZATIO N | 24,675.56 | SY | \$ | 3.80 | \$ | 93,767.11 |
| 285-709 | OPTIO NAL BASE,BASE GROUP 09 | 17,716.56 | SY | \$ | 17.00 | \$ | 301,181.4 |
| 327-70-4 | MIШNG EXISTASPH PAVT, 3"AVG DEPTH | 270.78 | SY | \$ | 2.40 | \$ | 649.87 |
| 334-1-24 | SUPERPAVE ASPH C ONC, TRAF D, PG 76-22,PMA | 3,570.20 | TN | \$ | 100.00 | \$ | 357,020.00 |
| 337-7-41 | ASPH CONC FC,TRAFFIC B,FC-12.5,PG 76-22 | 719.44 | TN | \$ | 105.00 | \$ | 75,541.20 |
| 430-175-112 | PIPE CULV, OPTMATL, ROUND, 12"S/CD | 658.24 | LF | \$ | 91.00 | \$ | 59,899.84 |
| 520-1-10 | CONCREIE CURB \& GUTIER, TYPE E | 3,590.40 | LF | \$ | 20.00 | \$ | 71,808.00 |
| 522-2 | CONCREIE SIDEWALK AND DRIVEWAYS, 5" | 1,994.44 | SY | \$ | 38.00 | \$ | 75,788.72 |
| 570-1-2 | PERFORMANCE TURF, SOD | 4,438.13 | SY | \$ | 2.60 | \$ | 11,539.14 |
| 715-511-140 | LGGTPOLE COMP,F\&I,SG LARM SM, AL, 40' | 11.90 | EA | \$ | 14,600.00 | \$ | 173,740.00 |
|  | Signa lization |  | PI | \$ | 250,000.00 | \$ |  |
|  | Partial Total |  |  |  |  | \$ | 1,328,690.45 |
|  | Roadway Total |  |  |  | , | \$ | 1,594,428.54 |
| 999-25 | INITIAL CONTING ENCY AMOUNT(DO NOTBID) | 10\% |  |  |  | \$ | 159,442.85 |
| - | Right of Way Cost Estimate | - | - |  | - | \$ | 30,000.00 |
|  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |
| Intersection Grand Total |  | , |  |  |  | \$ | 1,783,87 |

## SR 70 and Uihlein Road Partial Displaced Left-tum Intersection Cost Estimate

| Pay Item | Description | Total Quantity | Unit | Weighted Avg. Unit Price |  | Amount | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ROADWAY: Area of influence of intersection is 1800-ft or 0.34 miles along SR 70 |  |  |  |  |  |  | This area area will be fully reconstructed |
| 101-1 | MOBILZATION | 10.00 | \% |  | \$ | 181,258.17 |  |
| 102-1 | MAINTENANCE OF TRAFFIC | 10.00 | \% |  | \$ | 181,258.17 |  |
| 110-1-1 | CLEARING \& GRUBBING | 8.27 | AC | \$ 11,000.00 | \$ | 90,970.00 | Clear area within the right of way in the 1800-ft limits: ( 1800* 200 <br> ft) $/ 43560=8.27 \mathrm{AC}$ |
| 120-1 | REGULAR EXCAVATIO N | 3,291.20 | CY | \$ 5.10 | \$ | 16,785.12 | Cost per mile from model @ 0.34 miles |
| 160-4 | TYPE B STABILZATION | 22,173.78 | SY | \$ 3.80 | \$ | 84,260.36 | Area to be constructed and stabilized including unpaved shoulders Use shapes from DGN |
| 285-709 | OPTIONAL BASE,BASE GROUP 09 | 19,955.00 | SY | \$ 17.00 | \$ | 339,235.00 | Paved area to be constructed - Stabilization minus 10\% |
| 327-70-4 | MIШNG EXISTASPH PAVT, 3"AVG DEPTH | 340.22 | SY | \$ 2.40 | \$ | 816.53 | Area to be milled and resurfaced: Use typical section ( 3062 SF/9) for side street - shape |
| 334-1-24 | SUPERPAVE ASPH CONC, TRAF D, PG 76-22,PMA | 4,025.00 | TN | \$ 100.00 | \$ | 402,500.00 | Assume Traffic C: Area to be contructed +Area to be millied: ( $19955 * 400+340 * 200$ )/2000 - Use Optional Base Group Area for new construction |
| 337-7-41 | ASPH CONC FC,TRAFFIC B,FC-12.5,PG 76-22 | 811.80 | TN | \$ 105.00 | \$ | 85,239.00 | Assume Traffic C : $(19955 * 80+340 \mathrm{SY} * 80) / 2000$ |
| 430-175-112 | PIPE CULV, OPTMATL, ROUND, 12"S/CD | 658.24 | LF | \$ 91.00 | \$ | 59,899.84 | Cost per mile from model @ 0.34 miles |
| 520-1-10 | CONCREIE CURB \& GUTIER, TYPE E | 3,590.40 | LF | \$ 20.00 | \$ | 71,808.00 | Cost per mile from model @ 0.34 miles |
| 522-2 | CONCREIE SIDEWALK AND DRIVEWAYS, 5" | 1,994.44 | SY | \$ 38.00 | \$ | 75,788.72 | Cost per mile from model @ 0.34 miles |
| 570-1-2 | PERFORMANCE TURF, SOD | 4,438.13 | SY | \$ 2.60 | \$ | 11,539.14 | Cost per mile from model @ 0.34 miles |
| 715-511-140 | LGGHTPOLE COMP,F\&I,SGLARM SM, AL, 40' | 11.90 | EA | \$ 14,600.00 | \$ | 173,740.00 | Cost per mile from model @ 0.34 miles |
|  | Signa lization | 2.00 | PI | \$ 400,000.00 | \$ | 400,000.00 | $\$ 250,000$ for SR 70 @ Uihlein and $\$ 150,000$ for 1 displaced left intersections along SR 70) $=\$ 400,000$ |
|  | Partial Total |  |  |  | \$ | 1,812,581.71 |  |
|  | Roadway Total |  |  |  | \$ | 2,175,098.06 |  |
| 999-25 | INITAL CONTING ENCY AMOUNT(DO NOTBID) | 10\% |  |  | \$ | 217,509.81 |  |
| - | Right of Way Cost Estimate |  | - | - | \$ | 1,820,000.00 | Details of the right of way estimate are included in Atta chment E . |
|  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |
| Intersection Grand Total |  |  |  |  | \$ | 4,212,608 |  |
| Notes: |  |  |  |  |  |  |  |
| PAY ITEM list was created based on FDOTLRE Cost per Mile: MODEL WUUA24-U-19-BB. Contingency covers all other items not shown in Table |  |  |  |  |  |  |  |
| Pavement design was assumed to be 4-in fortravel lanes and 2-in for shoulders |  |  |  |  |  |  |  |
| MOTand MOBILZATION 10\%EACH |  |  |  |  |  |  |  |
| Right of way impacts are anticipated. |  |  |  |  |  |  |  |
| Potential impacts to one pole of the overhead transmission lines. |  |  |  |  |  |  |  |

## SR 70 and Uihlein Road Continuous Green Tee Intersection Cost Estimate

| Pay Item | Description | Total Quantity | Unit | Weighted Avg. Unit Price |  | Amount | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ROADWAY: Area of influence of intersection is 1800-ft or 0.34 miles along SR 70 |  |  |  |  |  |  | This area area will be fully reconstructed |
| 101-1 | MOBILZATION | 10.00 | \% |  | \$ | 162,734.89 |  |
| 102-1 | MAINTENANCE OF TRAFFIC | 10.00 | \% |  | \$ | 162,734.89 |  |
| 110-1-1 | CLEARING \& GRUBBING | 8.27 | AC | \$ 11,000.00 | \$ | 90,970.00 | Clear area within the right of way in the 1800-ft limits: ( 1800* 200 <br> ft) $/ 43560=8.27 \mathrm{AC}$ |
| 120-1 | REGULAR EXCAVATION | 3,291.20 | CY | \$ 5.10 | \$ | 16,785.12 | Cost per mile from model @ 0.34 miles |
| 160-4 | TYPE B STABILZATION | 21,339.00 | SY | \$ 3.80 | \$ | 81,088.20 | Area to be constructed and stabilized including unpaved shouldersUse shapes from DGN |
| 285-709 | OPTIONAL BASE,BASE GROUP 09 | 19,205.00 | SY | \$ 17.00 | \$ | 326,485.00 | Paved area to be constructed |
| 327-70-4 | MIUNG EXISTASPH PAVT, 3"AVG DEPTH | 270.78 | SY | \$ 2.40 | \$ | 649.87 | Area to be milled and resurfaced: Use typical section ( 2437 SF/9) for side street - shape |
| 334-1-24 | SUPERPAVE ASPH CONC, TRAF D, PG 76-22,PMA | 3,868.00 | TN | \$ 100.00 | \$ | 386,800.00 | Assume Traffic C: Area to be contructed +Area to be milled: ( $19205 * 400+270 * 200$ )/2000 - Use Optional Base Group Area for new construction |
| 337-7-41 | ASPH CONC FC,TRAFFIC B,FC-12.5,PG 76-22 | 779.00 | TN | \$ 105.00 | \$ | 81,795.00 | Assume Traffic C : $(19205 * 80+270 \mathrm{SY} * 80) / 2000$ |
| 430-175-112 | PIPE CULV, OPTMATL, ROUND, 12"S/CD | 658.24 | LF | \$ 91.00 | \$ | 59,899.84 | Cost per mile from model @ 0.34 miles |
| 520-1-10 | CONCREIE CURB \& GUTIER, TYPE E | 3,590.40 | LF | \$ 20.00 | \$ | 71,808.00 | Cost per mile from model @ 0.34 miles |
| 522-2 | CONCREIE SIDEWALK AND DRIVEWAYS, 5" | 1,994.44 | SY | \$ 38.00 | \$ | 75,788.72 | Cost per mile from model @ 0.34 miles |
| 570-1-2 | PERFORMANCE TURF, SOD | 4,438.13 | SY | \$ 2.60 | \$ | 11,539.14 | Cost per mile from model @ 0.34 miles |
| 715-511-140 | LG HTPOLE COMP,F\&I,SGLARM SM, AL, 40' | 11.90 | EA | \$ 14,600.00 | \$ | 173,740.00 | Cost per mile from model @ 0.34 miles |
|  | Signa lization | 1.00 | Pl | \$ 250,000.00 | \$ | 250,000.00 | \$250,000 for SR 70 @ Uihlein |
|  | Partial Total |  |  |  | \$ | 1,627,348.89 |  |
|  | Roadway Total |  |  |  | \$ | 1,952,818.67 |  |
| 999-25 | INITAL CONTING ENCY AMOUNT(DO NOTBID) | 10\% |  |  | \$ | 195,281.87 |  |
|  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |
| Intersection Grand Total |  |  |  |  | \$ | 2,148,101 |  |
| Notes: |  |  |  |  |  |  |  |
| PAY ITEM list was created based on FDOTLRE C ost per Mile: MODEL WUUA24-U-19-BB. C ontingency covers all other items not shown in Table |  |  |  |  |  |  |  |
| Pavement design was assumed to be 4-in for travel lanes and 2-in for shoulders |  |  |  |  |  |  |  |
| MOTand MOBILZATION 10\%EACH |  |  |  |  |  |  |  |
| No right of way impacts. Potential minor utility impacts to be covered by contingency pay item |  |  |  |  |  |  |  |

## SR 70 - ROW Cost Estimates for the Intersection Control Evaluation

| Intersection | Configuration | Square footage or ROW Aquisition | ROW Cost Per Square Foot |  | Estimate |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Uihlein at SR 70 | Partial Displaced Left-Turn (DLT) | 15178 | \$120 | \$ | 1,820,000 |
|  | Roundabout | 236 | \$120 | \$ | 30,000 |
| Del Webb at SR 70 | Partial Displaced Left-Turn (DLT) | 3456 | \$120 | \$ | 410,000 |
| Bourneside at SR 70 | Partial Displaced Left-Turn (DLT) | 9921 | \$120 | \$ | 1,190,000 |
|  |  | 9430 | \$120 | \$ | 1,130,000 |
|  | Quadrant roadway | 439976 | \$120 | \$ | 52,800,000 |
| CR 675 at SR 70 (2) | Quadrant roadway | 68504 | \$2,750 | \$ | 10,000 |

(1) ROW cost estimates are based on the table below
(2) For ROW needs for CR 675, it is assumed that the property will require a full take. The actual property value was used for this estimate.

## Property Value Estimates

| Folio | Total Just Value as of 2018 | Property Size (sq ft.) | Cost Per Sq. Ft. | Inflated cost <br> (factor by 3) | Recommended Cost/Sq Ft <br> to Apply to ROW |
| :---: | ---: | ---: | ---: | ---: | ---: |
| 586104409 | $\$$ | $291,876.00$ | 7640.424 | $\$$ | 38.20 |
| 586109109 | $\$$ | $425,015.00$ | 10672.2 | $\$ 14.6046345$ | 120 |

(1) Property cost estimates were obtained from 2 residential properties near the Lakewood Ranch area. Currently, the Lakewood Ranch residential area is under development and there are no property values from the Manatee County Property Appraiser. The alternative intersection ROW needs are impacting the residential area under development; therefore, there are no property values that could be use for ROW estimates.
(2) These property estimates are used for the intersections of Uihlein, Del Webb, and Bourneside. Since CR 675 is a full take, the property appraised value for that property will be used.

# ATTACHMENT F 

## Delay Calculations

## Delay Information

Use this sheet to enter the delay information for each of the included control strategies.

Note: Delay calculations for Displaced Left-Turn and Continuous Green-T Intersection have been adjusted to account for Experienced Travel Time (ETT) based on guidance from the Highway Capacity Manual, Chapter 23, Ramp Terminals and Alternative Intersections. The ETT method accounts for origin-destination (O-D) path of a distributed network of closely space intersections that operate in a cluster. This method results in a single LOS/delay for an alternative intersection configuration with multiple signalized intersections which include multiple LOS/delay results (e.g. Displaced left turns are modeled as multiple signalized intersections with separate LOS/delay results for each; this method computes the LOS/delay as one intersection). The HCM describes direct application of this concept to Displaced Left-Turns and RCUTs, however, it may also be extended to continuous green-t intersections to account for the major-street through movement which separated from the rest of the intersection and not accounted for in the Synchro analysis.


User must enter value on this sheet


Note: Intersections 2, 4, and 5 are a single intersection at an actual DTL.
Modeling in SYNCHRO requires 3 separate intersections



ATTACHMENT G Benefit / Cost Summary

Outputs
This sheet compiles the data from summary tables in individual alternatives sheets. To populate the output sheet press the "Setup Wor the Alternatives_MasterList tab.

| Agency: | FDOT District 1 |
| :--- | :--- |
| Project Name: | SR 70 from Lorraine Rd to CR 675 |
| Project Reference: | FDOT Project \#414506-2-22-01 |
| Intersection: | SR 70 and Uihlein Rd |
| City: | Unincorporated Manatee County |
| State: | Florida |
| Performing Department or <br> Organization: | Florida Department of Transportation District 1 |
| Date: | 6/24/2019 |
| Analyst: | CB |
| Analysis Type | At-Grade Intersection |

Analysis Summary

| Cost Categories | Net Present Value of Costs |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Traffic Signal |  | Roundabout |  |  | Displaced Left Turn (DLT) |  | Continuous Green-T Intersection |  |
| Planning, Construction \& Right of Way Costs | \$ | 2,090,000 | \$ |  | 1,756,000 | \$ | 2,754,000 | \$ | 2,150,000 |
| Auto Passenger Delay | \$ | 13,405,170 | \$ |  | 6,852,422 | \$ | 12,303,784 | \$ | 11,135,355 |
| Truck Delay | \$ | 4,700,485 | \$ |  | 2,409,071 | \$ | 4,342,152 | \$ | 3,922,714 |
| Safety | \$ | 11,307,425 | \$ |  | 8,562,933 | \$ | 9,950,298 | \$ | 9,688,590 |
| Total cost | \$31,601,308 |  | \$19,653,377 |  |  | \$29,588,511 |  | \$26,994,888 |  |




# ATTACHMENT H 

FDOT ICE Stage 1 Form, Capacity Analysis for Planning of Junctions (CAP-X), and Stage 1 SPICE

## Stage 1: Screening

To fulfill the requirements of Stage 1 (Screening) of FDOT's ICE procedures, complete the following form and append all supporting documentation. Completed forms can be submitted to the District Traffic Operations Engineer (DTOE) and District Design Engineer (DDE) for the project's approval.

| Project Name | SR 70 from Lorraine Rd to CR 675 |  |  | FDO | 414506-2-22-01 |  | Date | 06/14/19 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Subm | Nicole Harris, PE |  | Agency/Company |  | Stantec | Email | nicole.harris@stantec.com |  |
| FDOT Co | sificatio | C3R - Suburban Residential |  | FDOT Distric | District 1 | County | Manat |  |
| roje | , ty/ | illage) | Unincorporated Manatee County |  | Project Ty | Corridor Improvement Project |  |  |
| Project Purpose the catalyst | oject a ing un | hat is $y$ is it ken?) | A PD\&E Study is being completed with the purpose of increasing capacity and improving traffic operational conditions along the SR 70 corridor from Lorraine Road to CR 675/Waterbury Road. The Intersection Control Evaluation (ICE) is based on the future build improvements of the project which widen SR 70 to 4-lanes. This ICE will focus on the intersection with Uihlein Road. |  |  |  |  |  |
| Project Setting Description (Describe the area surrounding the intersection) |  |  | SR 70 at Uihlein Rd <br> Future Land Use is comprised of Mixed Use -Commerical. There is a major residential development that is changing the setting from rural to suburban/residential. |  |  |  |  |  |
| Multimodal Context (Describe the pedestrian, bicycle, and transit activity in the area and the potential for activity based on surrounding land uses and development patterns) |  |  | There are paved sidewalks on the both sides of Uihlein Road along with marked bike lanes. For SR 70, there are proposed sidewalks and paved shoulders on both sides of the road. |  |  |  |  |  |



FDOT ICE: Stage 1


| Crash History (Existing Intersections Only) |
| :--- |
| Append the most recent five-years of crash data for the intersection from the CAR System. If the crash data evidences any issues relating to safety |
| performance, discuss briefly here: |
| The crash history was not included in the analysis since the future conditions of SR 70 changes significantly from a 2 lane undivided to a 4-lane divided. |
| Instead, a predictive crash model was used for the analysis. |

FDOT ICE: Stage 1

Control Strategy Evaluation
Provide a brief justification as to why each of the following control strategies should be advanced or not. Justification should consider potential environmental impacts.

| Control Strategy | CAP-X Outputs |  |  | SPICE <br> Ranking | Strategy to Be Advanced? | Justification |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | V/C Ratio |  | Multimodal Score |  |  |  |
|  | Weekday AM Peak | Weekday PM Peak |  |  |  |  |
| Two-Way StopControlled | N/A | N/A | N/A | N/A | No | Future volumes exceed Peak Hour Volume Thresholds based on FDOT ICE Manual, Figure A1 |
| All-Way StopControlled | N/A | N/A | N/A | N/A | No | Future volumes exceed Peak Hour Volume Thresholds according to FDOT ICE Manual. |
| Signalized Control | 0.83 | 0.54 | 4.8 | 7 | Yes | Move to Stage 2 based on v/c for am and pm hours |
| Roundabout | 2x2: 1.52 1x2: 1.84 1x1: 2.33 | 2x2: 0.89 1x2: 0.89 1x1: 1.72 | 5.6 / 6.7 | 1 Lane: 1 | Yes | Although the CAP-X shows the V/C greater than one, this could be mitigated by a SB right-turn bypass lane which cannot be modeled in CAP-X |
| Median U-Turn | N/A | N/A | N/A | 2 Lane: 4 | No | Not applicable since this is a T-intersection. |
| RCUT (Signalized) | 0.91 | 0.66 | 6.3 | 3 | No | The future volumes seem to be near the limit fo Peak Hour Volume thresholds based on FDOT ICE Manual, Figure A3 |
| RCUT (Unsignalized) | 5.66 | 1.72 | 4.4 | 2 | No | V/C ratio exceeded during the PM Peak. |
| Jughandle |  |  |  | N/A | No | Not included in the analysis. |
| Displaced LeftTurn | . 70 (Partial) | . 45 (Partial) | 4.8 | 6 | Yes | Move to Stage 2 for Partial DLT |
| Continuous Green Tee | 0.61 | 0.53 | 3.0 | 5 | Yes | Move to Stage 2 |
| Quadrant Roadway | N/A | N/A | N/A |  | No | Not applicable since this is a T-intersection. |
| Partial MUT | N/A | N/A | N/A | N/A | No | Not applicable since this is a T-intersection. |
| Other 2 (Type) | N/A | N/A | N/A | N/A | No | No additional alternative intersection configurations were included in this analysis. |


| Resolution |  |  |
| :---: | :---: | :---: |
| To be filled out by FDOT District Traffic Operations Engineer and District Design Engineer |  |  |
| Project D | Multiple Viable Alternatives Identified: Continue to Stage 2 |  |
| Comments |  |  |
| DTOE Name | Signature | Date |
| DDE Name | Signature | Date |


| Project Name: | SR 70 @ Uihlein |
| ---: | :---: |
| Project Number: | 0 |
| Location: | Unincorporated Manatee County |
| Date: | 2045 AM |
| Number of Intersection Legs: | 3 |
| Which leg is the minor street? | N |


| Traffic Volume Demand |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Vol | /hr) |  |  | nt (\%) |
|  | U-Turn | Left | Thru |  | Heavy | Volume Growth |
| Eastbound | 0 | 430 | 846 | 0 |  | 0.00\% |
| Westbound | 0 | 0 | 1242 | 137 |  | 0.00\% |
| Southbound | 0 | 142 | 0 | 663 |  | 0.00\% |
| Northbound | 0 | 0 | 0 | 0 |  | 0.00\% |
| Adjustment Factor | 0.80 | 0.95 |  | 0.85 |  | $\cdots$ |
| Suggested | 0.80 | 0.95 |  | 0.85 |  | $2$ |
| Truck to PCE Factor |  |  |  | Suggest | 2.00 | 2.00 |
| FDOT Context Zon |  | C3R-Suburban Residential |  |  |  |  |
| Critical Lane Volume Threshold |  | 2-phase signal |  | Suggested = 1800 |  | 1800 |
|  |  | 3 -phase signal |  | Suggested = 1750 |  | 1750 |
|  |  | 4-phase signal |  | Suggested = 1700 |  | 1700 |


| TYPE OF INTERSECTION | $\begin{gathered} \text { Overall v/c } \\ \text { Ratio } \end{gathered}$ | V/C Ranking | Multimodal Score | Pedestrian Accommodation s | $\begin{gathered} \text { Bicycle } \\ \text { Accommodation } \\ s \end{gathered}$ | Transit Accommodatio ns |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Continuous Green T N | 0.61 | 1 | 3.0 | Poor | Poor | Good |
| Partial Displaced Left Turn E-W | 0.70 | 2 | 4.8 | Fair | Fair | Good |
| Traffic Signal | 0.83 | 3 | 4.8 | Fair | Fair | Good |
| Signalized Restricted Crossing U -Iurn E W | 0.91 | 4 | 6.3 | Good | Good | Fair |
| $2 \times 2$ | 1.52 | 5 | 5.6 | Fair | Good | Good |
| $1 \times 2$ | 1.84 | 6 | 5.6 | Fair | Good | Good |
| $1 \times 1$ | 2.33 | 7 | 6.7 | Good | Good | Good |
| Unsignalized Restricted Crossing $\mathrm{U}-$ Turn E-W | 5.66 | 8 | 4.4 | Fair | Fair | Fair |
| -- | -- | -- | -- | -- | -- | -- |
| -- | -- | -- | -- | -- | -- | -- |


| Project Name: | SR 70 @ Uihlein |
| ---: | :---: |
| Project Number: | 0 |
| Location: | Unincorporated Manatee County |
| Date: | 2045 AM |
| Number of Intersection Legs: | 3 |
| Major Street Direction: | North-South |


| Traffic Volume Demand |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Volume (Veh/hr) |  |  |  | Percent (\%) |  |
|  | U-Turn | Left | Thru | Right | Heavy | Volume Growth |
| Eastbound | 0 | 430 | 846 | 0 |  | 0.00\% |
| Westbound | 0 | 0 | 1242 | 137 |  | 0.00\% |
| Southbound | 0 | 142 | 0 | 663 |  | 0.00\% |
| Northbound | 0 | 0 | 0 | 0 |  | 0.00\% |
| Adjustment Factor | 0.80 | 0.95 |  | 0.85 |  |  |
| Suggested | 0.80 | 0.95 |  | 0.85 |  | , |
| Truck to PCE Factor |  |  |  | Suggest | 2.00 | 2.00 |
| FDOT Context Zone |  |  | C3R-Suburban Residential |  |  |  |
| Critical Lane Volume Threshold |  | 2-phase signal |  | Suggested = 1800 |  | 1800 |
|  |  | 3-phase signal |  | Suggested = 1750 |  | 1750 |
|  |  | 4-phase signal |  | Suggested = 1700 |  | 1700 |

Capacity Analysis for Planning of Junctions
Detailed Report - Page 2 of 4

| Number of Lanes for Non-roundabout Intersections |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TYPE OF INTERSECTION | Sheet | Northbound |  |  |  | Southbound |  |  |  | Eastbound |  |  |  | Westbound |  |  |  |
|  |  | U | L | T | R | U | L | T | R | U | L | T | R | U | L | T | R |
| Traffic Signal | FULL | - | 0 | 0 | 0 | - | 1 | 0 | 1 | 7 | 2 | 2 | 0 | - | 0 | 2 | 1 |
| Continuous Green T | N |  |  |  | - | - | 1 | - | 1 |  | 2 | 2 | - |  | \% | 2 | 1 |
| Partial Displaced Left Turn | E-W | , | 0 | 1 | 0 |  | 1 | 1 | 1 | , | 2 | 2 | 0 | - | 0 | 2 | 1 |
| Signalized Restricted Crossing U-Turn | E-W | , |  | 7 | 0 | , |  | $\square$ | 1 | 1 | 2 | 2 | 0 | 1 | 0 | 2 | 1 |
| Unsignalized Restricted Crossing U-Turn | E-W | , |  | - | 0 |  |  | , | 1 | 1 | 2 | 2 | 0 | 1 | 0 | 2 | 1 |


| Number of Lanes for Interchanges |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TYPE OF INTERCHANGE | Sheet | Northbound |  |  |  | Southbound |  |  |  | Eastbound |  |  |  | Westbound |  |  |  |
|  |  | U | L | T | R | U | L | T | R | U | L | T | R | U | L | T | R |


| Results for Non-roundabout Intersections |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TYPE OF INTERSECTION | Sheet | Zone 1 (North) |  | Zone 2 (South) |  | Zone 3 (East) |  | Zone 4 (West) |  | Zone 5 (Center) |  | Overall v/c Ratio |  |  |  |
| Traffic Signal | FULL |  |  |  |  | , |  |  |  | 1460 | 0.83 | 0.83 | Fair | Fair | Good |
| Continuous Green T | N |  |  |  |  |  |  |  |  | 1059 | 0.61 | 0.61 | Poor | Poor | Good |
| Partial Displaced Left Turn | E-W |  |  |  |  | 525 | 0.29 | 907 | 0.50 | 1218 | 0.70 | 0.70 | Falr | Falr | Good |
| Signalized Restricted Crossing U-Turn | E-W | 1630 | $\underline{0.91}$ | 525 | 0.29 | 738 | 0.41 | 864 | 0.48 |  |  | 0.91 | Good | Good | Fair |
| Unsignalized Restricted Crossing U-Turn | E-W | 1329 | 5.66 | 1050 | 0.00 | 1476 | 0.00 | 1365 | 0.38 |  |  | 5.66 | Fair | Fair | Fair |

Capacity Analysis for Planning of Junctions
Detailed Report - Page 4 of 4

| Results for Roundabouts |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TYPE OF | Zone 1 (North) |  |  | Zone 3 (East) |  |  | Zone 2 (South) |  |  | Zone 4 (West) |  |  | Overall v/c Ratio |  |  |  |
|  | Lane 1 | Lane 2 | Lane 3 | Lane 1 | Lane 2 | Lane 3 | Lane 1 | Lane 2 | Lane 3 | Lane 1 | Lane 2 | Lane 3 |  |  |  |  |
| 1×1 | 2.33 |  |  | 1.16 |  |  | 0.00 |  |  | 1.73 |  |  | 2.33 | Good | Good | Good |
| $1 \times 2$ | 1.84 |  |  | 0.56 | 0.59 |  | 0.00 |  |  | 0.81 | 0.84 |  | 1.84 | Fair | Good | Good |
| $\underline{2 \times 2}$ | 0.38 | 1.52 |  | 0.81 | 0.84 |  | 0.00 | 0.00 |  | 0.56 | 0.59 |  | 1.52 | Fair | Good | food |



| Project Name: | SR 70 @ Uihlein |
| ---: | :---: |
| Project Number: | 0 |
| Location: | Unincorporated Manatee County |
| Date: | 2045 PM |
| Number of Intersection Legs: | 3 |
| Which leg is the minor street? | N |


| Traffic Volume Demand |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Volu | /hr) |  |  | nt (\%) |
|  | U-Turn | Left | Thru个 |  | Heavy | Volume Growth |
| Eastbound | 0 | 698 | 1256 | 0 |  | 0.00\% |
| Westbound | 0 | 0 | 781 | 120 |  | 0.00\% |
| Southbound | 0 | 114 | 0 | 411 |  | 0.00\% |
| Northbound | 0 | 0 | 0 | 0 |  | 0.00\% |
| Adjustment Factor | 0.80 | 0.95 |  | 0.85 |  | $\cdots$ |
| Suggested | 0.80 | 0.95 | , | 0.85 |  |  |
| Truck to PCE Factor |  |  |  | Suggest | 2.00 | 2.00 |
| FDOT Context Zon |  | C3R-Suburban Residential |  |  |  |  |
| Critical Lane Volume Threshold |  | 2-phase signal |  | Suggested = 1800 |  | 1800 |
|  |  | 3 -phase signal |  | Suggested = 1750 |  | 1750 |
|  |  | 4-phase signal |  | Suggested = 1700 |  | 1700 |

## Capacity Analysis for Planning of Junctions

| TYPE OF INTERSECTION | Overall v/c Ratio | V/C <br> Ranking | Multimodal Score | Pedestrian Accommodation s | $\square$ | Transit Accommodatio ns |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Partial Displaced Left Turn E-W | 0.45 | 1 | 4.8 | Fair | Fair | Good |
| Continuous Green T N | 0.53 | 2 | 3.0 | Poor | Poor | Good |
| Traffic Signal | 0.54 | 3 | 4.8 | Fair | Fair | Good |
| Signalized Restricted Crossing U-Iurn W | 0.66 | 4 | 6.3 | Good | Good | Fair |
| $1 \times 2$ | 0.89 | 5 | 5.6 | Fair | Good | Good |
| $2 \times 2$ | 0.89 | 5 | 5.6 | Fair | Good | Good |
| $1 \times 1$ | 1.72 | 7 | 6.7 | Good | Good | Good |
| Unsignalized Restricted Crossing 0 - Turn E-W | 1.72 | 8 | 4.4 | Fair | Fair | Fair |
| -- | -- | -- | -- | -- | -- | -- |
| -- | -- | -- | -- | -- | -- | -- |


| Project Name: | SR 70 @ Uihlein |
| ---: | :---: |
| Project Number: | 0 |
| Location: | Unincorporated Manatee County |
| Date: | 2045 PM |
| Number of Intersection Legs: | 3 |
| Major Street Direction: | North-South |


| Traffic Volume Demand |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Volume (Veh/hr) |  |  |  | Percent (\%) |  |
|  | U-Turn | Left | Thru | Right | Heavy | Volume Growth |
| Eastbound | 0 | 698 | 1256 | 0 |  | 0.00\% |
| Westbound | 0 | 0 | 781 | 120 |  | 0.00\% |
| Southbound | 0 | 114 | 0 | 411 |  | 0.00\% |
| Northbound | 0 | 0 | 0 | 0 |  | 0.00\% |
| Adjustment Factor | 0.80 | 0.95 |  | 0.85 |  |  |
| Suggested | 0.80 | 0.95 |  | 0.85 |  | , |
| Truck to PCE Factor |  |  |  | Suggest | 2.00 | 2.00 |
| FDOT Context Zone |  |  | C3R-Suburban Residential |  |  |  |
| Critical Lane Volume Threshold |  | 2-phase signal |  | Suggested = 1800 |  | 1800 |
|  |  | 3-phase signal |  | Suggested = 1750 |  | 1750 |
|  |  | 4-phase signal |  | Suggested = 1700 |  | 1700 |

Capacity Analysis for Planning of Junctions
Detailed Report - Page 2 of 4

| Number of Lanes for Non-roundabout Intersections |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TYPE OF INTERSECTION | Sheet | Northbound |  |  |  | Southbound |  |  |  | Eastbound |  |  |  | Westbound |  |  |  |
|  |  | U | L | T | R | U | L | T | R | U | L | T | R | U | L | T | R |
| Traffic Signal | FULL | - | 0 | 0 | 0 | - | 1 | 0 | 1 | 7 | 2 | 2 | 0 | - | 0 | 2 | 1 |
| Continuous Green T | N |  |  |  | - | - | 1 | - | 1 |  | 2 | 2 | - |  | \% | 2 | 1 |
| Partial Displaced Left Turn | E-W | , | 0 | 1 | 0 |  | 1 | 1 | 1 | , | 2 | 2 | 0 | - | 0 | 2 | 1 |
| Signalized Restricted Crossing U-Turn | E-W | , |  | 7 | 0 | , |  | $\square$ | 1 | 1 | 2 | 2 | 0 | 1 | 0 | 2 | 1 |
| Unsignalized Restricted Crossing U-Turn | E-W | , |  | - | 0 |  |  | , | 1 | 1 | 2 | 2 | 0 | 1 | 0 | 2 | 1 |


| Number of Lanes for Interchanges |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TYPE OF INTERCHANGE | Sheet | Northbound |  |  |  | Southbound |  |  |  | Eastbound |  |  |  | Westbound |  |  |  |
|  |  | U | L | T | R | U | L | T | R | U | L | T | R | U | L | T | R |


| Results for Non-roundabout Intersections |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TYPE OF INTERSECTION | Sheet | Zon (No | 1 1 | Zon (So | 2 ${ }^{2}$ | Zone 3 | (East) | Zone 4 | West) V/C |  | 5 ter) V/C | Overall v/c Ratio |  |  |  |
| Traffic Signal | FULL |  |  |  |  |  |  |  |  | 940 | 0.54 | 0.54 | Fair | Fair | Good |
| Continuous Green T | N |  |  |  |  |  |  |  |  | 933 | 0.53 | 0.53 | Poor | Poor | Good |
| Partial Displaced Left Turn | E-W |  |  |  |  | 730 | 0.41 | 811 | 0.45 | 794 | 0.45 | 0.45 | Falr | Falr | Good |
| Signalized Restricted Crossing U-Turn | E-W | 1047 | $\underline{0.58}$ | 730 | 0.41 | 482 | 0.27 | 1191 | 0.66 |  |  | 0.66 | Good | Good | Fair |
| Unsignalized Restricted Crossing U-Turn | E-W | 836 | 1.72 | 1460 | $\underline{0.00}$ | 964 | $\underline{0.00}$ | 2091 | 0.61 |  |  | 1.72 | Fair | Fair | Fair |

Capacity Analysis for Planning of Junctions
Detailed Report - Page 4 of 4

| Results for Roundabouts |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| E | Zone 1 (North) |  |  | Zone 3 (East) |  |  | Zone 2 (South) |  |  | Zone 4 (West) |  |  | Overall v/c Ratio |  |  |  |
|  | Lane 1 | Lane 2 | Lane 3 | Lane 1 | Lane 2 | Lane 3 | Lane 1 | Lane 2 | Lane 3 | Lane 1 | Lane 2 | Lane 3 |  |  |  |  |
| 1×1 | 0.92 |  |  | 1.72 | - |  | 0.00 |  |  | 1.51 | - |  | 1.72 | Good | cood | cood |
| $1 \times 2$ | 0.79 |  |  | 0.84 | 0.89 |  | 0.00 |  |  | 0.69 | 0.70 |  | 0.89 | Fair | Good | Good |
| $\underline{2 \times 2}$ | 0.19 | 0.62 |  | 0.69 | 0.70 |  | 0.00 | 0.00 |  | 0.84 | 0.89 |  | 0.89 | Fair | Good | food |



| Federal Highway Administration (FHWA)Safety Performance for Intersection Control Evaluation Tool |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Results |  |  |  |  |  |  |  |
| Summary of crash prediction results for each alternative |  |  |  |  |  |  |  |
| Project Information |  |  |  |  |  |  |  |
| Project Name: | SR 70 from Lorraine Rd to CR 675 |  |  | Intersection Type |  | At-Grade Intersections |  |
| Intersection: | SR 70 @ Uihlein |  |  | Opening Year |  | 2025 |  |
| Agency: | D1 |  |  | Design Year |  | 2045 |  |
| Project Reference: | 414506-2-22-01 |  |  | Facility Type |  | On Urban and Suburban Arterial |  |
| City: | Unincorporated Manatee County |  |  | Number of Legs |  | 3-leg |  |
| State: | FL |  |  | 1-Way/2-Way |  | 2-way Intersecting 2-way |  |
| Date: | 6/14/2019 |  |  | \# of Major Street Lanes (both directions) |  | 5 or fewer |  |
| Analyst: | Nicole Harris, PE |  |  | Major Street Approach Speed |  | Less than 55 mph |  |
| Crash Prediction Summary |  |  |  |  |  |  |  |
| Control Strategy | Crash Type | Opening Yea | Design Year | Total Project Life Cycle | Rank | AADT Within Prediction Range? | Source of Prediction |
| Traffic Signal | Total | 5.18 | 12.49 | 184.01 | 7 | Yes | Calibrated SPF |
|  | Fatal \& Injury | 1.84 | 3.90 | 60.18 | 7 | Yes | Calibrated SPF |
| 1-lane Roundabout | Total | 1.22 | 1.96 | 33.58 | 1 | N/A | Uncalibrated SPF |
|  | Fatal \& Injury | 0.38 | 0.79 | 12.19 |  |  |  |
| 2-lane Roundabout | Total | 7.38 | 15.64 | 240.61 | 4 | N/A | Uncalibrated SPF |
|  | Fatal \& Injury | 1.32 | 3.22 | 47.04 |  |  | Uncalibrated SPF |
| Displaced Left Turn (DLT) | Total | 4.56 | 10.99 | 161.93 | 6 | N/A | CMF |
|  | Fatal \& Injury | 1.62 | 3.43 | 52.96 |  |  |  |
| Signalized RCUT | Total | 4.40 | 10.62 | 156.41 | 3 | A | CMF |
|  | Fatal \& Injury | 1.43 | 3.04 | 46.94 |  |  |  |
| Unsignalized RCUT | Total | 2.29 | 6.45 | 90.34 |  |  | CMF |
|  | Fatal \& Injury | 0.55 | 1.31 | 19.38 | 2 | N/A | CMF |
| Continuous Green-T Intersection | Total | 4.97 | 11.99 | 176.65 | 5 | N/A | CMF |
|  | Fatal \& Injury | 1.56 | 3.31 | 51.15 | 5 |  |  |

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