# DRAFT INTERSECTION CONTROL EVALUATION 

(DEL WEBB BOULEVARD AT SR 70)

Florida Department of Transportation
District 1
SR 70
Limits of Project: from Lorraine Road to CR 675/Waterbury Road
Manatee County, Florida
Financial Management Number: 414506-2
ETDM Number: 14263
Date: JUNE 2019

The environmental review, consultation, and other actions required by applicable federal environmental laws for this project are being, or have been, carried out by FDOT pursuant to 23 U.S.C. § 327 and a Memorandum of Understanding dated December 14, 2016 and executed by FHWA and FDOT.

## Memorandum

Date: June 18, 2019

To: David C. Turley, PE
FDOT District 1

From: Christopher Benitez, PE, PTOE<br>Stantec Consulting Services, Inc.

## Reference: Intersection Control Evaluation (ICE): Del Webb Boulevard at SR 70

The purpose of this memorandum is to document the Florida Department of Transportation (FDOT) Intersection Control Evaluation (ICE) for the intersection of SR 70 and Del Webb Boulevard. This ICE has been completed as part of the FDOT District 1 project: 414506-2 - SR 70 between Lorraine Road to CR 675. The project proposes to increase capacity along SR 70 by widening from a two-lane undivided, to a four-lane divided facility along with traffic operational improvements at the intersections. The ICE analysis was initiated during the Project Development \& Environment (PD\&E) phase of the project due to the failing traffic operations during future conditions. According to the project Design Traffic Technical Memorandum (dated October 2018), the intersection of Del Webb Boulevard and SR 70 will operate at Level of Service (LOS) F as a two-way stop-controlled intersection.

An FDOT ICE for the intersection of Del Webb Boulevard and SR 70 was completed for both Stage 1 and Stage 2 for several alternative intersection configurations. Based on an interpretation of the results of the ICE analysis, the roundabout is the recommended option. The analysis included an evaluation of the traffic operations, safety, cost, multimodal accommodations, and other impacts such as environmental, utility, and right of way. The evaluation focused on the SR 70 future build conditions as a four-lane divided facility with a design speed of 55 mph . The results are provided in the Stage 2 ICE Form in Attachment A. The memorandum is organized as follows:

- Attachment A: ICE Stage 2 Form and Results
- Attachment B: Conceptual Plans
- Attachment C: Traffic Operational Analysis
- Attachment D: Safety Performance for Intersection Control Evaluation (SPICE)
- Attachment E: Cost Estimates
- Attachment F: Delay Calculations
- Attachment G: Benefit/Cost Summary
- Attachment H: ICE Stage 1 Form, Capacity Analysis for Planning of Junctions (CAP-X), and Stage 1 SPICE


## Intersection Control Evaluation (ICE) Form

## Stage 2: Intial Control Strategy Assessment

To fulfill the requirements of Stage 2 (Intersection Control Strategy) of FDOT's ICE procedures, complete the following form and append all supporting documentation. Completed forms can be submitted to the District Traffic Operations Engineer (DTOE) and District Design Engineer (DDE) for the project's approval.

| Project Name | SR 70 from Lorraine Rd to CR 675 | 75 | 414506-2-22-01 |  | Date | 06/14/19 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Submitted By | Nicole Harris, PE | Agency/Company | Stantec | Email | nicole. | stantec.com |
| List all viable intersection control strategies identified in Stage 1 (Screening): |  |  |  |  |  |  |
| Signalized Control |  | Roundabout |  | RCUT (Signalized) |  |  |
| Displaced Left-Turn |  | Continuous Green Tee |  |  |  |  |



FDOT ICE: Stage 2

| Safety Performance |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Enter the most recent five (5) years of crash data from the CAR System. |  |  |  | Most recent year of crash data available |  |  | 2018 |
| Crash Type |  | 2014 | 2015 | 2016 | 2017 | 2018 | Total |
| Combined | Total |  |  |  |  |  |  |
|  | Fatal/Injury |  |  |  |  |  |  |
|  | PDO |  |  |  |  |  |  |
| Single-Vehicle | Total | 0 | 0 | 1 | 0 | 0 | 1 |
|  | Fatal/Injury | 0 | 0 | 1 | 0 | 0 | 1 |
|  | PDO | 0 | 0 | 0 | 0 | 0 | 0 |
| Multi-Vehicle | Total | 0 | 0 | 0 | 2 | 3 | 5 |
|  | Fatal/Injury | 0 | 0 | 0 | 2 | 2 | 4 |
|  | PDO | 0 | 0 | 0 | 0 | 1 | 1 |
| Vehicle-Pedestrian | Fatal/Injury | 0 | 0 | 0 | 0 | 0 | 0 |
| Vehicle-Bicycle | Fatal/Injury | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | All | 0 | 0 | 1 | 2 | 3 | 6 |

Apply the FDOT SPICE Tool to model anticipated safety performance of each control strategy. For intersection types not accommodated in the tool, manually apply crash modification factors detailed in the ICE procedures document or qualitatively describe anticipated safety impacts.

| Control Strategy | Opening Year | Design Year |  |  |  |
| :--- | :--- | :---: | :---: | :---: | :---: |
|  | Pricipated Impact on Safety Performance | Predicted <br> Total <br> Crashes | Predicted <br> Fatal+Injury <br> Crashes | Predicted <br> Total <br> Crashes | Predicted <br> Fatal+Injury <br> Crashes |
| Signalized Control | This option has a comparable Predicated Total Crashes for both <br> opening and design year between the other options. | 4.61 | 5.59 | 4.61 | 5.59 |
| Roundabout | This option has the lowst Predicted Fatal+Injury crashes for both <br> opening an design years | 4.56 | 0.99 | 7.19 | 1.16 |
| RCUT (Signalized) | This option has a comparable Predicated Total Crashes for both <br> opening and design year between the other options. | 3.92 | 4.36 | 3.92 | 4.36 |
| Displaced Left-Turn | This option has a comparable Predicated Total Crashes for both <br> opening and design year between the other options. | 4.06 | 4.92 | 4.06 | 4.92 |
| Continuous Green Tee | This option has a comparable Predicated Total Crashes for both <br> opening and design year between the other options. | 4.43 | 4.75 | 4.43 | 4.75 |
|  |  |  |  |  |  |


| Costs and Benefit/Cost Ratios |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Remaining cognizant of the current level of detail of each control strategy's conceptual design, provide a cost estimate for each. You may want to include costs for preliminary engineering, required right-of-way acquisitions, construction, and a contingency. Apply the FDOT ICE Tool to determine the delay benefit-cost ratio (B/C), safety B/C, overall B/C, and net-present value for each control stratetgy. |  |  |  |  |  |  |
| Control Strategy | ROW Costs (\$) | Construction Costs (\$) | FDOT ICE Tool Outputs |  |  |  |
|  |  |  | Delay B/C | Safety B/C | Overall B/C | Net Present Value |
| Signalized Control | - | \$2,340,000 | Base | Base | Base | Base |
| Roundabout | - | \$2,110,000 | Preferred | Preferred | Preferred | \$1,910,613 |
| RCUT (Signalized) | - | \$2,530,000 | Less than 0 | 3.24 | 1.62 | \$267,414 |
| Displaced Left-Turn | \$410,000 | \$2,650,000 | Less than 0 | 1.23 | Less than 0 | -\$2,718,400 |
| Continuous Green Tee | - | \$2,400,000 | 8.41 | 5.81 | 14.21 | \$2,090,554 |
|  |  |  |  |  |  |  |


| Multimodal Accomodations |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Note the existing/anticipated level of pedestrian/bicyclist activity at the study intersection during the peak hours of the typical day. See ICE procedures document for activity level thresholds: |  |  |  |  |  |  |  |  |  |  |
| Peak Hour: |  | Weekday AM Peak |  |  | Weekday PM Peak |  | Saturday Midday Peak |  | Acitivity Level |  |
|  |  | Major Street | Minor Street |  | Major Street | Minor Street | Major Street | Minor Street | Ped. | Bicycles |
| \# of ped. crossings (both approaches, if app.): |  |  |  |  |  |  |  |  | Low | Low |
| \# of cyclists (both approaches, if app.): |  |  |  |  |  |  |  |  |  |  |
| Summarize the ability of each viable control strategy to accommodate the exisitng/anticipated level of: |  |  |  |  |  |  |  |  |  |  |
| Control Strategy | Pedestrians and Bicyclists |  |  | Transit Services |  |  |  | Freight Needs |  |  |
| Signalized Control | Crosswalks and bicycle lanes can be accommodated with this option. |  |  | There is no transit service in the vicinity of this intersection. |  |  |  | This option was designed to accommodate the designs trucks at the turns. |  |  |
| Roundabout | Crosswalks and bicycle lanes can be accommodated with this option. |  |  | There is no transit service in the vicinity of this intersection. |  |  |  | This option was designed to accommodate the designs trucks at the turns. |  |  |
| RCUT (Signalized) | Crosswalks and bicycle lanes can be accommodated with this option. |  |  | There is no transit service in the vicinity of this intersection. |  |  |  | This option was designed to accommodate the designs trucks at the turns. |  |  |
| Displaced Left-Turn | Crosswalks and bicycle lanes can be accommodated with this option. |  |  | There is no transit service in the vicinity of this intersection. |  |  |  | This option was designed to accommodate the designs trucks at the turns. |  |  |
| Continuous Green Tee | Crosswalks and bicycle lanes can be accommodated with this option. |  |  | There is no transit service in the vicinity of this intersection. |  |  |  | This option was designed to accommodate the designs trucks at the turns. |  |  |
|  |  |  |  |  |  |  |  |  |  |  |


| Environmental, Utility, and Right-of-Way Impacts <br> Summarize any issues related to environmental, utility, or right-of-way (including relocation) impacts specific to each control strategy. Be sure to consider <br> the NEPA requirements for each control type. |  |
| :--- | :--- |
| Signalized Control | No right of way acquisition required and no new environmental impacts are anticipated. The overhead transmission lines on <br> the north side of the corridor are not expected to be impacted. |
| Roundabout | No right of way acquisition required and no new environmental impacts are anticipated. The overhead transmission lines on <br> the north side of the corridor are not expected to be impacted. |
| RCUT (Signalized) | No right of way acquisition required and no new environmental impacts are anticipated. The overhead transmission lines on <br> the north side of the corridor are not expected to be impacted. |
| Displaced Left-Turn | Right of way acquisition may be needed to accommodate displaced left turns. Potential for environmental impacts on the <br> south side of SR 70. No impacts to the overhead transmission lines on the north side. |
| Continuous Green Tee | No right of way acquisition required and no new environmental impacts are anticipated. The overhead transmission lines on <br> the north side of the corridor are not expected to be impacted. |

Provide a brief justification as to why each of the following is either viable or not viable. If a single control strategy is recommended, select it as the only strategy to be advanced.

| Control Strategy | Strategy to be <br> Advanced? |  |
| :---: | :--- | :--- |
| Signalized Control | No | This option was analyzed as the base intersection control which is why the B/C ratio is zero. The <br> Roundabout and Continuous Green-Tee higher benefits relative to their cost. |
| Roundabout | Yes | 1) Preferred option based on B/C analysis and NPV compared to base; 2) less severe crashes ; 3) <br> traffic operations at LOS B or better; 4) no right of way impacts; and, 5) enhances the livable <br> communities characteristic by lowering vehicle speeds and providing shorter crosswalk distances. |
| RCUT (Signalized) | No | Although this option has a high overall B/C ratio, it does not share the benefits to delay when <br> compared to the Roundabout and Continuos Green Tee options. |
| Displaced Left-Turn | No | This option had a negative Net Present Value (NPV); therefore, it is not cost feasible compared to <br> the base option of a signalized intersection. |
| Continuous Green Tee | No | This option had the second highest overall B/C. However, the roundabout is the preferred option <br> based on the B/C analysis. |
| No |  |  |


| Resolution |  |  |  |
| :---: | :---: | :---: | :---: |
| To be filled out by FDOT District Traffic Operations Engineer and District Design Engineer |  |  |  |
| Project Determination |  |  | \% |
| Comments |  |  |  |
| DTOE Name | Signature |  | Date |
| DDE Name | Signature |  | Date |

# ATTACHMENT B Conceptual Plans 

## SR 70 and Del Webb Boulevard <br> Signalized Intersection



## SR 70 and Del Webb Boulevard Roundabout



## SR 70 and Del Webb Boulevard Signalized Restricted Crossing U-Tum (RCUT)



## SR 70 and Del Webb Boulevard Partial Displaced Left-Tum (East-West)



## SR 70 and Del Webb Boulevard Continuous Green-Tee

## Key Features:

- One new signalized intersection
- Westbound-through is a free flow movement
- Acceleration lane for the northbound-left tum movement to merge with the westbound-through
- No right-of-way acquisition needed
- No impacts to overhead transmission lines on north side of roadway



## ATTACHMENT C

## Traffic Operational Analysis







## 8: U-turn \& SR 70




## 8: U-turn \& SR 70



|  | $\rightarrow$ | 7 | $\checkmark$ | 4 | 4 | $p$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |  |
| Lane Configurations | 44 | 「 | * | 44 |  | 「" |  |
| Traffic Volume (vph) | 793 | 150 | 38 | 1155 | 0 | 170 |  |
| Future Volume (vph) | 793 | 150 | 38 | 1155 | 0 | 170 |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |  |
| Total Lost time (s) | 6.0 | 6.0 | 6.0 | 4.0 |  | 6.0 |  |
| Lane Util. Factor | 0.95 | 1.00 | 1.00 | 0.95 |  | 0.88 |  |
| Frt | 1.00 | 0.85 | 1.00 | 1.00 |  | 0.85 |  |
| Flt Protected | 1.00 | 1.00 | 0.95 | 1.00 |  | 1.00 |  |
| Satd. Flow (prot) | 3374 | 1509 | 1687 | 3374 |  | 2787 |  |
| Flt Permitted | 1.00 | 1.00 | 0.34 | 1.00 |  | 1.00 |  |
| Satd. Flow (perm) | 3374 | 1509 | 599 | 3374 |  | 2787 |  |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |  |
| Adj. Flow (vph) | 835 | 158 | 40 | 1216 | 0 | 179 |  |
| RTOR Reduction (vph) | 0 | 56 | 0 | 0 | 0 | 104 |  |
| Lane Group Flow (vph) | 835 | 102 | 40 | 1216 | 0 | 75 |  |
| Heavy Vehicles (\%) | 7\% | 7\% | 7\% | 7\% | 2\% | 2\% |  |
| Turn Type | NA | Perm | D.P+P | NA |  | Over |  |
| Protected Phases | 2 |  | 1 | Free |  | 1 |  |
| Permitted Phases |  | 2 | 2 |  |  |  |  |
| Actuated Green, G (s) | 32.2 | 32.2 | 38.0 | 50.0 |  | 5.8 |  |
| Effective Green, g (s) | 32.2 | 32.2 | 38.0 | 50.0 |  | 5.8 |  |
| Actuated g/C Ratio | 0.64 | 0.64 | 0.76 | 1.00 |  | 0.12 |  |
| Clearance Time (s) | 6.0 | 6.0 | 6.0 |  |  | 6.0 |  |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 |  |  | 3.0 |  |
| Lane Grp Cap (vph) | 2172 | 971 | 581 | 3374 |  | 323 |  |
| v/s Ratio Prot | 0.25 |  | 0.01 | 0.36 |  | 0.03 |  |
| v/s Ratio Perm |  | 0.07 | 0.04 |  |  |  |  |
| v/c Ratio | 0.38 | 0.10 | 0.07 | 0.36 |  | 0.23 |  |
| Uniform Delay, d1 | 4.2 | 3.4 | 1.5 | 0.0 |  | 20.1 |  |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 |  |
| Incremental Delay, d2 | 0.5 | 0.2 | 0.1 | 0.3 |  | 0.4 |  |
| Delay (s) | 4.7 | 3.6 | 1.5 | 0.3 |  | 20.4 |  |
| Level of Service | A | A | A | A |  | C |  |
| Approach Delay (s) | 4.6 |  |  | 0.3 | 20.4 |  |  |
| Approach LOS | A |  |  | A | C |  |  |
| Intersection Summary |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  |  | 3.5 |  | HCM 2000 | Level of Service | A |
| HCM 2000 Volume to Capacity ratio |  |  | 0.47 |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 50.0 |  | Sum of lost | me (s) | 12.0 |
| Intersection Capacity Utilization |  |  | 37.9\% |  | ICU Level of | Service | A |
| Analysis Period (min) |  |  | 15 |  |  |  |  |
| C Critical Lane Group |  |  |  |  |  |  |  |

8: U-turn \& SR 70



## 8: U-turn \& SR 70





c Critical Lane Group



c Critical Lane Group

|  | $\rightarrow$ | $\checkmark$ | $\square$ | 7 |  | 4 | $p$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBT | EBR | WBU | WBL | WBT | NBL | NBR |  |
| Lane Configurations | 44 | 「 | $\square$ |  | 44 | ${ }^{1}$ |  |  |
| Traffic Volume (vph) | 793 | 150 | 0 | 0 | 1155 | 125 | 0 |  |
| Future Volume (vph) | 793 | 150 | 0 | 0 | 1155 | 125 | 0 |  |
| Ideal Flow (vphpl) | 1950 | 1950 | 1950 | 1950 | 1950 | 1950 | 1950 |  |
| Total Lost time (s) | 6.0 | 6.0 |  |  | 6.0 | 6.0 |  |  |
| Lane Util. Factor | 0.95 | 1.00 |  |  | 0.95 | 1.00 |  |  |
| Frt | 1.00 | 0.85 |  |  | 1.00 | 1.00 |  |  |
| Flt Protected | 1.00 | 1.00 |  |  | 1.00 | 0.95 |  |  |
| Satd. Flow (prot) | 3463 | 1549 |  |  | 3463 | 1816 |  |  |
| Flt Permitted | 1.00 | 1.00 |  |  | 1.00 | 0.95 |  |  |
| Satd. Flow (perm) | 3463 | 1549 |  |  | 3463 | 1816 |  |  |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |  |
| Adj. Flow (vph) | 835 | 158 | 0 | 0 | 1216 | 132 | 0 |  |
| RTOR Reduction (vph) | 0 | 57 | 0 | 0 | 0 | 0 | 0 |  |
| Lane Group Flow (vph) | 835 | 101 | 0 | 0 | 1216 | 132 | 0 |  |
| Heavy Vehicles (\%) | 7\% | 7\% | 2\% | 7\% | 7\% | 2\% | 2\% |  |
| Turn Type | NA | Perm | Perm |  | NA | Prot |  | - |
| Protected Phases | 12 |  |  |  | 12 | 34 |  |  |
| Permitted Phases |  | 12 | 12 |  |  |  |  |  |
| Actuated Green, G (s) | 60.6 | 60.6 |  |  | 60.6 | 22.4 |  |  |
| Effective Green, g (s) | 60.6 | 60.6 |  |  | 60.6 | 22.4 |  |  |
| Actuated g/C Ratio | 0.64 | 0.64 |  |  | 0.64 | 0.24 |  |  |
| Clearance Time (s) |  |  |  |  |  |  |  |  |
| Vehicle Extension (s) |  |  |  |  |  |  |  |  |
| Lane Grp Cap (vph) | 2209 | 988 |  |  | 2209 | 428 |  |  |
| v/s Ratio Prot | 0.24 |  |  |  | c0.35 | c0.07 |  |  |
| v/s Ratio Perm |  | 0.07 |  |  |  |  |  |  |
| v/c Ratio | 0.38 | 0.10 |  |  | 0.55 | 0.31 |  |  |
| Uniform Delay, d1 | 8.2 | 6.7 |  |  | 9.6 | 29.9 |  |  |
| Progression Factor | 1.00 | 1.00 |  |  | 1.00 | 0.20 |  |  |
| Incremental Delay, d2 | 0.1 | 0.0 |  |  | 0.3 | 0.4 |  |  |
| Delay (s) | 8.3 | 6.7 |  |  | 9.9 | 6.3 |  |  |
| Level of Service | A | A |  |  | A | A |  |  |
| Approach Delay (s) | 8.1 |  |  |  | 9.9 | 6.3 |  |  |
| Approach LOS | A |  |  |  | A | A |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  |  | 8.9 | HCM 2000 Level of Service |  |  |  | A |
|  |  |  | 0.57 |  |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 95.0 |  | Sum of los | ime (s) |  | 24.0 |
| Intersection Capacity Utilization |  |  | 47.9\% |  | CU Level | Service |  | A |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |
| c Critical Lane Group |  |  |  |  |  |  |  |  |



c Critical Lane Group



c Critical Lane Group





SR 70 @ DEL WEBB BLVD ROUNDABOUT ANALYSIS

| 2025 OPENING YEAR (HCM 6th Edition) |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach | Delay (s) |  | Level of Service |  | v/c Ratio |  | 95th \% Queue (ft) |  |
|  | AM | PM | AM | PM | AM | PM | AM | PM |
| Overall | 6.1 | 6.2 | A | A |  |  |  |  |
| SR 70 EB | 5.2 | 6.5 | A | A | 0.26 | 0.38 | 35 | 55 |
| SR 70 WB | 6.8 | 5.5 | A | A | 0.38 | 0.26 | 55 | 30 |
| Del Webb Blvd NB | 5.7 | 8.3 | A | A | 0.11 | 0.17 | 25 | 25 |


| 2025 OPENING YEAR (Sidra Standard) |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach | Delay (s) |  | Level of Service |  | v/c Ratio |  | 95th \% Queue (ft) |  |
|  | AM | PM | AM | PM | AM | PM | AM | PM |
| Overall | 4.1 | 4.3 | A | A |  |  |  |  |
| SR 70 EB | 3.6 | 3.6 | A | A | 0.22 | 0.31 | 35 | 55 |
| SR 70 WB | 3.7 | 3.8 | A | A | 0.31 | 0.21 | 60 | 35 |
| Del Webb Blvd NB | 11.6 | 13.4 | B | B | 0.12 | 0.16 | 25 | 25 |


| 2045 DESIGN YEAR (HCM 6th Edition) |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach | Delay (s) |  | Level of Service |  | v/c Ratio |  | 95th \% Queue (ft) |  |  |  |
|  | AM | PM | AM | PM | AM | PM | AM | PM |  |  |
|  | $\mathbf{8 . 9}$ | $\mathbf{9 . 7}$ | A | A |  |  |  |  |  |  |
| SR 70 EB | 7.1 | 9.9 | A | A | 0.41 | 0.58 | 60 | 115 |  |  |
| SR 70 WB | 10.2 | 7.4 | B | A | 0.57 | 0.40 | 100 | 55 |  |  |
| Del Webb Blvd NB | 10.1 | 18.2 | B | C | 0.30 | 0.45 | 30 | 50 |  |  |


| 2045 DESIGN YEAR (Sidra Standard) |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach | Delay (s) |  | Level of Service |  | v/c Ratio |  | 95th \% Queue (ft) |  |
|  | AM | PM | AM | PM | AM | PM | AM | PM |
| Overall | 4.7 | 5.0 | A | A |  |  |  |  |
| SR 70 EB | 3.8 | 3.9 | A | A | 0.34 | 0.48 | 65 | 110 |
| SR 70 WB | 4.3 | 4.4 | A | A | 0.47 | 0.33 | 105 | 65 |
| Del Webb Blvd NB | 12.7 | 16.0 | B | C | 0.29 | 0.37 | 30 | 40 |

## SITE LAYOUT

Site: [SR 70 \& Del Webb Blvd]
Site Category: (None)
Roundabout


SIDRA INTERSECTION 8.0 | Copyright © 2000-2018 Akcelik and Associates Pty Ltd | sidrasolutions.com
Organisation: STANTEC | Created: Thursday, January 24, 2019 7:28:11 PM
Project: C:IProjects\SR 70ISR70_del_webb_2025_2045_am_pm_hcm6.sip8

## MOVEMENT SUMMARY

Site: [SR 70 \& Del Webb Blvd]
2025 AM Peak-Hour
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ |  | Deman Total veh/h | $\begin{gathered} \text { lows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed mph |
| South: Del Webb Blvd |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 72 | 2.0 | 0.112 | 5.7 | LOS A | 0.4 | 10.1 | 0.51 | 0.47 | 0.51 | 33.0 |
| 18 | R2 | 16 | 2.0 | 0.112 | 5.7 | LOS A | 0.4 | 10.1 | 0.51 | 0.47 | 0.51 | 31.9 |
| Appr |  | 87 | 2.0 | 0.112 | 5.7 | LOS A | 0.4 | 10.1 | 0.51 | 0.47 | 0.51 | 32.8 |
| East: SR 70 |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 12 | 7.0 | 0.380 | 6.8 | LOS A | 2.0 | 53.5 | 0.26 | 0.12 | 0.26 | 34.9 |
| 8 | T1 | 883 | 7.0 | 0.380 | 6.8 | LOS A | 2.0 | 53.5 | 0.26 | 0.12 | 0.26 | 34.8 |
| Approach |  | 895 | 7.0 | 0.380 | 6.8 | LOS A | 2.0 | 53.5 | 0.26 | 0.12 | 0.26 | 34.8 |
| West: SR 70 |  |  |  |  |  |  |  |  |  |  |  |  |
| $\begin{aligned} & 4 \\ & 12 \end{aligned}$ | T1 | 552 | 7.0 | 0.263 | 5.2 | LOS A | 1.2 | 32.9 | 0.08 | 0.02 | 0.08 | 35.6 |
|  | R2 | 104 | 7.0 | 0.263 | 5.2 | LOS A | 1.2 | 32.9 | 0.08 | 0.02 | 0.08 | 34.2 |
| Approach |  | 656 | 7.0 | 0.263 | 5.2 | LOS A | 1.2 | 32.9 | 0.08 | 0.02 | 0.08 | 35.4 |
| All Vehicles |  | 1638 | 6.7 | 0.380 | 6.1 | LOS A | 2.0 | 53.5 | 0.20 | 0.10 | 0.20 | 34.9 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: Same as Sign Control.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement. LOS F will result if v/c>1 irrespective of movement delay value (does not apply for approaches and intersection). Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010). Roundabout Capacity Model: US HCM 6.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: Traditional M1.
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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Project: C:IProjects\SR 70ISR70_del_webb_2025_2045_am_pm_hcm6.sip8

## MOVEMENT SUMMARY

Site: [SR 70 \& Del Webb Blvd]
2025 AM Peak-Hour
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ |  | Deman Total veh/h | $\begin{gathered} \text { lows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance ft | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed mph |
| South: Del Webb Blvd |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 72 | 2.0 | 0.121 | 12.7 | LOS B | 0.4 | 11.2 | 0.50 | 0.77 | 0.50 | 34.5 |
| 18 | R2 | 16 | 2.0 | 0.121 | 6.3 | LOS A | 0.4 | 11.2 | 0.50 | 0.77 | 0.50 | 33.3 |
| Appr |  | 87 | 2.0 | 0.121 | 11.6 | LOS B | 0.4 | 11.2 | 0.50 | 0.77 | 0.50 | 34.3 |
| East: SR 70 |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 12 | 7.0 | 0.313 | 10.5 | LOS B | 2.2 | 57.7 | 0.29 | 0.37 | 0.29 | 37.7 |
| 8 | T1 | 883 | 7.0 | 0.313 | 3.6 | LOS A | 2.2 | 58.5 | 0.28 | 0.36 | 0.28 | 37.8 |
| Approach |  | 895 | 7.0 | 0.313 | 3.7 | LOS A | 2.2 | 58.5 | 0.28 | 0.36 | 0.28 | 37.8 |
| West: SR 70 |  |  |  |  |  |  |  |  |  |  |  |  |
| $\begin{aligned} & 4 \\ & 12 \end{aligned}$ | T1 | 552 | 7.0 | 0.217 | 3.6 | LOS A | 1.3 | 34.3 | 0.09 | 0.34 | 0.09 | 38.4 |
|  | R2 | 104 | 7.0 | 0.217 | 3.9 | LOS A | 1.3 | 34.3 | 0.08 | 0.36 | 0.08 | 36.8 |
| Approach |  | 656 | 7.0 | 0.217 | 3.6 | LOS A | 1.3 | 34.3 | 0.09 | 0.35 | 0.09 | 38.1 |
| All Vehicles |  | 1638 | 6.7 | 0.313 | 4.1 | LOS A | 2.2 | 58.5 | 0.21 | 0.38 | 0.21 | 37.7 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement. LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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Project: C:IProjects\SR 70ISR70_del_webb_2025_2045_am_pm_sidra.sip8

## MOVEMENT SUMMARY

Site: [SR 70 \& Del Webb Blvd]
2025 PM Peak-Hour
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ |  | Deman Total veh/h | $\begin{gathered} \text { lows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance ft | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed mph |
| South: Del Webb Blvd |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 94 | 2.0 | 0.173 | 8.3 | LOS A | 0.6 | 15.4 | 0.62 | 0.62 | 0.62 | 31.7 |
| 18 | R2 | 8 | 2.0 | 0.173 | 8.3 | LOS A | 0.6 | 15.4 | 0.62 | 0.62 | 0.62 | 30.6 |
| Appr |  | 102 | 2.0 | 0.173 | 8.3 | LOS A | 0.6 | 15.4 | 0.62 | 0.62 | 0.62 | 31.6 |
| East: SR 70 |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 14 | 7.0 | 0.255 | 5.5 | LOS A | 1.2 | 30.7 | 0.25 | 0.13 | 0.25 | 35.5 |
| 8 | T1 | 576 | 7.0 | 0.255 | 5.5 | LOS A | 1.2 | 30.7 | 0.25 | 0.13 | 0.25 | 35.5 |
| Approach |  | 589 | 7.0 | 0.255 | 5.5 | LOS A | 1.2 | 30.7 | 0.25 | 0.13 | 0.25 | 35.5 |
| West: SR 70 |  |  |  |  |  |  |  |  |  |  |  |  |
| $\begin{aligned} & 4 \\ & 12 \end{aligned}$ | T1 | 851 | 7.0 | 0.378 | 6.5 | LOS A | 2.1 | 55.0 | 0.10 | 0.03 | 0.10 | 34.9 |
|  | R2 | 91 | 7.0 | 0.378 | 6.5 | LOS A | 2.1 | 55.0 | 0.10 | 0.03 | 0.10 | 33.6 |
| Approach |  | 941 | 7.0 | 0.378 | 6.5 | LOS A | 2.1 | 55.0 | 0.10 | 0.03 | 0.10 | 34.8 |
| All Vehicles |  | 1633 | 6.7 | 0.378 | 6.2 | LOS A | 2.1 | 55.0 | 0.19 | 0.10 | 0.19 | 34.8 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: Same as Sign Control.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement. LOS F will result if v/c>1 irrespective of movement delay value (does not apply for approaches and intersection). Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010). Roundabout Capacity Model: US HCM 6.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: Traditional M1.
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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Project: C:IProjects\SR 70ISR70_del_webb_2025_2045_am_pm_hcm6.sip8

## MOVEMENT SUMMARY

Site: [SR 70 \& Del Webb Blvd]
2025 PM Peak-Hour
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ |  | Deman Total veh/h | $\begin{gathered} \text { lows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance ft | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed mph |
| South: Del Webb Blvd |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 94 | 2.0 | 0.164 | 14.0 | LOS B | 0.6 | 15.2 | 0.58 | 0.85 | 0.58 | 33.6 |
| 18 | R2 | 8 | 2.0 | 0.164 | 7.6 | LOS A | 0.6 | 15.2 | 0.58 | 0.85 | 0.58 | 32.5 |
| Appr |  | 102 | 2.0 | 0.164 | 13.4 | LOS B | 0.6 | 15.2 | 0.58 | 0.85 | 0.58 | 33.5 |
| East: SR 70 |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 14 | 7.0 | 0.212 | 10.5 | LOS B | 1.3 | 35.3 | 0.30 | 0.39 | 0.30 | 37.6 |
| 8 | T1 | 576 | 7.0 | 0.212 | 3.6 | LOS A | 1.4 | 36.1 | 0.29 | 0.38 | 0.29 | 37.7 |
| Approach |  | 589 | 7.0 | 0.212 | 3.8 | LOS A | 1.4 | 36.1 | 0.29 | 0.38 | 0.29 | 37.7 |
| West: SR 70 |  |  |  |  |  |  |  |  |  |  |  |  |
| $\begin{aligned} & 4 \\ & 12 \end{aligned}$ | T1 | 851 | 7.0 | 0.313 | 3.6 | LOS A | 2.1 | 56.2 | 0.11 | 0.34 | 0.11 | 38.3 |
|  | R2 | 91 | 7.0 | 0.313 | 3.9 | LOS A | 2.1 | 56.2 | 0.10 | 0.35 | 0.10 | 36.8 |
| Approach |  | 941 | 7.0 | 0.313 | 3.6 | LOS A | 2.1 | 56.2 | 0.11 | 0.34 | 0.11 | 38.2 |
| All Vehicles |  | 1633 | 6.7 | 0.313 | 4.3 | LOS A | 2.1 | 56.2 | 0.20 | 0.39 | 0.20 | 37.7 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement. LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## MOVEMENT SUMMARY

Site: [SR 70 \& Del Webb Blvd]
2045 AM Peak-Hour
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ |  | Deman Total veh/h | $\begin{gathered} \text { lows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance ft | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed mph |
| South: Del Webb Blvd |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 132 | 2.0 | 0.300 | 10.1 | LOS B | 1.2 | 29.5 | 0.65 | 0.67 | 0.71 | 31.3 |
| 18 | R2 | 47 | 2.0 | 0.300 | 10.1 | LOS B | 1.2 | 29.5 | 0.65 | 0.67 | 0.71 | 30.3 |
| Appr |  | 179 | 2.0 | 0.300 | 10.1 | LOS B | 1.2 | 29.5 | 0.65 | 0.67 | 0.71 | 31.1 |
| East: SR 70 |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 40 | 7.0 | 0.565 | 10.2 | LOS B | 3.7 | 98.7 | 0.45 | 0.28 | 0.45 | 33.0 |
| 8 | T1 | 1216 | 7.0 | 0.565 | 10.2 | LOS B | 3.7 | 98.7 | 0.45 | 0.28 | 0.45 | 33.1 |
| Approach |  | 1256 | 7.0 | 0.565 | 10.2 | LOS B | 3.7 | 98.7 | 0.45 | 0.28 | 0.45 | 33.1 |
| West: SR 70 |  |  |  |  |  |  |  |  |  |  |  |  |
| $\begin{aligned} & 4 \\ & 12 \end{aligned}$ | T1 | 835 | 7.0 | 0.409 | 7.1 | LOS A | 2.3 | 61.2 | 0.20 | 0.08 | 0.20 | 34.6 |
|  | R2 | 158 | 7.0 | 0.409 | 7.1 | LOS A | 2.3 | 61.2 | 0.20 | 0.08 | 0.20 | 33.3 |
| Approach |  | 993 | 7.0 | 0.409 | 7.1 | LOS A | 2.3 | 61.2 | 0.20 | 0.08 | 0.20 | 34.4 |
| All Vehicles |  | 2427 | 6.6 | 0.565 | 8.9 | LOS A | 3.7 | 98.7 | 0.36 | 0.23 | 0.37 | 33.4 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: Same as Sign Control.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement. LOS F will result if v/c>1 irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010). Roundabout Capacity Model: US HCM 6.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: Traditional M1.
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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Project: C:IProjectsISR 70ISR70_del_webb_2025_2045_am_pm_hcm6.sip8

## MOVEMENT SUMMARY

Site: [SR 70 \& Del Webb Blvd]
2045 AM Peak-Hour
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ |  | Deman Total veh/h | $\begin{aligned} & \text { lows } \\ & \text { HV } \\ & \% \end{aligned}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance ft | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed mph |
| South: Del Webb Blvd |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 132 | 2.0 | 0.294 | 14.3 | LOS B | 1.2 | 30.2 | 0.63 | 0.86 | 0.63 | 34.0 |
| 18 | R2 | 47 | 2.0 | 0.294 | 8.0 | LOS A | 1.2 | 30.2 | 0.63 | 0.86 | 0.63 | 32.8 |
| Appr |  | 179 | 2.0 | 0.294 | 12.7 | LOS B | 1.2 | 30.2 | 0.63 | 0.86 | 0.63 | 33.6 |
| East: SR 70 |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 40 | 7.0 | 0.468 | 11.0 | LOS B | 3.9 | 102.5 | 0.47 | 0.46 | 0.47 | 36.9 |
| 8 | T1 | 1216 | 7.0 | 0.468 | 4.0 | LOS A | 4.0 | 105.4 | 0.46 | 0.43 | 0.46 | 37.0 |
| Approach |  | 1256 | 7.0 | 0.468 | 4.3 | LOS A | 4.0 | 105.4 | 0.46 | 0.43 | 0.46 | 37.0 |
| West: SR 70 |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | T1 | 835 | 7.0 | 0.340 | 3.8 | LOS A | 2.5 | 65.7 | 0.22 | 0.36 | 0.22 | 37.9 |
|  | R2 | 158 | 7.0 | 0.340 | 4.0 | LOS A | 2.5 | 65.7 | 0.21 | 0.37 | 0.21 | 36.4 |
| Appr |  | 993 | 7.0 | 0.340 | 3.8 | LOS A | 2.5 | 65.7 | 0.21 | 0.36 | 0.21 | 37.6 |
| All V | icles | 2427 | 6.6 | 0.468 | 4.7 | LOS A | 4.0 | 105.4 | 0.37 | 0.43 | 0.37 | 37.0 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement. LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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Project: C:IProjects\SR 70ISR70_del_webb_2025_2045_am_pm_sidra.sip8

## MOVEMENT SUMMARY

Site: [SR 70 \& Del Webb Blvd]
2045 PM Peak-Hour
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \mathrm{Mov} \\ & \mathrm{ID} \end{aligned}$ |  | Deman Total veh/h | $\begin{aligned} & \text { lows } \\ & \text { HV } \\ & \% \\ & \hline \end{aligned}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance <br> ft | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed mph |
| South: Del Webb Blvd |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 155 | 2.0 | 0.448 | 18.2 | LOS C | 1.9 | 48.4 | 0.80 | 0.90 | 1.18 | 28.1 |
| 18 | R2 | 26 | 2.0 | 0.448 | 18.2 | LOS C | 1.9 | 48.4 | 0.80 | 0.90 | 1.18 | 27.2 |
| Appro |  | 181 | 2.0 | 0.448 | 18.2 | LOS C | 1.9 | 48.4 | 0.80 | 0.90 | 1.18 | 27.9 |
| East: SR 70 |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 48 | 7.0 | 0.396 | 7.4 | LOS A | 2.1 | 54.2 | 0.39 | 0.25 | 0.39 | 34.2 |
| 8 | T1 | 812 | 7.0 | 0.396 | 7.4 | LOS A | 2.1 | 54.2 | 0.39 | 0.25 | 0.39 | 34.4 |
| Approach |  | 860 | 7.0 | 0.396 | 7.4 | LOS A | 2.1 | 54.2 | 0.39 | 0.25 | 0.39 | 34.4 |
| West: SR 70 |  |  |  |  |  |  |  |  |  |  |  |  |
| $\begin{aligned} & 4 \\ & 12 \end{aligned}$ | T1 | 1244 | 7.0 | 0.578 | 9.9 | LOS A | 4.3 | 112.6 | 0.29 | 0.13 | 0.29 | 33.2 |
|  | R2 | 147 | 7.0 | 0.578 | 9.9 | LOS A | 4.3 | 112.6 | 0.29 | 0.13 | 0.29 | 32.0 |
| Approach |  | 1392 | 7.0 | 0.578 | 9.9 | LOS A | 4.3 | 112.6 | 0.29 | 0.13 | 0.29 | 33.1 |
| All Vehicles |  | 2433 | 6.6 | 0.578 | 9.7 | LOS A | 4.3 | 112.6 | 0.36 | 0.23 | 0.39 | 33.0 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: Same as Sign Control.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement. LOS F will result if v/c>1 irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010). Roundabout Capacity Model: US HCM 6.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: Traditional M1.
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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Project: C:IProjects\SR 70ISR70_del_webb_2025_2045_am_pm_hcm6.sip8

## MOVEMENT SUMMARY

Site: [SR 70 \& Del Webb Blvd]
2045 PM Peak-Hour
Site Category: (None)
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ |  | Deman Total veh/h | $\begin{array}{r} \text { lows } \\ \text { HV } \\ \% \\ \hline \end{array}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance ft | Prop. Queued | Effective Stop Rate | Aver. No. Cycles | Average Speed $\qquad$ mph |
| South: Del Webb Blvd |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 155 | 2.0 | 0.371 | 16.9 | LOS B | 1.6 | 41.8 | 0.73 | 0.94 | 0.84 | 32.4 |
| 18 | R2 | 26 | 2.0 | 0.371 | 10.5 | LOS B | 1.6 | 41.8 | 0.73 | 0.94 | 0.84 | 31.4 |
| Appr |  | 181 | 2.0 | 0.371 | 16.0 | LOS B | 1.6 | 41.8 | 0.73 | 0.94 | 0.84 | 32.3 |
| East: SR 70 |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 48 | 7.0 | 0.329 | 11.0 | LOS B | 2.3 | 61.9 | 0.45 | 0.47 | 0.45 | 36.9 |
| 8 | T1 | 812 | 7.0 | 0.329 | 4.0 | LOS A | 2.4 | 64.2 | 0.43 | 0.43 | 0.43 | 37.0 |
| Approach |  | 860 | 7.0 | 0.329 | 4.4 | LOS A | 2.4 | 64.2 | 0.44 | 0.44 | 0.44 | 37.0 |
| West: SR 70 |  |  |  |  |  |  |  |  |  |  |  |  |
|  | T1 | 1244 | 7.0 | 0.481 | 3.9 | LOS A | 4.2 | 110.3 | 0.28 | 0.37 | 0.28 | 37.6 |
|  | R2 | 147 | 7.0 | 0.481 | 4.2 | LOS A | 4.2 | 110.3 | 0.27 | 0.37 | 0.27 | 36.1 |
| Approach |  | 1392 | 7.0 | 0.481 | 3.9 | LOS A | 4.2 | 110.3 | 0.28 | 0.37 | 0.28 | 37.4 |
| All Vehicles |  | 2433 | 6.6 | 0.481 | 5.0 | LOS A | 4.2 | 110.3 | 0.37 | 0.43 | 0.38 | 36.8 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 2010). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement. LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

SIDRA INTERSECTION 8.0 | Copyright © 2000-2018 Akcelik and Associates Pty Ltd | sidrasolutions.com
Organisation: STANTEC | Processed: Thursday, January 24, 2019 9:22:43 PM
Project: C:IProjects\SR 70ISR70_del_webb_2025_2045_am_pm_sidra.sip8

# ATTACHMENT D Safety Performance for Intersection Control Evaluation (SPICE) 

| Federal Highway Administration (FHWA)Safety Performance for Intersection Control Evaluation Tool |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Results |  |  |  |  |  |  |  |
| Summary of crash prediction results for each alternative |  |  |  |  |  |  |  |
| Project Information |  |  |  |  |  |  |  |
| Project Name: | SR 70 from Lorraine Rd to CR 675 |  |  | Intersection Type |  | At-Grade Intersections |  |
| Intersection: | SR 70 @ Del Webb |  |  | Opening Year |  | 2025 |  |
| Agency: | D1 |  |  | Design Year |  | 2045 |  |
| Project Reference: | 414506-2-22-01 |  |  | Facility Type |  | On Urban and Suburban Arterial |  |
| City: | Unincorporated Manatee County |  |  | Number of Legs |  | 3-leg |  |
| State: | FL |  |  | 1-Way/2-Way |  | 2-way Intersecting 2-way |  |
| Date: | 6/14/2019 |  |  | \# of Major Street Lanes (both directions) |  | 5 or fewer |  |
| Analyst: | Nicole Harris, PE |  |  | Major Street Approach Speed |  | Less than 55 mph |  |
| Crash Prediction Summary |  |  |  |  |  |  |  |
| Control Strategy | Crash Type | Opening Year | Design Year | Total Project Life Cycle | Rank | AADT Within Prediction Range? | Source of Prediction |
| Traffic Signal | Fatal \& Injury | $\begin{aligned} & 3.26 \\ & 1.23 \end{aligned}$ | $\begin{aligned} & \hline 5.31 \\ & 1.91 \end{aligned}$ | $\begin{aligned} & 89.50 \\ & 32.85 \end{aligned}$ | 5 | Yes | Calibrated SPF |
| 2-lane Roundabout | Total |  | $8.01$ | $139.11$ | 1 | N/A | Uncalibrated SPF |
|  | Fatal \& Injury | 0.89 | 1.47 |  |  |  |  |
| Displaced Left Turn (DLT) | Total | 2.86 | 4.67 | 78.76 | 4 | N/A | CMF |
|  | Fatal \& Injury | 1.08 | 1.68 | 28.90 |  |  |  |
| Signalized RCUT | Total | 2.77 | 4.51 | 76.08 | 2 | N/A | CMF |
|  | Fatal \& Injury | 0.96 | 1.49 | 25.62 | 2 | N/A | CMF |
| Continuous Green-T Intersection | Total | 3.13 | 5.09 | 85.92 | 3 | N/A | CMF |
|  | Fatal \& Injury | 1.04 | 1.62 | 27.92 | 3 |  |  |

## SR 70 and Del Webb Boulevard Signalized Intersection (base condition) Cost Estimate



## SR 70 and Del Webb Boulevard Roundabout Intersection Cost Estimate



## SR 70 and Del Webb Boulevard Continuous Green Tee Intersection Cost Estimate



# SR 70 and Del Webb Boulevard Restricted Crossing U-Tum Intersection Cost Estimate 



## SR 70 and Del Webb Boulevard Partial Displaced Left Intersection Cost Estimate

| Pay Item | Description | Total Quantity | Unit | Weighted Avg. Unit Price |  | Amount | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ROADWAY: Area of influence of intersection is 2200 -ft or 0.42 miles along SR 70 |  |  |  |  |  |  | This area area will be fully reconstructed |
| 101-1 | MOBILZATION | 10.00 | \% |  | \$ | 200,589.91 |  |
| 102-1 | M AINTENANCE OF TRAFFIC | 10.00 | \% |  | \$ | 200,589.91 |  |
| 110-1-1 | CLEARING \& GRUBBING | 10.10 | AC | \$ 11,000.00 | \$ | 111,111.11 | C lear area within the right of way in the 1800-ft limits: ( $2200 * 200$ $\qquad \mathrm{ft}) / 43560=10.10 \mathrm{AC}$ |
| 120-1 | REGULAR EXCAVATION | 4,065.60 | CY | \$ 5.10 | \$ | 20,734.56 | Cost per mile from model @ 0.42 miles |
| 160-4 | TYPE B STABILZATION | 24,059.78 | SY | \$ 3.80 | \$ | 91,427.16 | Area to be constructed and stabilized including unpaved shoulders - Use shapes from DGN |
| 285-709 | OPTIONAL BASE,BASE GROUP 09 | 21,653.00 | SY | \$ 17.00 | \$ | 368,101.00 | Paved area to be constructed |
| 327-70-4 | MILUNG EXISTASPH PAVT, 3"AVG DEPTH | 321.22 | SY | \$ 2.40 | \$ | 770.93 | Area to be milled and resurfaced: Use typical section ( 2891 SF/9) for side street - shape |
| 334-1-24 | SUPERPAVE ASPH CONC, TRAF D, PG 76-22,PMA | 4,362.70 | TN | \$ 100.00 | \$ | 436,270.00 | Assume Traffic C: Area to be contructed +Area to be milled: ( $13538 * 400+$ 9351*200 )/2000 - Use Optional Base Group Area fornew construction |
| 337-7-41 | ASPH CONC FC,TRAFFIC B,FC-12.5,PG 76-22 | 878.96 | TN | \$ 105.00 | \$ | 92,290.80 | Assume Traffic C : $(13538 * 80+9351 \mathrm{SY} * 80) / 2000$ |
| 430-175-112 | PIPE CULV, OPTMATL, ROUND, 12"S/CD | 813.12 | LF | \$ 91.00 | \$ | 73,993.92 | Cost per mile from model @ 0.42 miles |
| 520-1-10 | CONCREIE CURB \& GUTIER, TYPE E | 4,435.20 | LF | \$ 20.00 | \$ | 88,704.00 | Cost per mile from model @ 0.42 miles |
| 522-2 | CONCREIE SIDEWALK AND DRIVEWAYS, 6" | 2,463.72 | SY | \$ 38.00 | \$ | 93,621.36 | Cost per mile from model @ 0.42 miles |
| 570-1-2 | PERFORMANCE TURF, SOD | 5,482.40 | SY | \$ 2.60 | \$ | 14,254.24 | Cost per mile from model @ 0.42 miles |
| 715-511-140 | UGHTPOLE COMP,F\&I,SGLARM SM, AL, 40' | 14.70 | EA | \$ 14,600.00 | \$ | 214,620.00 | Cost per mile from model @ 0.42 miles |
|  | Signa lization | 2.00 | PI | \$ 400,000.00 | \$ | 400,000.00 | $\$ 250,000$ for SR 70 @ Del Webb and $\$ 150,000$ for signal along SR 70 for displaced left $=\$ 400,000$ |
|  | Partial Total |  |  |  | \$ | 2,005,899.08 |  |
|  | Roadway Total |  |  |  | \$ | 2,407,078.89 |  |
| 999-25 | INITAL CONTING ENCY AMOUNT(DO NOTBID) | 10\% |  |  | \$ | 240,707.89 |  |
| - | Right of Way Cost Estimate |  | - | - | \$ | 410,000.00 | Details of the right of way estimate are included in Attachment E . |
|  |  |  |  |  |  |  |  |
| Intersection Grand Total |  |  |  |  | \$ | 3,057,787 |  |
| Notes: |  |  |  |  |  |  |  |
| PAY ITEM list was created based on FDOTLRE C ost per Mile: MODEL WUUA24-U-19-BB. Contingency covers all other items not shown in Table |  |  |  |  |  |  |  |
| Pavement design was assumed to be 4-in fortravel lanes and 2-in for shoulders |  |  |  |  |  |  |  |
| MOTand MOBILZATION 10\%EACH |  |  |  |  |  |  |  |
| Potential right of way impacts are included for this altemative intersection. |  |  |  |  |  |  |  |

## SR 70 - ROW Cost Estimates for the Intersection Control Evaluation

| Intersection | Configuration | Square footage or ROW Aquisition | ROW Cost Per Square Foot | ROW Cost Estimate |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Uihlein at SR 70 | Partial Displaced Left-Turn (DLT) | 15178 | \$120 | \$ | 1,820,000 |
| Del Webb at SR 70 | Partial Displaced Left-Turn (DLT) | 3456 | \$120 | \$ | 410,000 |
| Bourneside at SR 70 | Partial Displaced Left-Turn (DLT) | 9921 | \$120 | \$ | 1,190,000 |
|  |  | 9430 | \$120 | \$ | 1,130,000 |
|  | Quadrant roadway | 439976 | \$120 | \$ | 52,800,000 |
| CR 675 at SR 70 (2) | Quadrant roadway | 68504 | \$2,750 | \$ | 10,000 |

(1) ROW cost estimates are based on the table below
(2) For ROW needs for CR 675, it is assumed that the property will require a full take. The actual property value was used for this estimate.

Property Value Estimates

| Folio | Total Just Value as of 2018 | Property Size (sq ft.) | Cost Per Sq. Ft. | Inflated cost <br> (factor by 3) | Recommended Cost/Sq Ft <br> to Apply to ROW |  |
| :---: | ---: | :---: | :---: | :---: | :---: | :---: |
| 586104409 | $\$$ | $291,876.00$ | 7640.424 | $\$$ | 38.20 | 114.6046345 |

(1) Property cost estimates were obtained from 2 residential properties near the Lakewood Ranch area. Currently, the Lakewood Ranch residential area is under development and there are no property values from the Manatee County Property Appraiser. The alternative intersection ROW needs are impacting the residential area under development; therefore, there are no property values that could be use for ROW estimates.
(2) These property estimates are used for the intersections of Uihlein, Del Webb, and Bourneside. Since CR 675 is a full take, the property appraised value for that property will be used.

## ATTACHMENT F

## Delay Calculations

## Delay Information

Use this sheet to enter the delay information for each of the included control strategies.

Note: Delay calculations for Displaced Left-Turn, Signalized Restricted Crossing U-turn, and Continuous Green-T Intersection have been adjusted to account for Experienced Travel Time (ETT) based on guidance from the Highway Capacity Manual, Chapter 23, Ramp Terminals and Alternative Intersections. The ETT method accounts for origin-destination (O-D) path of a distributed network of closely space intersections that operate in a cluster. This method results in a single LOS/delay for an alternative intersection configuration with multiple signalized intersections which include multiple LOS/delay results (e.g. Displaced left turns are modeled as multiple signalized intersections with separate LOS/delay results for each; this method computes the LOS/delay as one intersection). The HCM describes direct application of this concept to Displaced Left-Turns and RCUTs, however, it may also be extended to continuous green-t intersections to account for the major-street through movement which separated from the rest of the intersection and not accounted for in the Synchro analysis.

|  |  |  |  | Opening Year |  |  | Design Year |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| At-Grade Intersections |  |  |  | Average vehicle delay |  |  | Average vehicle delay |  |  |
| Control Strategy |  | Delay Type | Units | AM peak | PM peak | Weekend peak | AM peak | PM peak | Weekend peak |
| Traffic Signal | Single Input | Single Input | sec/veh | 5.9 | 7.8 |  | 8.2 | 10.5 |  |
| Roundabout | Single Input | Single Input | sec/veh | 6.1 | 6.2 |  | 8.9 | 9.7 |  |
| Displaced Left Turn (DLT) | Single Input | Worksheet (Partial E-W) | sec/veh | 8.9 | 11.4 |  | 12.5 | 14.5 |  |
| Signalized Restricted Crossing U-Turn (RCUT) | Select Input Type | Worksheet (E-W) | sec/veh | 7.1 | 8.1 |  | 10.3 | 10.9 |  |
| Continuous Green-T Intersection | Single Input | See worksheet | sec/veh | 4.2 | 6.4 |  | 6.4 | 9.6 |  |
|  |  |  |  |  |  |  |  |  |  |









## Continuous Green T Intersection - Delay Calculation

Del Webb and SR 70


ATTACHMENT G Benefit / Cost Summary button in the Alternatives_MasterList tab.

| Agency: | FDOT District 1 |
| :--- | :--- |
| Project Name: | SR 70 from Lorraine Rd to CR 675 |
| Project Reference: | FDOT Project \#414506-2-22-01 |
| Intersection: | SR 70 and Del Webb Blvd |
| City: | Unincorporated Manatee County |
| State: | Florida |
| Performing Department or <br> Organization: | Florida Department of Transportation District 1 |
| Date: | 6/14/0019 |
| Analyst: | CB |
| Analysis Type | At-Grade Intersection |

Analysis Summary

| Cost Categories | Net Present Value of Costs |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Traffic Signal |  | Roundabout |  | Displaced Left Turn (DLT) |  | Signalized Restricted Crossing UTurn (RCUT) |  | Continuous Green-T Intersection |  |
| Planning, Construction \& Right of Way Costs | \$ | 2,340,000 | \$ | 2,110,000 | \$ | 2,732,000 | \$ | 2,530,000 | \$ | 2,400,000 |
| Auto Passenger Delay | \$ | 4,295,198 | \$ | 3,950,585 | \$ | 6,369,038 | \$ | 4,797,225 | \$ | 3,331,768 |
| Truck Delay | \$ | 1,633,786 | \$ | 1,502,525 | \$ | 2,422,701 | \$ | 1,824,694 | \$ | 1,267,171 |
| Safety | \$ | 6,455,259 | \$ | 5,177,569 | \$ | 5,680,628 | \$ | 5,066,635 | \$ | 5,536,522 |
| Total cost |  | \$14,822,472 |  |  |  |  |  |  |  |  |


| Select Base Case for Benefit-Cost Comparison: (Choose from list) | Traffic Signal |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Net Present Value of Benefits Relative to Base Case |  |  |  |  |  |
| Benefit Categories | Traffic Signal | Roundabout | Displaced Left Turn (DLT) | Signalized Restricted Crossing U- <br> Turn (RCUT) | Continuous Green-T Intersection |
| Auto Passenger Delay |  | \$ 344,613 | \$ $(2,073,840)$ | $(502,026)$ | 963,430 |
| Truck Delay |  | 131,261 | (788,915) | $(190,907)$ | 366,615 |
| Safety |  | \$ 1,277,690 | \$ 774,631 | 1,388,624 | \$ 918,736 |
| Net Present Value of Benefits |  | \$ 1,753,565 | (2,088,124) | 695,690 | \$ 2,248,782 |
| Net Present Value of Costs |  | \$ (157,048) | \$ 630,276 | 428,276 | 158,229 |
| Net Present Value of Improvement |  | \$ 1,910,613 | \$ $(2,718,400)$ | 267,414 | \$ 2,090,554 |
| Benefit-Cost (B/C) Ratio |  | Control strategy preferred. Benefits are greater than base case and cost is less than base case. | Control Strategy not preferred. Benefits are less than base case and cost is greater than base case. | 1.62 | 14.21 |
| Delay B/C |  | Control strategy preferred. Benefits are greater than base case and cost is less than base case. | Control Strategy not preferred. Benefits are less than base case and cost is greater than base case. | Control Strategy not preferred. Benefits are less than base case and cost is greater than base case. | 8.41 |
| Safety B/C |  | Control strategy preferred. Benefits are greater than base case and cost is less than base case. | 1.23 | 3.24 | 5.81 |



## ATTACHMENT H

FDOT ICE Stage 1 Form, Capacity Analysis for Planning of Junctions (CAP-X), and Stage 1 SPICE

## Stage 1: Screening

To fulfill the requirements of Stage 1 (Screening) of FDOT's ICE procedures, complete the following form and append all supporting documentation. Completed forms can be submitted to the District Traffic Operations Engineer (DTOE) and District Design Engineer (DDE) for the project's approval.



FDOT ICE: Stage 1


| Crash History (Existing Intersections Only) |
| :--- |
| Append the most recent five-years of crash data for the intersection from the CAR System. If the crash data evidences any issues relating to safety |
| performance, discuss briefly here: |
| The crash history was not included in the analysis since the future conditions of SR 70 changes significantly from a 2 lane undivided to a 4-lane divided. |
| Instead, a predictive crash model was used for the analysis. |

FDOT ICE: Stage 1

Control Strategy Evaluation
Provide a brief justification as to why each of the following control strategies should be advanced or not. Justification should consider potential environmental impacts.

| Control Strategy | CAP-X Outputs |  |  | SPICE <br> Ranking | Strategy to Be Advanced? | Justification |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | V/C Ratio |  | Multimodal Score |  |  |  |
|  | Weekday AM Peak | Weekday PM Peak |  |  |  |  |
| Two-Way StopControlled | 3.90 | 4.93 | 3.70 | 3 | No | V/C capacity ratios are exceeded. |
| All-Way StopControlled | 1.64 | 1.64 | 6.7 | N/A | No | V/C capacity ratios are exceeded. |
| Signalized Control | 0.43 | 0.49 | 4.8 | 8 | Yes | Move to Stage 2 based on v/c for am and pm hours |
| Roundabout | $1 \times 2.55$ 2x2. 55 $1 \times 11.07$ |  | $\begin{aligned} & 5.6 \\ & 5.6 \\ & 6.7 \\ & \hline \end{aligned}$ | 1 \& 4 | Yes | Move to Stage 2 based on SPICE recommendation and $v / c$ less than 1 |
| Median U-Turn | N/A | N/A | N/A | N/A | No | Not applicable since this is a T-intersection. |
| RCUT (Signalized) | 0.44 | 0.47 | 6.3 | 5 | Yes | Move to Stage 2 based on v/c for am and pm hours |
| RCUT <br> (Unsignalized) | 0.57 | 1.10 | 4.4 | 2 | No | V/C ratio exceeded during the PM Peak. |
| Jughandle |  |  |  | N/A | No | Not included in the analysis. |
| Displaced LeftTurn | 0.43 | 0.45 | 4.8 | 7 | Yes | Partial Displaced Left-Turn: Move to Stage 2 based on v/c for am and pm hours |
| Continuous Green Tee | 0.34 | 0.48 | 3.0 | 6 | Yes | Move to Stage 2 based on v/c for am and pm hours |
| Quadrant Roadway | N/A | N/A | N/A |  | No | Not applicable since this is a T-intersection. |
| Partial MUT | N/A | N/A | N/A | N/A | No | Not applicable since this is a T-intersection. |
| Other 2 (Type) | N/A | N/A | N/A | N/A | No | No additional alternative intersection configurations were included in this analysis. |


| Resolution |  |  |
| :---: | :---: | :---: |
| To be filled out by FDOT District Traffic Operations Engineer and District Design Engineer |  |  |
| Project D | Multiple Viable Alternatives Identified: Continue to Stage 2 |  |
| Comments |  |  |
| DTOE Name | Signature | Date |
| DDE Name | Signature | Date |


| Project Name: | SR 70 @ Del Webb |
| ---: | :---: |
| Project Number: | 0 |
| Location: | Unincorporated Manatee County |
| Date: | $2045 \quad$ AM |
| Number of Intersection Legs: | 3 |
| Which leg is the minor street? | S |


| Traffic Volume Demand |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Volu | /hr) |  |  | nt (\%) |
|  | U-Turn | Left | Thru个 | Right | Heavy | Volume Growth |
| Eastbound | 0 | 0 | 793 | 150 |  | 0.00\% |
| Westbound | 0 | 38 | 1155 | 0 |  | 0.00\% |
| Southbound | 0 | 0 | 0 | 0 |  | 0.00\% |
| Northbound | 0 | 125 | 0 | 45 |  | 0.00\% |
| Adjustment Factor | 0.80 | 0.95 |  | 0.85 |  | $\cdots$ |
| Suggested | 0.80 | 0.95 | , | 0.85 |  |  |
| Truck to PCE Factor |  |  |  | Suggest | 2.00 | 2.00 |
| FDOT Context Zon |  | C3R-Suburban Residential |  |  |  |  |
| Critical Lane Volume Threshold |  | 2-phase signal |  | Suggested = 1800 |  | 1800 |
|  |  | 3 -phase signal |  | Suggested = 1750 |  | 1750 |
|  |  | 4-phase signal |  | Suggested = 1700 |  | 1700 |


| TYPE OF INTERSECTION | $\begin{gathered} \text { Overall v/c } \\ \text { Ratio } \end{gathered}$ | V/C <br> Ranking | Multimodal Score | Pedestrian Accommodation s | Bicycle Accommodation s | Transit Accommodatio ns |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Continuous Green T S | 0.34 | 1 | 3.0 | Poor | Poor | Good |
| Traffic Signal | 0.43 | 2 | 4.8 | Fair | Fair | Good |
| Partial Displaced Left Turn E-W | 0.43 | 2 | 4.8 | Fair | Fair | Good |
| SIgnalized Restricted Crossing U-Iurn E- <br> $W$ | 0.44 | 4 | 6.3 | Good | Cood | Fair |
| $1 \times 2$ | 0.55 | 5 | 5.6 | Fair | Good | Good |
| 2 X 2 | 0.55 | 5 | 5.6 | Fair | Good | Good |
| Unsignalized Restricted Crossing $0-$ Turn E-W | 0.57 | 7 | 4.4 | Fair | Fair | Fair |
| $1 \times 1$ | 1.07 | 8 | 6.7 | Good | Good | Good |
| All-Way Stop Control | 1.64 | 9 | 6.7 | Good | Good | Good |
| Two-Way Stop Control E-W | 3.90 | 10 | 3.7 | Poor | Fair | Good |


| Project Name: | SR 70 @ Del Webb |
| ---: | :---: |
| Project Number: | 0 |
| Location: | Unincorporated Manatee County |
| Date: | $2045 \quad$ AM |
| Number of Intersection Legs: | 3 |
| Major Street Direction: | North-South |


| Traffic Volume Demand |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Volume (Veh/hr) |  |  |  | Percent (\%) |  |
|  | U-Turn | Left | Thru | Right | Heavy | Volume Growth |
| Eastbound | 0 | 0 | 793 | 150 |  | 0.00\% |
| Westbound | 0 | 38 | 1155 | 0 |  | 0.00\% |
| Southbound | 0 | 0 | 0 | 0 |  | 0.00\% |
| Northbound | 0 | 125 | 0 | 45 |  | 0.00\% |
| Adjustment Factor | 0.80 | 0.95 |  | 0.85 |  |  |
| Suggested | 0.80 | 0.95 |  | 0.85 |  | , |
| Truck to PCE Factor |  |  |  | Suggest | 2.00 | 2.00 |
| FDOT Context Zone |  |  | C3R-Suburban Residential |  |  |  |
| Critical Lane Volume Threshold |  | 2-phase signal |  | Suggested = 1800 |  | 1800 |
|  |  | 3-phase signal |  | Suggested = 1750 |  | 1750 |
|  |  | 4-phase signal |  | Suggested = 1700 |  | 1700 |

Capacity Analysis for Planning of Junctions
Detailed Report - Page 2 of 4

| Number of Lanes for Non-roundabout Intersections |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TYPE OF INTERSECTION | Sheet | Northbound |  |  |  | Southbound |  |  |  | Eastbound |  |  |  | Westbound |  |  |  |
|  |  | U | L | T | R | U | L | T | R | U | L | T | R | U | L | T | R |
| Traffic Signal | FULL | - | 1 | 0 | 1 | - | 0 | 0 | 0 | - | 0 | 2 | 1 |  | 1 | 2 | 0 |
| Two-Way Stop Control | E-W | - | 1 | 0 | 1 | - | 0 | 0 | 0 | - | 0 | 2 | 1 | , | 1 | 2 | 0 |
| All-Way Stop Control | FULL | - | 1 | 0 | 1 | - | 0 | 0 | 0 |  | 0 | 2 | 1 | - | 1 | 2 | 0 |
| Continuous Green T | $\underline{\text { S }}$ | - | 1 | - | 1 |  |  | - | , |  | - | 2 | 1 | - | 1 | 2 | - |
| Partial Displaced Left Turn | E-W |  | 1 | 1 | 1 |  | 0 | 1 | 0 | - | 0 | 2 | 1 | - | 1 | 2 | 0 |
| Signalized Restricted Crossing U-Turn | E-W |  |  | , | 1 |  |  | 2 | 0 | 1 | 0 | 2 | 1 | 1 | 1 | 2 | 0 |
| Unsignalized Restricted Crossing U-Turn | E-W |  |  | $\square$ | 1 |  |  |  | 0 | 1 | 0 | 2 | 1 | 1 | 1 | 2 | 0 |


| Number of Lanes for Interchanges |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TYPE OF INTERCHANGE | Sheet | Northbound |  |  |  | Southbound |  |  |  | Eastbound |  |  |  | Westbound |  |  |  |
|  |  | U | L | T | R | U | L | T | R | U | L | T | R | U | L | T | R |


| Results for Non-roundabout Intersections |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TYPE OF INTERSECTION | Sheet | Zon <br> (No | V/C | Zon (So | v/C | Zone | East) | Zone 4 | (West) | Zon (Cen | 5 er) V/C | Overall v/c Ratio |  |  |  |
| Traffic Signal | FULL |  |  |  |  |  |  |  |  | 760 | 0.43 | 0.43 | Fair | Fair | Good |
| Two-Way Stop Control | E-W |  |  |  |  |  |  |  |  | -- | 3.90 | 3.90 | Poor | Fair | Good |
| All-Way Stop Control | FULL |  |  |  |  |  |  |  |  | 2461 | 1.64 | 1.64 | Good | Good | Good |
| Continuous Green T | S | $7$ |  |  |  |  |  |  |  | 602 | 0.34 | 0.34 | Poor | Poor | Good |
| Partial Displaced Left Turn | E-W |  |  |  |  | 468 | 0.26 | 682 | 0.38 | 753 | 0.43 | 0.43 | Fair | Fair | Good |
| Signalized Restricted Crossing U-Turn | E-W | 682 | 0.38 | 629 | 0.35 | 799 | 0.44 | 505 | 0.28 |  |  | 0.44 | Good | Good | Falr |
| Unsignalized Restricted Crossing U-Turn | E-W | 1364 | 0.00 | 849 | 0.57 | 1277 | 0.31 | 1010 | 0.00 |  |  | 0.57 | Fair | Fair | Fair |

Capacity Analysis for Planning of Junctions
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| Results for Roundabouts |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TYPE OF ROUNDABOUT | Zone 1 (North) |  |  | Zone 3 (East) |  |  | Zone 2 (South) |  |  | Zone 4 (West) |  |  | Overall v/c Ratio |  |  |  |
|  | Lane 1 | Lane 2 | Lane 3 | Lane 1 | Lane 2 | Lane 3 | Lane 1 | Lane 2 | Lane 3 | Lane 1 | Lane 2 | Lane 3 |  |  |  |  |
| $1 \times 1$ | 0.00 |  |  | 0.77 |  |  | 0.30 |  |  | 1.07 |  |  | 1.07 | Good | Good | Good |
| $1 \times 2$ | 0.00 |  |  | 0.38 | 0.40 |  | 0.26 |  |  | 0.52 | 0.55 |  | 0.55 | Fair | Good | Good |
| $\underline{2 \times 2}$ | 0.00 | 0.00 |  | 0.52 | 0.55 |  | 0.21 | 0.07 |  | 0.38 | 0.40 |  | 0.55 | Fair | Good | Good |


| Project Name: | SR 70 @ Del Webb |
| ---: | :---: |
| Project Number: | 0 |
| Location: | Bradenton, FL |
| Date: | $2045 \quad$ PM |
| Number of Intersection Legs: | 3 |
| Which leg is the minor street? | S |


| Traffic Volume Demand |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Volu | /hr) |  |  | nt (\%) |
|  | U-Turn | Left | Thru个 | Right | Heavy | Volume Growth |
| Eastbound | 0 | 0 | 1182 | 140 |  | 0.00\% |
| Westbound | 0 | 46 | 771 | 0 |  | 0.00\% |
| Southbound | 0 | 0 | 0 | 0 |  | 0.00\% |
| Northbound | 0 | 147 | 0 | 25 |  | 0.00\% |
| Adjustment Factor | 0.80 | 0.95 |  | 0.85 |  | $\cdots$ |
| Suggested | 0.80 | 0.95 | , | 0.85 |  |  |
| Truck to PCE Factor |  |  |  | Suggest | 2.00 | 2.00 |
| FDOT Context Zon |  | C3R-Suburban Residential |  |  |  |  |
| Critical Lane Volume Threshold |  | 2-phase signal |  | Suggested = 1800 |  | 1800 |
|  |  | 3 -phase signal |  | Suggested = 1750 |  | 1750 |
|  |  | 4-phase signal |  | Suggested = 1700 |  | 1700 |

## Capacity Analysis for Planning of Junctions

| TYPE OF INTERSECTION | Overall v/c Ratio | V/C <br> Ranking | Multimodal Score | Pedestrian Accommodation s | Bicycle Accommodation s | Transit Accommodatio ns |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Partial Displaced Left Turn E-W | 0.45 | 1 | 4.8 | Fair | Fair | Good |
| SIgnailzed Restricted Crossing 0 -Iurn $E-$ $W$ | 0.47 | 2 | 6.3 | Good | Good | Fair |
| Continuous Green T S | 0.48 | 3 | 3.0 | Poor | Poor | Good |
| Traffic Signal | 0.49 | 4 | 4.8 | Fair | Fair | Good |
| $1 \times 2$ | 0.57 | 5 | 5.6 | Fair | Good | Good |
| $2 \times 2$ | 0.57 | 5 | 5.6 | Fair | Good | Good |
| $1 \times 1$ | 1.09 | 7 | 6.7 | Good | Good | Good |
| Unsignalized Restricted Crossing $0-$ Turn E-W | 1.10 | 8 | 4.4 | Fair | Fair | Fair |
| All-Way Stop Control | 1.64 | 9 | 6.7 | Good | Good | Good |
| Two-Way Stop Control E-W | 4.93 | 10 | 3.7 | Poor | Fair | Good |


| Project Name: | SR 70 @ Del Webb |
| ---: | :---: |
| Project Number: | 0 |
| Location: | Bradenton, FL |
| Date: | $2045 \quad$ PM |
| Number of Intersection Legs: | 3 |
| Major Street Direction: | North-South |


| Traffic Volume Demand |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Volume (Veh/hr) |  |  |  | Percent (\%) |  |
|  | U-Turn | Left | Thru介 |  | Heavy Vehicles | Volume Growth |
| Eastbound | 0 | 0 | 1182 | 140 | 7.00\% | 0.00\% |
| Westbound | 0 | 46 | 771 | 0 | 7.00\% | 0.00\% |
| Southbound | 0 | 0 | 0 | 0 | 0.00\% | 0.00\% |
| Northbound | 0 | 147 | 0 | 25 | 2.00\% | 0.00\% |
| Adjustment Factor | 0.80 | 0.95 | - | 0.85 | , | - |
| Suggested | 0.80 | 0.95 | , | 0.85 | , |  |
| Truck to PCE Factor |  |  |  | Suggested $=2.00$ |  | 2.00 |
| FDOT Context Zone |  |  | C3R-Suburban Residential |  |  |  |
| Critical Lane Volume Threshold |  | 2-phase signal |  | Suggested = 1800 |  | 1800 |
|  |  | 3 -phase signal |  | Suggested = 1750 |  | 1750 |
|  |  | 4-phase signal |  | Suggested = 1700 |  | 1700 |

Capacity Analysis for Planning of Junctions
Detailed Report - Page 2 of 4

| Number of Lanes for Non-roundabout Intersections |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TYPE OF INTERSECTION | Sheet | Northbound |  |  |  | Southbound |  |  |  | Eastbound |  |  |  | Westbound |  |  |  |
|  |  | U | L | T | R | U | L | T | R | U | L | T | R | U | L | T | R |
| Traffic Signal | FULL | - | 1 | 0 | 1 | - | 0 | 0 | 0 | - | 0 | 2 | 1 |  | 1 | 2 | 0 |
| Two-Way Stop Control | E-W | - | 1 | 0 | 1 | - | 0 | 0 | 0 | - | 0 | 2 | 1 | , | 1 | 2 | 0 |
| All-Way Stop Control | FULL | - | 1 | 0 | 1 | - | 0 | 0 | 0 |  | 0 | 2 | 1 | - | 1 | 2 | 0 |
| Continuous Green T | $\underline{\text { S }}$ | - | 1 | - | 1 |  |  | - | , |  | - | 2 | 1 | - | 1 | 2 | - |
| Partial Displaced Left Turn | E-W |  | 1 | 1 | 1 |  | 0 | 1 | 0 | - | 0 | 2 | 1 | - | 1 | 2 | 0 |
| Signalized Restricted Crossing U-Turn | E-W |  |  | , | 1 |  |  | 2 | 0 | 1 | 0 | 2 | 1 | 1 | 1 | 2 | 0 |
| Unsignalized Restricted Crossing U-Turn | E-W |  |  | $\square$ | 1 |  |  |  | 0 | 1 | 0 | 2 | 1 | 1 | 1 | 2 | 0 |


| Number of Lanes for Interchanges |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TYPE OF INTERCHANGE | Sheet | Northbound |  |  |  | Southbound |  |  |  | Eastbound |  |  |  | Westbound |  |  |  |
|  |  | U | L | T | R | U | L | T | R | U | L | T | R | U | L | T | R |


| Results for Non-roundabout Intersections |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TYPE OF INTERSECTION | Sheet | Zo <br> (No <br>  <br> CLV | V/C | Zon (So | V/C | Zone 3 | East) | Zone 4 | (West) | Zon (Ce | 5 <br> V/C | Overall v/c Ratio |  |  |  |
| Traffic Signal | FULL |  |  |  |  |  |  |  |  | 850 | 0.49 | 0.49 | Fair | Fair | Good |
| Two-Way Stop Control | E-W |  |  |  |  |  |  |  |  | -- | 4.93 | 4.93 | Poor | Fair | Good |
| All-Way Stop Control | FULL |  |  |  |  |  |  |  |  | 2465 | 1.64 | 1.64 | Good | Good | Good |
| Continuous Green T | S |  |  |  |  |  |  |  |  | 842 | 0.48 | 0.48 | Poor | Poor | Good |
| Partial Displaced Left Turn | E-W |  |  |  |  | 684 | 0.38 | 488 | 0.27 | 790 | 0.45 | 0.45 | Fair | Fair | Good |
| Signalized Restricted Crossing U-Turn | E-W | 488 | 0.27 | 840 | 0.47 | 625 | 0.35 | 708 | 0.39 |  |  | 0.47 | Good | Good | Falr |
| Unsignalized Restricted Crossing U-Turn | E-W | 975 | 0.00 | 1265 | 1.10 | 874 | 0.25 | 1415 | 0.00 |  |  | 1.10 | Fair | Fair | Fair |

Capacity Analysis for Planning of Junctions
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| Results for Roundabouts |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TYPE OF | Zone 1 (North) |  |  | Zone 3 (East) |  |  | Zone 2 (South) |  |  | Zone 4 (West) |  |  | Overall v/c Ratio |  |  |  |
|  | Lane 1 | Lane 2 | Lane 3 | Lane 1 | Lane 2 | Lane 3 | Lane 1 | Lane 2 | Lane 3 | Lane 1 | Lane 2 | Lane 3 |  |  |  |  |
| 1X1 | 0.00 |  |  | 1.09 |  |  | 0.47 |  |  | 0.75 | - |  | 1.09 | Good | Good | cood |
| 1×2 | 0.00 |  |  | 0.53 | 0.57 |  | 0.37 |  |  | 0.36 | 0.38 |  | 0.57 | Fair | Good | Good |
| $\underline{2 \times 2}$ | 0.00 | 0.00 |  | 0.36 | 0.38 |  | 0.37 | 0.06 |  | 0.53 | 0.57 |  | 0.57 | Fair | Good | Bood |



| Federal Highway Administration (FHWA) <br> Safety Performance for Intersection Control Evaluation Tool |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Results |  |  |  |  |  |  |  |
| Summary of crash prediction results for each alternative |  |  |  |  |  |  |  |
| Project Information |  |  |  |  |  |  |  |
| Project Name: | SR 70 from Lorraine Rd to CR 675 |  |  | Intersection Type |  | At-G | rsections |
| Intersection: | SR 70 @ Del Webb |  |  | Opening Year |  |  |  |
| Agency: | D1 |  |  | Design Year |  |  |  |
| Project Reference: | 414506-2-22-01 |  |  | Facility Type |  | On Urban | urban Arterial |
| City: | Unincorporated Manatee County |  |  | Number of Legs |  | 3-leg |  |
| State: | FL |  |  | 1-Way/2-Way |  | 2-way Intersecting 2-way |  |
| Date: | 6/14/2019 |  |  | \# of Major Street Lanes (both directions) |  | 5 or fewer |  |
| Analyst: | Nicole Harris, PE |  |  | Major Street Approach Speed |  | Less than 55 mph |  |
| Crash Prediction Summary |  |  |  |  |  |  |  |
| Control Strategy | Crash Type | Opening Year | Design Year | Total Project Life Cycle | Rank | AADT Within Prediction Range? | Source of Prediction |
| Traffic Signal | Fatal \& Injury | $\begin{aligned} & \hline 3.50 \\ & 1.32 \end{aligned}$ | $\begin{aligned} & 5.70 \\ & 2.05 \end{aligned}$ | $\begin{aligned} & 96.15 \\ & 35.27 \end{aligned}$ | 8 | Yes | Calibrated SPF |
| Minor Road Stop | Total | $\begin{aligned} & 2.21 \\ & 0.80 \end{aligned}$ | $\begin{aligned} & \hline 3.64 \\ & 1.27 \end{aligned}$ | $\begin{aligned} & \hline 61.06 \\ & 21.68 \end{aligned}$ | 3 | Yes | Calibrated SPF |
| All Way Stop | Fatal \& Injury | No SPF <br> No SPF | No SPF <br> No SPF | No SPF <br> No SPF | -- | N/A | N/A |
| 1-lane Roundabout | Fatal \& Injury | $\begin{aligned} & 1.02 \\ & 0.28 \end{aligned}$ | $\begin{aligned} & 1.31 \\ & 0.42 \end{aligned}$ | $\begin{gathered} 24.47 \\ 7.35 \end{gathered}$ | 1 | N/A | Uncalibrated SPF |
| 2-Iane Roundabout | Fatal \& Injury |  | $\begin{aligned} & 8.29 \\ & 1.52 \end{aligned}$ | $\begin{gathered} 143.87 \\ 25.48 \end{gathered}$ | 4 | N/A | Uncalibrated SPF |
| Displaced Left Turn (DLT) | Fatal \& Injury | 3.08 1.16 | $\begin{aligned} & \hline 5.02 \\ & 1.80 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 84.61 \\ & 31.03 \\ & \hline \end{aligned}$ | 7 | N/A | CMF |
| Signalized RCUT | Fatal \& Injury | 2.97 1.03 | $\begin{aligned} & 4.85 \\ & 1.60 \end{aligned}$ | $\begin{aligned} & \hline 81.73 \\ & 27.51 \end{aligned}$ | 5 | N/A | CMF |
| Unsignalized RCUT | Fatal \& Injury | 1.44 0.37 | $\begin{aligned} & \hline 2.37 \\ & 0.59 \\ & \hline \end{aligned}$ | $\begin{gathered} \hline 39.69 \\ 9.97 \\ \hline \end{gathered}$ | 2 | N/A | CMF |
| Continuous Green-T Intersection | Fatal \& Injury | $\begin{aligned} & \hline 3.36 \\ & 1.12 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 5.47 \\ & 1.74 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 92.30 \\ & 29.98 \\ & \hline \end{aligned}$ | 6 | N/A | CMF |

