FINAL POND SITING REPORT

SR 710 From US 441 to the L-63N Canal

Financial Project ID 419344-3-32-01

Okeechobee County, Florida



Prepared For:

Florida Department of Transportation

District 1 801 North Broadway Avenue Bartow, FL 33830-3809

Prepared By:

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March 28, 2017

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PROFESSIONAL ENGINEER CERTIFICATION

I hereby certify that I am a registered professional engineer in the State of Florida practicing engineering with **The Balmoral Group** and that I have supervised the preparation of and approve the analysis, findings, opinions, conclusions and technical advice hereby reported for:

PROJECT: SR 710 New Alignment

From US 441 to the L-63N Canal Financial Project ID: 419344-3-32-01

Okeechobee County, Florida

The engineering work represented by this document was performed through the following duly authorized engineering business:

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through professional judgment and experience.

This report provides the results of the analysis of the existing drainage conditions and the analysis required for the determination of the recommended locations for the proposed stormwater management facilities. I acknowledge that the procedures and references used to develop the results contained in this report are standard to the professional practice of hydrologic analysis and hydraulic engineering as applied

Any engineering analysis, documents, conclusions or recommendations relied upon from other professional sources or provided with responsibility by the client are referenced accordingly in the following report.

FLORIDA REGISTERED ENGINEER:

Lori C. Stanfill, State of Florida, Professional Engineer, License No. 52107 This item has been electronically signed and sealed by:

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Executive Summary

The State of Florida Department of Transportation (FDOT) proposes a new alignment for SR 710 that begins at the intersection with US 441 and extends southeasterly to south of the L-63N Canal (Interceptor Creek), where it ties into the existing SR 710, in Okeechobee County, Florida. The Balmoral Group has subcontracted with Wantman Group, Inc. to provide the Pond Siting Report for the project. A four-lane suburban typical section is proposed. The roadway will consist of two 12-foot wide travel lanes in each direction, separated by a raised 30-foot wide grassed median. This roadway section will also include four foot shoulders to the inside of the travel lanes and six and one-half-foot (eight-foot useable) shoulders adjacent to the outside travel lanes. Type E curb and gutter will be provided along the median and outside edges of the roadway along with a closed storm-water conveyance system. The total length of the project is 3.8 miles. The project datum is NAVD, 1988. All stations are referenced to Centerline of Construction. The project is located in Sections 10, 11, 13, 14, 15, and 24, Township 37 South, and Range 35 East.

In the existing drainage condition, the project is located within Lake Okeechobee Watershed drainage basin S-133. Runoff during rainfall events is conveyed as sheet flow or shallow concentrated flow to localized depressions or wetlands, eventually outfalling to the L-63N Canal or Taylor Creek, an unnamed historic canal, or Mosquito Creek. Within Taylor Creek, the L-63N Canal, and Mosquito Creek, water levels and flow are controlled with drainage structures. Runoff within this basin eventually drains into Lake Okeechobee.

South Florida Water Management District (SFWMD) environmental resource permits (ERP's) for existing residential and commercial areas were obtained. These permits were researched and utilized to create a regional pre-development ICPR model.

Six pre-development drainage basins have been identified to the east of Taylor Creek. As the SR 710 project consists primarily of a new alignment, there are currently no existing cross drains within the limits of the project except the bridge crossing over the L-63N Canal.

For the proposed drainage condition, there are five post-development drainage basins. Sixteen pond alternatives have been evaluated throughout the project. Generally, three pond sites were evaluated per basin.

The objective of this report is to provide ideal locations for the construction of stormwater facilities to manage the runoff from the proposed improvements of SR 710. Design considerations for each pond site location include hydraulic data, hydrology (land use cover, soil types and seasonal high water elevations), environmental impacts, wetland impacts, impacts to protected conservation areas and species, economic factors affecting each pond location, cost of right-of-way (ROW) acquisition and impacts to cultural resources. The following table, ES Table 1, provides a summary of the results of the analysis.

Executive Summary (Cont.) SR 710

ES Table 1: Pond Site Evaluation Matrix

				Cultural Impact Potential	Potential for	Potential	Contamination Risk Potential		
Pond Site	Treatment Method	Construction Feasibility	Total Cost	Level I (All Sites)	Involvement of Jurisdictional Wetland	For Involvement of Protected	Level I (All Sites)	Floodplain (2015)	Pond Site Rating
				Level II (Preferred Sites)	Systems	Species	Level II (Preferred Sites)		Rating
1A	Wet Detention	Fair	\$355,012	Low	None	Low	No	Yes	Fair
1B	Dry Retention	Good	\$320,073	Level I-Low Level II-No	Medium*	Low	Level I-Low Level II-No	No	Good
1C	Dry Retention	Fair	\$324,664	Low	High	Low	No	Yes	Fair
2A Option 1	Wet Detention	Good	\$1,337,314	Level I-Moderate Level II-No	None*	Low	Level I-No Level II-No	No	Good
2A Option 2	Wet Detention	Good	\$1,644,419	Moderate	None	Low	No	No	Fair
2A Option 3	Wet Detention	Good	\$1,976,879	Moderate	None	Low	No	No	Fair
2B Option 1	Wet Detention	Good	\$1,330,064	Moderate	None	Low	No	No	Fair
2B Option 2	Wet Detention	Good	\$1,601,045	Moderate	None	Low	No	No	Fair
2B Option 3	Wet Detention	Good	\$1,898,262	Moderate	None	Low	No	No	Fair
2C Option 1	Wet Detention	Good	\$1,339,526	Low	Low**	Low	No	No	Good
2C Option 2	Wet Detention	Good	\$1,655,070	Low	Low**	Low	No	No	Fair
3A	Wet Detention	Good	\$901,448	Low	None	Low	Medium	No	Fair
3B	Wet Detention	Good	\$701,565	Level I-Low Level II-No	Low*	Low	Level I-No Level II-No	No	Good
3C	Wet Detention	Good	\$773,483	Low	None	Low	Low	No	Good
4A Option 1	Wet Detention	Good	\$1,088,121	Low	None	Medium	Low	No	Good
4A Option 2	Wet Detention	Good	\$1,342,958	Low	None	Medium	Low	No	Fair
4B/4C Option 1	Wet Detention	Good	\$1,223,843	Moderate	Low	Low	Medium	No	Fair
4B Option 2	Wet Detention	Good	\$904,222	Level I-Moderate Level II-No	Low*	Low	Level I-No Level II-No	No	Good
4D Option 1	Wet Detention	Good	\$1,071,066	Low	None	Medium	Medium	No	Good
4D Option 2	Wet Detention	Good	\$1,279,153	Low	None	Medium	Medium	No	Fair
5A	Dry Retention	Fair	\$444,696	Level I-Low Level II-No	Medium*	Low	Level I-No Level II-No	Yes	Good
5B	Dry Retention	Fair	\$466,083	Moderate	Low	Low	No	No	Good
5C	Dry Retention	Fair	\$461,723	Low	None	Low	Low	No	Good
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*Note: Pond Sites 1B, 3B, and 5A were determined to have wetland impacts of 0.47 ac., 0.35 ac., and 0.11 ac., respectively. Pond Sites 2A-Option 1 and 4B-Option 2 were determined to have no wetland impacts.

It is recommended to use Pond Site 1B in Basin 1 to provide water quality treatment and peak discharge attenuation for a drainage area of 5.20 acres (including pond). This pond site will outfall to Taylor Creek and eventually discharge to Lake Okeechobee.

It is recommended to use Pond Site 2A-Option 1 in Basin 2 to provide water quality treatment and peak discharge attenuation for a drainage area of 46.49 acres (including pond). This pond site will outfall to Taylor Creek and eventually discharge to Lake Okeechobee.

^{**}Note: Pond Sites 2C-Option 1 and 2C-Option 2 were initially assessed low for wetland impacts, but the site was subsequently reconfigured around the wetland.

It is recommended to use Pond Site 3B in Basin 3 to provide water quality treatment and peak discharge attenuation for a drainage area of 12.83 acres (including pond). For the pond siting analysis, this pond site will outfall to an unnamed historic ditch and eventually discharge to Lake Okeechobee. For Final Design, this pond will likely outfall to the L-63N canal which is not impaired for nutrients.

It is recommended to use Pond Sites 4B-Option 2 in Basin 4 to provide water quality treatment and peak discharge attenuation for a drainage area of 31.65 acres (including pond). This option does not require the road to be raised 1 foot. For the pond siting analysis, this pond site will outfall to an unnamed historic ditch and eventually discharge to Lake Okeechobee. For Final Design, this pond will likely outfall to the L-63N canal which is not impaired for nutrients.

It is recommended to use Pond Site 5A in Basin 5 to provide water quality treatment and peak discharge attenuation for a drainage area of 11.12 acres (including pond). This pond site will outfall to Mosquito Creek and eventually discharge to Lake Okeechobee.

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I. GENERAL INFORMATION

A. Background

The project limits for State Road 710 span from Station 500+34 (US 441) to Station 703+50 (Mosquito Creek). The previous Preliminary Engineering Report, PD&E Study (September 2012) for SR 710 from US 441 to CR 714 identified the need for the proposed urban principal arterial for the following reasons.

- To improve regional connectivity as SR 710 is part of the Strategic Intermodal System (SIS) and connects to other SIS facilities (SR 70).
- To serve as an evacuation route for the City of Okeechobee. SR 710 is one of the few east to west roads in this area with the ability to connect the east coast to the inland.
- To accommodate Okeechobee County's future population and growth. Much of the population is located near the City of Okeechobee and the intersection of US 441 and SR 70.
- To meet local government goals and objectives. The SR 710 extension is included in the Okeechobee County Long Range Transportation Needs Assessment Study (Needs Plan for 2035). It is also included as a four-lane roadway in the Okeechobee County Year 2020 Comprehensive Plan, amended May 7, 2009.

There are a number of existing and proposed facilities which will require consideration during the early design process. This would include the US 441/Okeechobee Health Care Facility, Okeechobee Utility Authority Impacts/Well Heads, Hamrick & Sons, Inc. Property, Northshore Village/SR 70, SE Community Access/Everglades Elementary. See Figures 8A to 8G, Existing SFWMD Permits Map in Appendix 1.

B. PROJECT OVERVIEW

The State of Florida Department of Transportation (FDOT) proposes a new alignment for SR 710 from the intersection with US 441 to the L-63N Canal, where it ties into the existing SR 710 in Okeechobee County, Florida. The new alignment for the SR 710 project begins at US 441 (Station 500+34 and connects with the existing SR 710 alignment just south of SR 70 (Station 675+00), ending at Station 703+50 in the vicinity of Mosquito Creek.

SR 710 is designated as an Urban and Rural Principal Arterial and a Strategic Intermodal System (SIS) facility. The existing SR 710 is currently classified by FDOT as an Access Management Class four facility. The proposed access classification for the new roadway extension is class three from U.S. 441 to Taylor Creek and class two from Taylor Creek to S.R. 70, the remainder of the corridor would be classified as class three from S.R. 70 to Mosquito Creek. The design speed for the entire facility is 50 miles-per-hour (mph).

A four-lane suburban typical section is proposed. The roadway will consist of two twelve foot wide travel lanes in each direction, separated by a raised 30-foot wide grassed median. This roadway section will also include four foot shoulders to the inside of the travel lanes and six and one-half-foot (eight-foot useable) shoulders adjacent to the outside travel lanes. Type E curb and gutter will be provided along the median and outside edges of the roadway along with a closed storm-water conveyance system. A continuous five foot wide concrete sidewalk will be provided on the south side of the roadway and a ten foot wide shared-use path will be provided on the north side of the roadway. Appropriate left and/or right turn lanes will be provided at major intersections. This typical section has a twenty nine foot border width and is to be constructed within one-hundred sixty foot minimum of right-of-way. The surrounding land uses consist primarily of large areas of rangeland, pastureland, residential developments, and rural residences. The total length of this project is 3.8 miles. See Figure 2 in Appendix 1 for the proposed typical section.

The project is located in Sections 10, 11, 13, 14, 15, and 24, Township 37 South, and Range 35 East. The new alignment will cross Taylor Creek and L-63 N Canal which are both structure controlled waterways and eventually outfall into Lake Okeechobee. Bridge Hydraulics Reports have been prepared for these crossings under separate cover. Near the southern end of the project where the new alignment connects with existing SR 710, the roadside ditches are currently permitted to provide water quality treatment prior to outfall into the L-63N Canal and Mosquito Creek.

The project employs the North American Vertical Datum of 1988 (NAVD88) (feet). The conversion from NGVD to NAVD is as follows: 1.17 ft NGVD = 0.00 ft NAVD. All Stations are referenced to the Centerline Construction.

C. LAND USE

The existing land use along SR 710 is agricultural/undeveloped (woods and pasture), commercial and industrial (See Figure 6). The general topography of the project area is flat terrain with elevations ranging from 15 feet to 30 feet NAVD88 based on LiDAR contours and USGS topographic map (See Figure 3). The future land uses within the project area are depicted on Figure 7. The project is located in mainly urban residential mixed use with some portions shown in agriculture.

The existing SFWMD Environmental Resource Permits (ERP) were investigated through the project area. South of the SR 710 alignment, there is an existing Wastewater Treatment Plant located on the east side limits of the City of Okeechobee. The Okeechobee City Commerce Center is southeast of the Wastewater Treatment Plant and just west of the residential subdivision Douglas Park (a.k.a. Cypress Quarters). According to the SFWMD permit, the water management system consists of roadside swales/ditches collecting runoff and routing it to Taylor Creek via existing ditches. Six (6) water supply wells for the City of Okeechobee are located north of the Okeechobee City of Commerce Center and south of the new SR 710 alignment. Minor commercial properties include the BP Gas Station just west of the L63-N Canal bridge and the Total Roadside Services on the existing SR 710 to remain. The existing SFWMD ERP Exhibit can be found in Figure 8. A planned unit development,

Northshore Village, is shown in Figure 9, and is located where SR 710 turns to the south.

Historically, the hydrology of the area has been substantially changed by the channelization of Taylor Creek and subsequent downstream control of water levels by the S-133 Pump Station. Water Elevations at S-133 are maintained at an elevation of 13.5 feet NGVD (12.33 feet NAVD) by pumped discharge into Lake Okeechobee. If Lake Okeechobee stages are below 13.5 feet NGVD (12.33 feet NAVD), then the flood gates remain open and Taylor Creek is controlled by the lower Lake Okeechobee stage (from permit information for City of Okeechobee Commerce Center, Permit Application No.040130-34).

D. SOIL CHARACTERISTICS

The USDA National Resources Conservation Service (NRCS) Custom Soil Resource Report for Okeechobee County was used to identify the soil types within and adjacent to the proposed project on the SR 710 corridor. The primary soil series encountered along the project are Immokalee fine sand (11) (0 to 2 percent slopes), poorly drained soil; Manatee loamy fine sand, depressional, (6) (0 to 2 percent slopes) very poorly drained soil; Pineda fine sand (8) (0 to 2 slope percent slopes), poorly drained soil; Basinger fine sand (2) (0 to 2 percent slopes) poorly drained soil; Riviera fine sand (9) (0 to 2 percent slopes) poorly drained soils, and Basinger and Placid soils, depressional (3) (0 to 1 percent slopes), very poorly drained soils. These soils generally have a high water table depth. The permeability averages of the most limiting layers range from 0.06 to 0.20 in/hr to 6 to 20 in/hr. These are poorly drained soils found on South Florida Flatwoods, sloughs, and freshwater marshes/ponds. See Figure 4, Appendix 1 for the SCS Soils Map. Table 1 below summarizes the soils within the project limits.

Table 1 - Existing Soils

SCS MAP		Hydrologic Soil	Depth of Seasonal High
SYMBOL	SOIL NAME	Group	Water Table (ft)
2	Basinger fine sand	A/D	0-1
3	Basinger and Placid soils, depressional	A/D	0
5	Valkaria fine sand	A/D	0-1
6	Manatee loamy fine sand, depressional	B/D	0
7	Floridana, Riveria, and Placid soils, depressional	C/D	0
8	Pineda fine sand	C/D	0-1
9	Riviera fine sand	C/D	0-1
10	Ft. Drum fine sand	B/D	0.5-1.5
11	Immokalee fine sand	B/D	0.5-1.5
12	Udorthents, 2 to 35 percent slopes	Α	>6.7
14	Myakka fine sand	A/D	0.5-1.5
18	Parkwood fine sand	C/D	0-1
	Floridana, Placid, and Okeelanta soils, frequently		
19	flooded	C/D	0-1
20	Pomello fine sand	Α	2-3.5
23	St. Johns fine sand	B/D	0-0.5
25	Wabasso fine sand	C/D	0.5-1.5

The Florida Department of Transportation, District 1 Geotechnical Department, performed a geotechnical investigation report dated October 31, 2013. The report is presented in **Appendix 2**. Soil borings were taken at each potential pond site to determine existing groundwater table and to estimate the SHWT. The pond locations where the borings have been taken can be found in **Figure 11** in **Appendix 1**. The estimated SHGT elevations ranged in depth from ground surface to approximately 2 feet below the existing ground surface. A subsequent investigation was performed by the FDOT Dist. 1 Geotechnical Department on November 2, 2016 to obtain data for Pond Site 4B. **Table 2** below summarizes the boring data collected at the pond sites.

Table 2 - Pond Site Seasonal High Water Table Estimation

		Estimated Location		_	Boring	Measured	Estimated Seasonal	
Pond	Boring Number	Station	Offset	Date Performed	Depth (feet)	Groundwater Depth (feet)	High Groundwater Depth (feet)	Indicators
1A	PB-1A	Offs	ite	10/16/2013	15.0	2.5	1.50 +/- 0.5	Stain Line
1B	PB-1B	509+35	122 Rt.	10/16/2013	20.0	2.5	0.75 +/- 0.5	Root System
1C	PB-1C	508+60	440 Rt.	10/16/2013	20.0	1.0	0.00 +/- 0.5	Ground Surface
2A	PB-2A	554+60	230 Lt.	10/22/2013	20.0	2.0	0.67 +/- 0.5	Root System
2B	PB-2B	553+50	280 Rt.	10/23/2013	20.0	3.0	0.75 +/- 0.5	Root System
2C	PB-2C	523+10	350 Lt.	10/23/2013	20.0	3.5	0.67 +/- 0.5	Root System
3A	PB-3A	630+10	1120 Lt.	10/16/2013	20.0	3.5	1.92 +/- 0.5	Root System/Stain Line
3B	PB-3B	629+25	250 Lt.	10/16/2013	20.0	+0.2	0.50 +/- 0.5	Ground Surface
3C	PB-3C	642+30	310 Lt.	10/22/2013	20.0	3.0	1.25 +/- 0.5	Root System
4A	PB-4A	680+40	75 Lt.	10/23/2013	20.0	3.0	1.08 +/- 0.5	Root System/Stain Line
4A	PB-4A	683+15	100 Lt.	10/23/2013	20.0	4.5	1.08 +/- 0.5	Root System/Stain Line
4B	PB-4B	659+06	384 Rt.	11/2/2016	20.0	2.0	2.00 +/- 0.5	Stain Line
4B/4C	PB-4BC	659+75	410 Rt.	10/22/2013	20.0	2.5	1.25 +/- 0.5	Root System
4D	PB-4D	671+75	400 Rt.	10/22/2013	20.0	3.0	1.17 +/- 0.5	Root System
5A	PB-5A	696+10	190 Lt.	10/22/2013	20.0	2.0	0.75 +/- 0.5	Root System
5B	PB-5B	688+50	210 Lt.	10/22/2013	20.0	2.0	0.50 +/- 0.5	Root System
5C	PB-5C	698+75	220 Rt.	10/23/2013	20.0	2.5	1.00 +/- 0.5	Root System

Note: "+" in the Water Table Depth represents standing water

For estimation purposes for the proposed pond sites, the SHWT was assumed to be 0.5 foot lower as indicated.

E. WETLANDS, PROTECTED SPECIES AND PROTECTED SPECIES HABITAT

Scheda Ecological Associates, Inc. has prepared a Protected Species and Wetlands Pond Siting Assessment Report for SR 710 within the project area, dated February 2014. Please note that the pond areas have been adjusted after the initial survey, but the pond locations have not changed.

According to the report, data was collected and reviewed from a variety of sources to determine if any wetlands and/or protected species or their habitats occur within or adjacent to the proposed pond locations. Pedestrian field surveys of the proposed pond locations were conducted to verify preliminary data and to assess existing ecological conditions at each site. The proposed sites were field reviewed within a 50-foot buffer around each location to visually scan for evidence of listed species and general wildlife utilization. See **Appendix 3** for the SR 710 Protected Species and Wetlands Pond Siting Assessment Report.

Scientist from the Wantman Group conducted on-site surveys to locate jurisdictional wetlands and/or surface waters within or immediately adjacent to each proposed pond site. Wetlands were identified and characterized according to the USFWS Classification System of Wetlands and Deepwater Habitats of the United States (Cowardin et al. 1979). The boundaries were delineated using handheld GPS, and the existing land use/land cover was classified according to FLUCFCS. The wetlands associated with the pond sites are identified in the Protected Species and Wetlands Pond Siting Assessment Report (See Appendix 3). A summary of the evaluations for potential impacts to wetlands, protected species and their habitats for each proposed pond site is provided as Table 3.

According to the Environmental Report, the wetland mitigation cost assumes moderate wetland quality scores. The description of the wetland/surface water involvement ratings are as follows:

- None No wetland/surface water impacts; no protected species anticipated to occur based on habitat quality, no observations or records.
- Low Wetlands/surface waters comprise 1% to 24% of pond footprint; potential but unlikely presence of protected species.
- Medium Wetlands/surface water comprise 25%to 49% of pond footprint; indication of species where mitigation is reasonable and possible.
- High Wetlands/surface waters comprise 50% or more of pond footprint; indication of species where mitigation is difficult, costly, or not possible.

The Table 3 matrix summarizes the results of field surveys, literature searches, and evaluations for wetlands, protected species and their habitats in the areas of the SR 710 proposed pond sites. According to this study, for Wetland/Surface Water Involvement, the proposed Pond Sites 1A, 2A, 2B, 3A, 3C, 4A, 4C, 4D, and 5C have a rating of "None". Pond Sites 2C, 3B, 4B, and 5B have ratings of "Low"; Pond Sites 1B and 5A have a rating of "Medium"; and Pond Site 1C has a rating of "High" for Wetland/Surface Water Involvement. For all pond sites except those with a rating of "None", wetland mitigation costs were assessed. For Pond Sites 2C-Option 1, and 2C-Option 2, the rating was initially assessed as "Low", but the pond options were subsequently reconfigured to provide a 25 foot buffer around the wetland.

All pond sites were assessed a rating of "Low" for Protected Species Involvement except for Pond 4A and Pond 4D. Protected gopher tortoise burrows were identified at these two sites. The cost associated with mitigation at these two sites is estimated to be \$18,000 and \$15,000 for Pond 4A and Pond 4D, respectively. This would include relocation of the gopher tortoise with the associated permits from the FWC.

 Table 3 - SMF Site Descriptions and Wetlands/Protected Species Involvement

SMF Site	SMF Acreage	Description	FLUCFCS Code	Soils (NRCS Soil Survey)	Wetland Acreage	Percent Wetland Coverage	Wetland Mitigation Cost*	Wetlands / Surface Water Involvement	Protected Species Involvement/Concerns
1A	2.32	Undeveloped Parcel dominated by exotic vegetation (woody and herbaceous)	3200 - Shrub & Brushland	Immokalee Fine Sand (11)	0	0%	\$0	None	Low
1 B	1.21	Undeveloped parcel containing mix of shrub and wooded areas	4340 – Hardwood – Conifer Mixed; 6410 - Freshwater Marsh	Manatee Loamy Fine Sand, Depressional (6)	0.5	40%	\$30,000	Medium	Low
1C	0.88	Forested wetland (mix of exotic and native species); existing small pond near southern limit	6170 - Mixed Wetland Hardwoods	Manatee Loamy Fine Sand, Depressional (6)	0.88	100%	\$52,800	High	Low
2A	7.84	Undeveloped parcel containing mix of open pasture and wooded areas	2110 - Improved Pasture; 4271 - Oak - Cabbage Palm Forest	Immokalee Fine Sand (11), Riviera Fine Sand (9)	0	0%	\$0	None	Low
2B	9.95	Undeveloped parcel containing mix of pasture and wooded areas	2110 - Improved Pasture;	Immokalee Fine Sand (11)	0	0%	\$0	None	Low
2C	10.55	Undeveloped parcel containing mix of pasture and wooded areas	2110 - Improved Pasture; 4271 - Oak - Cabbage Palm Forest; 6170 Mixed Wetland Hardwoods; 6410 - Freshwater Marsh	Basinger Fine Sand (2); Pindea Fine Sand (8); Floridana, Placid, and Okeelanta Soils, Frequently Flooded (19)	0.7	7%	\$42,000	Low	Low
3A	3.82	Unimproved pasture with some slash pine and saw palmetto	2110 - Improved Pasture	Immokalee Fine Sand (11)	0	0%	\$0	None	Low
3B	3.74	Unimproved pasture	2120 - Unimproved Pasture; 2110 - Improved Pasture; 6410 Freshwater Marsh	Immokalee Fine Sand (11); Basinger and Placid Soils, Depressional (3)	0.3	8%	\$18,000	Low	Low
3C	3.78	Undeveloped parcel containing mix of pasture and wooded areas	4340 – Hardwood – Conifer mixed	Immokalee Fine Sand (11); Basinger and Placid Soils, Depressional (3)	0	0%	\$0	None	Low
4A	7.79	Undeveloped parcel containing mix of distrubed herbaceous uplands (spoil berms), palmetto-dominated shrub, and wooded areas	3100 Herbaceous Dry Prairie; 4340 – Hardwood – Conifer mixed	Immokalee Fine Sand (11)	0	0%	\$0	None	Medium
4B	4.58	Undeveloped parcel containing mix of pasture and wooded areas	2120 - Unimproved Pasture; 4340 – Hardwood – Conifer Mixed; 5100 - Streams and Waterways	Immokalee Fine Sand (11); Basinger and Placid Soils, Depressional (3)	0.1	2%	\$6,000	Low	Low
4C	3.57	Undeveloped parcel containing mix of pasture and wooded areas	2120 - Unimproved Pasture; 4340 - Hardwood - Conifer Mixed	Immokalee Fine Sand (11)	0	0%	\$0	None	Low
4D	8.61	Wooded area disturbed by frequent ATV activity adjacent to a medium density residential area	4340 – Hardwood – Conifer Mixed; 1130 - Mixed Use, Low Density Fixed and Mobile Home Units; 1210 - Fixed Single Family Units - Medium Density	Immokalee Fine Sand (11)	0	0%	\$0	None	Medium
5A	2.63	Undeveloped parcel dominated by wooded areas	4340 – Hardwood – Conifer Mixed; 6170 Mixed Wetland Hardwoods	Immokalee Fine Sand (11); Floridana, Placid, and Okeelanta Soils, Frequently Flooded (19)	0.8	30%	\$48,000	Medium	Low
5B	2.53	Unimproved pasture with some laurel oak, cabbage palm, and saw palmetto	2510 – Horse Farm; 6410 - Freshwater Marsh	Immokalee Fine Sand (11)	0.5	20%	\$30,000	Low	Low
5C	3.53	Undeveloped parcel dominated by wooded areas	4340 – Hardwood – Conifer Mixed	Immokalee Fine Sand (11); Floridana, Placid, and Okeelanta Soils, Frequently Flooded (19)	0	0%	\$0	None	Low

^{* =} Approximate wetland mitigation cost assumes moderate wetland quality scores (UMAM = 0.5 per acre) and \$120,000 per credit

NOTES:

None No wetland/surface water impacts; no protected species anticipated to occur based on habitat quality, no observations or records

Wetlands/surface waters comprise 1% to 24% of pond footprint; potential but unlikely presence of protected species

Medium Wetlands/surface waters comprise 25% to 49% of pond footprint; indication of species where mitigation is reasonable and possible

High Wetlands/surface waters comprise 50% or more of pond footprint; indication of species where mitigation is difficult, costly, or not possible

After preferred pond sites were chosen, the wetland impacts to each site were further field evaluated by the Wantman Group. The wetland impacts were then surveyed and presented as a design file with text notes indicating the wetland impact area. Pond Site 1B, Pond Site 3B, and Pond Site 5A were determined to have wetland impacts of 0.47 acres, 0.35 acres, and 0.11 acres, respectively. Pond Site 2A-Option 1 and Pond Site 4B-Option 2 do not have wetland impacts. Prior to stormwater permitting of the selected pond sites, the sites will need to be resurveyed for Listed Species, including caracara.

F. FLOODPLAINS

The Federal Emergency Management Agency (FEMA) has developed Flood Insurance Rate Maps (FIRM) for unincorporated Okeechobee County Areas. The project is covered by FIRM Map Numbers 12093C0415C, 12093C0420C, 12093C0480C, and 12093C0485C which became effective July 16, 2015. There are areas defined as Zone A and Zone AE (floodplain elevation determined) within the 100 year floodplain. See Figure 5 in Appendix 1 for the updated FEMA FIRM Map with pond alternatives. Table 4 shows the effective FEMA floodplains for each proposed pond site.

Table 4 - 2015 Effective FEMA Floodplains

Pond Site	2015 Effective FEMA
	Floodplain
1A	Yes
1B	No
1C	Yes
2A	No
2B	No
2C	No
3A	No
3B	No
3C	No
4A	No
4B/4C	No
4D	No
5A	Yes
5B	No
5C	No

A preliminary ICPR model of the existing region was performed to determine the 100 year floodplain. The 100 year storm (FDOT 14 inches) was input into the analysis. The resulting floodplain depicts a similar floodplain to the 2015 FEMA FIRM Maps.

During actual pond design, the depressional areas impacted by the roadway will be analyzed for the pre-post conditions. Importer/exporter calculations will be used as opposed to providing compensating ponds. The hydroperiod in the wetlands will be maintained in the offsite design. For this reason, floodplains are not considered to be a critical factor in the pond design.

G. CONTAMINATION SCREENING

An initial Draft Level I PSR Contamination Screening Evaluation Report (CSER) - Proposed Ponds was conducted by Tierra, Inc. for the subject project dated November 22, 2013. The initial report was updated to the Draft Level I PSR CSER (Rev. 2) and dated July 14, 2014 (See **Appendix 4**). This screening is based on historical aerial and topographic map reviews, governmental database reviews and site reconnaissance.

From the Level I Report, the pond sites within the project corridor were assigned a risk rating for potential contamination. For sites ranked "No" or "Low", additional work is not recommended at this time. If a facility's permitting/regulatory status changes before acquisitions are initiated, additional screening should be performed.

For the sites with rankings of "Medium" or "High", Tierra recommends Level II field screening which will determine if environmental impacts exist at the preferred pond sites. A Level II field screening was required for the five preferred pond sites. This should include, at a minimum, soil borings to the proposed pond depth and soil sampling for total arsenic. Table 5 has been taken from the CSER (Rev. 2) and shows the Pond Site Potential Contamination Risk Ratings for each proposed site.

Table 5 - Pond Site Potential Contamination Risk Rating

Pond Site	Risk Rating	Comment
1A	No	2.32 Acres. Current and historic woodlands
		1.20 Acres. Risk ranking low for possible onsite use as water pipeline
1B	Low	construction staging area in 1994. Current and historic woodlands with an
		apiary (bee hives) and open, grassy area
1C	No	0.88 Acres. Current and historic woodlands
2A - Option 1	No	14.23 Acres. Current and historic pastureland and woodlands
2A - Option 2	No	7.93 Acres. Current and historic pastureland and woodlands
2A - Option 3	No	6.42 Acres. Current and historic pastureland and woodlands
2B - Option 1	No	15.37 Acres. Current and historic pastureland and woodlands
2B - Option 2	No	10.00 Acres. Current and historic pastureland and woodlands
2B - Option 3	No	7.08 Acres. Current and historic pastureland and woodlands
2C - Option 1	No	6.86 Acres. Current and historic pastureland and woodlands
2C - Option 2	No	6.14 Acres. Current and historic pastureland and woodlands
3A (formerly 3B)	Medium	4.18 Acres. Risk ranking Medium for onsite livestock holding pen.
, , ,	Medium	Current pastureland, historic woodlands, wetlands, pastureland and cleared land
3B (formerly 3A)	No	2.44 Acres. Current and historic pastureland and woodlands
3C	Low	3.81 Acres. Risk ranking Low for onsite stormwater pond. Current and historic
30	LOW	woodlands
4A - Option 1	Low	3.98 Acres. Risk ranking Low for non-adjoining Townstar #40/BP gas station to
чи орион і	LOW	the southwest. Current woodlands, historic wetlands in northeast corner
4A - Option 2	Low	3.34 Acres. Risk ranking Low for non-adjoining Townstar #40/BP gas station to
option 2		the southwest. Current woodlands, historic wetlands in northeast corner
		8.17 Acres. Risk ranking Medium for onsite livestock holding pen.
4B/4C - Option 1	Medium	Current and historic woodlands with two (2) sheds, a livestock holding pen and
		unpaved trails
4B - Option 2	No	4.59 Acres. Current and historic woodlands with unpaved trails
		6.08 Acres. Risk ranking Medium for east adjoining Townstar #40/BP gas station.
		Current and historic woodlands with unpaved trails/tracks;
		historic wetlands in northeast corner on-site from 1940 to 1960s;
4D Ontion 1	Maralitum	Adjoining operational Townstar #40/BP gas station to the east since 1986;
4D - Option 1	Medium	three (3) groundwater monitor wells were installed on Pond 4D in 2007 to assess
		potential petroleum impacts. The laboratory analytical results did not indicate
		petroleum contaminants in exceedance of the GCTLs. The highest OVA reading during monitor well installation was one (1) ppm. No soil samples were
		collected for laboratory analytical testing during this Level I investigation.
		4.33 Acres. Risk ranking Medium for east adjoining east Townstar #40/BP gas
4D - Option 2	Medium	station. Current and historic woodlands with unpaved trails/tracks; historic
		station. Current and historic woodiands with dispaved transfit dcks, historic

Pond Site	Risk Rating	Comment
		wetlands in northeast corner onsite from 1940 to 1960s
5A	No	2.62 Acres. Current and historic woodlands/wetlands/pastureland
5B	No	2.53 Acres. Pastureland and wetlands associated with north adjacent Paddock Farms (miniature horses)
5C	Low	3.53 Acres. Risk ranking Low for offsite livestock holding pen, approximately 50 feet south. Current and historic woodlands

The contamination screening evaluation has resulted in four "Medium" rankings for pond sites. A "Low" ranking was issued for five pond sites and a "No" ranking was issued for the remaining fourteen pond sites.

Subsequent to this, a Draft Level II Field Screening Report (FSR) - Preferred Ponds was performed by Tierra, Inc. dated January 13, 2017. This included a Level II soil and groundwater field screening at the preferred pond locations. The results of the Level II preferred pond sites contamination analysis are shown in Table 6 below. Both reports (Level I-Rev. 2 and Level II Screenings) are included in Appendix 4.

Table 6 - Level II Contamination Risk Rating Summary for Preferred Pond Sites

Preferred Pond	Pre-Level II Risk	Post-Level II Risk	Arsenic
	Rank	Rank	Contamination in
			Tested Locations
Pond 1B	LOW	NO	NOT INDICATED
Pond 2A-Option 1	LOW	NO	NOT INDICATED
Pond 3B	NO	NO	NOT INDICATED
Pond 4B-Option 2	NO	NO	NOT INDICATED
Pond 5A	NO	NO	NOT INDICATED

Notes: Undesirable buried debris was not encountered in the borings for all 5 pond sites.

As the preferred pond sites did not indicate arsenic in soils tested, Tierra recommends no additional work at this time. Further, all soils identified in this analysis contained less than 2.1 mg/kg total arsenic RDE SCTL, and are unrestricted in the reuse and placement. Also, material (glass fragments, pieces of metal rods, & debris) was observed in the borings for the southern portion of Pond 4B-Option 2 which is not considered to be a contamination concern but should be removed and properly disposed of prior to construction activities.

H. CULTURAL RESOURCE ASSESSMENT

Archaeological Consultants, Inc. (ACI) prepared the Preliminary Cultural Resource Assessment (CRAS) of the proposed pond sites for SR 710, dated October 2013. The CRAS was subsequently updated in April 2015 (See Appendix 5). The survey was necessary to determine if any significant or potentially significant cultural resources, including archaeological sites or historic structures, will be impacted by the sixteen alternate pond sites. Known or potentially significant cultural resources are defined as those sites which are listed, determined eligible, or considered potentially eligible for listing in the National Register of Historic Places (NRHP).

The study included an investigation of project aerials, review of Florida Master Site File (FMSF) records, NRHP listings, the cultural resource assessment for the Project Development and Environmental (PD&E) Study, the Okeechobee County Soil Survey, and cultural resource survey reports for the project vicinity.

According to this study, each proposed pond site was evaluated for archaeological potential (high, moderate or low). All of the proposed pond alternates were assigned either a "Low" or "Moderate" potential for prehistoric or historic archaeological sites; and none of the proposed pond sites were assigned a high potential.

The cultural resource impact potential is included in the Archaeological Data found in **Table 7** and in **Appendix 5**, Cultural Resource Assessment of Proposed Pond Sites.

Table 7 - Cultural Resource Assessment

Soil Type, Archeological						
Pond ID	Acres	Elevation, Drainage, and Environmental Association	Potential/Comments			
1A	2.238	Immokalee fine sand; Nearly level, poorly drained in broad flatwoods	Low			
1B	1.203	Manatee, Delray, and Okeelanta soils; Nearly level, very poorly drained on marshy plains	Low			
1C	0.929	Manatee, Delray, and Okeelanta soils; Nearly level, very poorly drained on marshy plains	Low			
2A	14.227	Immokalee fine sand; Nearly level, poorly drained in broad flatwoods	Moderate			
2B	15.372	Immokalee fine sand; Nearly level, poorly drained in broad flatwoods	Moderate			
2C	6.864	Pompano fine sand; Nearly level, poorly drained in grassy sloughs and depressions	Low			
3A	4.181	Basinger and Pompano fine sands: Nearly level, poorly drained, in sloughs and isolated depressions in the flatwoods Immokalee fine sand; Nearly level, poorly drained in broad flatwoods	Low			
3B	7.244	Immokalee fine sand; Nearly level, poorly drained in broad flatwoods	Low			
3C	5.778	Immokalee fine sand; Nearly level, poorly drained in broad flatwoods	Low; a portion previously tested with negative results (Janus Research 2010)			
4A	7.882	Myakka fine sand: Nearly level, poorly drained in broad flatwoods Placid fine sand; Nearly level, very poorly drained in low areas	Low			
4B	8.168	Immokalee fine sand; Nearly level, poorly drained in broad flatwoods	Moderate			
4C	Combined with 4B	Immokalee fine sand; Nearly level, poorly drained in broad flatwoods	Moderate; dilapidated sheds, ca. 1990 (not historic)			
4D	8.616	Myakka fine sand: Nearly level, poorly drained in broad flatwoods Immokalee fine sand; Nearly level, very poorly drained in low areas	Low			
5A	2.624	Immokalee fine sand; Nearly level, poorly drained in broad flatwoods	Low			
5B	2.534	Immokalee fine sand; Nearly level, poorly drained in broad flatwoods	Moderate			
5C	3.528	Immokalee fine sand; Nearly level, poorly drained in broad flatwoods	Low			

It was determined that five of the potential stormwater management sites had a "Moderate" archaeological potential. The remaining sites were given a rating of "Low" due to the generally level and poorly drained soils at these locations. Another

reason for a "Low" rating is development within or adjacent to potential pond sites. Several historic resources were identified in the surrounding vicinity of the potential pond sites. The report further indicates that <u>no</u> historic buildings (50 years of age or older) were within or adjacent to any proposed pond sites.

After the preferred pond selections were determined, a Cultural Resource Assessment Survey (CRAS) of Preferred Pond Sites was performed by ACI, dated November 2016. Based on background research and field investigations, no prehistoric archaeological sites or historic buildings or structures were recorded or identified within the APE (defined as area of potential effects within each pond site). From this analysis, ACI concluded that, based on the results of the CRAS, this undertaking will have no effect on resources listed, determined eligible, or potentially eligible for listing in the NRHP. The updated April, 2015 CRAS and the CRAS for the Preferred Pond Sites prepared by ACI are included in **Appendix 5**.

I. EXISTING PERMITS

Within the project corridor, there is a number of current SFWMD Permits. Included among these are the Okeechobee Utility Authority (SFWMD Permit #47-00004-W, App. No. 010614-23); the Okeechobee Commerce Center (SFWMD Permit #47-00638-P, App. No. 040130-34); Northshore Village (SFWMD Permit Denied, App. No. 061031-17); SR 710 (SFWMD Permit #47-00327-S, App. No. 910827-3); and SR 70 Widening (SFWMD Permit No. 47-01151-P, App. No. 121210-2). See Figure 8, Appendix 1 for existing permits.

Table 8 summarizes the pond sites located within existing permits or applications. None of these sites are developed as of this submittal.

Table 8 - Summary of Existing Permits

Pond	Map Label	Permit/Application Number	Permit Name
1A	44	47-00847-P/ 051213-5	Southern Trace
3A	41	47-00786-P/ 061031-17, 070807-9	Northshore Village
3B	41	47-00786-P/ 061031-17, 070807-9	Northshore Village
5A	28	47-00582-P/ 071024-1, 061102-4, 040607-11, 020909-5	Okeechobee County Agri-Civic Center

II. DESIGN CONSIDERATIONS

A. Roadway Geometry

Typical Section

A four-lane suburban typical section is proposed. The roadway will consist of two twelve-foot wide travel lanes in each direction, separated by a raised thirty-foot wide grassed median. This roadway section will also include four foot shoulders to the inside of the travel lanes and six and one-half-foot (eight-foot useable) shoulders adjacent to the outside travel lanes. Type E curb and gutter will be provided along the median and outside edges of the roadway along with a closed storm-water conveyance system. A continuous five-foot wide concrete sidewalk will be provided on the south side of the roadway and a ten-foot wide shared-use path will be provided on the north side of the roadway. Appropriate left and/or right turn lanes will be provided at major intersections. This suburban typical section has a twenty nine-foot border width and is to be constructed within one hundred sixty foot minimum of right-of-way.

Horizontal Alignment

The proposed SR 710 runs west to east through the project area. The horizontal alignment consists of several tangents and four major horizontal curves. The design speed for the proposed alignment is 50 miles per hour for the suburban section. There are four sections of superelevated roadway through the curves located throughout the project. The first two curves are near the beginning of the project just before and after the crossing over Taylor Creek, the third curve is a major curve to the south, and the last curve is at the easterly transition to existing SR 710.

<u>Vertical Alignment</u>

The proposed SR 710 vertical alignment is relatively flat for the entire project. Grades appear to generally be 0.30% to 0.50% with some variations above and below. There are two bridge crossings along the new alignment: over Taylor Creek and over L-63N Canal. In these locations, there are uphill grades to accommodate the crossings. The elevation of the roadway Profile Grade Line varies from 23.85 to 34.96 feet NAVD based on the updated profile that incorporated the 15% line and grade meeting comments.

The profile grade has been coordinated with the roadway engineers during the pond site evaluation. There are several areas that are being coordinated during the design to determine if raising the profile 1, 2 or 3 feet will be more cost effective. A Preliminary Design High Water/Base Clearance Memo was prepared by The Balmoral Group under separate cover to determine minimum base clearance and the current profile is based on this document and other factors determined during the 15% line and grade meeting. It was prepared using a minimum of 2 feet of base clearance, as a variance from the required 3 foot base clearance is expected. Costs have been

estimated for right-of-way and additional construction costs for raising the road 1, 2, or 3 feet and these were used to refine the pond sizes in Basin 2 and 4. See **Appendix** 6 for cost calculations.

B. RIGHT-OF-WAY

The proposed right-of-way width through the project area will generally be 160 foot minimum. Additional right-of-way will be acquired in various locations along the corridor to construct stormwater treatment facilities. A meeting with the FDOT Right-of-Way personnel was held on September 9, 2013 at FDOT, District 1 offices (See Appendix 9)

C. UTILITIES

As the proposed SR 710 is a new alignment, there are very few existing utilities within the corridor.

Pond 3A conflicts with both FPL Distribution and Transmission pole lines. This will require additional coordination and a possible relocation to the north of the lines.

Pond 4C has existing FPL Distribution facilities (aerial pole line) and Centurylink facilities (BT/BFO) along the southern side of Pond 4C. These utilities are not expected to be impacted.

D. PERMIT AGENCY COORDINATION

South Florida Water Management District (SFWMD)

This project is considered to be within the South Florida Water Management District (SFWMD). The SFWMD will regulate and control stormwater discharge and impacts to wetlands and surface waters for this project. The SFWMD will require an Environmental Resource Permit (ERP) for this project prior to initiating construction. The office responsible for the technical review of the permit application package will be the South Florida Water Management District in Okeechobee, Florida. A preapplication meeting was held on May 29, 2013, to discuss and determine SFWMD treatment criteria for the project. A copy of the meeting minutes is located in Appendix 9. The following is a summary of the stormwater criteria -

- a. The project is mostly located in the S-133 Basin which has an allowable discharge of 15.6 CSM. It was agreed that the SR 710 project could utilize a pre-post method. Kelly Cranford added the pre-development calculations needed to be reasonable and to review the permit for North Shore Village for additional information. Likewise, the Industrial Park at the beginning of the project has a permitted discharge through the Industrial Park project which would be considered the allowable discharge at that outfall location.
- b. 2 ½ inches over the impervious area will be the controlling factor for water quality. The additional 50% requirements for impaired water bodies will not be

needed as the pre-post nutrient loading calculations will show that there are no offsite water quality impacts. Basin will be top of slope to top of slope for the Typical Section.

- c. Pasture is acceptable for EMC values for the areas that are currently pasture.
- d. Drawdown in the wet ponds will be ½" of runoff over the basin in 24 hours. It is expected that the minimum 3" bleeder will be utilized on the control structures.

Additional meetings were held with the SFWMD on July 31, 2014; March 24, 2015; July 7, 2015; to discuss the regional pond option. See **Appendices 9** and **10** for Correspondence and the Regional Pond Study.

United States Fish and Wildlife Service (USFWS)

The United States Fish and Wildlife Service has jurisdiction over federally listed species. All of the proposed Pond Sites are located within the following USFWS Consultation Areas: crested caracara, Florida grasshopper sparrow, Everglade snail kite, Florida bonneted bat, and Okeechobee Gourd. These are addressed in **Appendix 3**.

Florida Fish and Wildlife Conservation Commission

The Florida Fish and Wildlife Conservation Commission will provide commentary during the ERP review process. The Commission will conduct field reviews and comment to the SFWMD on any adverse effects the proposed activity may have on state protected wildlife species and their habitat.

US Army Corps of Engineers

The United States Army Corps of Engineers (USACE) has jurisdiction over all wetlands classified as waters of the United States. The Corps requires the acquisition of a Section 404 Dredge and Fill Permit for activities in all waters of the United States prior to beginning construction. The USACE provides a separate and independent review of the Wetland Resource Management Permit from the SFWMD.

Environmental Protection Agency (EPA)

The EPA requires permits for stormwater discharge in association with the National Pollutant Discharge Elimination System (NPDES) and the Clean Water Act. The application requirements include a stormwater pollution prevention plan indicating both structural and non-structural controls to be implemented. Since it is anticipated that project impacts will be greater than one acre, an NPDES permit will be required.

E. POLLUTANT LOADING REQUIREMENTS

A Stormwater Quality Memorandum was initially prepared separately for the PSR to address Nutrient Loading Requirements. For the Final PSR, the preliminary Pollutant Loading design calculations for the preferred pond sites have been performed and are located in **Appendix 7**. These calculations are subject to change during final design.

Based on the final design, Basins 1 and 2 will drain to Taylor Creek (WBID 3205) and Basin 5 will drain to Mosquito Creek (WBID 3203B). According to FDEP's 2013 Comprehensive Verified List of Impaired Waters, both of these water bodies have nutrients listed in the "Parameters Assessed under the Impaired Waters Rule" column and both have exceeded the threshold for Total Phosphorus (TP) and Total Nitrogen (TN). As such, both TP and TN are considered in this analysis. According to FDOT guidance (*Nutrient Loading Calculations for FDOT Projects*), SFWMD requires demonstration that the project will not result in increased nutrient loading compared to current conditions. Basins 3, 4, and EX-4 (an existing FDOT pond for SR 70) will outfall to the L-63 Canal (WBID 3203C) which is not considered impaired and therefore was not evaluated. EX-4 discharges to Taylor Creek in the existing condition, but will discharge to the L-63N Canal in the post condition.

The procedure for calculating the Existing and Post nutrient loadings is a two-step process. First, the potential for runoff is determined based on an analysis of curve number (CN) for pervious areas and impervious cover to determine a runoff coefficient. Second, Event Mean Concentrations (EMCs) are estimated based on values from the literature. Nutrient loading is then calculated as the product of the annual runoff and the EMC.

To calculate the runoff coefficient, the Directly Connected Impervious Area (DCIA) percentage and non-DCIA CN must be known. In the case of a dual hydrologic soil group, the well-drained assumption was used (e.g., A/D soils were considered to be A soils). This assumption is conservative because it will tend to under-estimate runoff in existing conditions, and thus increase the difference in runoff when it is compared to post conditions. The lookup table used to define the curve number from the land use and soil type is provided in Table 9.

Table 9 - Curve Numbers Based on Land Use and Soils

LanditJseb	Hydrologicl S oill t Groupb			
Landwseb	Ab	Bb	Cb	Db
Imperviouss	98s	98s	98s	98s
Pasture:Good:Cond.s	39s	61s	74s	80s
Waters	100s	100s	100s	100s
OpensGoodsCond.s	39s	61s	74s	80s
Woods@ood@ond.s	30s	55s	70s	77s
Woods&Fair&Cond.s	36s	60s	73s	79s

DCIA percentage was calculated based on land use:

- Impervious and water were assumed to be 100% DCIA
- Pasture, open, and woods were assumed to be 5% DCIA

The area-weighted non-DCIA CN and percent DCIA were calculated for each basin. For the non-DCIA CN, the GIS coverages of land use and soil were overlain and a CN was assigned to every unique combination of land use / soil type within each basin. The area-weighted CN was then computed accordingly. Appendix 7 provides the details of this analysis for Existing and Post conditions, respectively. Based on the non-DCIA CN and percent DCIA, the runoff coefficient was interpolated from the tables in Appendix E of the Applicants Handbook. For each basin, the area-weighted EMC values were calculated based on the Water Quality land use categories and EMC reference values. The EMC values used in this study are provided in Table 10.

Table 10 - EMC Values Based on Land Use

WQlCategoryb	Land b Use b Categoryb (Source ¹)b	TNb	TPb
Highways	Highways(3)s	1.190s	0.155s
	Undeveloped, Rangeland, s		
Opens	andsForests(2)s	1.150s	0.055s
Pastures	Pastures(1)s	2.480s	0.700s
Waters	Waters(4)s	0.000s	0.000s
	Undeveloped, Rangeland, s		
Woodss	andsForests(2)s	1.150s	0.055s

¹Sourcesæreæssfollows:ss1s-sTables3.4sofsAH;s2s:sHarpersandsBaker,s2007;s3s-sFDOT,s 2011as&sFDOT,s2011b;s4s-snosloadingsassumedsforswatersbodiessandswatersqualitys pondss

For the nutrient loading assessment of Existing and Post conditions, the basins were divided into land use categories by digitizing. Two sets of land use categories were used. The land use categories used to calculate the CN differentiates highways into pervious and impervious surfaces, whereas the WQ land use categories (used to look

up the EMC value) lump impervious and pervious surfaces together. Figures 1 to 5 within Appendix 7 show the land use for each basin for Existing and Post conditions, according to the two sets of land use categories (for CNs and EMCs).

Once the Existing and Post nutrient loading values are calculated, the required nutrient removal efficiency is determined based on the applicable regulations. Ponds 1 and 5 provide dry retention. Ponds 2, 3, and 4 provide wet detention.

Nutrient removal efficiency for wet detention is related to pond permanent pool volume using an empirically-derived equation based on the average annual hydraulic residence time (pond permanent pool volume divided by the annual runoff). Nutrient removal efficiency for retention is related to the depth of runoff retained, allowing water to percolate through soils and foster pollutant removal.

Nutrient removal was assessed within the UCF BMPTRAINS (Best Management Practices Treatment for Removal on an Annual Basis in Stormwater) spreadsheet model. The model was set up separately for basins discharging to Taylor Creek and the basin discharging to Mosquito Creek. The objective was to show a net reduction in the pollutant loadings for TN and TP to each of these waterbodies. The BMPTRAINS uses FDEP guidance (*Stormwater Quality Applicant's Handbook*, March 2010) to determine treatment efficiencies and allows input of treatment trains to maximize pollutant removal. The complete input and results for the BMPTRAINS is provided in **Appendix** 7. These results are summarized in **Table 11**, showing the pre/post phosphorous and nitrogen loading results for the post-development condition.

Table 11 - Phosphorus and Nitrogen Loading Analysis Summary

		Pre-	Post-	Pre-	Post-
		Development	Development	Development	Development
Receiving	Post Basins	Phosphorous	Phosphorous	Nitrogen	Nitrogen
Water		Outflow Mass	Outflow Mass	Outflow Mass	Outflow Mass
		Loading	Loading	Loading	Loading
		(kg/yr)	(kg/yr)	(kg/yr)	(kg/yr)
Taylor Creek	1, 2	17.35	4.69	90.19	82.34
(WBID 3205)	., _	17100	1107	70117	02.01
Mosquito Creek	5	1.37	0.62	17.24	5.03
(WBID 3203B)	3	1.37	0.02	17.24	3.03

III. STORMWATER CONVEYANCE

A. EXISTING CONDITIONS

In the existing condition, the area in the vicinity of the project discharges to Taylor Creek, a historic ditch, and Mosquito Creek. The existing bridge over the L-63N canal discharges to the L-63N canal. All ultimately discharge to Lake Okeechobee. Control structures are utilized along L-63N Canal and Taylor Creek. The project area is characterized by open drainage basins. For the majority of the project, runoff during rainfall events is conveyed as sheet flow or shallow concentrated flow to localized depressions or wetlands, eventually outfalling to the Taylor Creek. Each depression impacted by the roadway is to be analyzed for its pre-post conditions in order to ensure there are not adverse impacts to water stages to offsite property owners.

As this is a new alignment, and connects with existing SR 710 for only 2540 feet to the project end, there are no existing cross drains on the alignment. However, there are several side drains conveying runoff toward SR 710 existing alignment and one cross drain on the existing SR 710 that will be removed. There is one existing bridge at the L-63N Canal (Station 685+00) which will require replacement and/or an additional bridge constructed on the north side.

B. Drainage Basins

The topography surrounding the project is flat to gently sloping. The elevations range from 30 feet to 10 feet NAVD. Six pre-development basins have been identified to the east of Taylor Creek which all eventually drain to Lake Okeechobee through Taylor Creek, L-63N Canal, Mosquito Creek, and a historic ditch. For the purposes of establishing drainage basins for this project, data was collected from the original FDOT drainage maps for SR 710 and SR 70, existing SFWMD permits and Okeechobee County Basin Studies. CatchmentSIM™ software was utilized to delineate basins using contour LiDAR data. The drainage basins were then confirmed by field review. See Figures 10A to 10H in Appendix 1 for the Pre-Development Drainage Basin exhibits. Discharge locations are labeled TWA through TWE (Tailwater A through Tailwater E).

A regional ICPR model was performed for the pre-development areas surrounding the SR 710 alignment. The pre-development basins are delineated as Basin A, Basin B, Basin CC, Basin C, Basin D, and Basin E. Basin A consists of a large tract of rural land located predominantly to the north of and within the proposed SR 710 alignment. It is bounded by Taylor Creek on the west and L-63N Canal on the north and east. Basin A has ten sub-basins which discharge to Taylor Creek. Basin B (aka Douglas Park) has seven sub-basins and discharges to the east side of Taylor Creek south of SR 710. Basin CC (aka Okeechobee City Commerce Center) also discharges to the east side of Taylor Creek and is one large basin. Basin C has six sub-basins which are located which are located to the north of SR 70 and are bounded by the railroad on the southwest. Basin C discharges to the roadside ditches of SR 70 R/W. Basin D has sixteen sub-basins which are located to the north of SR 70. Basin D discharges to the roadside ditches of SR 70 R/W. It is located approximately between Stations 571+00

and 638+00 from the west side to the east side of SR 710, and consists of rural land as well as a residential area. Basin E is located south of SR 70 and is bounded by L-63N Canal on the east side. It is located from the west side to the east side of SR 710 from Station 638+00 to 684+00, and has thirteen sub-basins.

Basin 1

The pre-development SR 710 roadway and pond basins are summarized below. Pre-development Basin 1 is on the eastern side of the City of Okeechobee and is located between US 441 to Taylor Creek, and just south of the Okeechobee Healthcare Facility. The existing basin consists of undeveloped land and spans from Station 500+34 to Station 511+20. The northern half of the basin discharges to the existing ditch to the north which conveys the runoff to the east through a culvert at US 441 and into Taylor Creek. The southern half of the basin discharges into an existing depression which overflows to the east into Taylor Creek. The pre development roadway is within Basins AIRNOFF2 and TCEAST from the regional ICPR model.

The basin for pre-development Pond 1A is located on a vacant parcel west of NW 3rd Avenue and north of NW 13th Street. Runoff from this area is conveyed to the existing ditch to the north which discharges east to Taylor Creek. (Pre Pond 1A is located within Basin SWDITC).

The basin for pre-development Pond 1B is located on a vacant parcel which is west of and adjacent to Taylor Creek. Runoff from this area discharges into Taylor Creek. (Pre Pond 1B is within Basin AIRNOFF2)

The basin for pre-development Pond 1C is located on a vacant parcel which is west of and adjacent to Taylor Creek. Runoff from this area discharges into Taylor Creek. (Pre Pond 1C is within Basin AIRNOFF2)

Basin 2

The Pre-development Basin 2 consists of rural, undeveloped land. From Station 511+20 to Station 571+00, the runoff is conveyed overland to the north filling depressional areas which overflow to the west eventually discharging to Taylor Creek (Tailwater A). From Station 571+00 to Station 602+00, the runoff flows overland to the southwest to depressional areas which fill up and overtop to each other or constructed ditches and flow south to SR 70 (Tailwater D). From Station 602+00 to Station 610+20, the runoff is generally conveyed to the southwest filling depressional areas which overflow and eventually discharge to SR 70 joining the previous basin and flowing to Tailwater D (west of existing SR 710). From there, the runoff is conveyed through existing ditches to the south eventually discharging to Taylor Creek. (The predevelopment basins are designated Basins A and D). There is a permitted discharge rate through the City of Okeechobee Commerce park which includes Basin B.

The basin for pre-development Pond 2A is located on undeveloped land north of and adjacent to the SR 710 R/W. Runoff from this area is conveyed overland to the north

filling depressional areas which overflow to the west eventually discharging to Taylor Creek. (Pre Pond 2A is located within Basin A).

The basin for pre-development Pond 2B is located on undeveloped land to the east of Taylor Creek and north of and adjacent to the SR 710 R/W. Runoff from this area is conveyed overland to the west to an existing wetland within the Okeechobee City Commerce Center. This wetland is connected with Commerce Center system which eventually outfalls to the west to Taylor Creek. (Pre Pond 2B is located within Basin A and B.)

The basin for pre-development Pond 2C is located on undeveloped land south of and adjacent to the SR 710 R/W. Runoff from this area is conveyed overland to the north filling depressional areas which overflow to the west eventually discharging to Taylor Creek. (Pre Pond 2C is located within Basin A).

Basin 3

The Pre-development Basin 3 consists of rural, undeveloped land. From Station 610+20 to Station 638+36.94, the runoff is conveyed to the southwest through a residential development eventually outfalling through an existing culvert at SR 70 (west of existing SR 710). From there, the runoff is conveyed through existing ditches to the south eventually discharging to Taylor Creek. (The pre-development basin is designated Basin D).

The basin for pre-development Pond 3A is located on undeveloped land east of and adjacent to the SR 710 R/W. As this location is within a low area, the runoff from this area stays within the depression. The depression will overflow to the south to the existing historic unnamed ditch, and is conveyed by culverts through existing SR 710 and E. Center Street. From there, the runoff is conveyed through existing ditches to the southwest eventually discharging to Taylor Creek. Pre Pond 3A is located within Basin D and discharges to Tailwater D.

The basin for pre-development Pond 3B is located on undeveloped land east of SR 710 R/W, adjacent to and west of L-63N Canal, and north of SR 70. Runoff from this area is conveyed to the historic unnamed ditch, and is conveyed by culverts through existing SR 710 and E. Center Street. From there, the runoff is conveyed through existing ditches to the southwest eventually discharging to Taylor Creek. Pre Pond 3B is located within Basin E and discharges to Tailwater E.

The basin for pre-development Pond 3C is located on undeveloped land east of and adjacent to SR 710 R/W. Runoff from this area is conveyed to the historic unnamed ditch, and is conveyed by culverts through existing SR 710 and E. Center Street. From there, the runoff is conveyed through existing ditches to the southwest eventually discharging to Taylor Creek. Pre Pond 3C is located within Basin E and discharges to Tailwater E.

Basin 4

The Pre-development Basin 4 consists of rural, undeveloped land. From Station 638+36.94 to Station 685+00, the runoff is conveyed to the southwest through a historic unnamed ditch, and is conveyed by culverts through existing SR 710 and E. Center Street. From there, the runoff is conveyed through existing ditches to the southwest eventually discharging to Taylor Creek. The pre-development basin is designated Basin E.

The basin for pre-development Pond 4A is located on undeveloped land north of and adjacent to SR 710 R/W, also bounded on the east by L-63N Canal. Runoff from this area is conveyed to the historic unnamed ditch, and is conveyed by culverts through existing SR 710 and E. Center Street. From there, the runoff is conveyed through existing ditches to the southwest at Tailwater E eventually discharging to Taylor Creek. Pre Pond 4A is located within Basin E.

The basin for pre-development Pond 4B/4C is located on undeveloped land southwest of and adjacent to proposed SR 710 R/W. These connected ponds are located in the area bounded by proposed SR 710, existing SR 710, and NE 34th Avenue. Runoff from this area is conveyed to the historic unnamed ditch, and is conveyed by culverts through existing SR 710 and E. Center Street. From there, the runoff is conveyed through existing ditches to the southwest eventually discharging to Taylor Creek. Pre Pond 4B/4C is located within Basin E.

The basin for pre-development Pond 4C is located on undeveloped land southwest of and adjacent to SR 710 R/W. Runoff from this area is conveyed to the historic unnamed ditch, and is conveyed by culverts through existing SR 710 and E. Center Street. From there, the runoff is conveyed through existing ditches to the southwest eventually discharging to Taylor Creek. Pre Pond 4C is located within Basin E.

The basin for pre-development Pond 4D is located on undeveloped land southwest of and adjacent to proposed SR 710 R/W. Runoff from this area fills the existing depression in Basin E10 and then oveflows to the west to Tailwater E. Pre Pond 4C is located within Basin E.

Basin 5

The Pre-development Basin 5 consists of rural, undeveloped land and existing SR 710 roadway. From Station 685+00 to Station 703+50, the runoff from the north side of the roadway is conveyed to the north, and the runoff from the south side of the roadway is conveyed to the south. From there, the runoff flows overland to the southeast toward Mosquito Creek. This is considered a simple basin and detailed modeling is not included.

The basin for pre-development Pond 5A is located on undeveloped land north of and adjacent to proposed SR 710 R/W. It is bounded by the entrance to the Okeechobee Agricultural Center on the west side. Runoff from this area flows overland to the

southeast to Mosquito Creek. Mosquito Creek drains into L-63N Canal which ultimately discharges into Lake Okeechobee.

The basin for pre-development Pond 5B is located on undeveloped land north of and adjacent to proposed SR 710 R/W. It is bounded by the L-63N Canal on the west side and the entrance to the Okeechobee Agricultural Center on the east side. Runoff from this area fills a depressional area in the vicinity of the pond, and then it is conveyed to through a culvert to the southeast to Mosquito Creek. Mosquito Creek drains into L-63N Canal which ultimately discharges into Lake Okeechobee.

The basin for pre-development Pond 5C is located on undeveloped land south of and adjacent to proposed SR 710 R/W. Runoff from this area flows overland to the southeast to Mosquito Creek. Mosquito Creek drains into L-63N Canal which ultimately discharges into Lake Okeechobee.

C. PROPOSED CONDITIONS

The proposed basin maps are included in Figures 11 and 13. The proposed drainage system will consist of curb and gutter inlets connected to the ponds with a systems of storm sewers and manholes. The majority of the roadway is being built in fill. Offsite drainage sheet flows to depressional areas where it will be bypassed through the roadway through piped cross drains along its original drainage path. The offsite areas are too low to be brought into the ponds.

In order to evaluate the cost associated with the pipe system, preliminary storm sewer tabulations were developed for Basins 1 through 4 using the preliminary profile and areas. These tabulations are included in **Appendix 8**. The results were used to develop a cost comparison between each pond site within a basin. The details of these calculations are included the construction cost estimates which are located in **Appendix 6**.

IV. ALTERNATIVE STORMWATER MANAGEMENT FACILITY LOCATIONS

A. Basis of Evaluation

An alternative comparison analysis was developed which consists of the location and description of each Stormwater Management Facility (SMF) location (see **Table 15** in Sub-section C of Section IV.) Each alternative was evaluated based on the following factors:

<u>Constructability</u>: Accommodation of the required pond area including the required setback limits, maintenance access, side slopes and pond bottom area.

<u>Maintainability</u>: Adequate area needed for regular cleaning, sediment removal, mowing and other required maintenance.

<u>Hazardous Materials</u>: Pertains to the presence of hazardous materials or petroleum contamination on or near the site location.

<u>Utilities</u>: Addresses impacts to existing and known future utilities at each alternative location.

<u>Environmental Impacts</u>: Pertains to impacts to floodplain and wetland areas, and to habitats for threatened, endangered or significant wildlife species.

<u>Cultural Resources</u>: Addresses impacts to prehistoric or historic archaeological or historic structures for each site.

<u>Economics</u>: Costs associated with right-of-way acquisition, residential/business relocation, contamination remediation, wetland mitigation and construction costs (see **Appendix 6** for associated costs).

B. ALTERNATIVE STORMWATER MANAGEMENT FACILITY (SMF) LOCATIONS

There will be five drainage basins for the proposed roadway. For the proposed condition, roadway runoff will flow through storm sewer system to stormwater treatment ponds. There are five discharge locations for the proposed pond alternatives locations lower Taylor Creek, the wetland East of Okeechobee Commerce Center, L-63N Canal, an unnamed historic ditch (crosses SR 70 & SR 710), and Mosquito Creek. The ultimate outfall for the project is Lake Okeechobee.

Sixteen pond alternative locations were evaluated as possible stormwater management facilities for the five open basins. All pond alternatives are proposed to be wet detention except for Pond alternates 1B, 1C, 5A, 5B, and 5C which are proposed to be dry retention with underdrains. The amount of proposed pavement contributing runoff to these potential ponds is estimated at 45.10 acres. See **Appendix 8** for treatment volume calculations. Pond site descriptions are as follows:

Basin 1

Basin 1 limits start at the beginning of the project at US 441 (Station 500+34) and extends to Station 511+20. The drainage area for this basin is 4.00 acres, and includes only the SR 710 right-of-way. It is an open basin discharging to Taylor Creek with an eventual outfall to Lake Okeechobee. The soils encountered in Basin 1 are Manatee loamy fine sand, depressional (#6) and Immokalee fine sand (#11). The proposed pond sites within the basin are identified as 1A, 1B, and 1C. The proposed profile was utilized to determine the allowable peak stages within the ponds.

Pond Site 1A is located on an empty parcel located west of US 441 (at begin project) and southwest of an existing FDOT pond. It is located at the northwest quadrant of the intersection of NW 13th Street and NW 3rd Avenue. Access to this site would be from US 441 and NW 13th Street Avenue. The pond outfall is the City Ditch north of the site which runs west to east and outfalls into Taylor Creek. The piped pond outfall will be 270 feet long and is estimated to be a 36" pipe at this time. This potential location consists primarily of grass, brush, and trees. As Pond 1A is within 10,000 feet of the airport, rubble riprap must be constructed around the pond perimeter as a wildlife deterrent.

The soil encountered at this site is Immokalee fine sand (Type B/D) which has an estimated SHGT at 0.5 feet to 1.5 feet below existing ground. The FDOT Geotechnical Department performed a boring at Pond 1A (to a depth of 15 feet) which determined that the site soil consists of gray and brown fine sand with some rock; and gray, tan, and brown fine sand. From Boring PB-1A, the observed water table elevation on October 16, 2013 was 2.5 feet below ground surface, and the seasonal high groundwater table (SHGT) was estimated to be 1.5 feet +/- 0.5 feet. From contours, the ground elevation at the boring is 26 feet NAVD. Therefore, the SHGT elevation was estimated to be 24 feet NAVD. There is an adjacent wet pond which serves US 441 (Pond 1) located diagonal and directly northeast of the proposed site. The normal water elevation in the adjacent pond is at elevation 22.7 feet NGVD (21.53 feet NAVD) from US 441 Plans. According to the FDOT Maintenance in Okeechobee, the adjacent US 441 pond site is not problematic. Therefore, the same normal water elevation (21.50 feet NAVD) was used for the analysis of Pond 1A.

Pond 1A is within the 100 year floodplain as determined from the Effective 2015 FEMA Maps. It has a rating of "None" for wetlands/surface water involvement and "Low" for protected species involvement. A wetland was identified on Pond Site 1A from the National Wetlands Inventory, however, no wetlands were observed during field inspection. The contamination screening designated Pond site 1A as having a risk ranking of "No" as the site is historically undeveloped and wooded. Pond Site 1A was assessed as having a "Low" potential for archaeological sites and historic resources. This potential site has no impacts to existing or known future utilities.

The pond site is estimated at 2.24 acres based on information from the Okeechobee County Property Appraiser. The piped pond outfall to the City Ditch will be within the

local road (NW 5th Avenue) and the City Ditch R/W. The FDOT Right-of-Way Department has provided estimates for proposed Pond 1A. The estimated right-of-way cost associated with this parcel is \$141,000, and the construction cost is estimated to be \$214,012 for a total cost of \$355,012. The construction cost is for comparison purposes only and includes savings due to import of fill to roadway (\$30,843); the drainage trunkline cost (\$150,826); and other miscellaneous costs including sodding, clearing and grubbing, rubble riprap (ditch lining) and sediment barrier (\$94,029).

Pond Site 1B is located adjacent to and south of SR 710 R/W at Station 509+00 and west of Taylor Creek. Access to this site would be from SR 710. The pond outfall into Taylor Creek is estimated to be a 140-foot long, 18" pipe at this time. This potential location consists primarily of grass, brush, and trees.

The soil encountered at this site is Manatee loamy fine sand (Type B/D), depressional which has an estimated SHGT at existing ground level. The FDOT Geotechnical Department performed a boring at Pond 1B (to a depth of 20 feet) which determined that the site soil consists of gray and brown fine sand with some rock; and dark brown fine sand with organics. From Boring PB-1B, the observed water table elevation on October 16, 2013 was 2.5 feet below ground surface, and the seasonal high groundwater table (SHGT) was estimated to be 0.75 feet +/- 0.5 feet. From contours, the ground elevation at the boring is 18 feet NAVD. Therefore, the SHGT elevation was estimated to be 16.75 feet NAVD.

Pond 1B is <u>not</u> within the 100 year floodplain as determined from the Effective 2015 FEMA Maps. It has a rating of "Medium" for wetlands/surface water involvement as the property impacts an estimated 0.5 acre of wetlands and "Low" for protected species involvement. The contamination screening designated Pond site 1B as having a risk ranking of "Low" as the site was noted to have unidentified modifications to the property in historical aerials. Pond Site 1B was assessed as having a "Low" potential for archaeological sites and historic resources. This potential site has no impacts to existing or known future utilities.

The pond site is estimated at 1.08 acres based on R/W parcel size and surveyed property lines. The piped pond outfall to Taylor Creek will be within SR 710 R/W. The FDOT Right-of-Way Department has provided estimates for proposed Pond 1B. The estimated right-of-way cost associated with this parcel is \$146,000, and the construction cost is estimated to be \$144,073 for a total cost of \$320,073. The construction cost is for comparison purposes only and includes embankment cost (\$19,230); the drainage trunkline cost (\$56,704); underdrain (\$49,280); and other miscellaneous costs including sodding, clearing and grubbing, and sediment barrier (\$18,859). Other costs include wetland mitigation (\$30,000).

As Pond Site 1B was determined to be the preferred site for Basin 1, further analysis was performed for this site. To summarize, the results indicated that this site will impact 0.47 acre of wetlands; the risk rank for contamination is "No" with arsenic contamination "Not Indicated" in the tested locations; and there are no archaeological or historic resources within the APE of this site.

Pond Site 1C is located south of SR 710 R/W at Station 509+00 and just west of Taylor Creek. Access to this site would be from SR 710 and access roadway. The pond outfall into Taylor Creek is estimated to be a 215-foot long, 18" pipe at this time. This potential location consists primarily of grass, brush, and trees.

The soil encountered at this site is Manatee loamy fine sand (Type B/D), depressional which has an estimated SHWT at existing ground level. The FDOT Geotechnical Department performed a boring at Pond 1C (to a depth of 20 feet) which determined that the site soil consists of gray and orange sandy clay; gray and brown fine sand with some rock; and dark brown organic clay. From Boring PB-1C, the observed water table elevation on October 16, 2013 was 1.0 foot below ground surface, and the seasonal high groundwater table (SHGT) was estimated to be 0.00 feet +/- 0.5 feet. From contours, the ground elevation at the boring is 15 feet NAVD. Therefore, the SHGT elevation was estimated to be 14.50 feet NAVD.

Pond 1C is within the 100 year floodplain as determined from the Effective 2015 FEMA Maps. It has a rating of "High" for wetlands/surface water involvement and "Low" for protected species involvement. The contamination screening designated this site as having a risk ranking of "No". Pond Site 1C was assessed as having a "Low" potential for archaeological sites and historic resources. This potential site has <u>no</u> impacts to existing or known future utilities.

The pond site is estimated at 0.93 acres based on R/W parcel size. As the pond is not adjacent to the SR 710 R/W, an outfall easement (0.22 ac) from the pond site to Taylor Creek will be necessary. The FDOT Right-of-Way Department has provided estimates for proposed Pond 1C. The estimated right-of-way costs and construction costs associated with this parcel are \$105,000 and \$166,864, respectively. Other costs include wetland mitigation (\$52,800). The total of the costs associated with this parcel are \$324,664. The construction cost is for comparison purposes only and includes embankment (\$42,954); underdrains (\$19,200); the drainage trunkline cost (\$86,844); and other miscellaneous costs including sodding, clearing and grubbing, and sediment barrier (\$17,866).

Basin 2

The limit of Basin 2 consists of the SR 710 roadway right-of-way from Station 511+20 to Station 610+20. Basin 2 is an open basin that has two potential outfalls depending on the chosen pond site, Taylor Creek or the wetland area located south of SR 710 R/W and east of the Okeechobee Commerce Center. The eventual outfall for both is Lake Okeechobee. The soils encountered in Basin 2 are Basinger fine sand (#2); Basinger and Placid soils, depressional (#3), Manatee loamy fine sand, depressional (#6), Floridana, Riviera, and Placid soils, depressional (#7), Pindea fine sand (#8), Riviera fine sand (#9), Immokalee fine sand (#11), and Parkwood fine sand (#18).

Pond Site 2A is located adjacent to and north of SR 710 R/W at Station 554+50 and to the east of Taylor Creek. Access to this site would be from SR 710. The pond outfall

into the existing wetland is estimated to be a 300-foot long, 18" pipe. This potential location consists primarily of grass with some trees.

The soil type encountered at this site is Immokalee fine sand (Type B/D) which has an estimated depth to the SHWT at 0.5 feet to 1.5 feet below existing ground. The FDOT Geotechnical Department performed a boring at Pond 1C (to a depth of 20 feet) which determined that the site soil consists of gray and brown fine sand with some rock. From Boring PB-1C, the observed water table elevation on October 22, 2013 was 2.0 feet below ground surface, and the seasonal high groundwater table (SHGT) was estimated to be 0.67 feet +/- 0.5 feet. From contours, the ground elevation at the boring is 22.2 feet NAVD. Therefore, the SHGT elevation was estimated to be 21.03 feet NAVD.

Pond 2A is <u>not</u> within the 100 year floodplain as determined from the Effective 2015 FEMA Maps. It has a rating of "None" for wetlands/surface water involvement and "Low" for protected species involvement. The contamination screening designated this site as having a risk ranking of "No". Pond Site 2A was assessed as having a "Moderate" potential for archaeological sites and historic resources. This potential site has no impacts to existing or known future utilities.

Three potential stormwater management facility options were analyzed for Pond 2A. This was done to determine if raising the roadway and thereby reducing the required pond area would be more cost effective than acquiring a large stormwater management facility. The additional storage volume afforded by raising the roadway reduces the pond size. The FDOT Right-of-Way Department has provided estimates for each proposed pond option and for raising the roadway by one foot intervals. The information for raising the roadway was modified for use per basin. Each option will utilize a piped outfall to the wetland east of the Commerce Center and will be within SR 710 R/W. See **Appendix 6** for right-of-way cost estimate information and calculations.

Pond 2A - Option 1 area is estimated at 9.43 acres based on measurement. This is the required pond area for the currently proposed roadway profile. The estimated right-of-way cost and construction cost associated with this parcel are \$265,000 and \$1,072,314, respectively. The total costs associated with this option are \$1,337,314. The construction cost is for comparison purposes only and includes savings due to import of fill to roadway (\$54,610); the drainage trunkline cost (\$1,022,729); and other miscellaneous costs including sodding, clearing and grubbing, and sediment barrier (\$104,195).

As Pond Site 2A - Option 1 was determined to be the preferred site for Basin 2, further analysis was performed for this site. To summarize, the results indicated that this site will not impact wetlands; the risk rank for contamination is "No" with arsenic contamination "Not Indicated" in the tested locations; and there are no archaeological or historic resources within the APE of this site.

Pond 2A - Option 2 area is estimated at 7.20 acres based on measurement. This is the required pond area determined by analysis of raising the roadway profile one foot for

the western portion (approx. 5000 feet) of Basin 2. The cost associated with raising the roadway one foot within this area is estimated at \$317,812. The estimated right-of-way cost and construction cost associated with this parcel are \$212,000 and \$1,114,607. The total of the costs associated with this option are \$1,644,419. The construction cost is for comparison purposes only and includes the cost due to import of fill to roadway (\$6,293); the drainage trunkline cost (\$1,022,729); and other miscellaneous costs including sodding, clearing and grubbing, and sediment barrier (\$85,585).

Pond 2A - Option 3 area is estimated at 6.42 acres based on measurement. This is the required pond area determined by analysis of raising the roadway profile two feet for the western portion (approx. 5000 feet) of Basin 2. The cost associated with raising the roadway two feet within this area is estimated at \$635,625. The estimated right-of-way costs and construction costs associated with this parcel are \$193,000 and \$1,148,255. The total of the costs associated with this option are \$1,976,879. The construction cost is for comparison purposes only and includes the cost due to import of fill to roadway (\$44,449); the drainage trunkline cost (\$1,022,729); and other miscellaneous costs including sodding, clearing and grubbing, and sediment barrier (\$81,076).

Pond Site 2B is located adjacent to and south of SR 710 at Station 554+00 and to the east of Taylor Creek. Access to this site would be from SR 710. The pond outfall into the wetland is estimated to be a 200-foot long, 18" pipe at this time. This potential location consists primarily of grass with some trees.

The soil type encountered at this site is Immokalee fine sand (Type B/D) which has a estimated depth to the SHWT at 0.5 feet to 1.5 feet below existing ground. The FDOT Geotechnical Department performed a boring at Pond 2B (to a depth of 20 feet) which determined that the site soil consists of gray and brown fine sand with some rock. From Boring PB-2B, the observed water table elevation on October 23, 2013 was 3.0 feet below ground surface, and the seasonal high groundwater table (SHGT) was estimated to be 0.75 feet +/- 0.5 feet. From contours, the ground elevation at the boring is 23.2 feet NAVD. Therefore, the SHGT elevation was estimated to be 21.95 feet NAVD.

Pond 2B is <u>not</u> within the 100 year floodplain as determined from the Effective 2015 FEMA Maps. It has a rating of "None" for wetlands/surface water involvement and "Low" for protected species involvement. The contamination screening designated this site as having a risk ranking of "No". Pond Site 2A was assessed as having a "Moderate" potential for archaeological sites and historic resources. This potential site has no impacts to existing or known future utilities.

Three potential stormwater management facility options were analyzed for Pond 2B. This was done to determine if raising the roadway and thereby reducing the required pond area would be more cost effective than acquiring a large stormwater management facility. The additional storage volume afforded by raising the roadway reduces the pond size. The FDOT Right-of-Way Department has provided estimates for each proposed pond option and for raising the roadway by one foot intervals. The

information for raising the roadway was modified for use per basin. Each option will utilize a piped outfall to the wetland east of the Commerce Center and will be within SR 710 R/W. See Appendix 6 for right-of-way cost estimate information and calculations.

Pond 2B - Option 1 area is estimated at 15.37 acres based on measurement. This is the required pond area for the currently proposed roadway profile. The estimated right-of-way cost and construction cost associated with this parcel are \$405,000 and \$925,064. The total costs associated with this option are \$1,330,064. The construction cost is for comparison purposes only and includes savings due to import of fill to roadway (\$241,563); the drainage trunkline cost (\$1,016,479); and other miscellaneous costs including sodding, clearing and grubbing, and sediment barrier (\$150,147).

Pond 2B - Option 2 area is estimated at 10.00 acres based on measurement. This is the required pond area determined by analysis of raising the roadway profile one foot for the western portion (approx. 5000 feet) of Basin 2. The cost associated with raising the roadway one foot within this area is estimated at \$317,812. The estimated right-of-way cost and construction cost associated with this parcel are \$278,000 and \$1,005,232. The total of the costs associated with this option are \$1,601,045. The construction cost is for comparison purposes only and includes savings due to import of fill to roadway (\$115,526); the drainage trunkline cost (\$1,016,479); and other miscellaneous costs including sodding, clearing and grubbing, and sediment barrier (\$104,280).

Pond 2B - Option 3 area is estimated at 7.08 acres based on measurement. This is the required pond area determined by analysis of raising the roadway profile two feet for the western portion (approx. 5000 feet) of Basin 2. The cost associated with raising the roadway two feet within this area is estimated at \$635,625. The estimated right-of-way costs and construction costs associated with this parcel are \$209,000 and \$1,053,637. The total of the costs associated with this option are \$1,898,262. The construction cost is for comparison purposes only and includes savings due to import of fill to roadway (\$42,854); the drainage trunkline cost (\$1,016,479); and other miscellaneous costs including sodding, clearing and grubbing, and sediment barrier (\$80,012).

Pond Site 2C is located adjacent to and north of SR 710 at Station 522+50 and to the east of Taylor Creek. Access to this site would be from SR 710. The pond outfall into Taylor Creek is estimated to be an 800-foot long, 18" pipe at this time. This potential location consists primarily of grass, brush and trees. As Pond 2C is within 10,000 feet of the airport, rubble riprap must be constructed around the pond perimeter as a wildlife deterrent.

The soil types encountered at this site are Basinger fine sand (Type A/D) and Pindea fine sand (Type C/D) which both have an estimated depth to the SHWT from 0 feet to 1.0 feet below existing ground. The FDOT Geotechnical Department performed a boring at Pond 2C (to a depth of 20 feet) which determined that the site soil consists of gray and brown fine sand with some rock. From Boring PB-2C, the observed water

table elevation on October 23, 2013 was 3.5 feet below ground surface, and the seasonal high groundwater table (SHGT) was estimated to be 0.67 feet +/- 0.5 feet. From contours, the ground elevation at the boring is 19.5 feet NAVD. Therefore, the SHGT elevation was estimated to be 18.33 feet NAVD.

Pond 2C is <u>not</u> within the 100 year floodplain as determined from the Effective 2015 FEMA Maps. It has a rating of "Low" for wetlands/surface water involvement and "Low" for protected species involvement. The contamination screening designated this site as having a risk ranking of "No". Pond Site 2C was assessed as having a "Low" potential for archaeological sites and historic resources. This potential site has <u>no impacts</u> to existing or known future utilities.

Two potential stormwater management facility options were analyzed for Pond 2C. This was done to determine if raising the roadway and thereby reducing the required pond area would be more cost effective than acquiring a large stormwater management facility. The additional storage volume afforded by raising the roadway reduces the pond size. The FDOT Right-of-Way Department has provided estimates for each proposed pond option and for raising the roadway by one foot intervals. The information for raising the roadway was modified for use per basin. Each option will utilize a piped outfall to Taylor Creek and will be within SR 710 R/W. See Appendix 6 for right-of-way cost estimate information and calculations.

Pond 2C - Option 1 area is estimated at 6.86 acres based on measurement. This is the required pond area for the currently proposed roadway profile. The estimated right-of-way cost and construction cost associated with this parcel are \$297,000 and \$1,042,526. The total costs associated with this option are \$1,339,526. The construction cost is for comparison purposes only and includes the cost due to import of fill to roadway (\$18,529); the drainage trunkline cost (\$828,989); and other miscellaneous costs including sodding, clearing and grubbing, rubble riprap and sediment barrier (\$195,008).

Pond 2C - Option 2 area is estimated at 6.14 acres based on measurement. This is the required pond area determined by analysis of raising the roadway profile one foot for the western portion (approx. 5000 feet) of Basin 2. The cost associated with raising the roadway one foot within this area is estimated at \$317,812. The estimated right-of-way cost and construction cost associated with this parcel are \$280,000 and \$1,067,257. The total of the costs associated with this option are \$1,665,070. The construction cost is for comparison purposes only and includes the cost due to import of fill to roadway (\$59,770); the drainage trunkline cost (\$828,989); and other miscellaneous costs including sodding, clearing and grubbing, rubble riprap and sediment barrier (\$178,498).

Basin 3

The limit of Basin 3 consists of the SR 710 roadway right-of-way from Station 610+20 to Station 638+46.43. Basin 3 is an open basin that has two potential outfalls, L-63N Canal or the unnamed historic ditch that crosses SR 70 and proposed SR 710. The eventual outfall for both is Lake Okeechobee. The soils encountered in Basin 3 are

Basinger fine sand (#2); Basinger and Placid soils, depressional (#3), and Immokalee fine sand (#11).

Pond Site 3A is located east of SR 710 (in vicinity of Sta. 636+00) and north of SR 70 R/W. As this site is not adjacent to SR 710, access to this site would be from SR 70. The pond outfall into L-63N Canal is estimated to be a 140-foot long, 18" pipe at this time. This potential location consists primarily of grass with minimal trees.

The soil type encountered at this site is Immokalee fine sand (Type B/D) which has an estimated depth to the SHWT from 0.5 feet to 1.5 feet below existing ground. The FDOT Geotechnical Department performed a boring at Pond 3A (to a depth of 20 feet) which determined that the site soil consists of gray and brown fine sand with some rock; and gray, tan, and brown fine sand. From Boring PB-3A, the observed water table elevation on October 16, 2013 was 3.5 feet below ground surface, and the seasonal high groundwater table (SHGT) was estimated to be 1.92 feet +/- 0.5 feet. From contours, the ground elevation at the boring is 31.0 feet NAVD. Therefore, the SHGT elevation was estimated to be 28.58 feet NAVD. As this site is located adjacent to the L-63N Canal and a wetland, a SHGT of 24.73 feet NAVD was used, and it was assumed that a clay liner would be utilized in the design.

This site is <u>not</u> within the 100 year floodplain as determined from the Effective 2015 FEMA Maps. It has a rating of "None" for wetlands/surface water involvement and "Low" for protected species involvement. The contamination screening designated this site as having a risk ranking of "Medium". As a result of this ranking, this site was preliminarily assessed a cost of \$125,000 for cleanup of livestock holding pens, however, further investigation is required. Pond Site 3A was assessed as having a "Low" potential for archaeological sites and historic resources. Pond 3A conflicts with both FPL Distribution and Transmission pole lines. This will require additional coordination and a possible relocation to the north of the lines.

The pond site is estimated at 3.47 acres based on measurement. The piped pond outfall to the L-63N Canal will be within SR 70 R/W. The FDOT Right-of-Way Department has provided estimates for proposed Pond 3A. The estimated right-of-way costs and construction costs associated with this parcel are \$471,000 and \$430,448. The total costs associated with this parcel are \$901,448. The construction cost is for comparison purposes only and includes savings due to import of fill to roadway (\$49,061); the drainage trunkline cost (\$337,704); clay liner (\$98,851); and other miscellaneous costs including sodding, clearing and grubbing, and sediment barrier (\$42,954).

Pond Site 3B is located adjacent to and east of SR 710 R/W at Station 629+00. Access to this site would be from SR 710. The pond outfall into the unnamed historic ditch is estimated to be a 1211-foot long, 18" pipe at this time. This potential location consists primarily of grass, brush and trees.

The soil type encountered at this site is Immokalee fine sand (Type B/D) which has an estimated depth to the SHWT from 0.5 feet to 1.5 feet below existing ground. The FDOT Geotechnical Department performed a boring at Pond 3B (to a depth of 20 feet)

which determined that the site soil consists of gray and brown fine sand with some rock; gray, tan, and brown fine sand; and light gray clayey sand with rock. From Boring PB-3B, the observed water table elevation on October 16, 2013 was 0.2 feet above the ground surface, and the seasonal high groundwater table (SHGT) was estimated to be 0.50 feet +/- 0.5 feet. From contours, the ground elevation at the boring is 26.4 feet NAVD. Therefore, the SHGT elevation was estimated to be 25.4 feet NAVD.

This site is <u>not</u> within the 100 year floodplain as determined from the Effective 2015 FEMA Maps. It has a rating of "Low" for wetlands/surface water involvement and "Low" for protected species involvement. The contamination screening designated this site as having a risk ranking of "No". Pond Site 3B was assessed as having a "Low" potential for archaeological sites and historic resources. This potential site has <u>no impacts</u> to existing or known future utilities.

The pond site is estimated at 2.44 acres based on measurement. The piped pond outfall (0.03 ac.) to the historic ditch will be within SR 710 and SR 70 R/W. The FDOT Right-of-Way Department has provided estimates for proposed Pond 3B. The estimated right-of-way costs and construction costs associated with this parcel are \$383,000 and \$300,565. Other costs associated with this parcel are mitigation costs (\$18,000). The total costs associated with this parcel are \$701,565. The construction cost is for comparison purposes only and includes savings due to import of fill to roadway (\$1,967); the drainage trunkline cost (\$269,624); and other miscellaneous costs including sodding, clearing and grubbing, and sediment barrier (\$32,908).

As Pond Site 3B was determined to be the preferred site for Basin 3, further analysis was performed for this site. To summarize, the results indicated that this site will impact 0.35 acre of wetlands; the risk rank for contamination is "No" with arsenic contamination "Not Indicated" in the tested locations; and there are no archaeological or historic resources within the APE of this site.

Pond Site 3C is located adjacent to and east of SR 710 R/W at Station 643+50. Access to this site would be from SR 710. The pond outfall into the unnamed ditch is estimated to be an 85-foot long, 18" pipe at this time. This potential location consists primarily of grass, brush and trees. The northern portion of the parcel is currently being used as a wet detention pond for SR 70. As the SR 70 widening project is currently under design, this pond will be modified to accommodate the additional runoff from the improvements. The proposed SR 70 stormwater calculations were reviewed and used for design of a larger wet detention pond which will accommodate runoff from both SR 70 and SR 710.

The soil encountered at this site is Immokalee fine sand (Type B/D) which has an estimated depth to the SHWT from 0.5 feet to 1.5 feet below existing ground. The FDOT Geotechnical Department performed a boring at Pond 3C (to a depth of 20 feet) which determined that the site soil consists of gray and brown fine sand with some rock. From Boring PB-3C, the observed water table elevation on October 22, 2013 was 3.0 feet below the ground surface, and the seasonal high groundwater table

(SHGT) was estimated to be 1.25 feet +/- 0.5 feet. From contours, the ground elevation at the boring is 24.2 feet NAVD. Therefore, the SHGT elevation was estimated to be 22.95 feet NAVD.

This site is <u>not</u> within the 100 year floodplain as determined from the Effective 2015 FEMA Maps. It has a rating of "None" for wetlands/surface water involvement and "Low" for protected species involvement. The contamination screening designated this site as having a risk ranking of "Low". Pond Site 3C was assessed as having a "Low" potential for archaeological sites and historic resources. This potential site has no impacts to existing or known future utilities.

The pond site is estimated at 3.81 acres based on measurement. The piped pond outfall to the historic ditch will require a minimal outfall easement. The FDOT Right-of-Way Department has provided estimates for proposed Pond 3C. The estimated right-of-way costs and construction costs associated with this parcel are \$365,000 and \$408,483. The total costs associated with this parcel are \$773,483. The construction cost is for comparison purposes only and includes savings due to import of fill to roadway (\$4,543); the drainage trunkline cost (\$378,759); and other miscellaneous costs including sodding, clearing and grubbing, and sediment barrier (\$34,267).

Basin 4

The limit of Basin 4 consists of SR 710 roadway from Station 638+36.94 to Station 685+00. Basin 4 consists of right-of-way and additional pavement used for connection of existing SR 710 to the new alignment of SR 710. Basin 4 is an open basin that has two potential outfalls, L-63N Canal or the unnamed ditch that crosses SR 70. The eventual outfall for both is Lake Okeechobee. The soils encountered in Basin 4 are Basinger fine sand (#2) and Immokalee fine sand (#11).

Pond Site 4A is located adjacent to and east of SR 710 at Station 680+50. Access to this site would be from SR 710. The pond outfall into the L-63N Canal is estimated to be a 150-foot long, 18" pipe at this time. This potential location consists primarily of grass, brush and trees.

The soil type encountered at this site is Immokalee fine sand (Type B/D) which has an estimated depth to the SHWT from 0.5 feet to 1.5 feet below existing ground. The FDOT Geotechnical Department performed two borings at Pond 4A (to a depth of 20 feet) which determined that the site soil consists of gray and brown fine sand with some rock. From the two Borings, both designated PB-4A, the observed water table elevation on October 23, 2013 was 3.0 feet and 4.5 feet below the ground surface, respectively. The seasonal high groundwater table (SHGT) was estimated to be 1.08 feet +/- 0.5 feet for both borings. From contours, the ground elevation at the borings is 25 feet NAVD and 26 feet NAVD, respectively. Therefore, the SHGT elevation was estimated to be 23.42 feet NAVD and 24.42 feet, respectively. For the pond site preliminary analysis, a SHGT elevation of 24.0 feet NAVD was used.

Pond 4A is <u>not</u> within the 100 year floodplain as determined from the Effective 2015 FEMA Maps. It has a rating of "None" for wetlands/surface water involvement and "Medium" for protected species involvement. The contamination screening designated this site as having a risk ranking of "Low". Pond Site 4A was assessed as having a "Low" potential for archaeological sites and historic resources. This potential site has <u>no impacts</u> to existing or known future utilities.

Two potential stormwater management facility options were analyzed for Pond 4A. This was done to determine if raising the roadway and thereby reducing the required pond area would be more cost effective than acquiring a large stormwater management facility. The additional storage volume afforded by raising the roadway reduces the pond size. The FDOT Right-of-Way Department has provided estimates for each proposed pond option and for raising the roadway by one foot intervals. The information for raising the roadway was modified for use per basin. Each option will utilize a piped outfall to the L-63N Canal and will be within the canal right-of-way. See Appendix 6 for right-of-way cost estimate information and calculations.

Pond 4A - Option 1 area is estimated at 3.98 acres based on measurement. This is the required pond area for the currently proposed roadway profile. The estimated right-of-way cost and construction cost associated with this parcel are \$435,000 and \$635,121. Other costs associated with this parcel include protected species mitigation (\$18,000). The total costs associated with this option are \$1,088,121. The construction cost is for comparison purposes only and includes the cost due to import of fill to roadway (\$27,006); the drainage trunkline cost (\$555,219); and other miscellaneous costs including sodding, clearing and grubbing, and sediment barrier (\$52,898).

Pond 4A - Option 2 area is estimated at 3.34 acres based on measurement. This is the required pond area determined by analysis of raising the roadway profile one foot within Basin 4. The cost associated with raising the roadway one foot within this area is estimated at \$296,392. The estimated right-of-way cost and construction cost associated with this parcel are \$391,000 and \$637,566. Other costs associated with this parcel include protected species mitigation (\$18,000). The total of the costs associated with this option are \$1,342,958. The construction cost is for comparison purposes only and includes the cost due to import of fill to roadway (\$35,863); the drainage trunkline cost (\$555,219); and other miscellaneous costs including sodding, clearing and grubbing, and sediment barrier (\$46,485).

Pond Site 4B is located adjacent to and west of SR 710 at Station 656+00. Access to this site would be from SR 710 or connector roads. This pond has been analyzed as a combined site with Pond Site 4C as they are both small remainder parcels between SR 710, SR 70, and connector roads as well as a single pond site. The pond outfall into the unnamed historic ditch is estimated to be a 135-foot long, 18" pipe at this time. This potential location consists primarily of grass, brush and trees.

The soil encountered at 4B is Immokalee (Type B/D) and Basinger fine sands (Type A/D) which have an estimated depth to the SHWT from 0.5 feet to 1.5 feet and 0 to 1.0 feet, respectively, below existing ground. The FDOT Geotechnical Department

performed a boring at Pond 4B (to a depth of 20 feet) which determined that the site soil consists of gray and brown fine sand with some rock. From Boring PB-4B, the observed water table elevation on November 2, 2016 was 2.0 feet below the ground surface, and the seasonal high groundwater table (SHGT) was estimated to be 2.00 feet +/- 0.5 feet. The FDOT Geotechnical Department determined that the ground elevation at the boring location was 23.04 feet NAVD. Therefore, the SHGT elevation is estimated to be 20.54 feet NAVD.

Pond 4B is <u>not</u> within the 100 year floodplain as determined from the Effective 2015 FEMA Maps. It has a rating of "Low" for wetlands/surface water involvement and "Low" for protected species involvement. The contamination screening designated this site as having a risk ranking of "No". Pond Site 4B was assessed as having a "Moderate" potential for archaeological sites and historic resources. This potential site has no impacts to existing or known future utilities.

The pond site is estimated at 4.20 acres based on measurement. The piped pond outfall to the historic ditch will be within local road R/W. The cost estimate for Pond 4B is located below Pond Site 4C information.

Pond Site 4C is located adjacent to and west of SR 710 at Station 663+00. Access to this site would be from SR 710 or connector roads. This pond has been analyzed as a combined site with Pond Site 4B as they are both small remainder parcels between SR 710, SR 70, and connector roads. The pond outfall into the unnamed historic ditch is estimated to be a 135-foot long, 18" pipe at this time. This potential location consists primarily of grass, brush and trees with several buildings.

The soil encountered at 4C is Immokalee fine sand (Type B/D) which has an estimated depth to the SHWT from 0.5 feet to 1.5 feet below existing ground. The FDOT Geotechnical Department performed a boring at Pond 4B/4C (to a depth of 20 feet) which determined that the site soil consists of gray and brown fine sand with some rock. From Boring PB-4BC, the observed water table elevation on October 22, 2013 was 2.5 feet below the ground surface, and the seasonal high groundwater table (SHGT) was estimated to be 1.25 feet +/- 0.5 feet. From contours, the ground elevation at the boring is 24.0 feet NAVD. Therefore, the SHGT elevation was estimated to be 22.25 feet NAVD.

This site is <u>not</u> within the 100 year floodplain as determined from the Effective 2015 FEMA Maps. It has a rating of "None" for wetlands/surface water involvement and "Low" for protected species involvement. The contamination screening designated this site as having a risk ranking of "Medium". As a result of this ranking, this site was preliminarily assessed a cost of \$125,000 for cleanup of livestock holding pens, however, further investigation is required. Pond Site 4C was assessed as having a "Moderate" potential for archaeological sites and historic resources. Pond 4C has existing FPL Distribution facilities (aerial pole line) and Centurylink facilities (BT/BFO) along the southern side of Pond 4C. These utilities are not expected to be impacted.

Two potential stormwater management facility options were analyzed for the Pond 4B/4C combination. This was done to determine if raising the roadway and thereby

reducing the required pond area would be more cost effective than acquiring a large stormwater management facility. The additional storage volume afforded by raising the roadway reduces the pond size. The FDOT Right-of-Way Department has provided estimates for each proposed pond option and for raising the roadway by one foot intervals. The information for raising the roadway was modified for use per basin. Each option will utilize a piped outfall to the to the historic ditch and will be within local road R/W. See Appendix 6 for right-of-way cost estimate information and calculations.

Pond 4B/4C - Option 1 area is estimated at 7.17 acres (Pond 4B (4.20 ac.)/Pond 4C (2.97 ac.) based on measurement. This is the required pond area for the currently proposed roadway profile. The estimated right-of-way cost and construction cost associated with this parcel are \$658,000 and \$559,843. Other costs associated with this parcel (Pond 4B) include wetland mitigation (\$6,000). The total costs associated with this option are \$1,223,843. The construction cost is for comparison purposes only and includes the cost due to import of fill to roadway (\$17,090); the drainage trunkline cost (\$442,625); and other miscellaneous costs including sodding, clearing and grubbing, and sediment barrier (\$100,128).

Pond 4B - Option 2 area is estimated at 4.20 acres based on measurement. This options works without raising the road. The estimated right-of-way cost and construction cost associated with this parcel are \$403,000 and \$501,222. Other costs associated with this parcel (Pond 4B) include wetland mitigation (\$6,000). The total of the costs associated with this option are \$904,222. The construction cost is for comparison purposes only and includes the cost due to import of fill to roadway (\$2,081); the drainage trunkline cost (\$442,625); and other miscellaneous costs including sodding, clearing and grubbing, and sediment barrier (\$56,516).

As Pond Site 4B - Option 2 was determined to be the preferred site for Basin 4, further analysis was performed for this site. To summarize, the results indicated that this site will not impact wetlands; the risk rank for contamination is "No" with arsenic contamination "Not Indicated" in the tested locations; and there are no archaeological or historic resources within the APE of this site.

Pond Site 4D is located adjacent to and southwest of SR 710 at Station 672+00. Access to this site would be from SR 710. The pond outfall into the historic ditch to the west is estimated to be an 860-foot long, 18" pipe at this time. This potential location consists primarily of grass, brush and trees.

The soil encountered at this site is Immokalee fine sand (Type B/D) which has an estimated depth to the SHWT from 0.5 feet to 1.5 feet below existing ground. The FDOT Geotechnical Department performed a boring at Pond 4D (to a depth of 20 feet) which determined that the site soil consists of gray and brown fine sand with some rock. From Boring PB-4D, the observed water table elevation on October 22, 2013 was 3.0 feet below the ground surface, and the seasonal high groundwater table (SHGT) was estimated to be 1.17 feet +/- 0.5 feet. From contours, the ground elevation at the boring is 25.5 feet NAVD. Therefore, the SHGT elevation was estimated to be 23.83 feet NAVD.

This site is <u>not</u> within the 100 year floodplain as determined from the Effective 2015 FEMA Maps. It has a rating of "None" for wetlands/surface water involvement and "Medium" for protected species involvement. The contamination screening designated this site as having a risk ranking of "Medium". This site was preliminarily assigned a ranking of "Medium" for contamination due to proximity to a retail fuel site, but a ranking of "Low" was considered after further investigation uncovered cleanup of the adjacent site. However, as this station is active and in close proximity to the project, the District Contamination Impact Coordinator (DCIC) has requested that the ranking remain "Medium". Pond Site 4D was assessed as having a "Low" potential for archaeological sites and historic resources. This potential site has <u>no</u> impacts to existing or known future utilities.

Two potential stormwater management facility options were analyzed for Pond 4D. This was done to determine if raising the roadway and thereby reducing the required pond area would be more cost effective than acquiring a large stormwater management facility. The additional storage volume afforded by raising the roadway reduces the pond size. The FDOT Right-of-Way Department has provided estimates for each proposed pond option and for raising the roadway by one foot intervals. The information for raising the roadway was modified for use per basin. Each option will utilize a piped outfall to the historic ditch and will be within the road right-of-way. See Appendix 6 for right-of-way cost estimate information and calculations.

Pond 4D - Option 1 area is estimated at 6.08 acres based on measurement of GIS parcel lines. This is the required pond area for the currently proposed roadway profile. The estimated right-of-way cost and construction cost associated with this parcel are \$491,000 and \$565,066. Other costs associated with this parcel include protected species mitigation (\$15,000). The total costs associated with this option are \$1,071,066. The construction cost is for comparison purposes only and includes savings due to import of fill to roadway (\$15,380); the drainage trunkline cost (\$506,593); and other miscellaneous costs including sodding, clearing and grubbing, and sediment barrier (\$73,853).

Pond 4D - Option 2 area is estimated at 4.33 acres based on measurement. This is the required pond area determined by analysis of raising the roadway profile one foot within Basin 4. The cost associated with raising the roadway one foot within this area is estimated at \$296,392. The estimated right-of-way cost and construction cost associated with this parcel are \$373,000 and \$594,761. Other costs associated with this parcel include protected species mitigation (\$15,000). The total of the costs associated with this option are \$1,279,153. The construction cost is for comparison purposes only and includes the cost due to import of fill to roadway (\$20,519); the drainage trunkline cost (\$506,593); and other miscellaneous costs including sodding, clearing and grubbing, and sediment barrier (\$67,650).

Basin 5

The limit of Basin 5 consists of the SR 710 roadway right-of-way from Station 685+00 to Station 703+40. Basin 5 is an open basin that has two potential outfalls, L-63N

Canal or Mosquito Creek. The eventual outfall for both is Lake Okeechobee. The soils encountered in Basin 5 are Immokalee fine sand (#11); and Floridana, Placid, and Okeelanta soils, frequently flooded (#19). The roadway within the basin currently being constructed as a transition section but is assumed to be the full typical section within the basin limits to accommodate the future widening to the east.

If Basin 5 discharges to Mosquito Creek, then nutrient removal will be required so underdrains are included in the pond cost estimates. Should the ponds be able to discharge to the L63-N canal without needing nutrient removal then dry detention will be utilized. The pond treatment volumes were based on dry detention.

Pond Site 5A is located adjacent to and northeast of SR 710 at Station 697+00. Access to this site would be from SR 710. The pond outfall into the Mosquito Creek to the east is estimated to be a 595-foot long, 18" pipe at this time. This potential location consists primarily of grass, brush and trees.

The soil encountered at this site is Immokalee fine sand (Type B/D) which has an estimated depth to the SHWT from 0.5 feet to 1.5 feet below existing ground. The FDOT Geotechnical Department performed a boring at Pond 5A (to a depth of 20 feet) which determined that the site soil consists of gray and brown fine sand with some rock. From Boring PB-5A, the observed water table elevation on October 22, 2013 was 2.0 feet below the ground surface, and the seasonal high groundwater table (SHGT) was estimated to be 0.75 feet +/- 0.5 feet. From contours, the ground elevation at the boring is 23.0 feet NAVD. Therefore, the SHGT elevation was estimated to be 21.75 feet NAVD.

Pond Site 5A is within the 100 year floodplain as determined from the Effective 2015 FEMA Maps. The area is within floodplain Zone AE, with a base flood elevation of 23.0 feet NAVD. It is expected that this site will minimally impact the floodplain with a floodplain depth of less than 0.5 foot. It has a rating of "Medium" for wetlands/surface water involvement and "Low" for protected species involvement. The contamination screening designated this site as having a risk ranking of "No". Pond Site 5A was assessed as having a "Low" potential for archaeological sites and historic resources. This potential site has <u>no impacts</u> to existing or known future utilities.

The pond site is estimated at 2.62 acres based on measurement. The piped pond outfall to Mosquito Creek will be within SR 710 R/W. The FDOT Right-of-Way Department has provided estimates for proposed Pond 5A. The estimated right-of-way costs and construction costs associated with this parcel are \$127,000 and \$269,696. Other costs associated with this parcel include wetlands mitigation (\$48,000). The total costs associated with this combined parcel are \$444,696. The construction cost is for comparison purposes only and includes embankment (\$51,768); the drainage outfall pipe cost (\$28,257); underdrains (\$142,800); and other miscellaneous costs including sodding, clearing and grubbing, and sediment barrier (\$46,871).

As Pond Site 5A was determined to be the preferred site for Basin 5, further analysis was performed for this site. To summarize, the results indicated that this site will not impact wetlands; the risk rank for contamination is "No" with arsenic contamination "Not Indicated" in the tested locations; and there are no archaeological or historic resources within the APE of this site.

Pond Site 5B is located adjacent to and northeast of SR 710 at Station 689+00. Access to this site would be from SR 710. The pond outfall into the L-63N Canal to the west is estimated to be a 125-foot long, 18" pipe at this time. This potential location consists primarily of grass with some trees.

The soil encountered at this site is Immokalee fine sand (Type B/D) which has an estimated depth to the SHWT from 0.5 feet to 1.5 feet below existing ground. The FDOT Geotechnical Department performed a boring at Pond 5B (to a depth of 20 feet) which determined that the site soil consists of gray and brown fine sand with some rock. From Boring PB-5B, the observed water table elevation on October 22, 2013 was 2.0 feet below the ground surface, and the seasonal high groundwater table (SHGT) was estimated to be 0.50 feet +/- 0.5 feet. From contours, the ground elevation at the boring is 23.0 feet NAVD. Therefore, the SHGT elevation was estimated to be 22.00 feet NAVD.

Pond 5B is <u>not</u> within the 100 year floodplain as determined from the Effective 2015 FEMA Maps. It has a rating of "Low" for wetlands/surface water involvement and "Low" for protected species involvement. The contamination screening designated this site as having a risk ranking of "No". Pond Site 5B was assessed as having a "Moderate" potential for archaeological sites and historic resources. This potential site has no impacts to existing or known future utilities.

The pond site is estimated at 2.53 acres based on measurement. The piped pond outfall to Mosquito Creek will be within SR 710 R/W. The FDOT Right-of-Way Department has provided estimates for proposed Pond 5B. The estimated right-of-way costs and construction costs associated with this parcel are \$171,000 and \$265,083. Other costs associated with this parcel include wetlands mitigation (\$30,000). The total costs associated with this combined parcel are \$466,083. The construction cost is for comparison purposes only and includes embankment cost (\$60,120); the drainage outfall pipe cost (\$5,936); underdrains (\$153,920); and other miscellaneous costs including sodding, clearing and grubbing, and sediment barrier (\$45,106).

Pond Site 5C is located adjacent to and south of SR 710 at Station 699+00. Access to this site would be from SR 710. The pond outfall into the L-63N Canal to the west is estimated to be a 400-foot long, 18" pipe at this time. This potential location consists primarily of grass brush, and trees.

The soil encountered at this site is Immokalee fine sand (Type B/D) which has an estimated depth to the SHWT from 0.5 feet to 1.5 feet below existing ground. The FDOT Geotechnical Department performed a boring at Pond 5C (to a depth of 20 feet) which determined that the site soil consists of gray and brown fine sand with some

rock. From Boring PB-5C, the observed water table elevation on October 23, 2013 was 2.5 feet below the ground surface, and the seasonal high groundwater table (SHGT) was estimated to be 1.00 feet +/- 0.5 feet. From contours, the ground elevation at the boring is 24.00 feet NAVD. Therefore, the SHGT elevation was estimated to be 22.50 feet NAVD.

This site <u>is</u> within the 100 year floodplain as determined from the Effective 2015 FEMA Maps. It has a rating of "None" for wetlands/surface water involvement and "Low" for protected species involvement. The contamination screening designated this site as having a risk ranking of "Low". Although this site was preliminarily assigned a ranking of "Medium" for contamination due to proximity to livestock holding pen, the ranking changed to "Low" after further investigation determined the holding pen was 50 feet away from the site. Pond Site 5B was assessed as having a "Low" potential for archaeological sites and historic resources. This potential site has <u>no impacts</u> to existing or known future utilities.

The pond site is estimated at 3.53 acres based on measurement of GIS Parcels. The piped pond outfall to Mosquito Creek will be within SR 710 R/W. The FDOT Right-of-Way Department has provided estimates for proposed Pond 5C. The estimated right-of-way costs and construction costs associated with this parcel are \$195,000 and \$266,723. The total costs associated with this parcel are \$461,723. The construction cost is for comparison purposes only and includes embankment cost (\$35,268); the drainage outfall pipe cost (\$18,996); underdrains (\$150,000); and other miscellaneous costs including sodding, clearing and grubbing, and sediment barrier (\$62,460).

C. Pond Sizing

Pond sizes for the Pond Siting Report are based on the proposed suburban typical section. The pond size requirements are based on SFWMD criteria for wet detention systems. According the Pre-Application Meeting with the SFWMD on May 29, 2013, the following criteria was determined for the proposed stormwater management design: (See Appendix 9, Correspondence for Meeting Minutes)

- Attenuation of the peak pre/post discharge
- Water quality treatment volume 2.5 inches over the impervious area (controlling factor)
- Additional 50% treatment requirements for impaired water bodies not required as the pre-post nutrient loading calculations show no offsite water quality impacts
- Drawdown (wet ponds) one half inch of runoff over the basin in 24 hours
- Minimum 3" bleeder utilized on control structures

Preliminary pond designs were performed which include storm routings for the SFWMD's 25 year, 72 hour storm. Stormwater routings for each storm were also performed for the 5 year, 1 hour storm to provide a realistic tailwater for the preliminary storm sewer calculations. These storm sewer calculations were

performed to determine if the proposed pond sites will work hydraulically given the proposed roadway profile (See **Appendix 8** for calculations).

Additional criterion used in the sizing of the stormwater management facilities:

- 1. The ponds will function similarly with regards to design stages.
- 2. Side slopes: 1:4 (includes back slopes of berms)
- 3. Level maintenance area width: 20 feet
- 4. One foot of freeboard
- 5. Pond allowed to stage up to one-half foot below low profile elevation
- 6. For dry detention facilities, treatment volume determined by the greater of 75% of 1 inch over the drainage area or 75% of 2.5 inches over the impervious area.

Each proposed pond site was preliminarily sized based on the above criteria. The calculated treatment volumes for each site are listed below in Table 12. The pond information including required size, 25 year, 72 hour peak stage, berm elevation, normal water elevations, basin profile low point elevation, maximum allowable stage, drainage area, allowable discharge, and outfall location are included in the Table 13 below.

For final pond design, the ponds will need to include storm routings for the SFWMD's 25 year, 72 hour storm and the FDOT's critical duration analysis for storms up through the 100-year, 3 day storm (Rule 14-86 criteria for open basins) will be included as this is a pumped outfall.

Table 12 - Pond Site Treatment Volumes

Tubic 12	rond site i	T Catifficity	rolanics		T		
			Wet De	tention	Dry De	tention	
Pond Site	Total Drainage Area (AT)1	Total Impervious Area For Treatment (Ai)1	1" over Basin Area2 (AT) x (1"/12)	2.5" over Impervious Area2 (Ai) x (2.5"/12)	75% of 1" over Basin Area3 (AT) x (1"/12)	75% of 2.5" over Impervious Area3 (Ai) x (2.5"/12)	Required Treatment Volume
	(acres)	(acres)	(ac-ft)	(ac-ft)			(ac-ft)
1A	6.32	2.40	0.53	0.50			0.53
1B (Dry)	5.20	2.40			0.32	0.38	0.38
1C (Dry)	4.87	2.39			0.30	0.37	0.37
2A-Option 1	46.49	22.35	3.87	4.66			4.66
2A-Option 2	44.26	22.35	3.69	4.66			4.66
2A-Option 3	43.48	22.35	3.62	4.66			4.66
2B-Option 1	52.43	22.35	4.37	4.66			4.66
2B-Option 2	47.06	22.35	3.92	4.66			4.66
2B-Option 3	44.15	22.35	3.68	4.66			4.66
2C-Option 1	43.93	22.35	3.66	4.66			4.66
2C-Option 2	43.20	22.35	3.60	4.66			4.66
3A	14.56	6.26	1.21	1.30			1.30
3B	12.83	6.26	1.07	1.30			1.30
3C	21.72	10.44	1.81	2.18			2.18
4A-Option 1	31.05	10.06	2.59	2.10			2.59
4A-Option 2	30.41	10.06	2.53	2.10			2.53
4B/4C- Option 1	35.23	10.06	2.94	2.10			2.94
4B-Option 2	31.65	10.06	2.64	2.10			2.64
4D-Option 1	33.14	10.06	2.76	2.10			2.76
4D-Option 2	31.39	10.06	2.62	2.10			2.62
5A (Dry)	11.12	4.03			0.69	0.63	0.69
5B (Dry)	11.03	4.03			0.69	0.63	0.69
5C (Dry)	12.02	4.03			0.75	0.63	0.75

Table 13 - Pond Design Parameters

Pond Site	Drainage Area (ac)	Control EI. (NHW or Dry Pond Bottom (ft NAVD)	Treatment Volume Stage (ft NAVD)	25 Yr/72 Hr Stage (ft NAVD)	Berm EI. (ft NAVD)	Max Stage (ft NAVD)	Profile Low Point El. (Station) (ft NAVD)	Discharge (cfs)	Disch./Ac. (cfs/ac)	Allowable Discharge (cfs)	Outfall Location
1A	6.32	21.60	22.15	22.94	24.50	23.50	23.85 (502+40)	6.33	1.00	12.14	City Ditch
1B	5.20	18.28 (dry)	19.38	19.85	21.28	20.28	23.85 (502+40)	10.50	2.02	12.14	Taylor
1C	4.87	17.0 (dry)	20.18	20.77	22.00	21.00	23.85 (502+40)	9.77	2.01	12.14	Taylor
2A- Option 1	46.49	21.03	21.76	23.35	24.43	23.43	24.03 (516+00)	20.07	0.43	24.62	Commerce
2A- Option 2	44.26	21.03	22.17	24.16	25.43	24.43	25.03 (516+00)	22.86	0.52	24.62	Commerce
2A- Option 3	43.48	21.03	22.47	25.29	26.43	25.43	26.03 (516+00)	23.51	0.54	24.62	Commerce
2B- Option 1	52.43	21.95	22.35	23.48	24.43	23.43	24.03 (516+00)	29.94	0.57	24.62	Commerce
2B- Option 2	47.06	21.95	22.62	24.34	25.43	24.43	25.03 (516+00)	21.40	0.45	24.62	Commerce
2B- Option 3	44.15	21.95	23.01	25.22	26.43	25.43	26.03 (516+00)	22.73	0.51	24.62	Commerce
2C- Option 1	43.93	18.33	19.67	23.34	24.43	23.43	24.03 (516+00)	8.11	0.18	9.93	Taylor
2C- Option 2	43.20	18.33	20.17	24.28	25.43	24.43	25.03 (516+00)	9.51	0.22	9.93	Taylor
3A	14.56	24.73	25.49	27.58	29.73	28.73	29.15 (636+50)	6.00	0.41	9.86	Historic ditch
3B	12.83	25.40	26.46	28.58	29.73	28.73	29.15 (636+50)	7.80	0.61	7.85	Historic ditch
3C	21.72	22.45	23.45	25.78	28.00	27.00	29.15 (636+50)	10.33	0.48	18.53	Historic ditch
4A- Option 1	31.05	24.00	25.13	27.89	29.00	28.00	28.56 (657+50)	15.11	0.49	15.78	L-63N
4A- Option 2	30.41	24.00	25.51	28.92	30.00	29.00	29.56 (657+50)	15.01	0.49	15.78	L-63N
4B/4C- Option 1	35.23	22.25	23.13	25.64	29.00	28.00	28.56 (657+50)	13.59	0.39	15.95	Historic Ditch
4B- Option 1	31.65	22.25	23.50	27.04	30.00	29.00	29.56 (657+50)	9.59	0.30	15.95	Historic Ditch
4D- Option 1	33.14	23.83	24.70	27.09	29.00	28.00	28.56 (657+50)	14.30	0.43	16.13	Historic Ditch
4D- Option 2	31.39	23.83	25.20	28.10	30.00	29.00	29.56 (657+50)	15.68	0.50	16.13	Historic Ditch
5A	11.12	24.00 (dry)	24.65	25.83	27.00	26.00	27.64 (703+50)	10.57	0.95	18.65	Mosquito
5B	11.03	24.00 (dry)	24.73	25.61	27.00	26.00	27.64 (703+50)	16.19	1.47	18.65	L-63N
5C	12.02	24.00 (dry)	24.40	25.26	27.00	26.00	27.64 (703+50)	11.57	0.96	18.65	Mosquito

The right-of-way area and estimated drainage outfall easements required for each potential site are listed in Table 14. It is estimated that only two of the pond sites will require drainage easements for outfall.

Table 14 - Summary of Required Right-of-Way for Pond Sites & Drainage Easements

Pond Site	Estimated Drainage Easement Area (ac)	Right-of-Way Area (ac)*
1A	0	2.24
1B	0	1.08
1C	0.22	1.15
2A-Option 1	0	9.43
2A-Option 2	0	7.20
2A-Option 3	0	6.42
2B-Option 1	0	15.37
2B-Option 2	0	10.00
2B-Option 3	0	7.08
2C-Option 1	0	6.86
2C-Option 2	0	6.14
3A	0	3.47
3B	0	2.44
3C	0.03	3.81
4A-Option 1	0	3.98
4A-Option 2	0	3.34
4B/4C-Option 1	0	7.17
4B-Option 2	0	4.20
4D-Option 1	0	6.08
4D-Option 2	0	4.33
5A	0	2.62
5B	0	2.53
5C	0	3.53

*Note: Pond Site 3C includes existing FDOT Pond for net 1.81 ac. R/W area required.

D. RECOMMENDATIONS

Table 15 presents the Pond Site Evaluation Matrix used to determine the recommended Stormwater Management Facilities for each basin.

Table 15 - Pond Site Evaluation Matrix

				Cultural Impact Potential	Potential for	Potential	Contamination Risk Potential		
Pond Site	Treatment Method	Construction Feasibility	Total Cost	Level I (All Sites)	Involvement of Jurisdictional Wetland	For Involvement of Protected	Level I (All Sites)	Floodplain (2015)	Pond Site Rating
		-		Level II (Preferred Sites)	Systems	Species	Level II (Preferred Sites)		Rating
1A	Wet Detention	Fair	\$355,012	Low	None	Low	No	Yes	Fair
1B	Dry Retention	Good	\$320,073	Level I-Low Level II-No	Medium*	Low	Level I-Low Level II-No	No	Good
1C	Dry Retention	Fair	\$324,664	Low	High	Low	No	Yes	Fair
2A Option 1	Wet Detention	Good	\$1,337,314	Level I-Moderate Level II-No	None*	Low	Level I-No Level II-No	No	Good
2A Option 2	Wet Detention	Good	\$1,644,419	Moderate	None	Low	No	No	Fair
2A Option 3	Wet Detention	Good	\$1,976,879	Moderate	None	Low	No	No	Fair
2B Option 1	Wet Detention	Good	\$1,330,064	Moderate	None	Low	No	No	Fair
2B Option 2	Wet Detention	Good	\$1,601,045	Moderate	None	Low	No	No	Fair
2B Option 3	Wet Detention	Good	\$1,898,262	Moderate	None	Low	No	No	Fair
2C Option 1	Wet Detention	Good	\$1,339,526	Low	Low	Low	No	No	Good
2C Option 2	Wet Detention	Good	\$1,655,070	Low	Low	Low	No	No	Fair
3A	Wet Detention	Good	\$901,448	Low	None	Low	Medium	No	Fair
3B	Wet Detention	Good	\$701,565	Level I-Low Level II-No	Low*	Low	Level I-No Level II-No	No	Good
3C	Wet Detention	Good	\$773,483	Low	None	Low	Low	No	Good
4A Option 1	Wet Detention	Good	\$1,088,121	Low	None	Medium	Low	No	Good
4A Option 2	Wet Detention	Good	\$1,342,958	Low	None	Medium	Low	No	Fair
4B/4C Option 1	Wet Detention	Good	\$1,223,843	Moderate	Low	Low	Medium	No	Fair
4B Option 2	Wet Detention	Good	\$904,222	Level I-Moderate Level II-No	Low*	Low	Level I-No Level II-No	No	Good
4D Option 1	Wet Detention	Good	\$1,071,066	Low	None	Medium	Medium	No	Good
4D Option 2	Wet Detention	Good	\$1,279,153	Low	None	Medium	Medium	No	Fair
5A	Dry Retention	Fair	\$444,696	Level I-Low Level II-No	Medium*	Low	Level I-No Level II-No	Yes	Good
5B	Dry Retention	Fair	\$466,083	Moderate	Low	Low	No	No	Good
5C	Dry Retention	Fair	\$461,723	Low	None	Low	Low	No	Good

*Note: Pond Sites 1B, 3B, and 5A were determined to have wetland impacts of 0.47 ac., 0.35 ac., and 0.11 ac., respectively. Pond Sites 2A-Option 1 and 4B-Option 2 were determined to have no wetland impacts.

Basin 1

The recommended pond site for Basin 1 is Pond 1B. It is located adjacent to SR 710 right-of-way and outfall, Taylor Creek. As such, it works best hydraulically and will not incur extra cost for an outfall easement or piping. Pond 1A is located offsite and approximately 800 feet to the west of the Begin Project Station 500+00, and will require piping to convey runoff to the pond as well as for outfall into the City Ditch. Pond 1C is a smaller site located just south of Pond 1B. Since it is not directly adjacent to SR 710, this site will require more piping for conveyance of runoff to the pond as well as outfall into Taylor Creek through an outfall drainage easement. Both Pond 1B and Pond 1C have wetland impacts, however, Pond 1B has less wetland impacts, therefore, will require less wetland mitigation cost. Pond 1A has a higher cost than Pond 1B and Pond 1C, partially due to the additional piping and cost of

rubble riprap. Pond 1A is less desirable as an alternative due to its close proximity to the airport which requires rubble riprap installation around the perimeter of wet detention ponds as a wildlife deterrent.

The initial screenings indicated that Pond 1B has a rating of "Medium" for wetlands/surface water involvement as the property impacts an estimated 0.5 acre of wetlands and "Low" for protected species involvement. The contamination screening designated Pond site 1B as having a risk ranking of "Low" as the site was noted to have unidentified modifications to the property in historical aerials. Pond Site 1B was assessed as having a "Low" potential for archaeological sites and historic resources.

After Pond Site 1B was determined to be the preferred site for Basin 1, a more indepth analysis of the site was performed. To summarize, the results indicated that this site will impact 0.47 acre of wetlands; the risk rank for contamination is "No" with arsenic contamination "Not Indicated" in the tested locations; and there are no archaeological or historic resources within the APE of this site.

Basin 2

The recommended pond site for Basin 2 is Pond 2A-Option 1. It is north of and adjacent to SR 710 R/W. It is located approximately 3,750 feet east of Taylor Creek. Pond 2A-Option 1 is almost the most cost effective option, and is very comparable to Pond 2B-Option 1. This option does not include raising the road. It is located close to the low point in the road, therefore, it is hydraulically more efficient for conveyance of runoff to the pond site. Further, Pond 2A - Option 1 has a lower estimated SHWT than Pond 2B - Option 1 and takes a portion of a parcel which is already being impacted by the roadway which makes it more desirable than Pond 2B - Option 1. In addition, the estimated cost difference between Ponds 2A - Option 1 and 2B - Option 1 is minimal at 0.5% of the total cost of Pond 2A - Option 1. Pond 2A - Option 1 is a smaller site, only 9.43 ac versus 15.37 ac for Pond 2B-Option 1. As the pond footprint is smaller, there will be less impact to the property owner. It does not need rubble riprap due to proximity to the airport as is needed by Pond 2C-Option 1. This site will not incur extra cost for an outfall easement.

The initial screenings indicated that Pond 2A-Option 1 has ratings of "Moderate" for Cultural Impact Potential; "None" for Wetland/Surface Water Involvement; and "Low" for Protected Species Involvement. It has a rating of "No" for Contamination Risk Potential.

After Pond Site 2A - Option 1 was determined to be the preferred site for Basin 2, a more in-depth analysis of the site was performed. To summarize, the results indicated that this site will not impact wetlands; the risk rank for contamination is "No" with arsenic contamination "Not Indicated" in the tested locations; and there are no archaeological or historic resources within the APE of this site.

Basin 3

The recommended pond site for Basin 3 is Pond 3B. It is adjacent to and just east of SR 710 R/W, and therefore, conveyance of runoff to the pond site would be more efficient. Pond 3B is the least costly alternative in Basin 3. This site will not incur extra cost for an outfall easement. Pond 3A and Pond 3C have a greater total cost than Pond 3B. Pond 3A is not adjacent to SR 710 and is located over 700 feet east of the SR 710 R/W. Pond 3C would include modification of an existing FDOT pond site. The initial screenings indicated that Pond 3B has ratings of "Low" for Cultural Impact Potential, Protected Species Involvement, and Wetland/Surface Water Involvement. It has a rating of "No" for Contamination Risk Potential.

After Pond Site 3B was determined to be the preferred site for Basin 3, a more indepth analysis of the site was performed. To summarize, the results indicated that this site will impact 0.35 acre of wetlands; the risk rank for contamination is "No" with arsenic contamination "Not Indicated" in the tested locations; and there are no archaeological or historic resources within the APE of this site.

Basin 4

The recommended pond site for Basin 4 is Site 4B-Option 2. This site is located adjacent to SR 710 right-of-way in the infield area between the proposed SR 710 alignment, existing SR 710, and NE 34th Avenue. It is located close to the low point in the roadway profile, therefore, pipe costs are lower for these sites. This site will not incur extra cost for an outfall easement. Pond 4A and Pond 4D have an additional protected species mitigation cost associated with them for the relocation of gopher tortoise burrows. Pond 4B-Option 2 has a lower cost than all other options for this basin.

The initial screenings indicated that Pond 4B-Option 2 had ratings of "Low" for Wetland/Surface Water Involvement and Protected Species Involvement. Pond 4B-Option 2 had a rating of "No" for Contamination Risk Potential. Pond 4B-Option 2 had a rating of "Moderate" for Cultural Impact Potential.

After Pond Site 4B - Option 2 was determined to be the preferred site for Basin 4, a more in-depth analysis of the site was performed. To summarize, the results indicated that this site will not impact wetlands; the risk rank for contamination is "No" with arsenic contamination "Not Indicated" in the tested locations; and there are no archaeological or historic resources within the APE of this site.

Basin 5

The recommended pond site for Basin 5 is Pond 5A. Pond 5A is directly adjacent to and northeast of SR 710 R/W. All three pond sites in Basin 5 are comparable; however, Pond 5A is the most cost effective option.

The initial screenings indicated that Pond 5A had ratings of "Medium" for Wetland/Surface Water Involvement and "Low" for Protected Species Involvement. Pond 5A had a rating of "No" for Contamination Risk Potential. Pond 5A had a rating of "Low" for Cultural Impact Potential. It is located within the 100 year floodplain.

After Pond Site 5A was determined to be the preferred site for Basin 5, a more indepth analysis of the site was performed. To summarize, the results indicated that this site will impact 0.11 acres of wetlands; the risk rank for contamination is "No" with arsenic contamination "Not Indicated" in the tested locations; and there are no archaeological or historic resources within the APE of this site.

General

Several of the chosen sites will work with underdrains and the discharge to the L63-N will be further discussed with the SFWMD. Pre-Application Meetings were held with the SJRWMD for the purpose of assessing the stormwater criteria and discussion of use of a single large onsite regional pond for project stormwater treatment. Documentation of the Regional Pond Analysis has been included in **Appendix 10**, SR 710 Regional Pond Feasibility Study.

V. REFERENCES

Archaeological Consultants, Inc. *Preliminary Cultural Resource Assessment Proposed Pond Sites for SR 710*, April, 2015.

Scheda Ecological Associates. *Protected Species and Wetlands Pond Siting Assessment Report for SR 710*, February, 2014.

Florida Department of Transportation - *Geotechnical Considerations for Pond Siting Report*, November 2, 2016.

Tierra, Inc. Draft Level I PSR Contamination Screening Evaluation Report (CSER) for the Proposed Pond Sites (Rev. 2), July 14, 2014.

Tierra, Inc. Draft Level II Field Screening Report - Preferred Ponds, January 13, 2017.

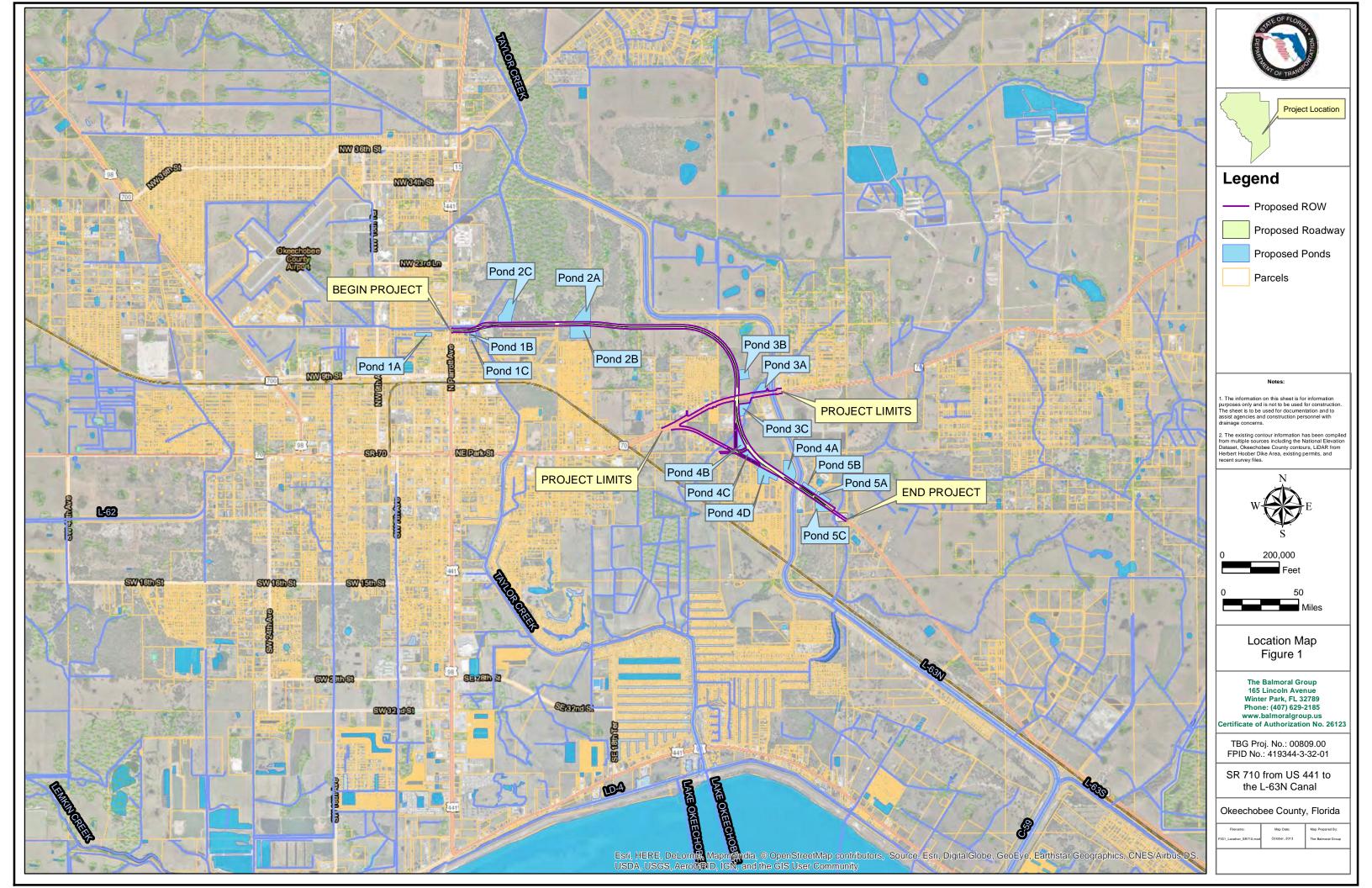
Inwood Consulting Engineers. *Preliminary Engineering Report, PD&E Study for SR 710 from US 441 to CR 714*, September 2012.

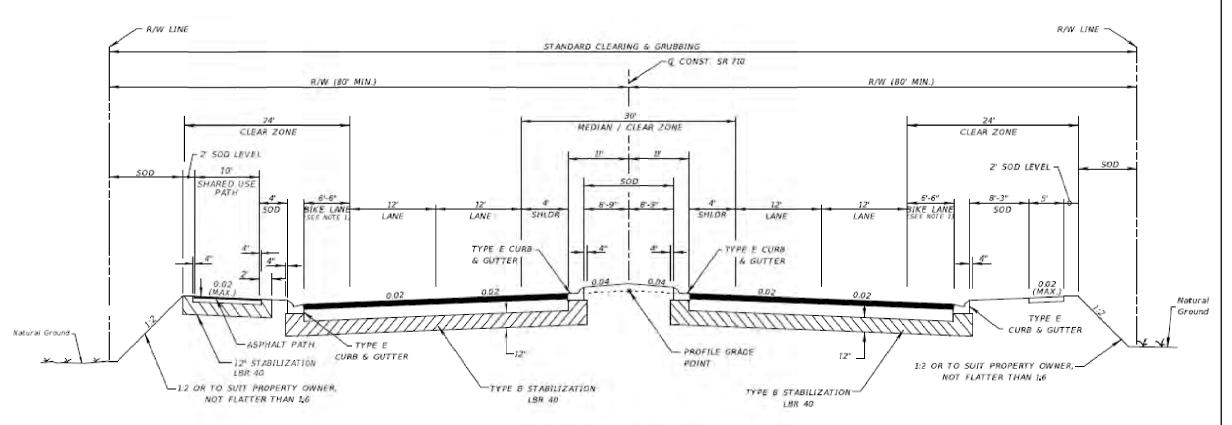
Federal Emergency Management Agency. 2015 Flood Insurance Rate Maps, Okeechobee County, Florida and Incorporated Areas. Map Numbers 12093C0415C, 12093C0420C, 12093C0480C, and 12093C0485. July 16, 2015.

South Florida Water Management District http://www.sfwmd.gov/

Florida Department of Transportation. *Memorandum on Event Mean Concentration (EMC) Values for FDOT proejcts,* April 25, 2011.

Appendix 1 Figures





TYPICAL SECTION NOTES:

1. PROVIDES FOR 8' USABLE SHOULDER.

NEW CONSTRUCTION

TYPICAL SECTION NO. 1 SR 710

STA. 500+00.00 TO STA. 703+50.00

OPTIONAL BASE GROUP 11 WITH TYPE SP STRUCTURAL COURSE (TRAFFIC C) (4") AND FRICTION COURSE FC-5 (34") (RUBBER)

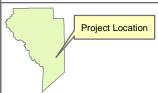
PATH

OPTIONAL BASE GROUP I WITH TYPE SP STRUCTURAL COURSE (TRAFFIC A) (1")

TRAFFIC DATA

= 2013 AADT = 7,100CURRENT YEAR ESTIMATED OPENING YEAR = 2015 AADT = 11,400 ESTIMATED DESIGN YEAR = 2035 AADT = 14,190 K = 9.0% D = 56.2% T = 20.9% (24 HOUR) DESIGN HOUR T = 10.5%DESIGN SPEED = 50 MPH





cccTypical Section cccccFigure 2

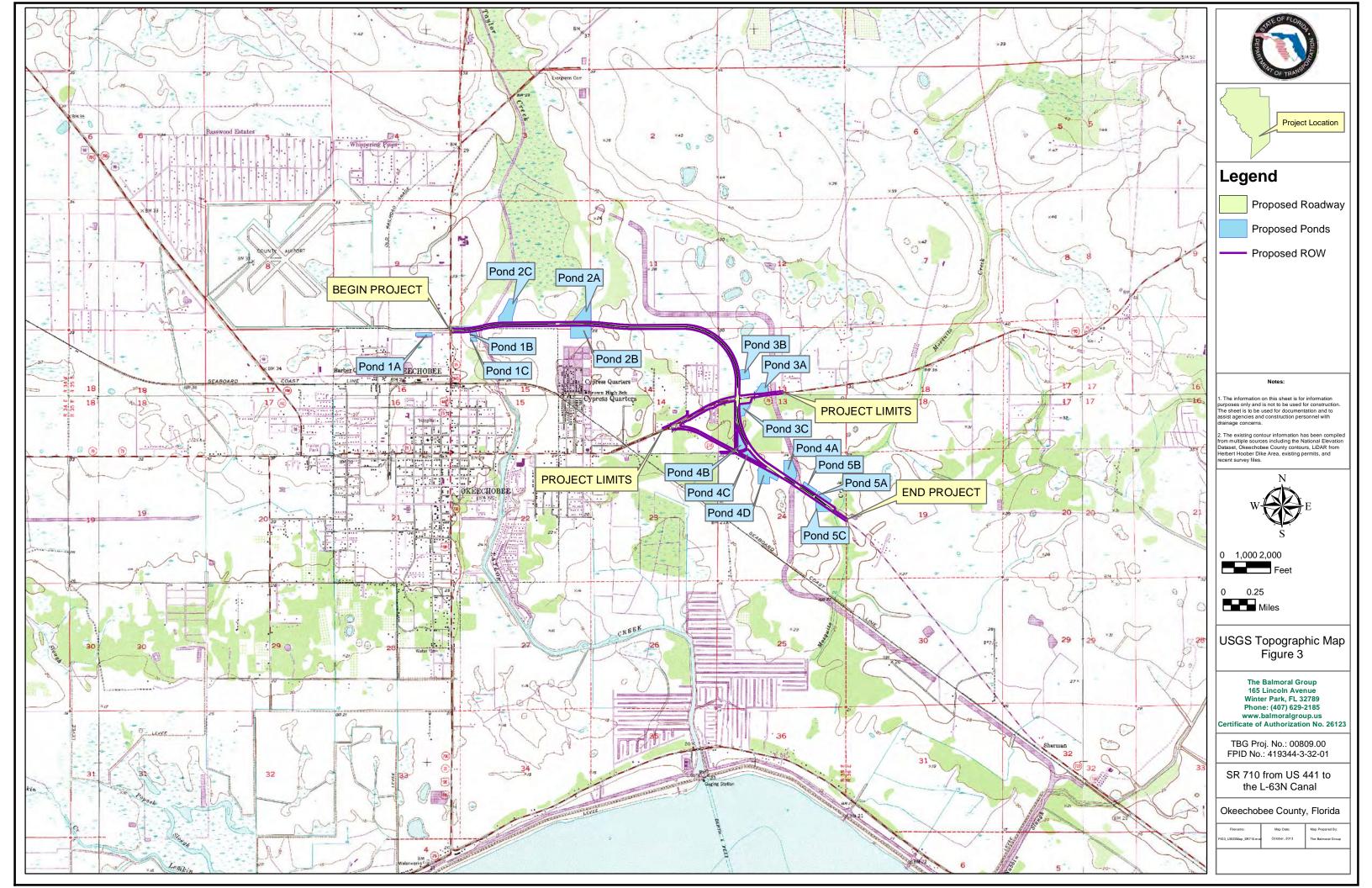
The Balmoral Group 165 Lincoln Avenue Winter Park, FL 32789 Phone: (407) 629-2185 www.balmoralgroup.us Certificate of Authorization No. 26123

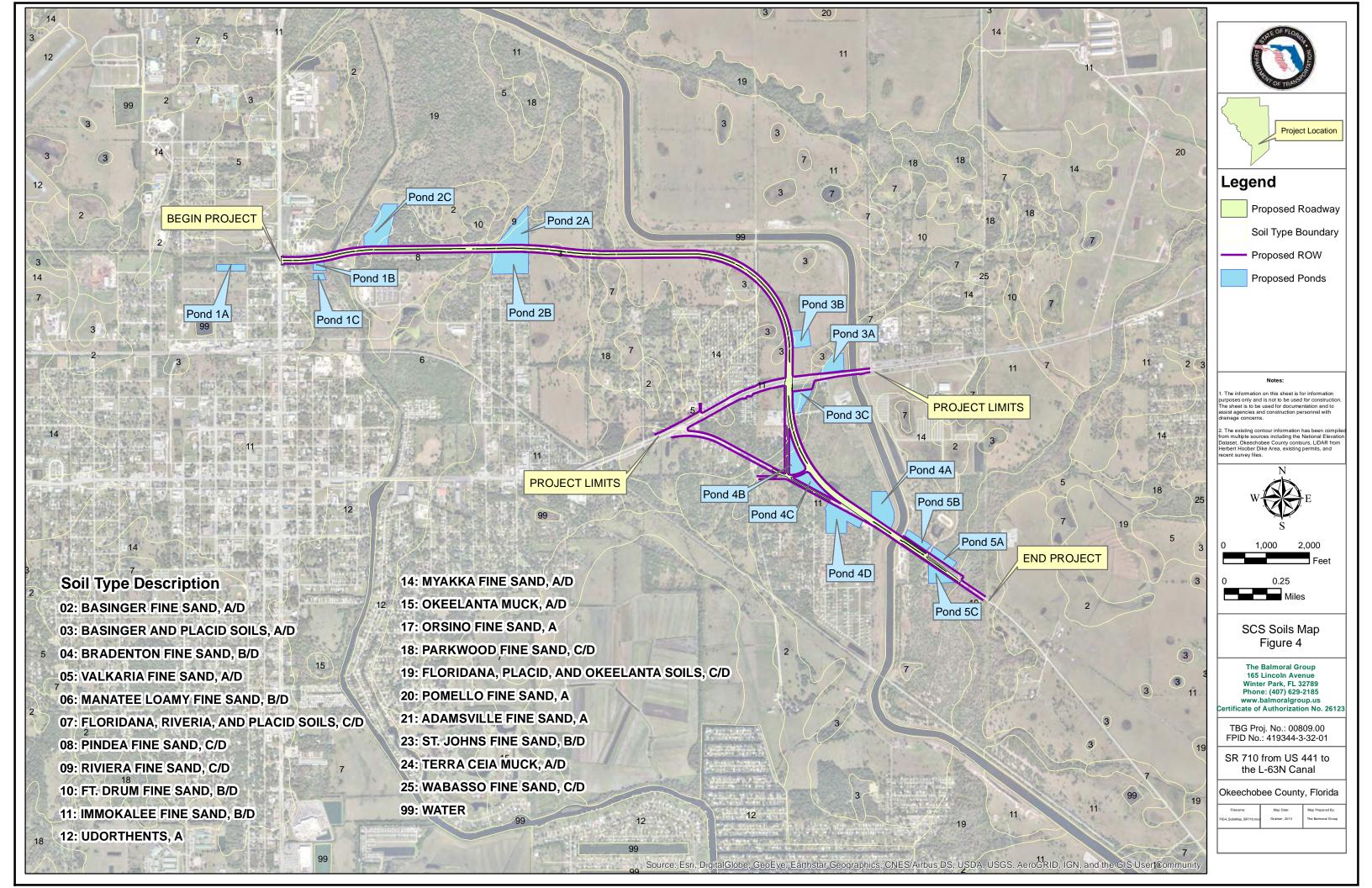
TBG Proj. No.: 00809.00 FPID No.: 419344-3-32-01

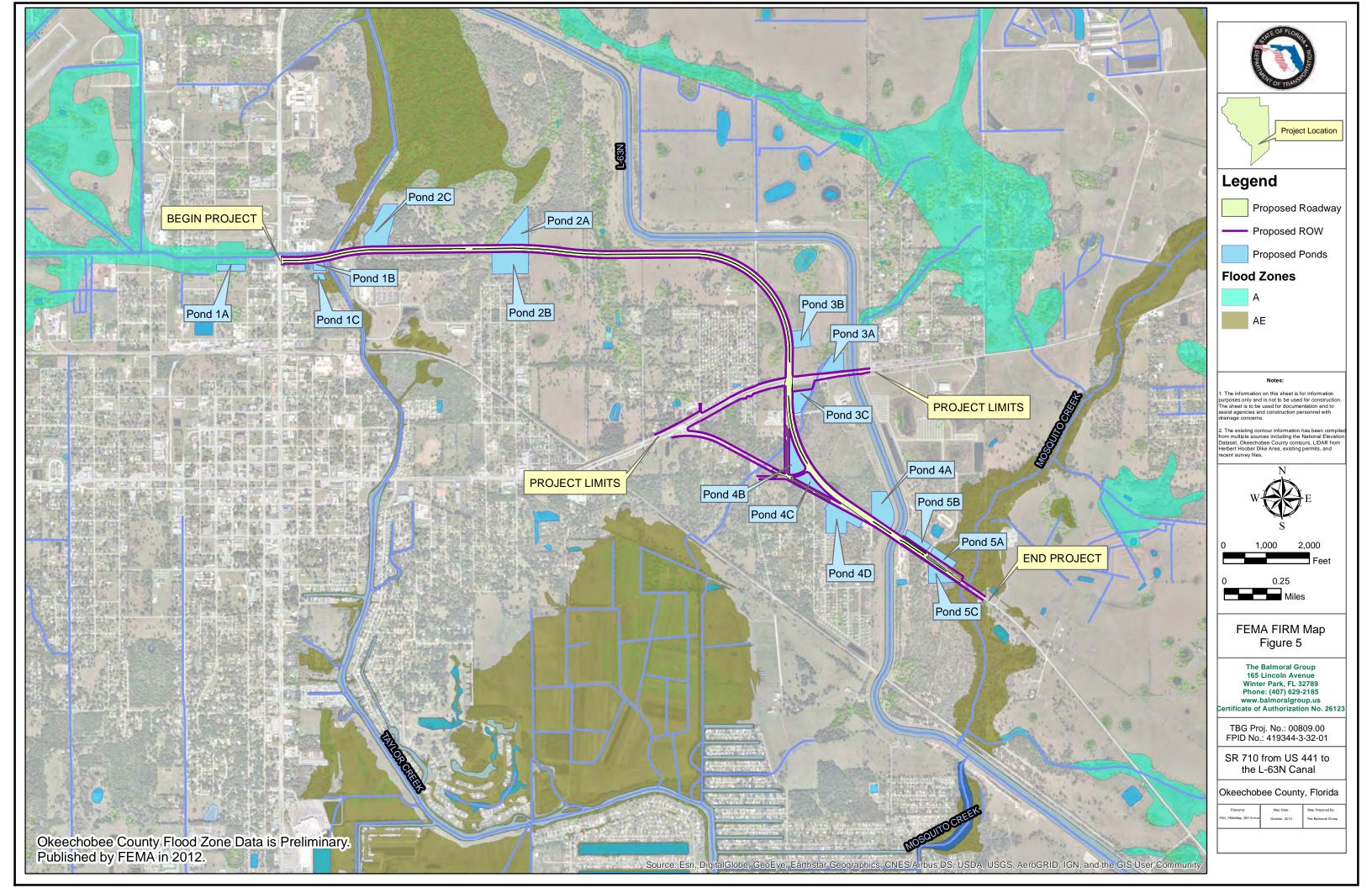
SR 710 from US 441 to the L-63N Canal

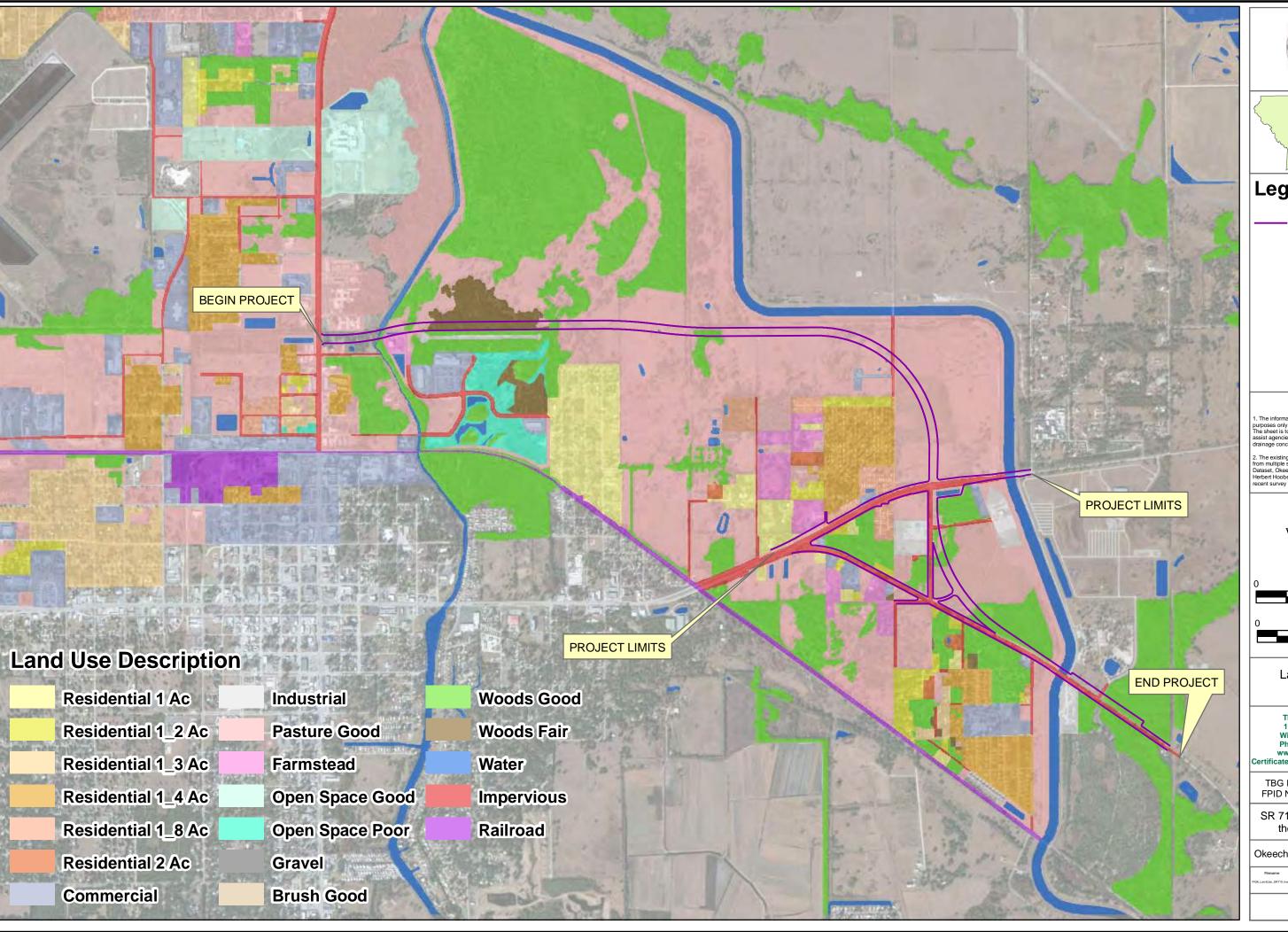
Okeechobee County, Florida

Filename:	Map Date:	Map Prepared By:	ı
ricalSection_SR710.mxd	October, 2013	The Balmoral Group	
			1













Legend

— Proposed ROW

Notes:

- The information on this sheet is for information purposes only and is not to be used for construction. The sheet is to be used for documentation and to assist agencies and construction personnel with
- The existing contour information has been compile from multiple sources including the National Elevation Dataset, Okeechobee County contours, LiDAR from Herbert Hoober Dike Area, existing permits, and recent survey files







Land Use Map Figure 6

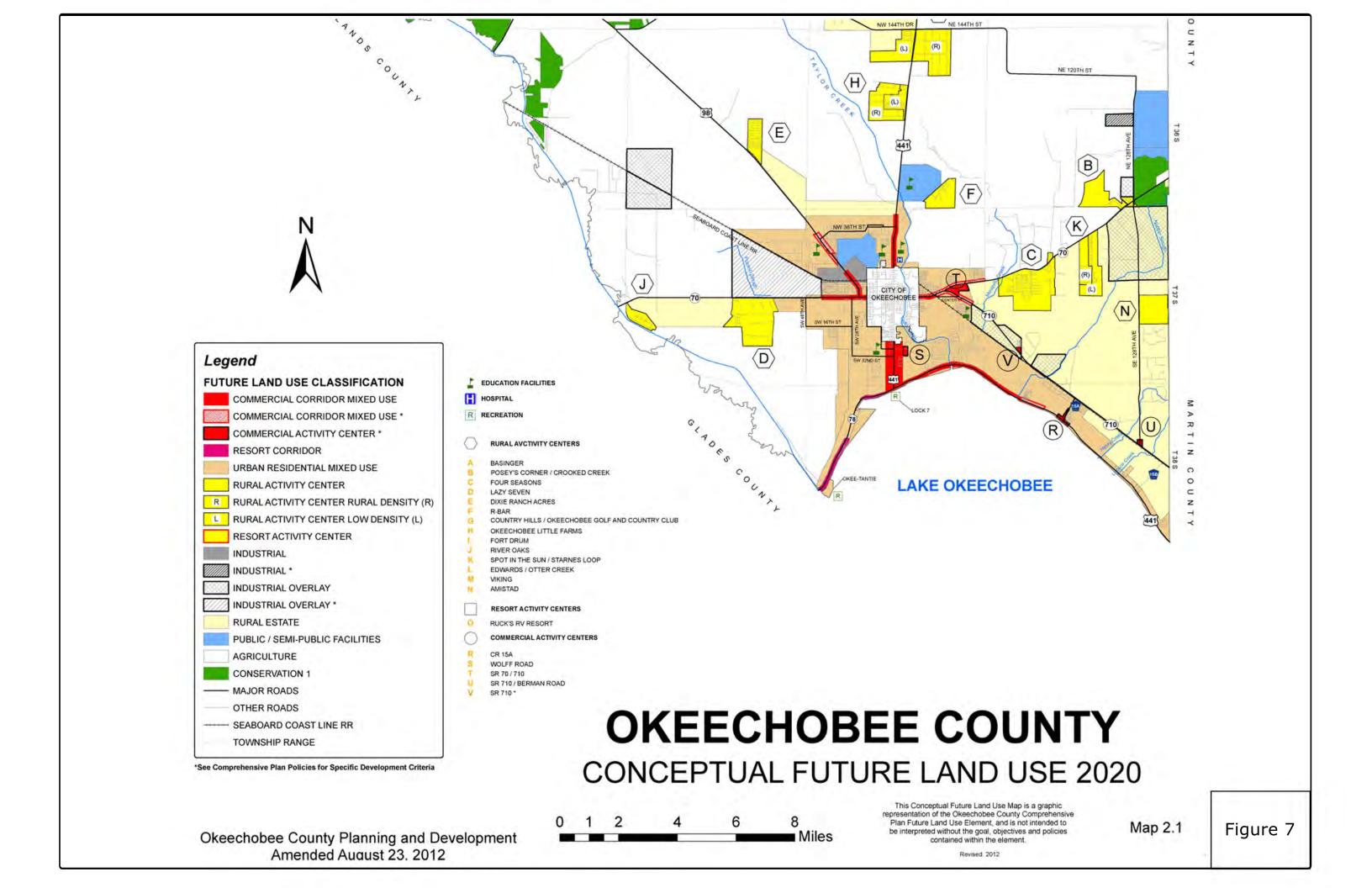
The Balmoral Group 165 Lincoln Avenue Winter Park, FL 32789 Phone: (407) 629-2185 www.balmoralgroup.us Certificate of Authorization No. 26123

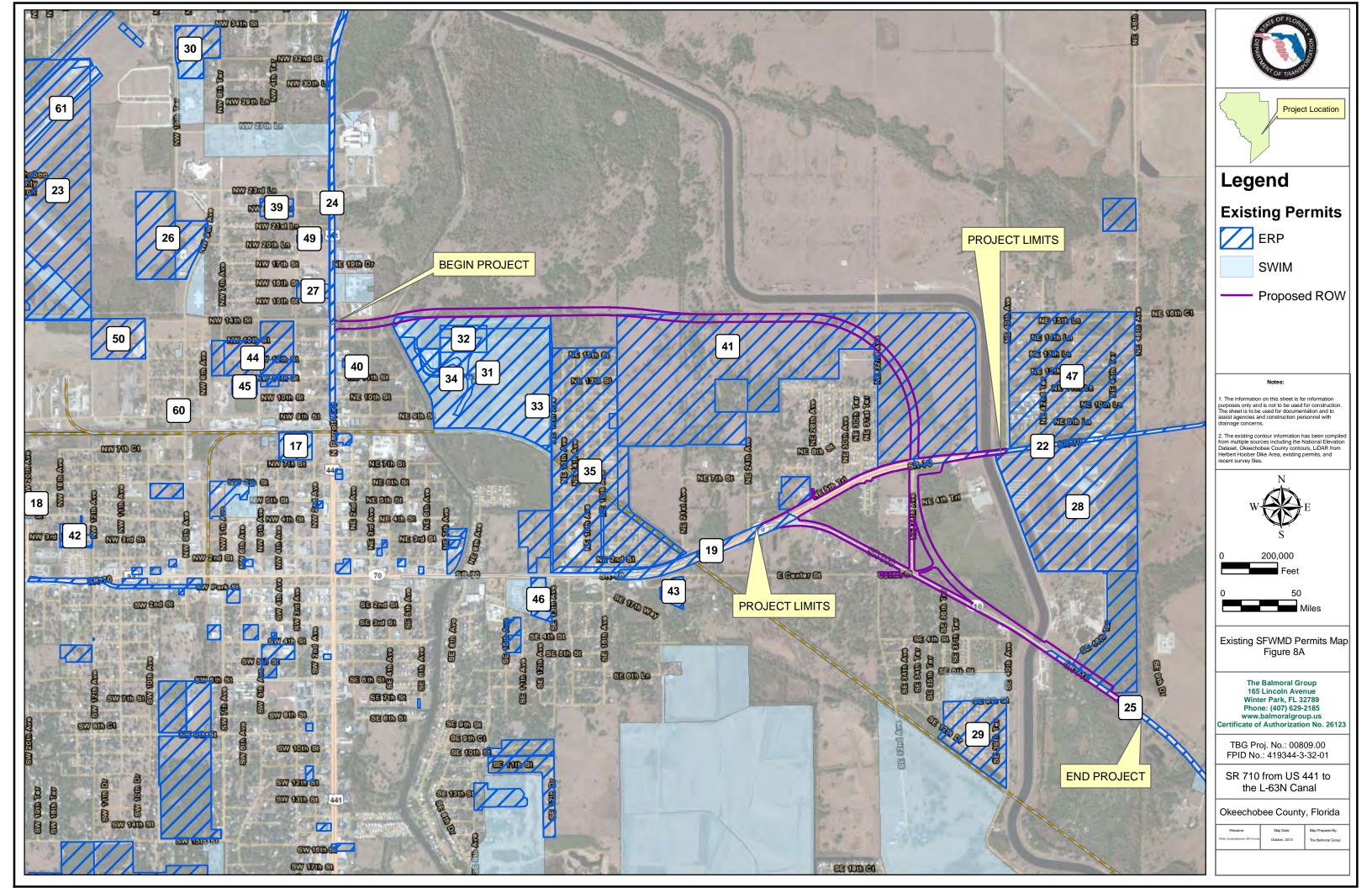
TBG Proj. No.: 00809.00 FPID No.: 419344-3-32-01

SR 710 from US 441 to the L-63N Canal

Okeechobee County, Florida

Filename:	Map Date:	Map Prepared By





	OK 7 to involved 1 ethins										
Number	Project Name	Date Issued	Permit No./App. No.	Туре	Description	Station	Involvement	Resolution			
1	RaymondsC.sMelear,sInc.	3-Jun-94	47-00010-D/940504-1-D	Wetland:Resource Exemption	Commercial						
2	RaulersonsHospital	28-Jul-97,&4- Jan-96,s16- Dec-94,s11- Feb-93,s11- May-78	47-00050/970529-10,s 950614-18,941205-5,s 920717-7,£12027-G	SurfacesWatersManagements (GeneralsPermitsModification,s PermitsTransfer,sCompliances LettersMod,s Construction/Operations Modification,sNews Construction/Operation)	Institutional						
3	OkeechobeesCountySchoolsBoard	7-Jun-79	47-00063-S/s03219-A,s X000012007	SurfacesWatersManagements (News Construction/Operation)	Institutional						
4	OkeechobeesAirport/sT-Hangers Addition	12-Aug-03,s 07-May-02,s 24-May-96,s 25-Apr-96,s 21-Nov-95	47-00074-S/030521-4,s 020124-11,\$60325-13,s 960202-12,\$950803-8,s 910829-2	SurfacesWatersManagements (GeneralsPermitsModification,s CompliancesLettersMod,s EngineersCertifieds Modification)	Airport:Relateds Facilities						
5	HamricksAndsSonssInc.	22-Feb-01,s 12-Apr-90	47-00086-Q/£010129-13,s 900124-5-Q	WorkssofsthesDistrictsLoks (PermitsTransfer),sLoksSwims WorkssofsthesDistricts Modification							
6	AirportsIndustrialsParks(Okechobee CosBdsOf)	10-May-84	47-00091-S/\$X000012018	SurfacesWatersManagements (News Construction/Operation)	Industrial						
7	NathanielsHazellief	11-Jan-01,s14- Jun-90	47-00134-Q/幻01027-5,s 900129-14-Q	LoksSwimsWorkssofsthes DistrictsModification							
8	Okeechobee-Sherman#1sTrans4.n	1-Jul-87	47-00154-S/\$04097-4	SurfacesWatersManagements (News Construction/Operation)	Highway						
9	Sloane Ray Dairy / Lanier / Melears Ray mond £	09-Sep-05,s 15-Oct-98,s 12-Jun-97,s 29-Jan-96,s 13-Aug-92,s 15-Nov-90	47-00169-Q/s050718-2,s 980727-21,s940907-1-Q,s 960102-8,s920318-1-Q,s 900820-1-Qs	WorkssofsthesDistrictsLoks (PermitsTransfer),ssLoksSwims WorkssofsthesDistricts AddendumsModification,s Modification,sNewsLoksSwims WorkssofsthesDistrict							

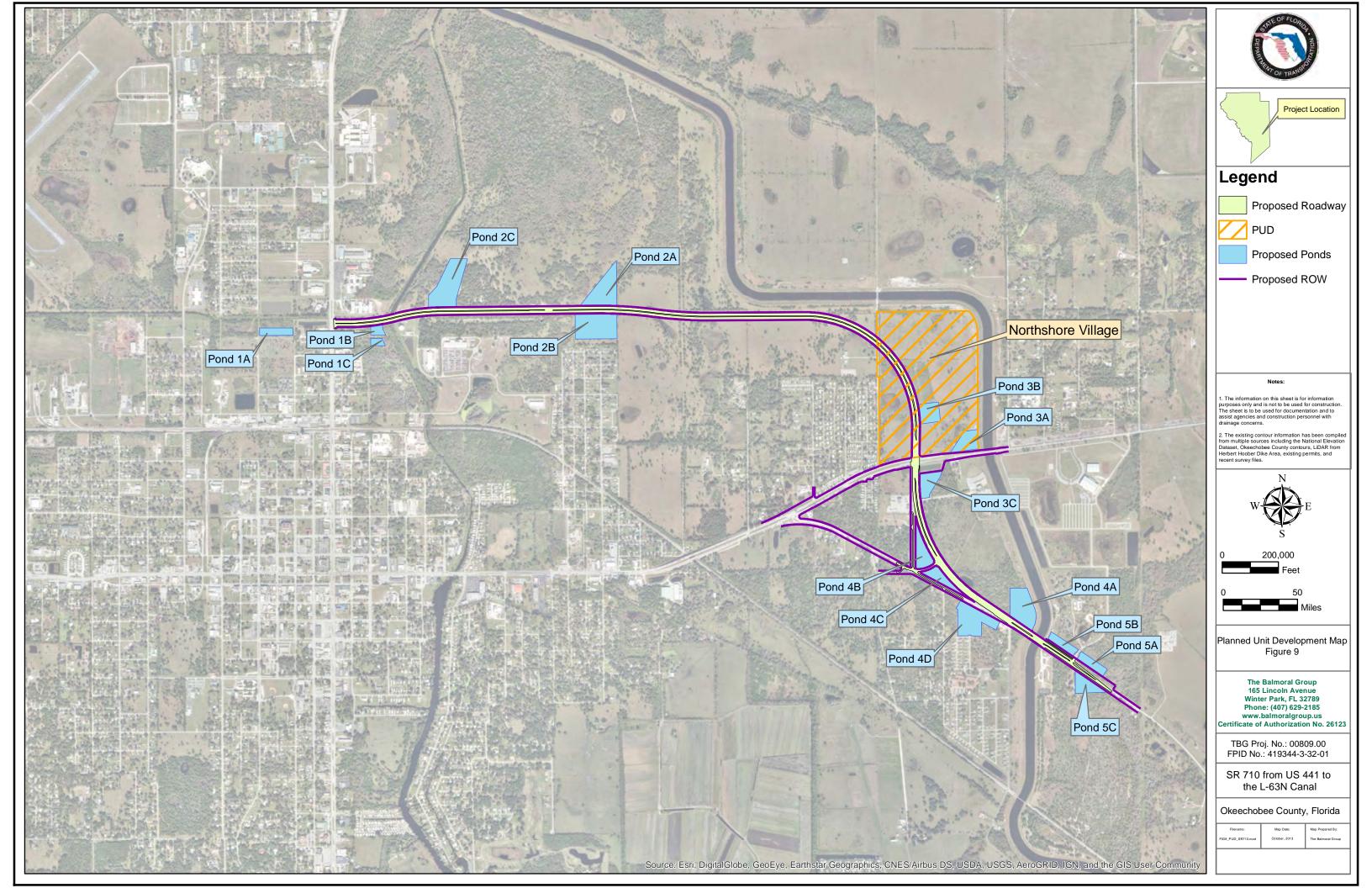
Number	Project Name	Date Issued	Permit No./App. No.	Туре	Description	Station	Involvement	Resolution
10	OkeechobeesCountysAirport	20-Jul-88	47-00180-S/£06138-1	SurfacesWatersManagements (News Construction/Operation)	Commercial			
11	Okeechobee £ lementary \$ chool	07-Nov-08,s 23-Jun-89	47-00242-S/\$080926-19,s 890309-6	SurfacesWatersManagements (General PermitsModification, s New Seneral Permit)	Institutional			
12	OkeechobeesCountysRecreations Center	8-Sep-89	47-00253-S/&90718-5	SurfacesWatersManagements (NewsGeneralsPermit)	Recreational			
13	Okeechobee £ ounty \$ chool £ oards Transportation	12-May-98,s 29-Aug-90	47-00293-S/\$980217-10,s 900824-5	SurfacesWatersManagements (GeneralsPermitsModification,s NewsEngineersCertifieds GeneralsPermit)	Institutional			
14	Consolidateds Hrss Facility	2-Jan-91	47-00303-S/901214-11	SurfacesWatersManagements (NewsEngineersCertifieds GeneralsPermit)	Commercial			
15	PublicsSupplysWellfield	14-May-96,s 09-Oct-92,s 27-May-92,s 13-Jun-91	47-00314-S/960417-2,s 920925-14,920511-3,s 901228-22	SurfacesWatersManagements (PermitsTransfer/sCompliances LettersMod/sNrmsLettersMod/s NewsConstruction/Operation)	Industrial			
16	StatesRoads710	6-Nov-91	47-00327-S/\$910827-3	SurfacesWatersManagements (NewsEngineersCertifieds GeneralsPermit)	Highway			
17	United₅FeedsCo-Op	01-Mar-12şs 06-Oct-10,s 14-Oct-92	47-00352-S/120201-7,s 100813-8,920707-9	Environmental Resources (Compliance Letter Mod,s General Permit Modification),s Surface Water Managements (New General Permit)	Commercial,s Industrial			

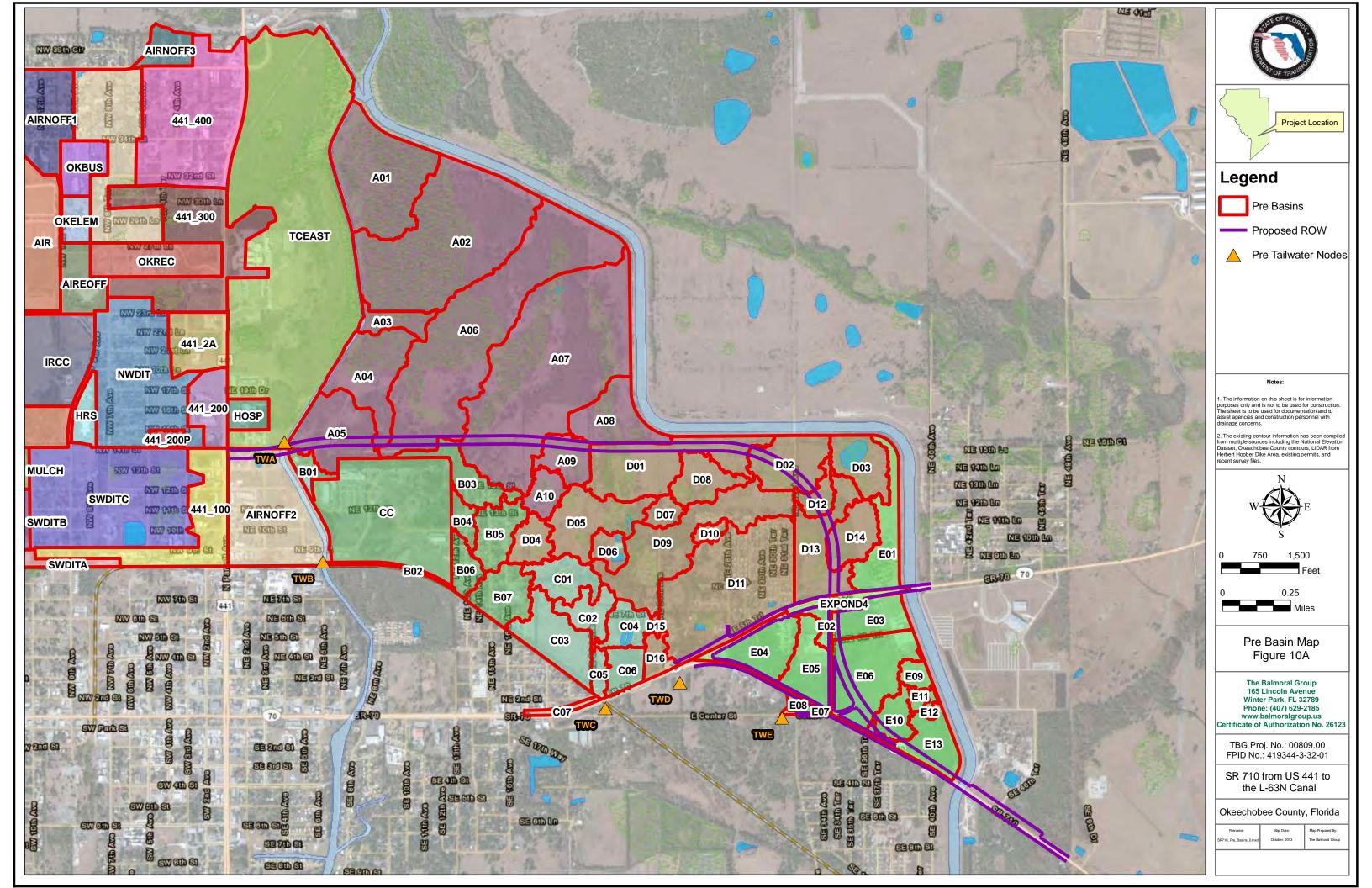
Number	Project Name	Date Issued	Permit No./App. No.	Туре	Description	Station	Involvement	Resolution
18	SRs700/US\$98sDrainages Improvements	14-Sep-07,s 22-Jun-07,s 14-Dec-01,s 15-Apr-93	47-00371-S/\$070813-3,s 070423-32,\$011015-10,s 930216-13	SurfacesWatersManagements (CompliancesLettersMod,s GeneralsPermitsModification,s NewsGeneralsPermit),s EnvironmentalsResources (CompliancesLettersMod)	Highway			
19	SRs70s	11-Jul-03,£09- Dec-93	47-00401-S/幻30612-3,s 930719-16	Environmental Resources (Compliance Letter Mod),s Surface Water Managements (News Construction/Operation)	Highway			
20	Sloane-Ray Subdivision	5-Jan-95	47-00430-S	SurfacesWatersManagements (NewsGeneralsPermit)	Residential			
21	Nichols S anitation	16-Apr-96	47-00442-P/&51004-11	EnvironmentalsResources(News GeneralsPermit)	Commercial			
22	SRs70	30-Oct-96	47-00446-P	Environmental sesources (News General sermit)	Highway			
23	Airportss	13-Dec-02,s 10-Oct-02,s 09-Oct-02,s 23-Jul-02,s16- Apr-98,s08- Nov-96,s14- Nov-96	47-00447-P/100930-28,s 080806-2,980103-4,970928 17,970822-5,970813-1,s 061003-22,960828-1,s 060320-7,940301-4,921016 22,920910-19,920909-1,s 020524-4,910212-1,980114 8,961101-8,960202-13	(General&Permits Modification,Construction/Op erations Modification,Compliances	Industrial,s Commercial			
24	FDOTsUSs441	21-Sep-05,s 12-Jan-04,£04 Sep-98	47-00489-P/幻50815-4,s 031103-3,980311-13	EnvironmentalResources (CompliancesLettersMod,sNews GeneralPermit)	Highway			

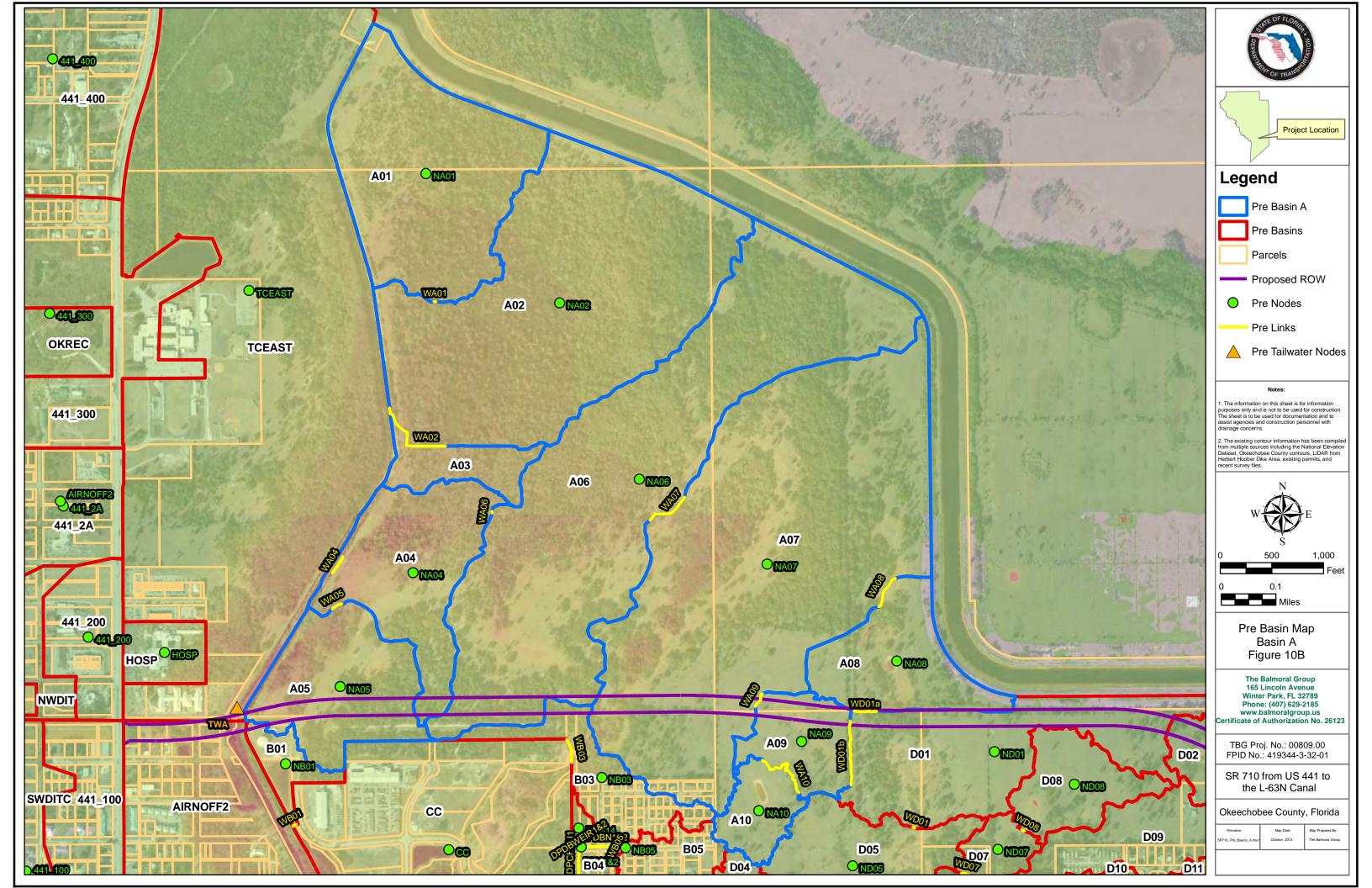
Number	Project Name	Date Issued	Permit No./App. No.	Туре	Description	Station	Involvement	Resolution
25	SR <i>s</i> 710	05-Jan-01,s16- Jul-99	47-00510-P/s001204-1,s 990126-13	EnvironmentalResources (CompliancesLettersMod,sNews GeneralPermit)	Highway			
26	Indian&iver&community&college-s Dixon-Hendry&campus	12-Jul-07,£02- Mar-01,£01- Oct-99	47-00514-P/£070228-75,s 010124-2,£990624-10	Environmental Resources (General Permits Modification, s New General Permit) s	Institutional			
27	OkeechobeesMedicalsCenter	8-Jul-02	47-00562-P/s020313-12	Environmental Resources (News General Permit)	Commercial			
28	OkeechobeesCountysAgri-Civics Center	02-Jul-12,s17- Nov-06,s23- Nov-04,s10- Apr-03	47-00582-P/s071024-1,s 061102-4,s040607-11,s 020909-5	Environmental Resources (Construction/Operations Modification, Compliances Letter Mod, General Permits Modification, News Construction/Operation)	Commercial			
29	Conner's Gables Subdivision	15-May-03	47-00590-P/s021213-17	Environmental Resources (News General Permit)	Residential			
30	OkeechobeesAchievements Academy/SchoolsBoardsBuss Facility	04-Mar-10,s 19-Mar-07,s 21-Apr-04	47-00636-P/s091203-14,s 070126-12,s040113-19	Environmental Resources (General Permit Modification, s Compliance Letter Mod, s News General Permit)	Institutional,s Commercial			
31	OkeechobeesCommercesCenter	30-Mar- 2007,s12-Jan- 07,s26-Oct- 06,s11-Aug- 04	47-00638-P/\$\text{970227-31,s} \\ 061115-11,\$\text{960929-24,s} \\ 040130-34	EnvironmentalResources (CompliancedettersMod,SNos NoticesGeneralPermit,SNews Construction/Operation)	Industrial			
32	OkeechobeesCommercesCenter	17-Aug-06,s 31-Jan-06,s 15-Nov-04	47-00638-P-02/s060314-11,s 050906-4,s041004-12	EnvironmentalResources (GeneralPermitsModification)	Industrial,s Commercial			
33	AdronsFence	14-May-07	47-00638-P-03/s070221-1	EnvironmentalsResources (GeneralsPermitsModification)s	Commercial			
34	OkeechobeesCommercesCenters Bridge	21-Jul-04	47-00645-P/s040716-15	EnvironmentalsResources(News GeneralsPermit)	Industrial			
35	Douglas 乎 ark	22-Jan-09,Ձ6- May-08,Ձ6- Jan-05	47-00652-P/s081124-8,s 080314-2,s040604-15	EnvironmentalResources (GeneralPermitModification,s NewGeneralPermit)s	Government,s Residential			

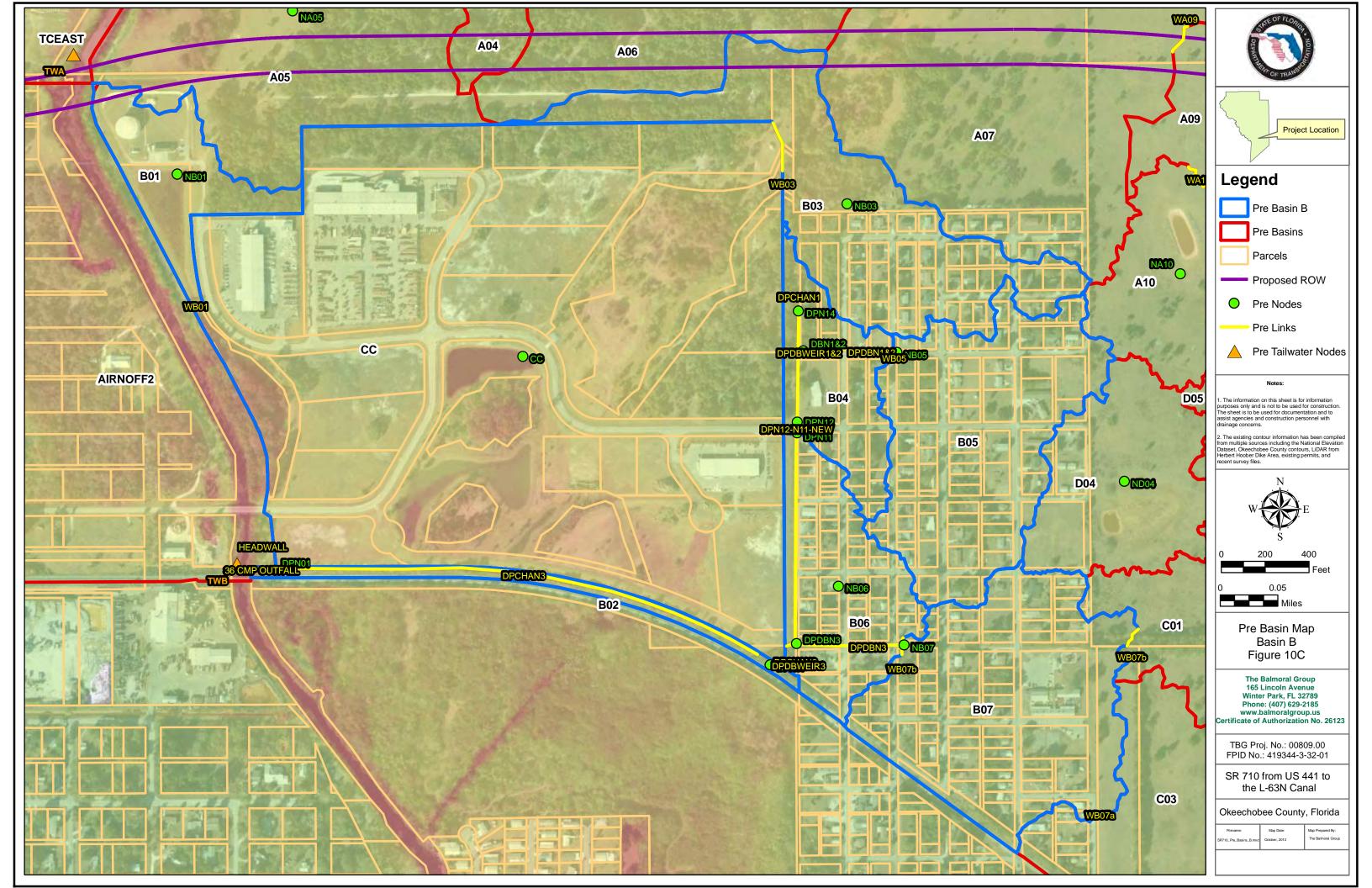
Number	Project Name	Date Issued	Permit No./App. No.	Туре	Description	Station	Involvement	Resolution
36	SuperiorsWater/sMcCoins CommercialsDevelopment	03-Feb-11,s 08-Oct-07,s 24-Jun-05	47-00677-P/⊴101207-1,s 070822-2,£050427-1	Environmental Resources (Letters Mods W/Transfer, s Compliance Letters Mod, s News General Permit)	Commercial			
37	Driveway&ulvert-sSecuritysFencing	30-Nov-05	47-00711-P/:051102-18	Environmental Resource (News General Permit)	AirportsRelateds Facilities			
38	RoyalsConcretesConcepts	14-Sep-07,s 30-May-07,s 08-Mar-06	47-00717-P/幻70720-16,s 070220-40,幻50909-3	Environmental Resources (Compliance Mod Nrm,s General Permit Modification,s Conceptual Approval and News Construction/Operation)	Industrial			
39	TownessofsOkeechobee	6-Apr-06	47-00726-P/s060310-10	EnvironmentalsResources(News GeneralsPermit)	Residential			
40	Utahs Apartments	15-Jun-06	47-00727-P/£051222-3	EnvironmentalsResources(News GeneralsPermit)	Residential			
41	NorthshoresVillage	08-Sep-11,s 11-Aug-11	47-00786-P/�061031-17,s 070807-9	Environmental Resource (News Construction/Operation), News Water Use (General Permit)				
42	LaurelsOakssSeniorsApartments	03-Oct-07,s 04-May-07	47-00804-P/幻70831-18,s 061010-16	Environmental Resources (Compliance Letter Mod, News General Permit)	Residential			
43	Center&treet&torage	22-Sep-08,s 26-Oct-07	47-00830-P/幻80725-4,s 070803-19	Environmental Resources (General Permit Modificaton, s New General Permit)	Commercial			
44	SouthernsTrace	4-Apr-08	47-00847-P/s051213-5	Environmental Resource (News General Permit)	Residential			
45	CasasBella	7-Mar-08	47-00879-P/s071121-20	EnvironmentalsResources(News GeneralsPermit)	Residential			
46	Park : Place	29-Aug-12,s 18-Oct-11,s 07-Jul-08	47-00920-P/⊴120816-6,s 110729-7,£071105-6	Environmental Resources (Compliance Letter Mod,s General Permit Modification,s New General Permit)	Commercial			
47	Hancock Property Bmps	17-Jan-13	47-00921-P-02/s121228-6	EnvironmentalsResources (CompliancesLettersMod)s	Publicsands Institutional			

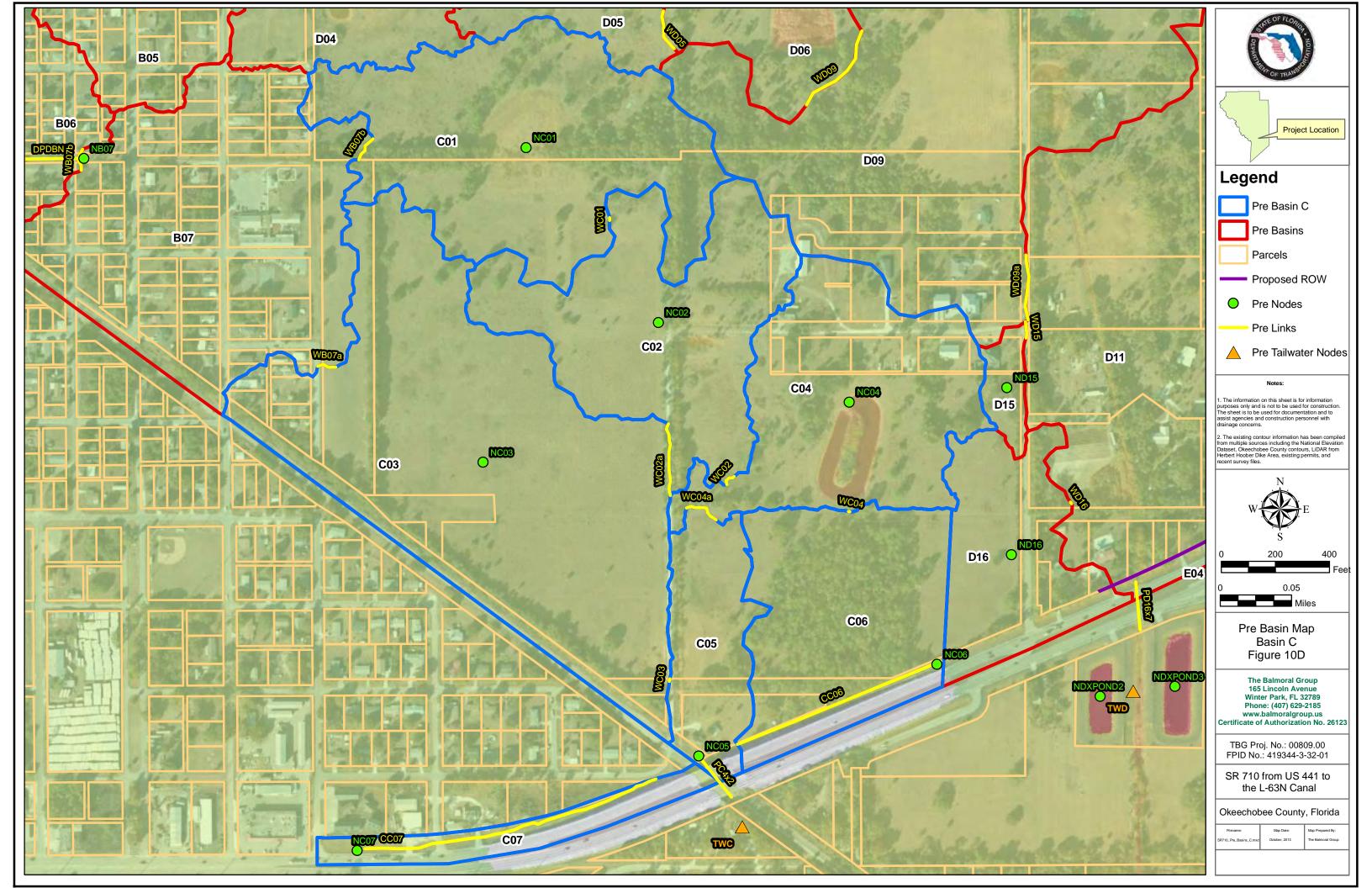
Number	Project Name	Date Issued	Permit No./App. No.	Туре	Description	Station	Involvement	Resolution
48	OkeechobeesGardenssCulverts Replacements	14-Jul-08	\$47-00921-P/\$071206-14	EnvironmentalsResources(News GeneralsPermit)	Publicsands Institutional			
49	Dr.:Red:Brown:Children's:Healths Center	5-Nov-09	47-00992-P/\$090812-1	EnvironmentalsResources(News GeneralsPermit)	Commercial			
50	EarthwisesMulch	7-Jan-11	47-01047-P/£090824-9	Environmental Resource (News General Permit)	Industrial			
51	OkeechobeesCountys2008sDisasters Recovery	4-Aug-11	47-01069-P/s110520-5	EnvironmentalsResources(News GeneralsPermit)	Governments			
52	OkeechobeesAutosSalvage	27-Dec-11	47-01089-P/s111104-6	EnvironmentalsResources(News Deminimus £xemption)	Commercial			
53	SRs70sBridgesOversTaylorsCreek	27-Mar-78	78-00046-S/\$X000005952	SurfacesWatersManagements (NewsGeneralsPermit)	Highway			
54	SRs70sfromsHamricksRoadstosSRs 710	21-May-79	79-00076-S/\$X000006232	SurfacesWatersManagements (NewsGeneralsPermit)	Highway			
55	SRs15&ridgesReplacements	25-Mar-83	83-00057-S/\$X000007884	SurfacesWatersManagements (NewsGeneralsPermit)	Highway			
56	Okeechobee&lementary&chool	12-Aug-86	86-00105-S/£06116-D	SurfacesWatersManagements (NewsGeneralsPermit)	Institutional			
57	Chandler £quipment € co.	3-Oct-85	138-85-S/\$X000001149	SurfacesWatersManagements (NewsExemption)	Commercial			
58	Pineland £ reserve	17-Jun-08	060206-21	EnvironmentalsResources(News GeneralsPermit)	Residential			
59	Armstrong:Automotive:Facility	2-May-03	021004-13	EnvironmentalResource(Nos NoticeGeneralPermit)	Commercial			
60	FirstsMissionarysBaptistsChurch	18-Mar-04	030828-5	EnvironmentalResource(Nos NoticeGeneralPermit)				
61	TaxiwayA&CRehabilitation	7-Oct-10	101007-57	EnvironmentalsResources(News GeneralsPermit)	AirportsRelateds Facilities			
62	SRs70sWidening&roms31sStstos 3200sFt&astsofs80thsAve	10-Dec-12	121210-2	Environmental Resource (News Construction/Operation)	Roadway			

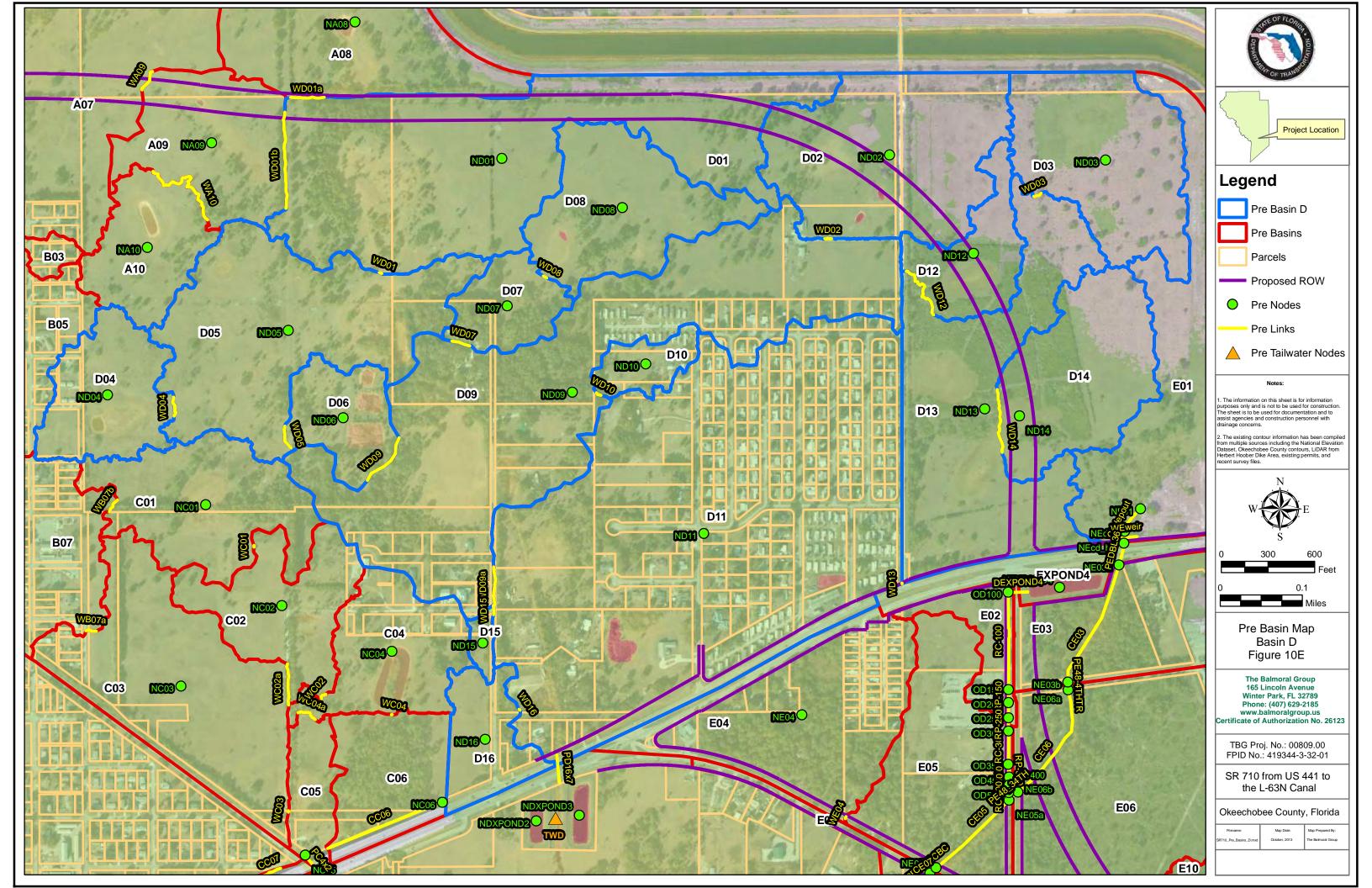


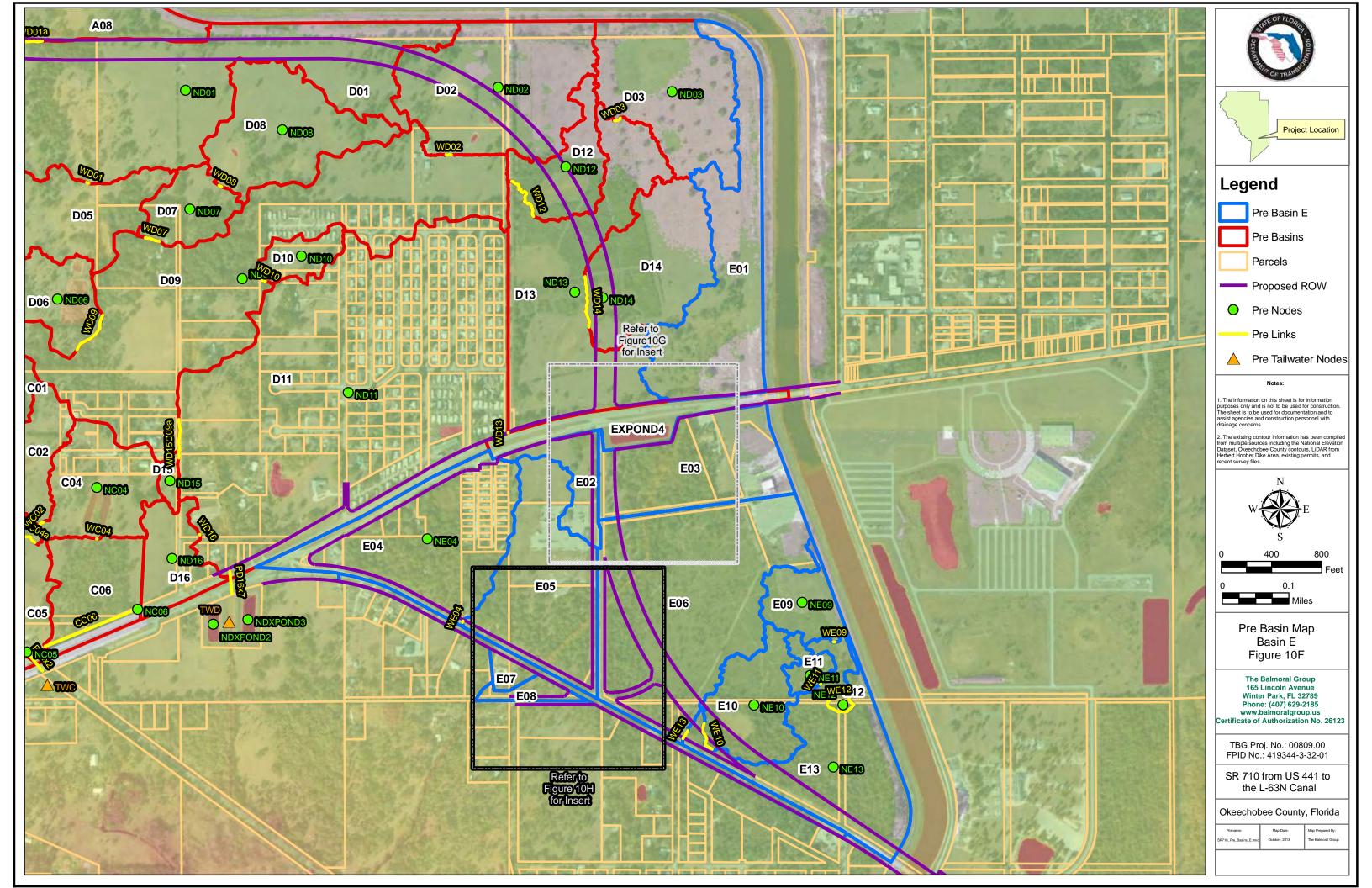


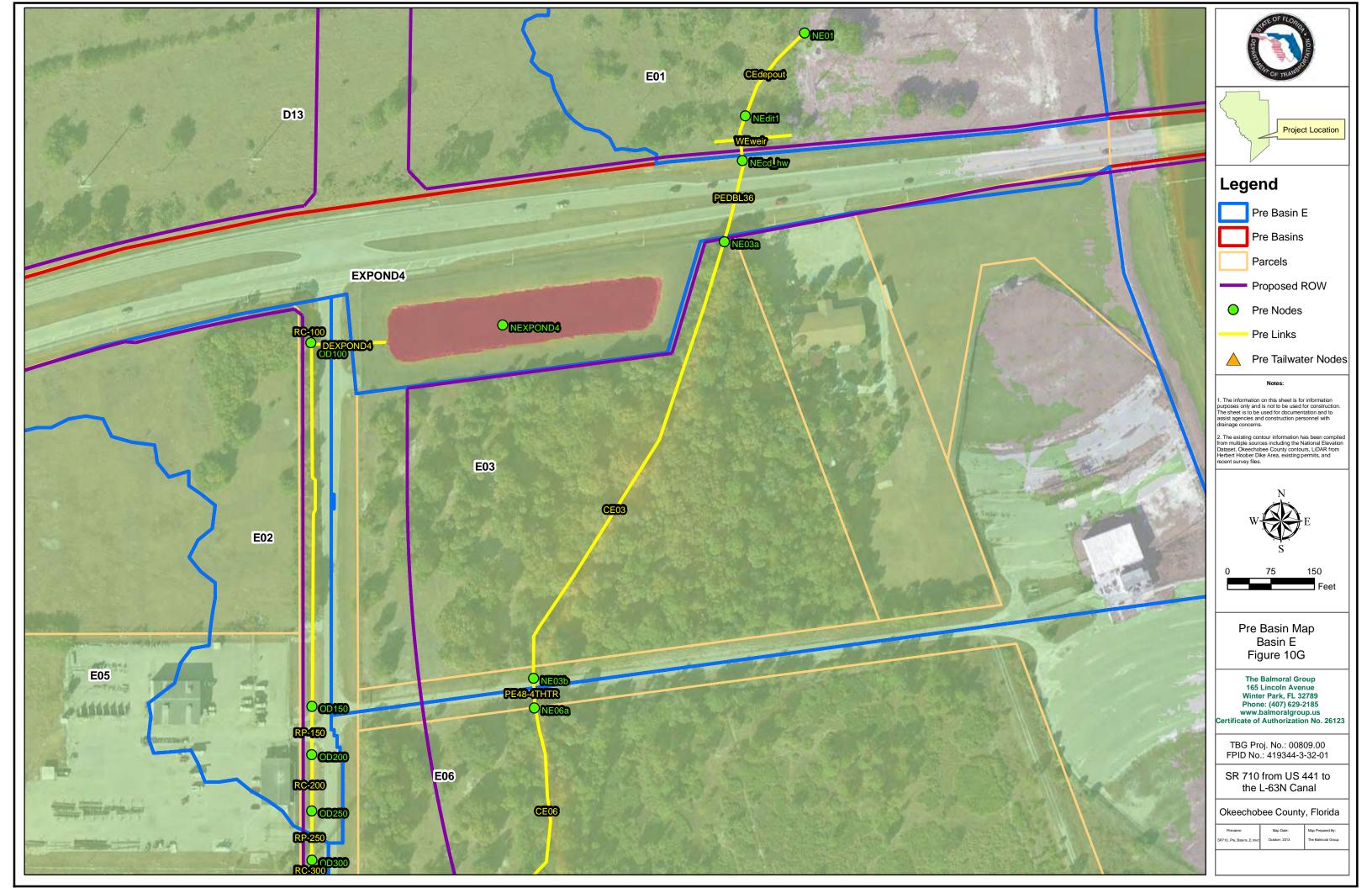


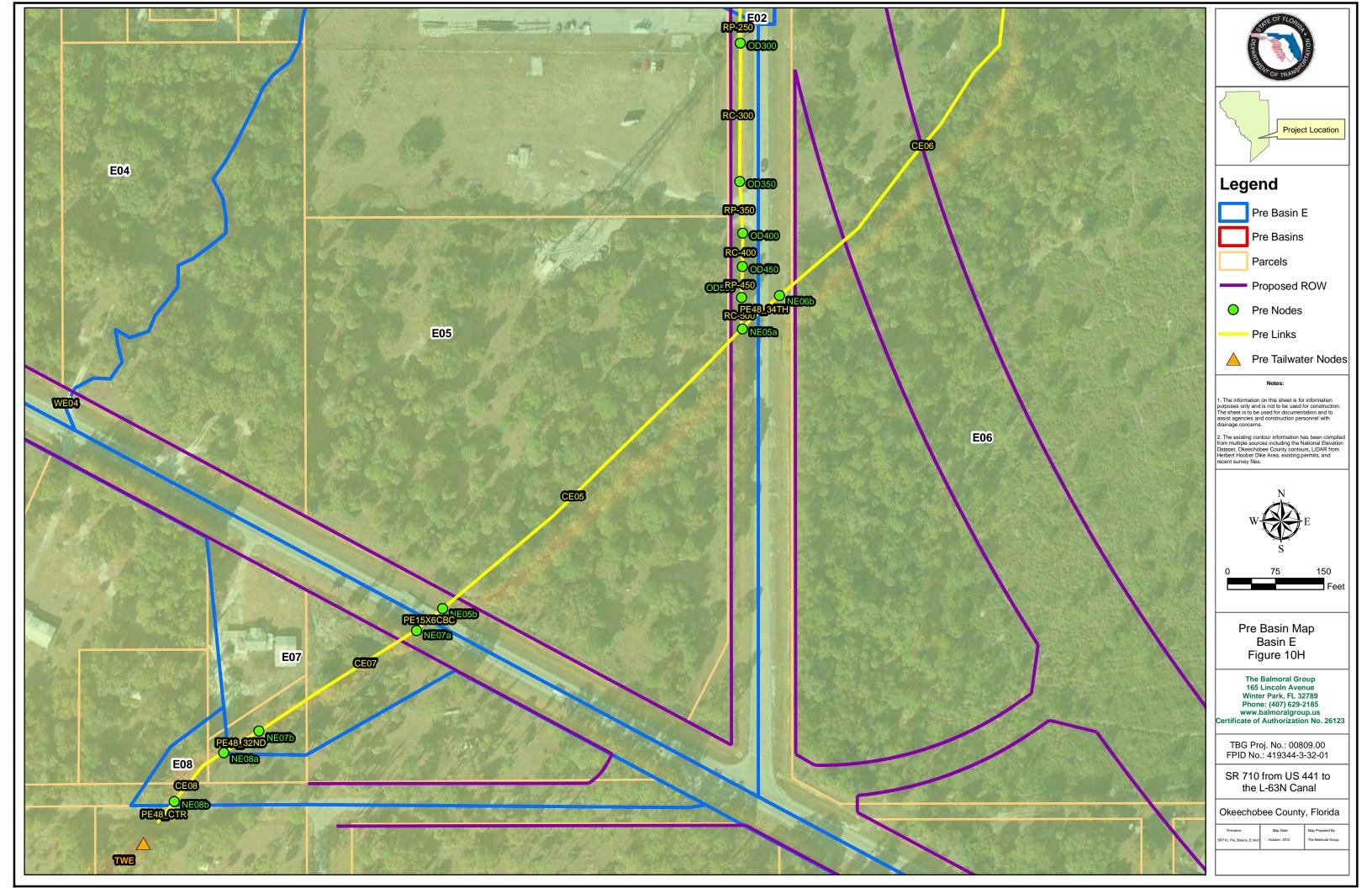


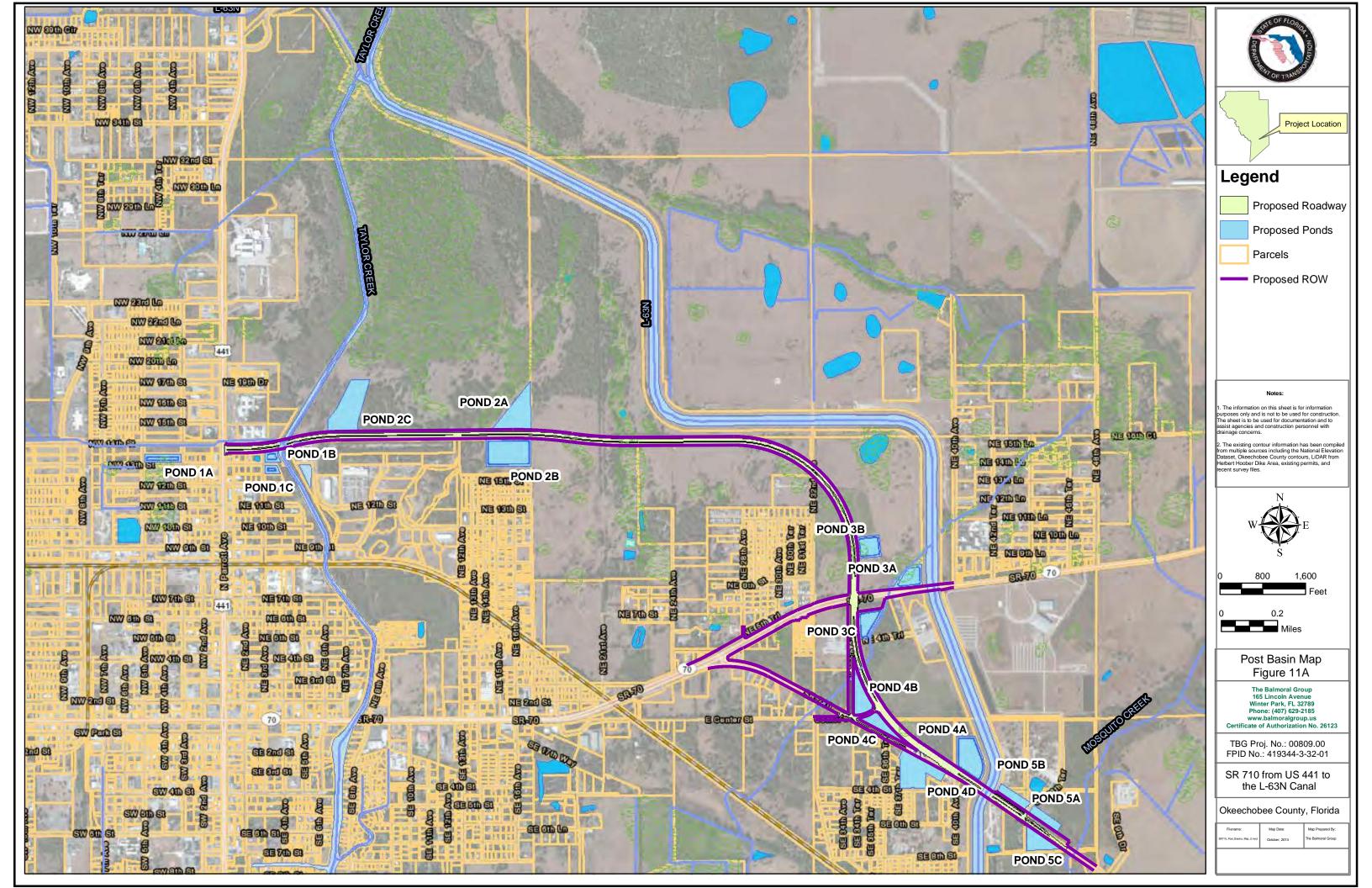


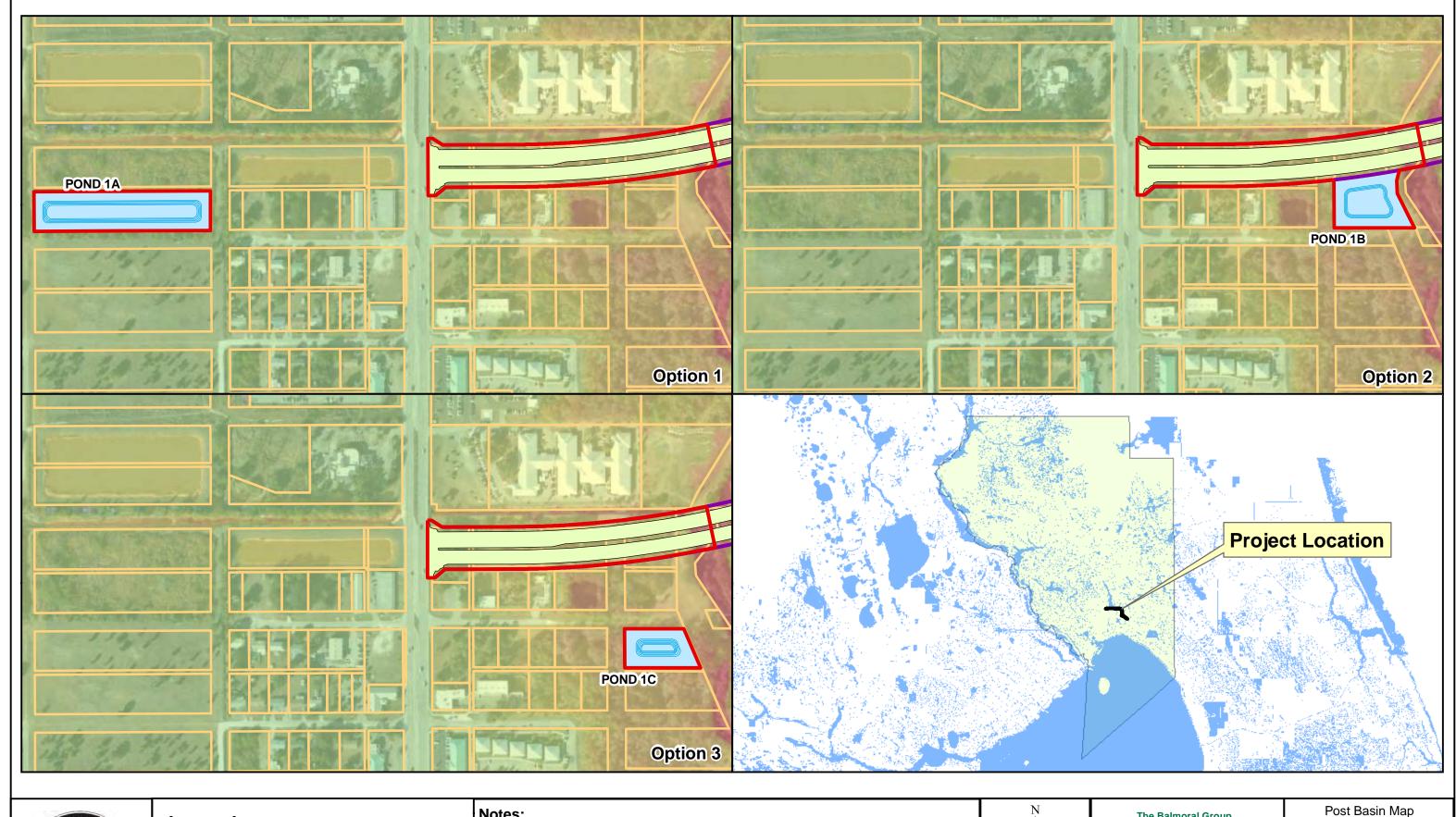














Legend Proposed Roadway Post Basins Proposed Ponds Proposed ROW Parcels

Notes:

1. The information on this sheet is for information purposes only and is not to be used for construction. The sheet is to be used for documentation and to assist agencies and construction personnel with drainage concerns.

2. The existing contour information has been compiled from multiple sources including the National Elevation Dataset,
Okeechobee County contours, LiDAR from
Herbert Hoober Dike Area, existing permits, and recent survey files.



The Balmoral Group 165 Lincoln Avenue Winter Park, FL 32789
Phone: (407) 629-2185
www.balmoralgroup.us
Certificate of Authorization No. 26123

Map Prepared By:

The Balmoral Group

Map Date:

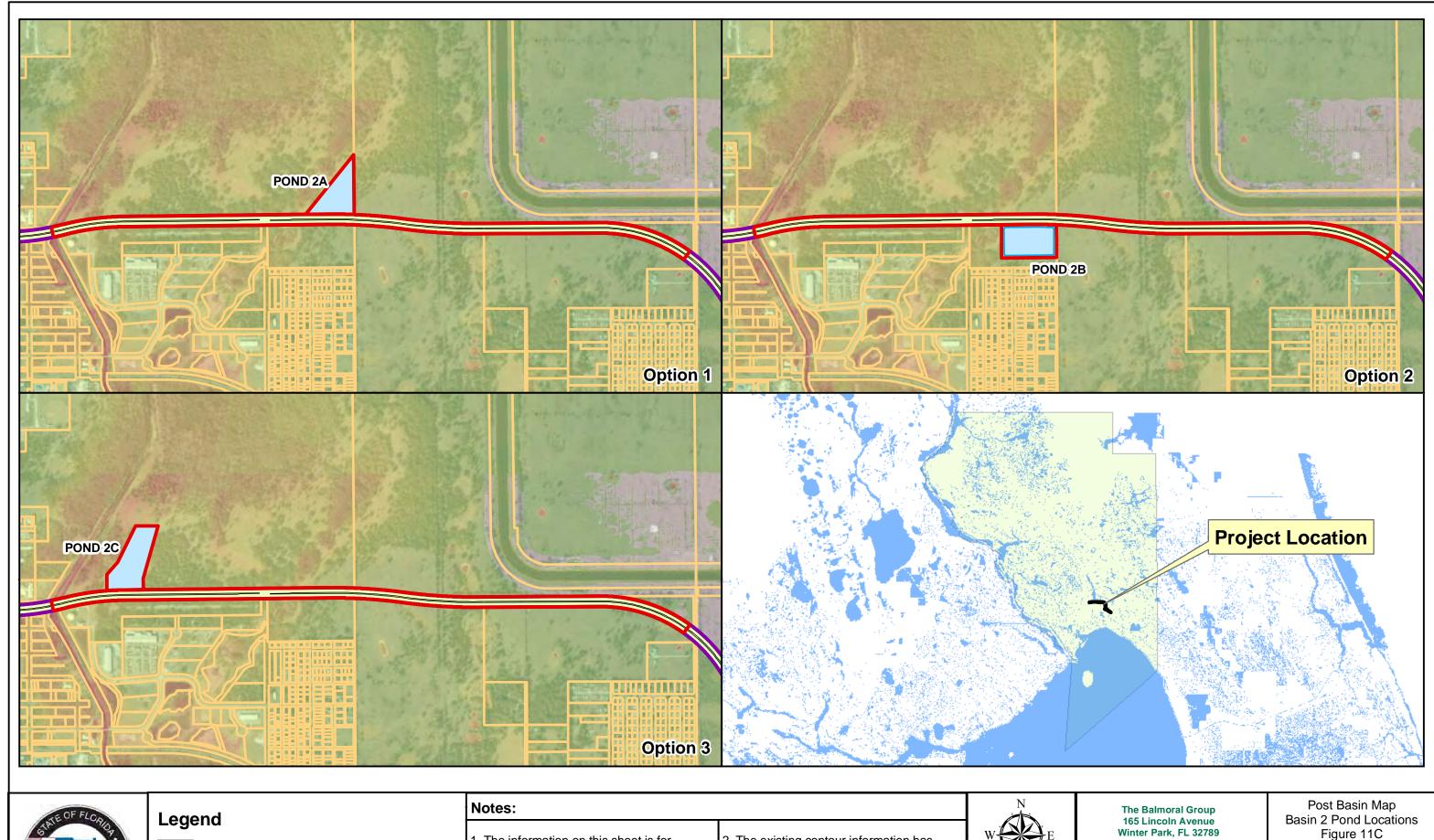
October, 2013

TBG Proj. No.: 00809.00 FPID No.: 419344-3-32-01

Basin 1 Pond Locations

Figure 11B

SR 710 from US 441 to the L-63N Canal





Proposed Roadway —— Post Basins Proposed Ponds Proposed ROW

Parcels

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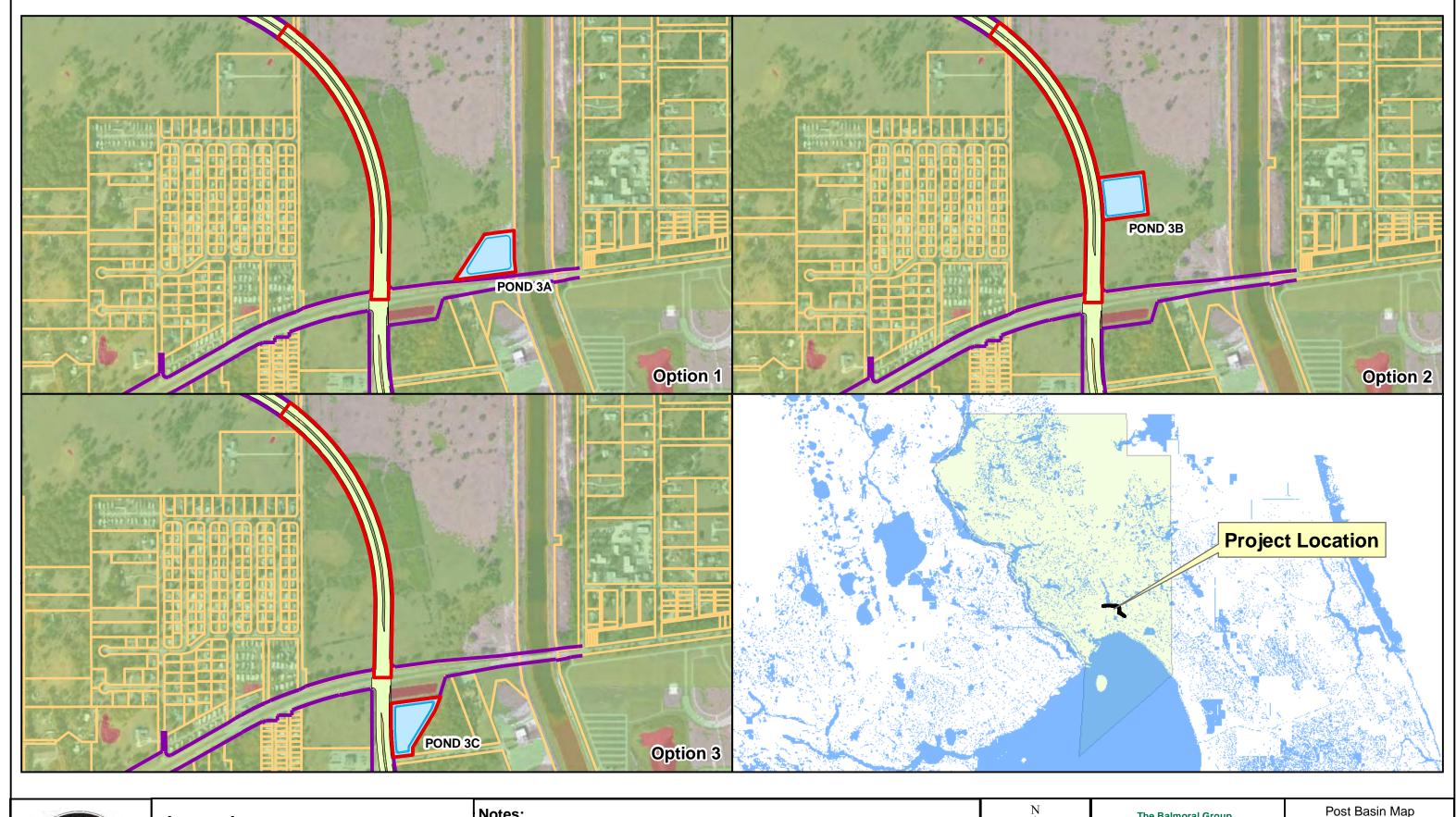
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October, 2013

TBG Proj. No.: 00809.00 FPID No.: 419344-3-32-01 Map Prepared By: Map Date:

The Balmoral Group

SR 710 from US 441 to the L-63N Canal





Legend Proposed Roadway -Post Basins **Parcels** Proposed ROW Proposed Ponds

Notes:

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Map Date:

October, 2013

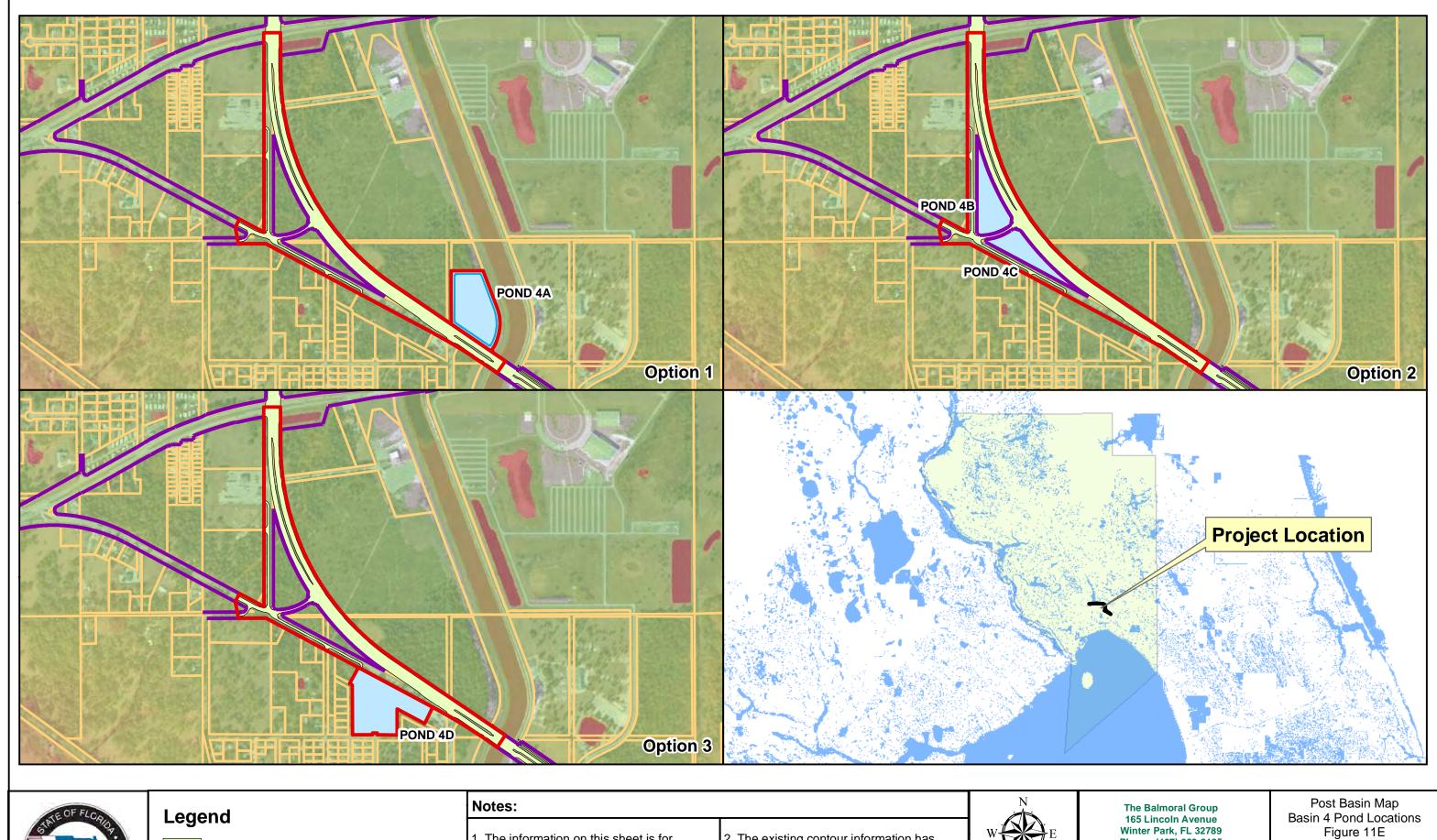
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Basin 3 Pond Locations

Figure 11D

SR 710 from US 441 to the L-63N Canal





Legend Proposed Roadway -Post Basins Proposed Ponds Proposed ROW **Parcels**

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Map Date:

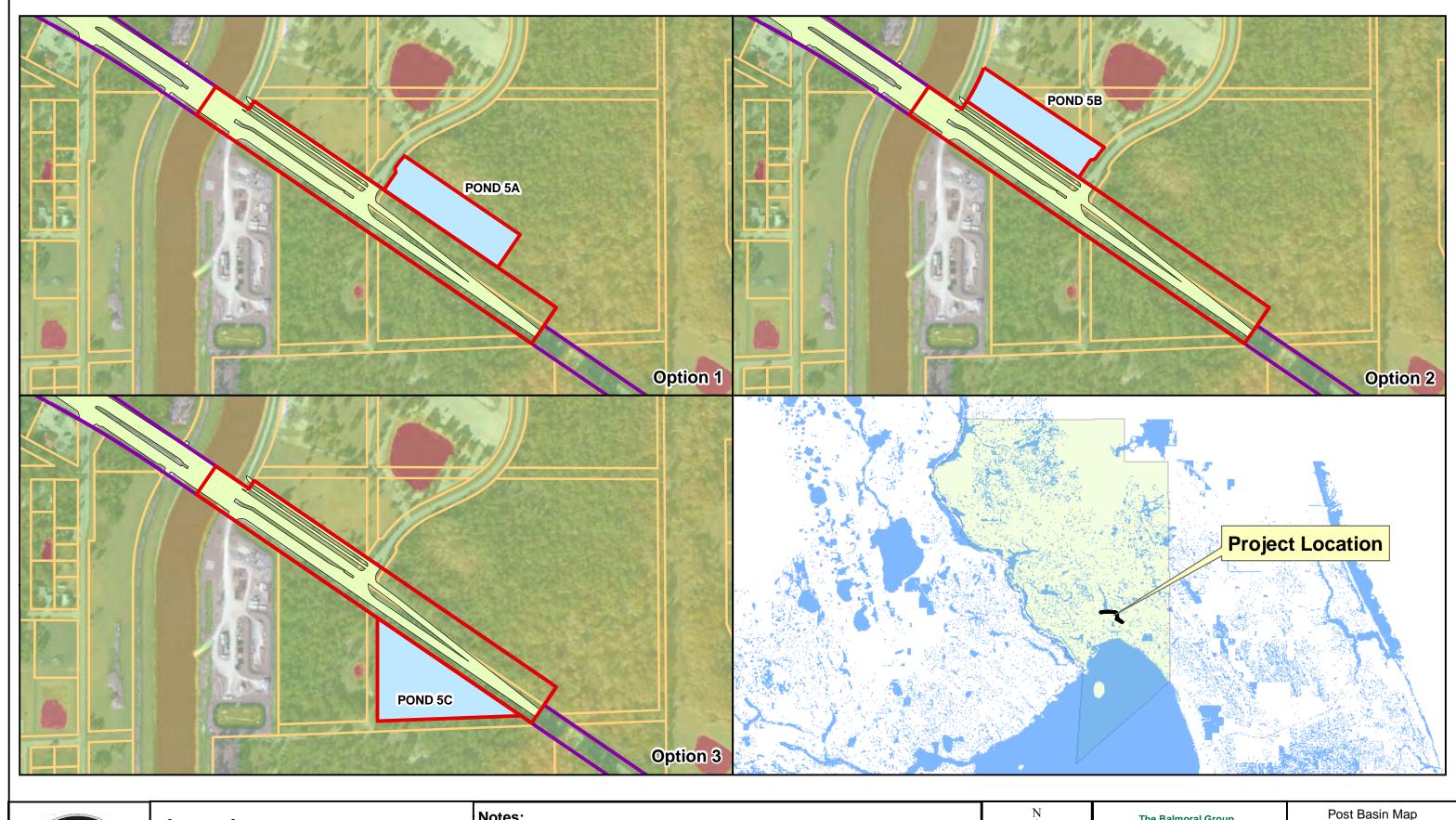
October, 2013

Map Prepared By:

The Balmoral Group

TBG Proj. No.: 00809.00 FPID No.: 419344-3-32-01

SR 710 from US 441 to the L-63N Canal





Legend Proposed Roadway Post Basins Proposed Ponds Proposed ROW **Parcels**

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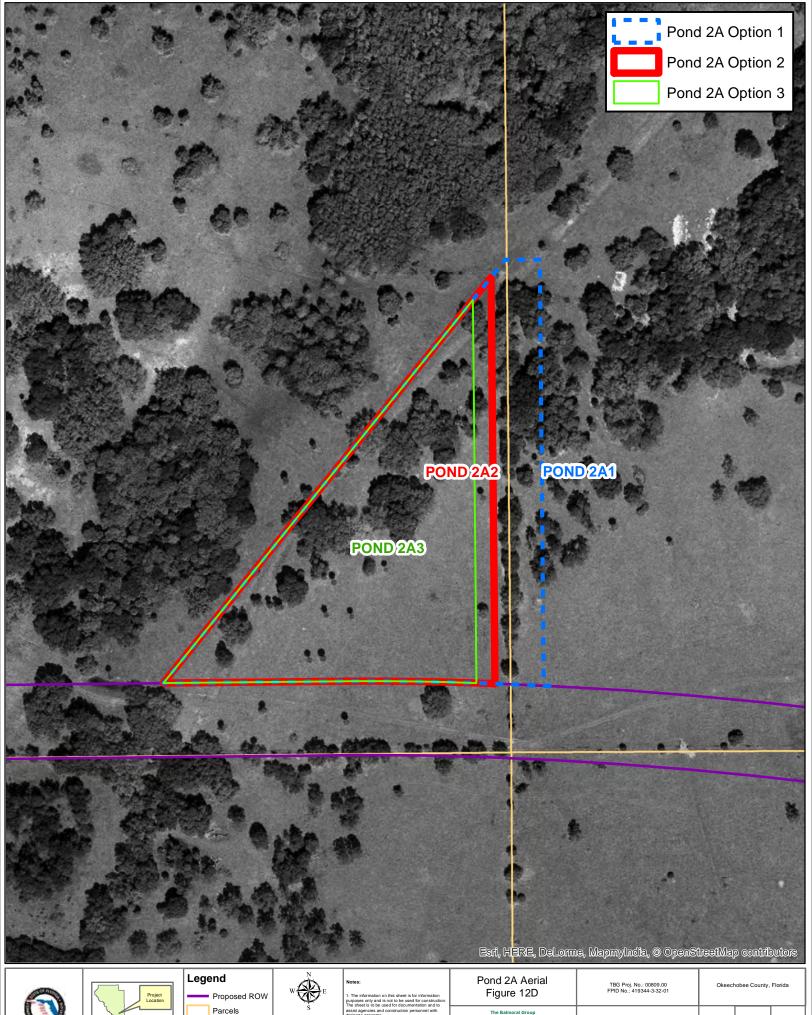
Basin 5 Pond Locations Figure 11F

SR 710 from US 441 to the L-63N Canal









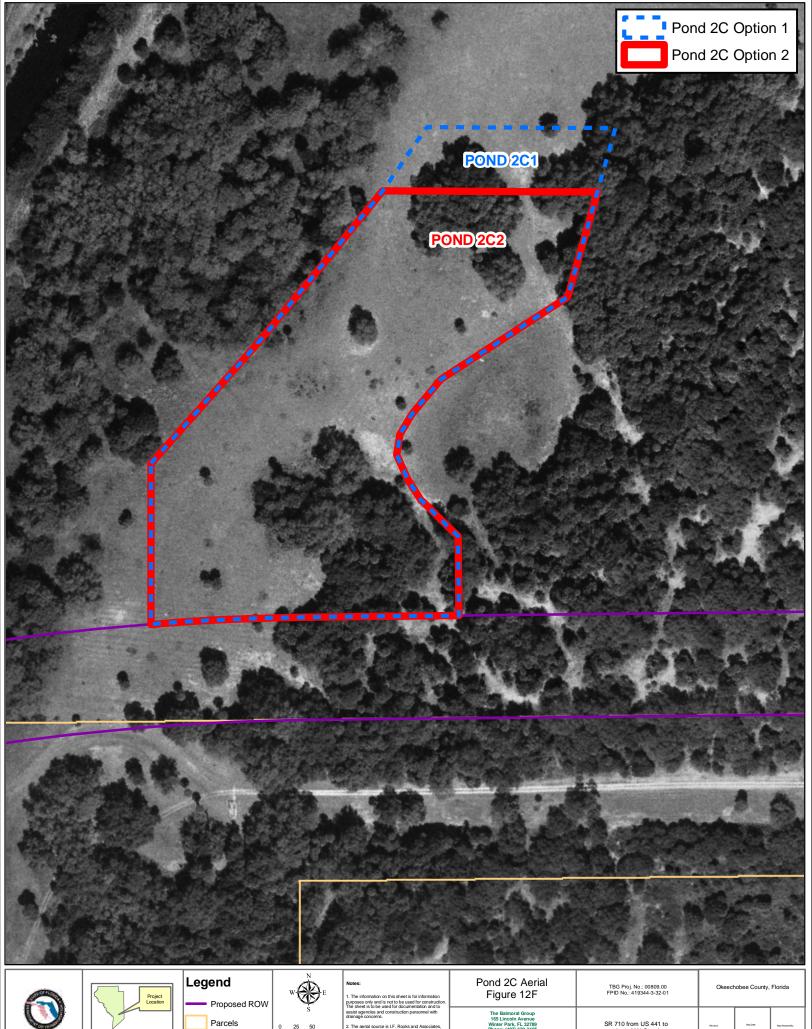










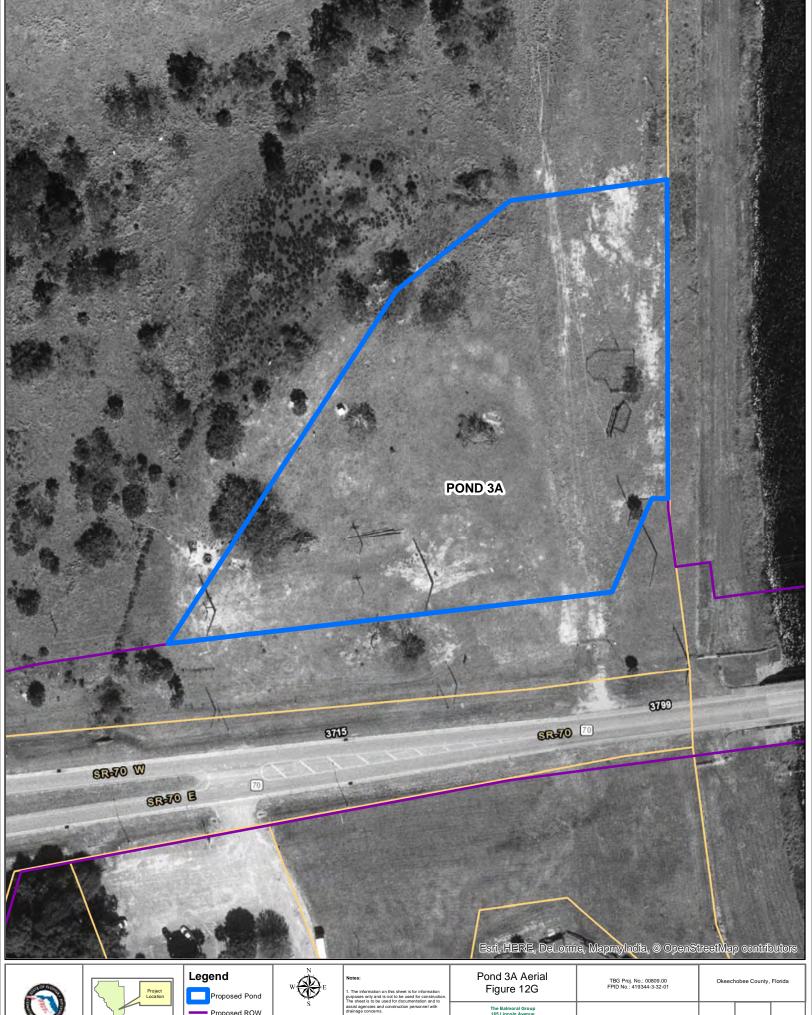








2. The aerial source is I.F. Rooks and Associates, March, 2013.













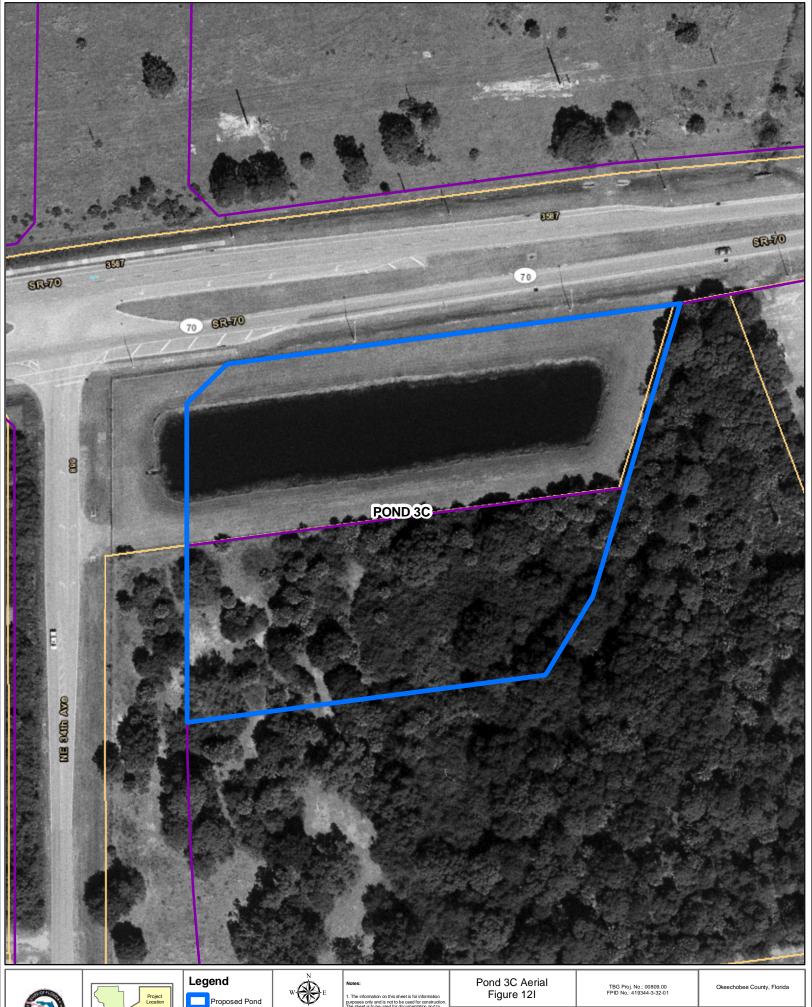






Parcels







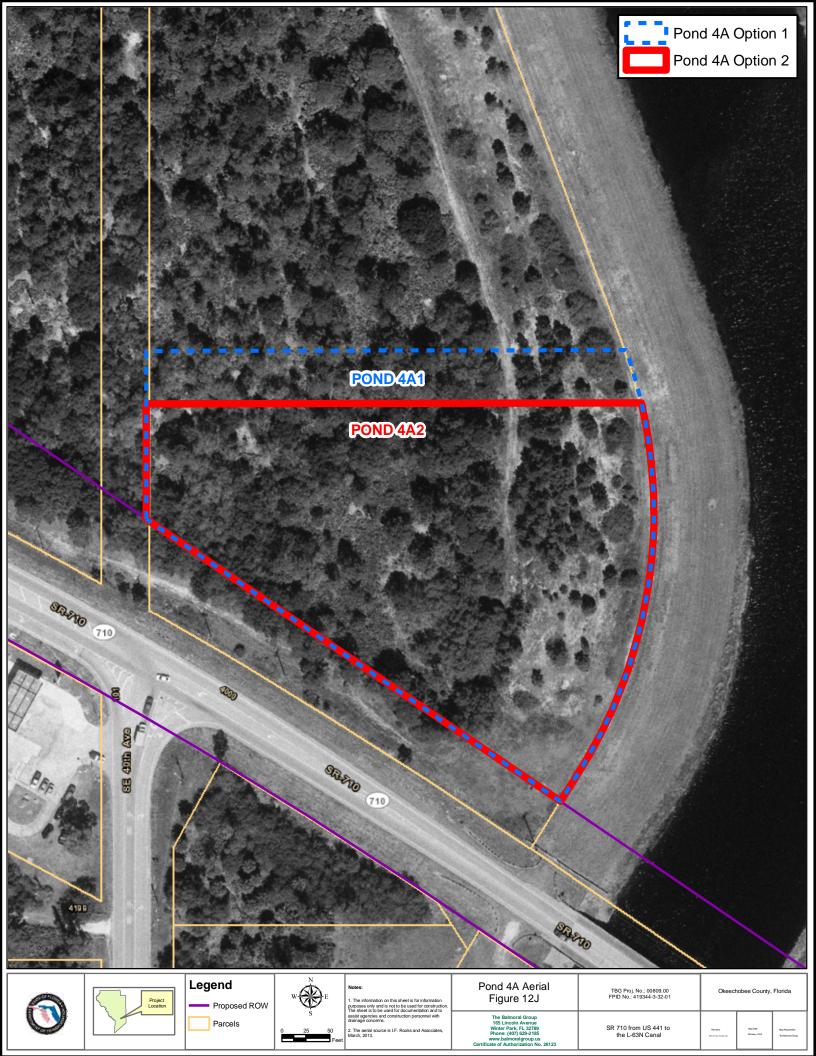


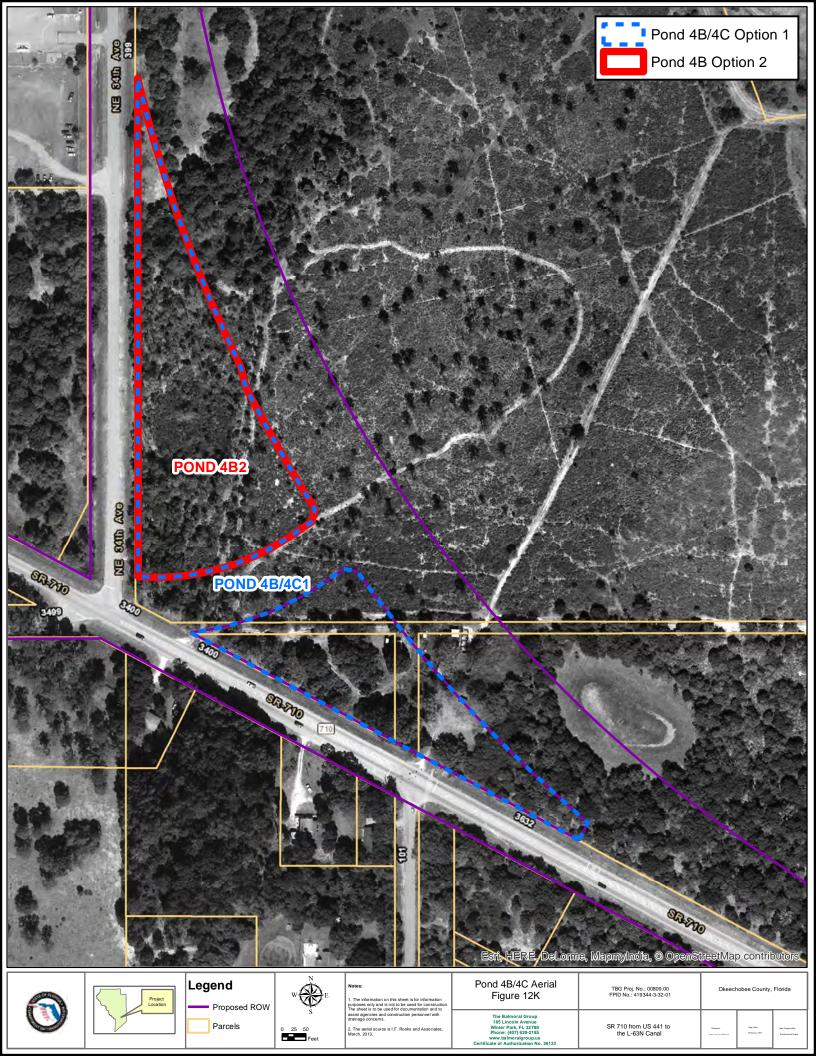


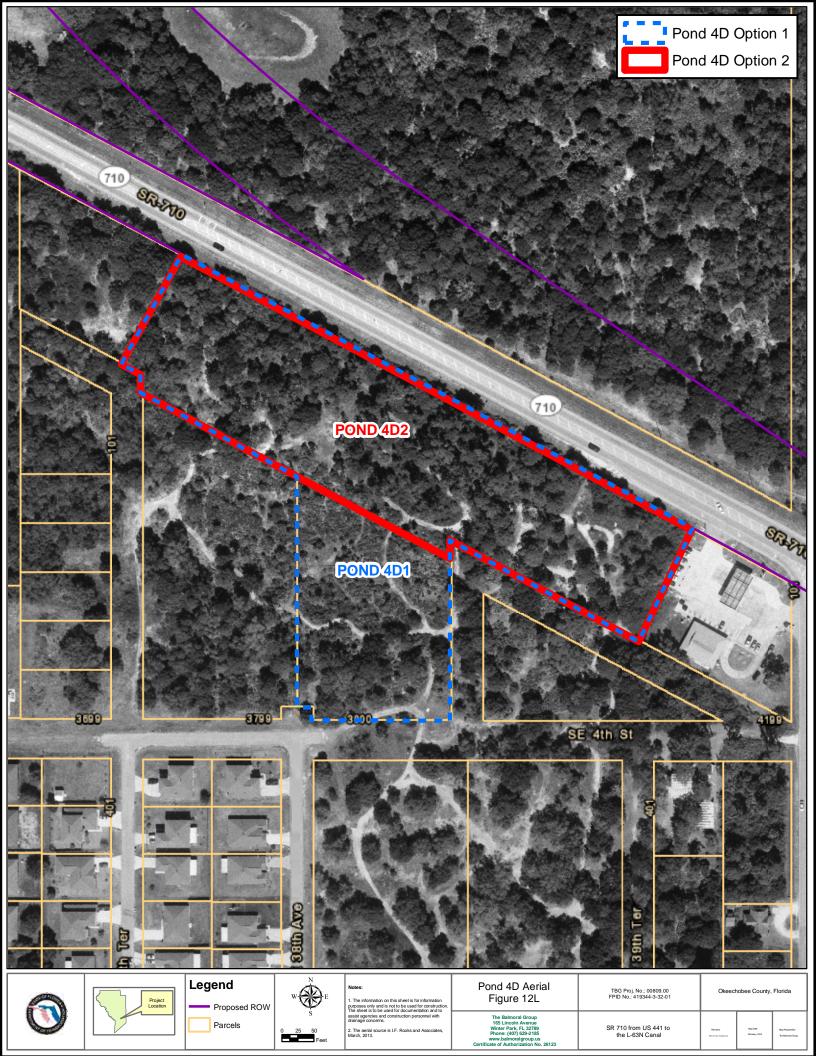
Proposed ROW Parcels

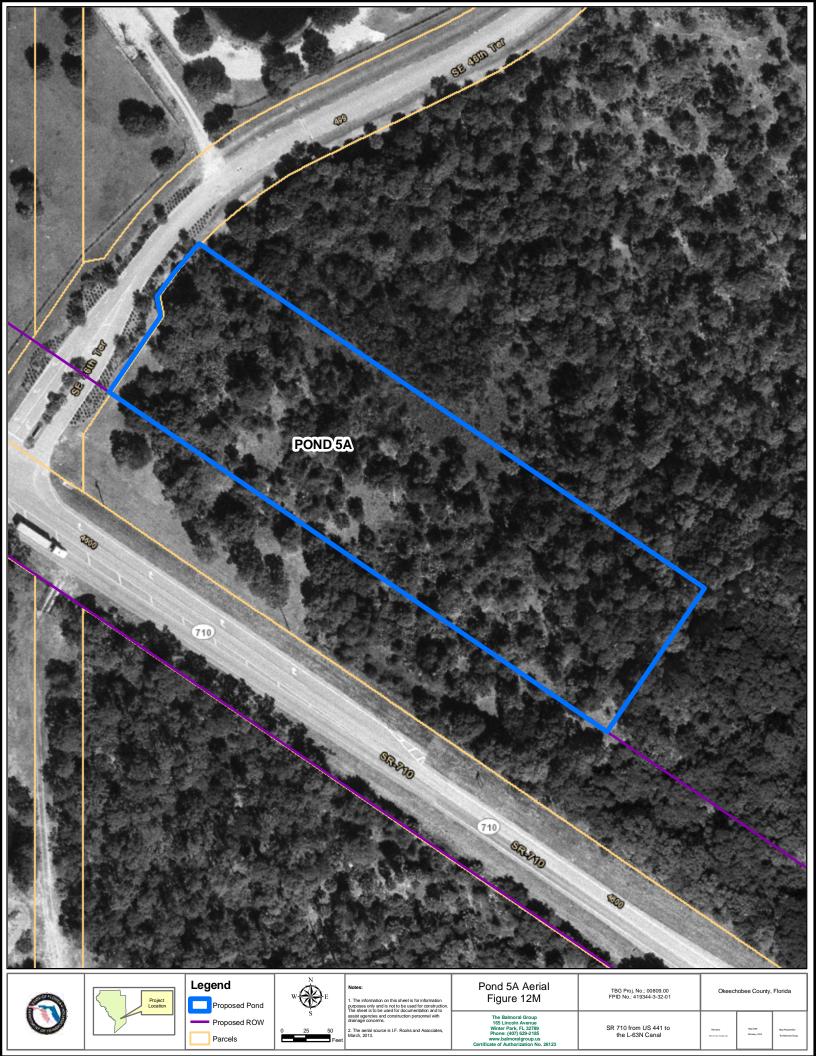


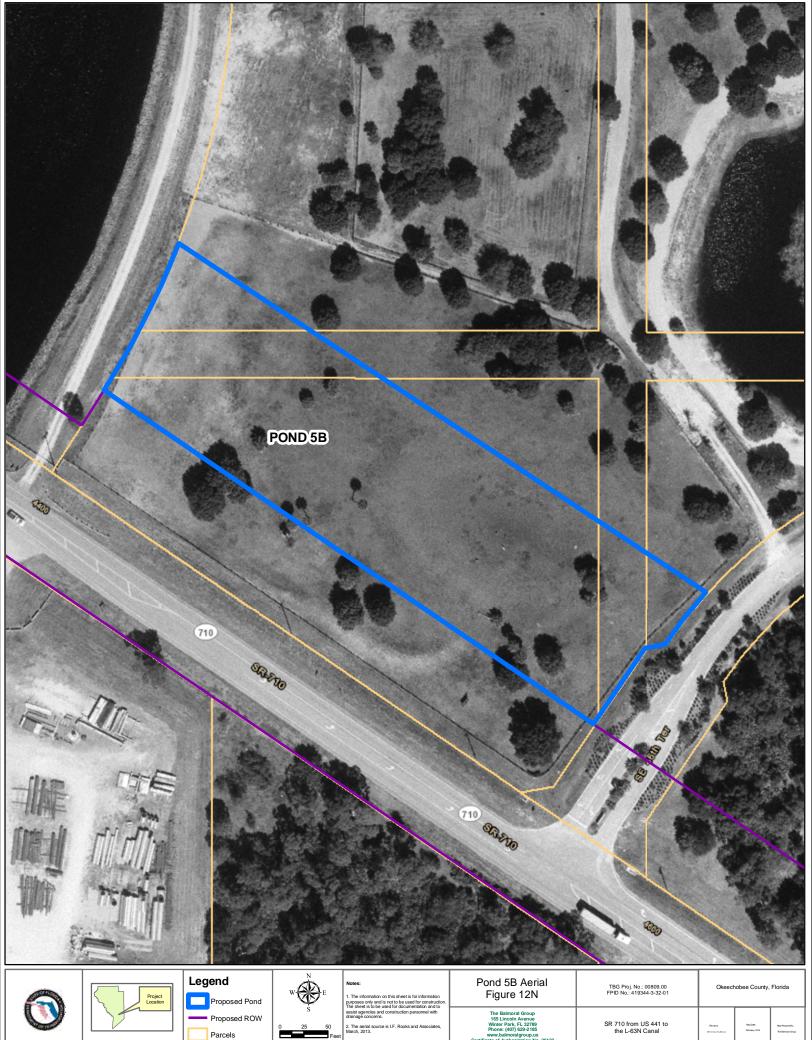
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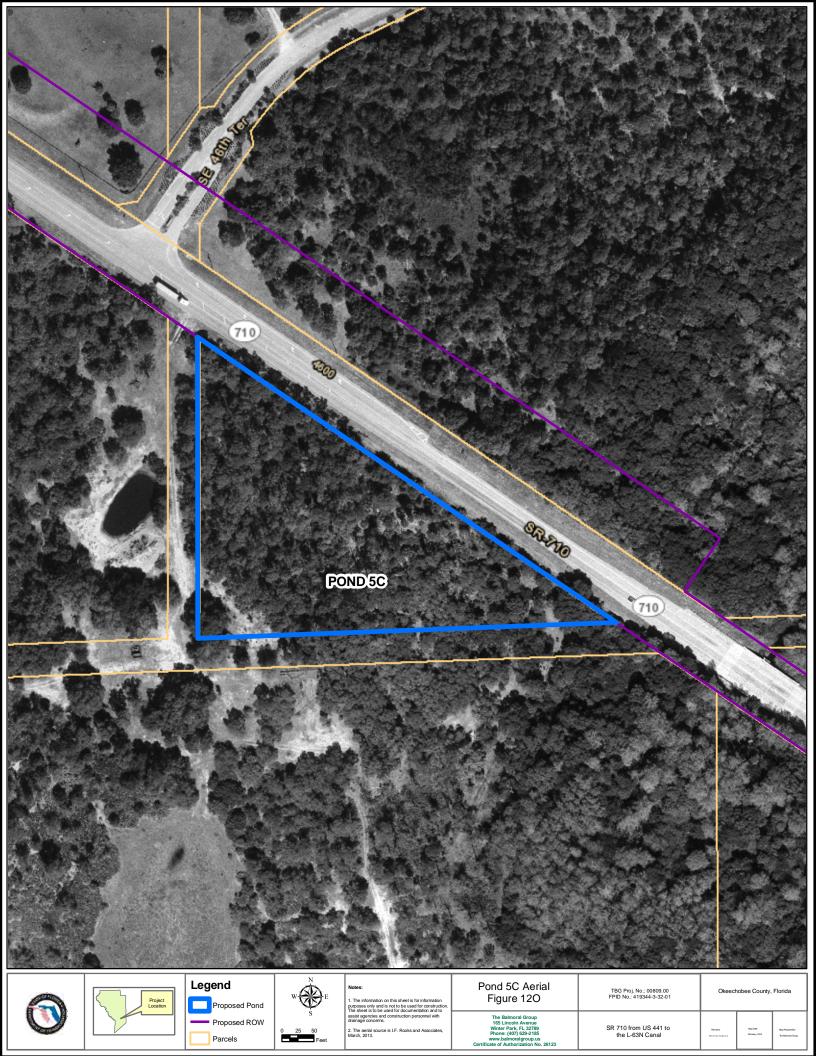


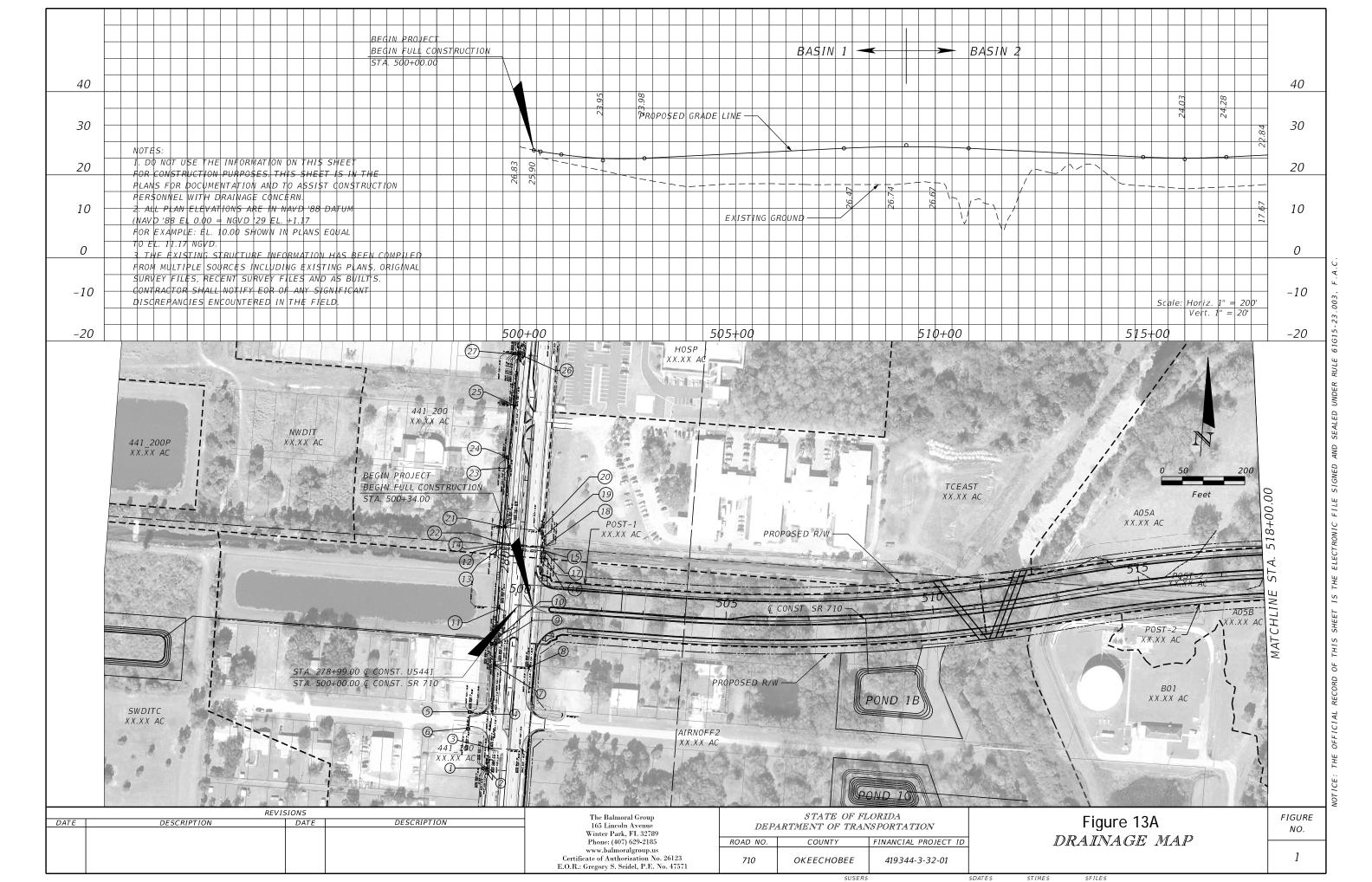


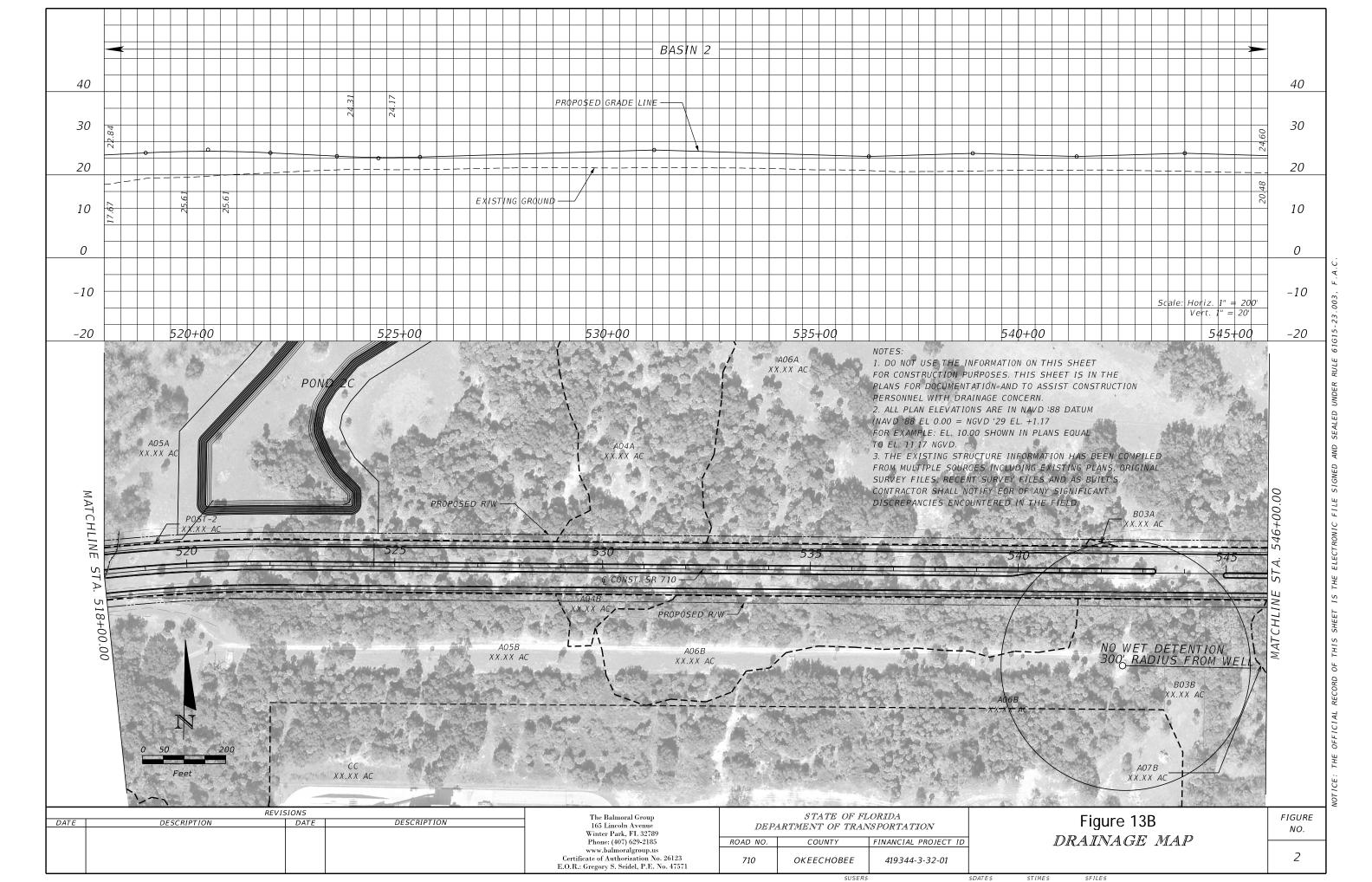


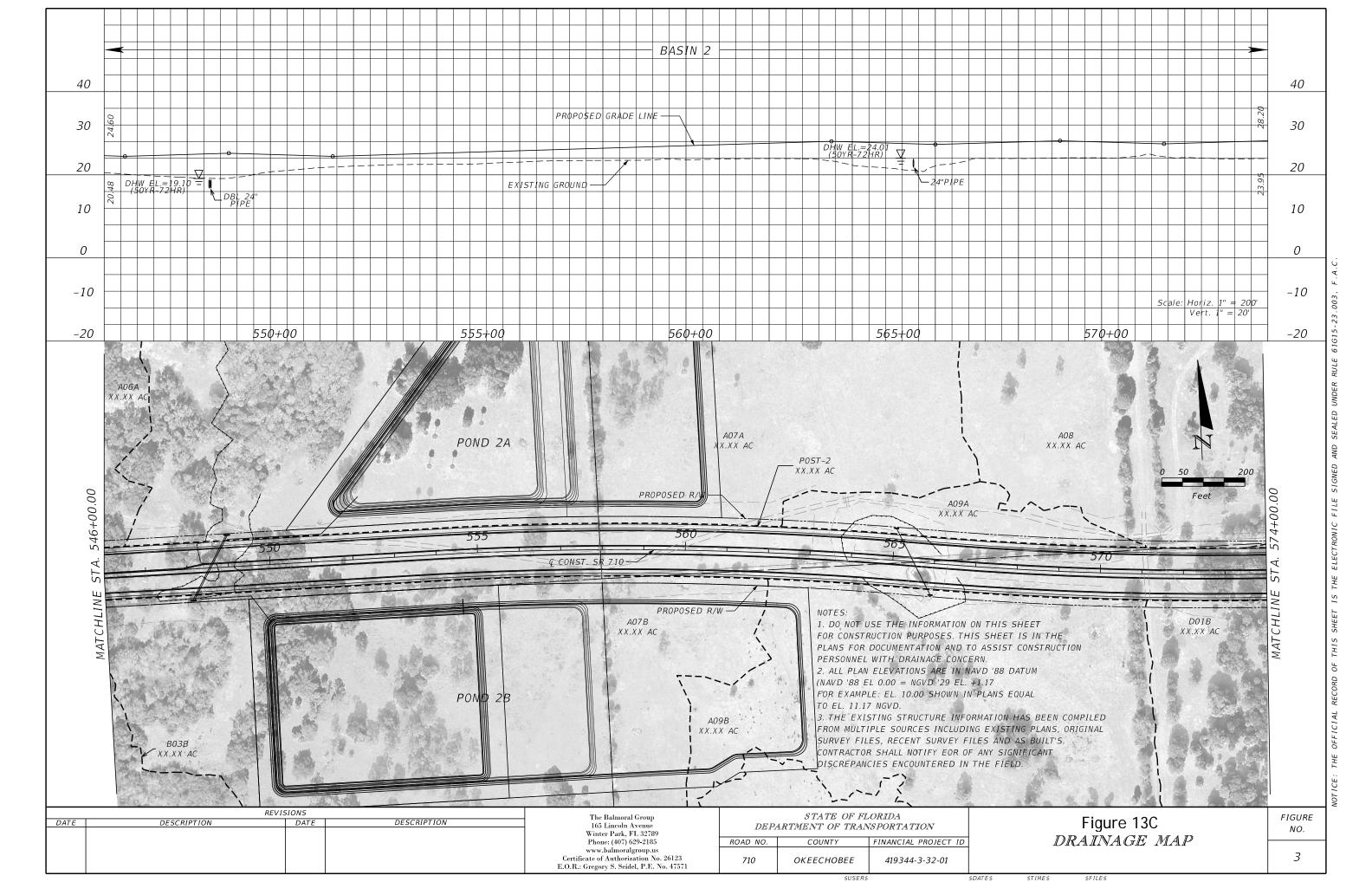


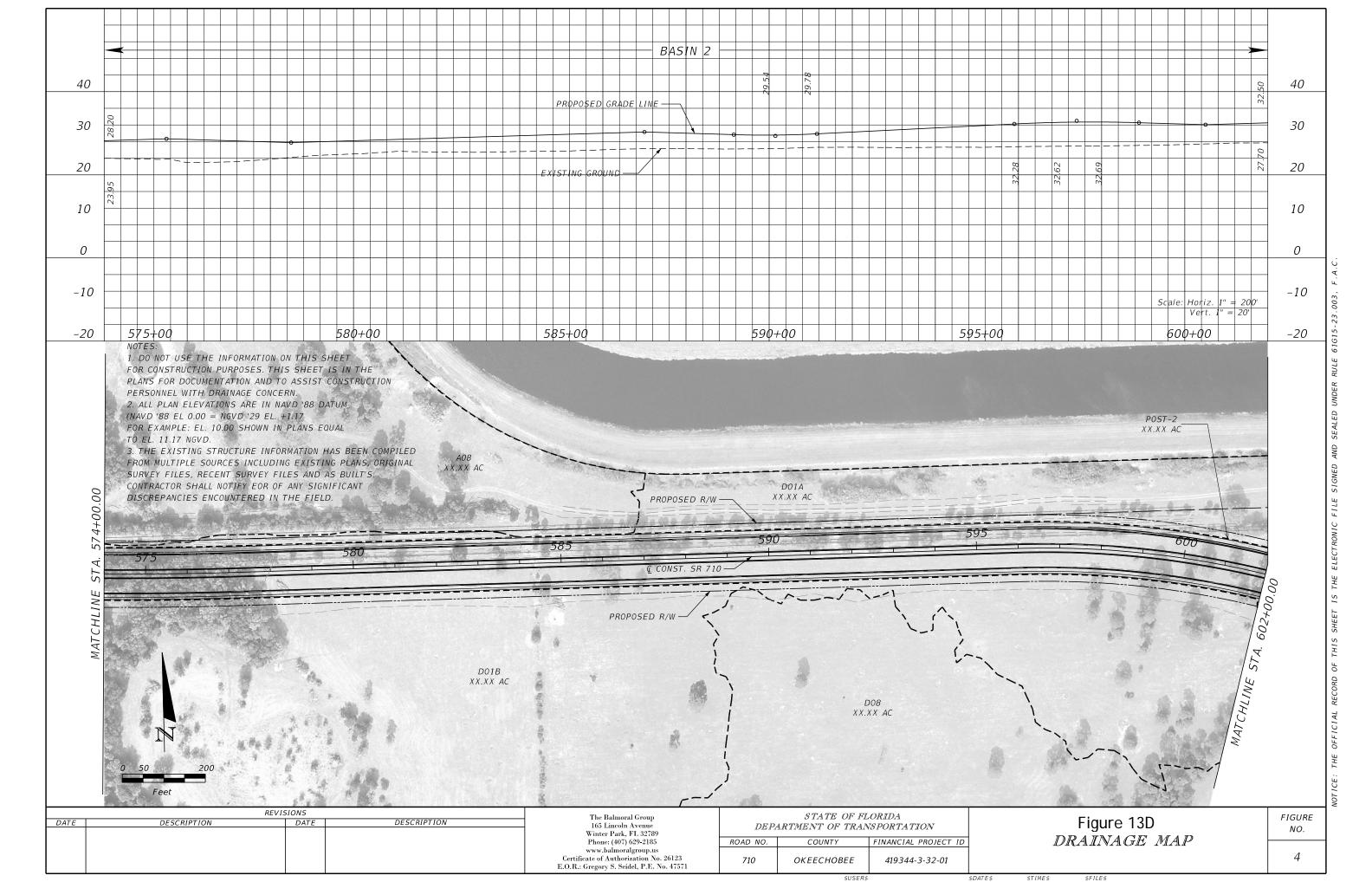
2. The aerial source is I.F. Rooks and Associates, March, 2013.

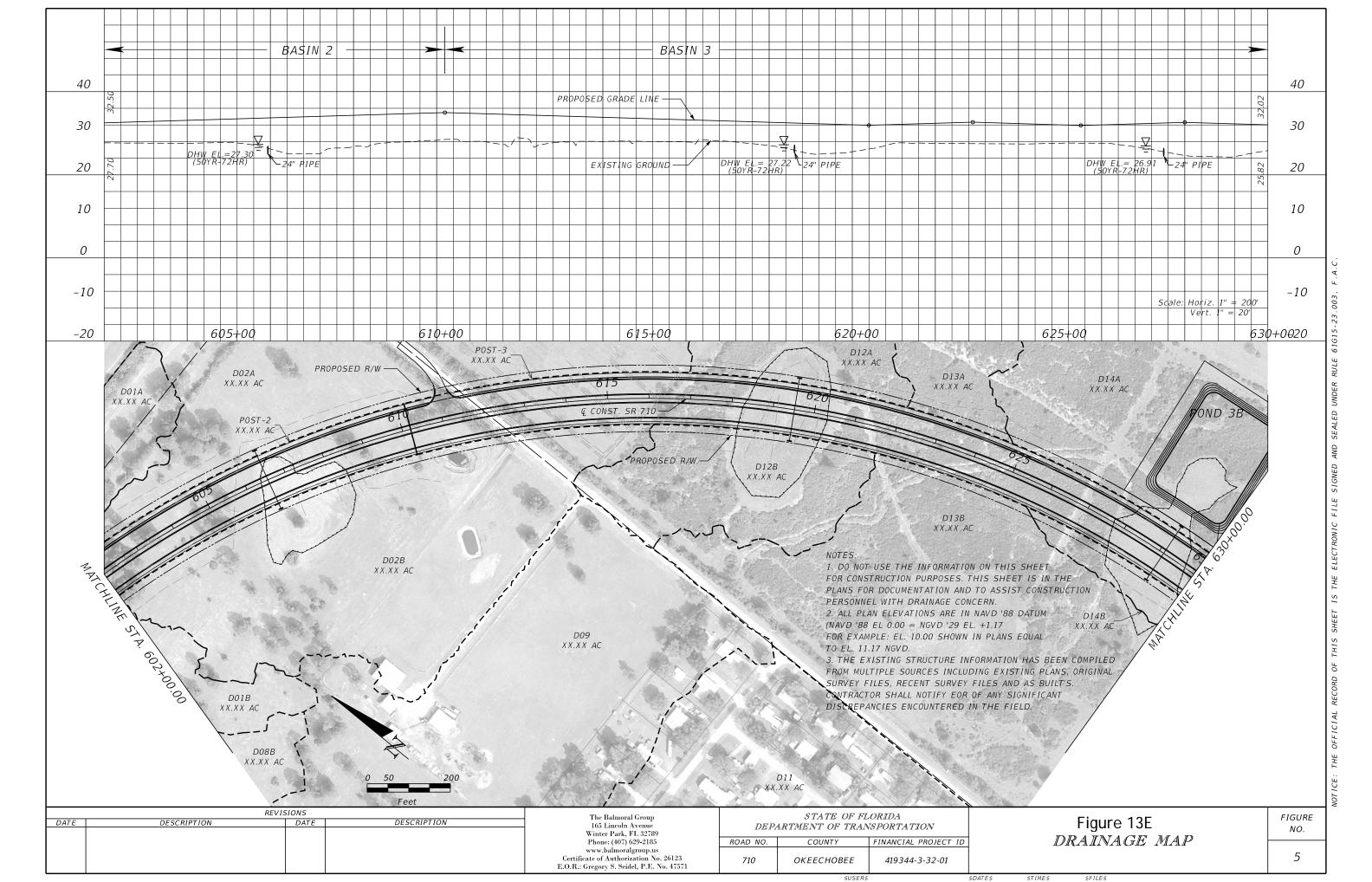


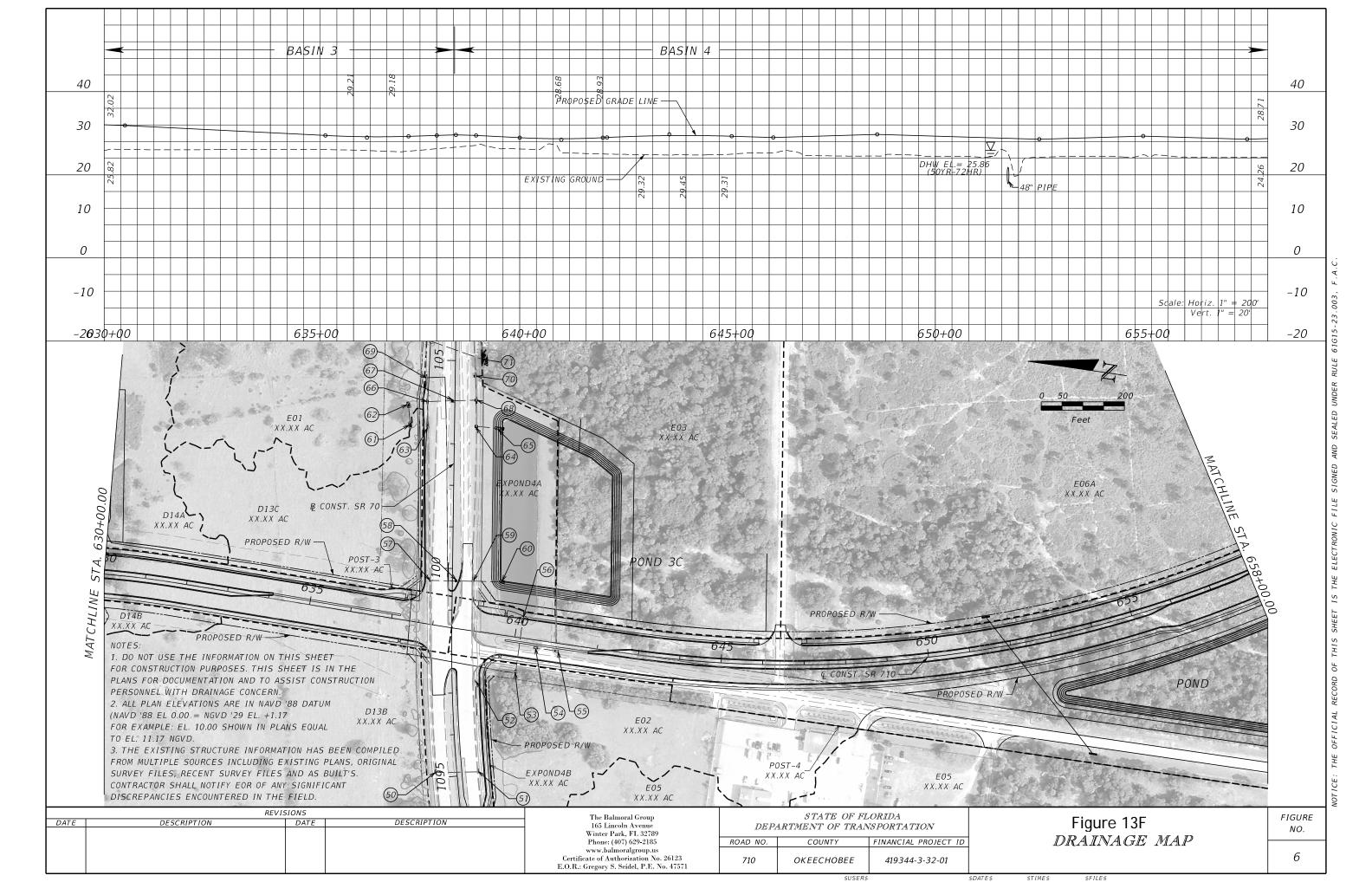


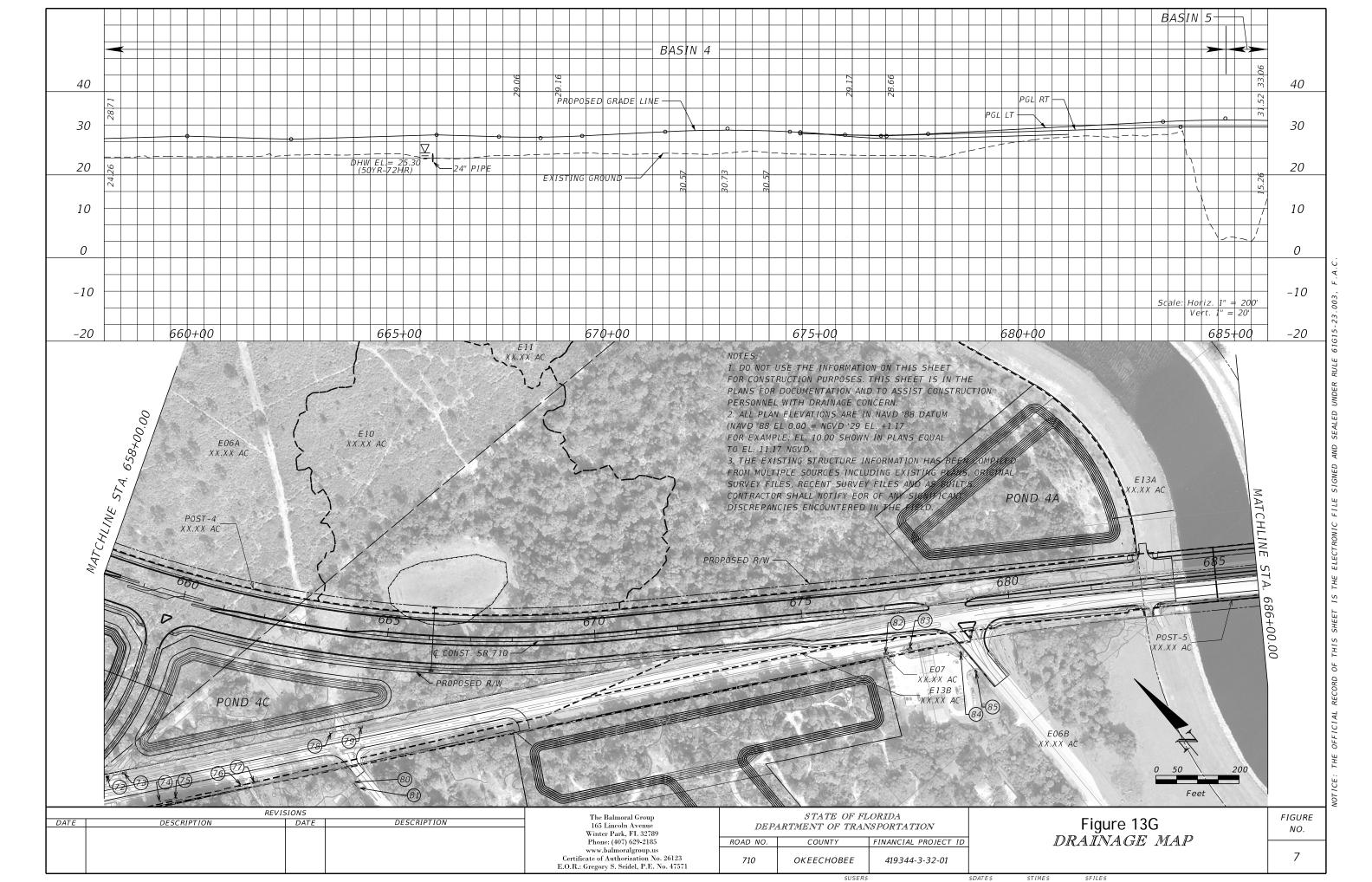


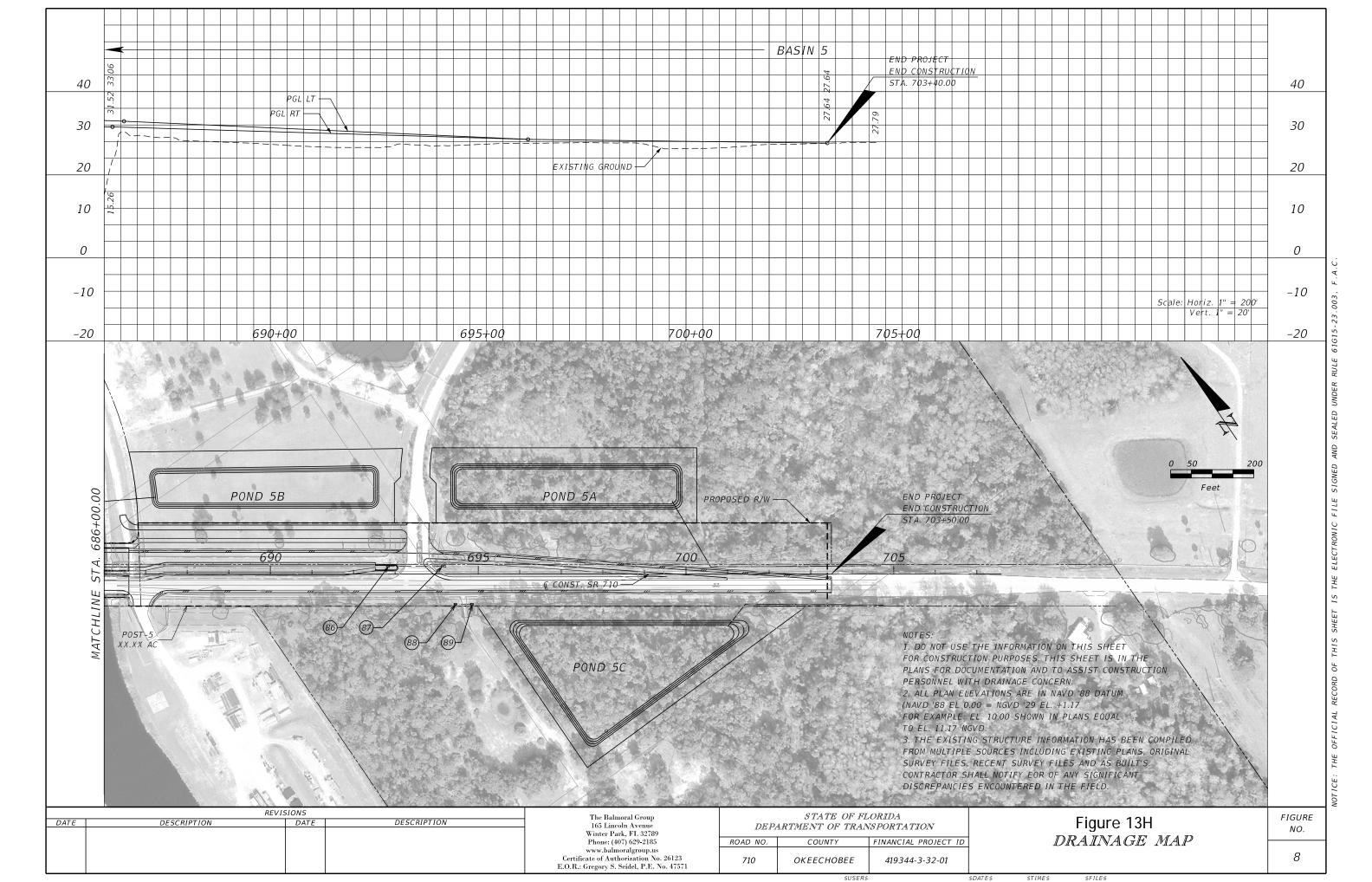












Appendix 2 Geotechnical Information (Ponds)



RICK SCOTT GOVERNOR 801 North Broadway Avenue Bartow, FL 33830 Jim Boxold SECRETARY

Date: November 11, 2016

To: Amy Setchell, P.E. – Senior Project Manager

Florida Department of Transportation – District 1 Project Management

Copies: Alfredo Rodriguez, P.E. – Project Manager

The Wantman Group, Inc.

From: Teresa N. Puckett, P.E., District Geotechnical Engineer (Districts 1 and 7)

By: Keith A. Ellis, P.E., Geotechnical Construction Engineer (Districts 1 and 7)

Subject: Results of Preliminary Geotechnical Exploration for Ponds

(Updated November 2016)

Description: SR 710 from US 441 to L-63 Canal

We have completed a preliminary geotechnical exploration for the ponds for the project in subject. This submittal contains the Report of Auger Borings and the Seasonal High Ground Water (SHGW) table estimates.

If you have any questions, or need further information, please call this office at 863-519-4225.

Report of Seasonal High Groundwater Tables

Financial Project ID: 419344-3-32-01

Project Description: SR 710 from US 441 to L-63 Canal - Geotech Exploration for Pond Alternatives

County: Okeechobee

Boring No.	Date Performed	Estimated Location		Coord	Ground Surface	Boring Depth	Water Table (GNE: Groundwater Not Encountered)		Estimated Seasonal High Groundwater Table		SCS Soil	Indicators	
		Station (ft)	Offset (ft)	Latitude	Longitude	Elevation	(ft)	Depth* (ft)	Elevation (ft)	Depth (ft)	Elevation (ft)	Туре	
PB-1A	10/16/2013	OFFSITE	-	N 27 ° 15 ′ 25.9 ″	W 80 ° 50 ′ 0.2 ″	N.A.	15.0	2.50	N.A.	1.50 ± 0.50	N.A.	To be identified	Stain Line
PB-1B	10/16/2013	509+35	122 RT	N 27 ° 15 ′ 27 ″	W 80 ° 49 ′ 37.2 ″	N.A.	20.0	2.50	N.A.	0.75 ± 0.50	N.A.	To be identified	Root System
PB-1C	10/16/2013	508+60	440 RT	N 27 ° 15 ′ 23.8 ″	W 80 ° 49 ′ 37.4 ″	N.A.	20.0	1.00	N.A.	0.00 ± 0.50	N.A.	To be identified	Ground Surface
PB-3B	10/16/2013	629+25	250 LT	N 27 ° 15 ′ 9.2 ″	W 80 ° 47 ′ 34 ″	N.A.	20.0	+0.20	N.A.	0.50 ± 0.50	N.A.	To be identified	Ground Surface
PB-3A	10/16/2013	630+10	1120 LT	N 27 ° 15 ′ 3.6 ″	W 80 ° 47 ′ 24.6 ″	N.A.	20.0	3.50	N.A.	1.92 ± 0.50	N.A.	To be identified	Root System, Stain Line
PB-3C	10/22/2013	642+30	310 LT	N 27 ° 14 ′ 54.9 ″	W 80 ° 47 ′ 33.6 ″	N.A.	20.0	3.00	N.A.	1.25 ± 0.50	N.A.	To be identified	Root System
PB-4BC	10/22/2013	659+75	410 RT	N 27 ° 14 ′ 37.5 ″	W 80 ° 47 ′ 35.1 ″	N.A.	20.0	2.50	N.A.	1.25 ± 0.50	N.A.	To be identified	Root System
PB-4D	10/22/2013	671+75	400 RT	N 27 ° 14 ′ 27.9 ″	W 80 ° 47 ′ 23.7 ″	N.A.	20.0	3.00	N.A.	1.17 ± 0.50	N.A.	To be identified	Root System
PB-5B	10/22/2013	688+50	210 LT	N 27 ° 14 ′ 23.7 ″	W 80 ° 47 ′ 4.9 ″	N.A.	20.0	2.00	N.A.	0.50 ± 0.50	N.A.	To be identified	Root System
PB-5A	10/22/2013	696+10	190 LT	N 27 ° 14 ′ 19.4 ″	W 80 ° 46 ′ 58.2 ″	N.A.	20.0	2.00	N.A.	0.75 ± 0.50	N.A.	To be identified	Root System
PB-2A	10/22/2013	554+60	230 LT	N 27 ° 15 ′ 32.7 ″	W 80 ° 48 ′ 47.1 ″	N.A.	20.0	2.00	N.A.	0.67 ± 0.50	N.A.	To be identified	Root System
PB-2B	10/23/2013	553+50	280 RT	N 27 ° 15 ′ 27.7 ″	W 80 ° 48 ′ 48.2 ″	N.A.	20.0	3.00	N.A.	0.75 ± 0.50	N.A.	To be identified	Root System
PB-2C	10/23/2013	523+10	350 LT	N 27 ° 15 ′ 33.6 ″	W 80 ° 49 ′ 22.1 ″	N.A.	20.0	3.50	N.A.	0.67 ± 0.50	N.A.	To be identified	Root System
PB-4A	10/23/2013	683+15	100 LT	N 27 ° 14 ′ 25.9 ″	W 80 ° 47 ′ 10.7 ″	N.A.	20.0	4.50	N.A.	1.08 ± 0.50	N.A.	To be identified	Root System, Stain Line
PB-4A	10/23/2013	680+40	75 LT	N 27 ° 14 ′ 27.3 ″	W 80 ° 47 ′ 13.4 ″	N.A.	20.0	3.00	N.A.	1.08 ± 0.50	N.A.	To be identified	Root System, Stain Line
PB-5C	10/23/2013	698+75	220 RT	N 27 ° 14 ′ 14.6 ″	W 80 ° 46 ′ 58.4 ″	N.A.	20.0	2.50	N.A.	1.00 ± 0.50	N.A.	To be identified	Root System
PB-4B	11/2/2016	659+06	384 RT	N 27 ° 14 ′ 38.8 ″	W 80 ° 47 ′ 35.6 ″	23.04	20.0	2.00	21.04	2.00 ± 0.50	21.04 ± 0.50	To be identified	Stain Line

Notes:

N.A.: Not Available at the time of this submittal.

Date Prepared: 11/10/2016

^{*: &}quot;+" in the Water Table Depth represents standing water.

Report of Auger Borings Date Prepared: 10/31/2013

Financial Project ID: 419344-3-32-01

Project Description: SR 710 from US 441 to L-63 Canal - Geotech Exploration for Pond Alt.s Prepared for: Keith Ellis, FDOT D1

County: Okeechobee Field Exploration Dates: 10/16/2013 - 11/02/2016

Auger Boring / SHWT	Approx. Station B/L Survey SR 710	Approx. Offset from B/L Survey (ft)	Date Performed		th (ft) n - To	•	Stratum No.	Soil Description	AASHTO Classific.	Measured Groundwater (ft)
PB-1A	OFFSITE	OFFSITE	10/16/13	0.0 10.0		10.0 15.0	N.A. N.A.	Gray and brown fine SAND w/ some rock Gray, tan, and brown fine SAND	N.A. N.A.	2.5
PB-1B	509+35	122.0 RT	10/16/13	0.0		10.0 20.0	N.A. N.A.	Gray and brown fine SAND w/ some rock Dark brown fine SAND w/ organics	N.A. N.A.	2.5
PB-1C	508+60	440. RT	10/16/13	2.0		2.0 15.0 20.0	N.A. N.A. N.A.	Gray and Orange sandy CLAY Gray and brown fine SAND w/ some rock Dark brown organic CLAY	N.A. N.A. N.A.	1.0
PB-2A	554+60	230.0 LT	10/22/13	0.0		20.0	N.A.	Gray and brown fine SAND w/ some rock	N.A.	2.0
PB-2B	553+50	280.0 RT	10/23/13	0.0	-	20.0	N.A.	Gray and brown fine SAND w/ some rock	N.A.	3.0
PB-2C	523+10	350.0 LT	10/23/13	0.0	-	20.0	N.A.	Gray and brown fine SAND w/ some rock	N.A.	3.5
PB-3A	630+10	1118.0 LT	10/16/13	0.0		18.0 20.0	N.A. N.A.	Gray and brown fine SAND w/ some rock Gray, tan, and brown fine SAND	N.A. N.A.	3.5
PB-3B	629+25	250.0 LT	10/16/13	10.0		10.0 15.0 20.0	N.A. N.A. N.A.	Gray and brown fine SAND w/ some rock Gray, tan, and brown fine SAND Light Gray clayey SAND with rock	N.A. N.A. N.A.	0.2
PB-3C	642+30	310.0 LT	10/22/13	0.0	-	20.0	N.A.	Gray and brown fine SAND w/ some rock	N.A.	3.0
PB-4A	680+40	75.0 LT	1/23/13	0.0	-	20.0	N.A.	Gray and brown fine SAND w/ some rock	N.A.	3.0
PB-4A	683+15	100.0 LT	1/23/13	0.0	-	20.0	N.A.	Gray and brown fine SAND w/ some rock	N.A.	4.5
PB-4BC	659+75	410.0 RT	10/22/13	0.0	-	20.0	N.A.	Gray and brown fine SAND w/ some rock	N.A.	2.5
PB-4D	671+75	400.0 RT	10/22/13	0.0	_	20.0	N.A.	Gray and brown fine SAND w/ some rock	N.A.	3.0
PB-5A	696+10	190.0 LT	10/22/13	0.0	-	20.0	N.A.	Gray and brown fine SAND w/ some rock	N.A.	2.0
PB-5B	688+50	210.0 LT	10/22/13	0.0	-	20.0	N.A.	Gray and brown fine SAND w/ some rock	N.A.	2.0
PB-5C PB-4B	698+75 659+06	220.0 RT 383.6 RT	10/23/13 11/2/16	0.0 0.0	-	20.0 20.0	N.A. N.A.	Gray and brown fine SAND w/ some rock Gray and brown fine SAND w/ some rock	N.A. A-3	2.5 2.0

Note:

N.A.: Not Available at the time of this submittal.

Appendix 3 Protected Species and Wetlands Pond Siting Assessment Report

PROTECTED SPECIES AND WETLANDS POND SITING ASSESSMENT REPORT

SR 710 FROM US 441 to L-63N Canal

Okeechobee County, Florida

Financial Project ID No. 419344-3-52-01

Prepared for:

Florida Department of Transportation
District One
801 North Broadway Avenue
Bartow, Florida 33831-1249

February 2014

INTRODUCTION

The proposed project includes a new urban roadway (SR 710) consisting of four 12-foot travel lanes (two in each direction), a 12-foot multi use path, and a 5-foot sidewalk from US 441 to the L-63 Canal, in Okeechobee County, a distance of approximately three miles. This project also includes a new bridge over Taylor Creek and Interceptor Creek. This project falls within Sections 10, 13, 15, 16, and 24 of Township 37S, Range 35E;

This report presents the methodology used and results of data collection and field investigation for potential involvement with threatened and endangered species and/or wetlands associated with development of the Stormwater Management Facilities (SMFs) with the project area.

DATA COLLECTION

Readily available data sources were reviewed to determine if any wetlands and/or protected species or their habitats occur within or adjacent to proposed SMF locations. The primary information sources utilized for protected species occurrences and potential wetland involvement within the project area included:

- 2008 South Florida Water Management District (SFWMD) Digital Orthographic imagery;
- 2008 SFWMD Florida Land Use, Cover and Forms Classification System (FLUCFCS);
- United States Fish and Wildlife Service (USFWS) National Wetland Inventory data;
- United States Department of Agriculture (USDA) & National Resources Conservation Service (NRCS) Soil Survey of Okeechobee County;
- Florida Natural Areas Inventory (FNAI) element occurrence records and protected resources data;
- Florida Fish and Wildlife Conservation Commission (FWC) bald eagle nest sites, wading bird rookeries, wildlife observation database, protected species occurrence records, managed areas, and wildlife management areas; and
- USFWS protected species Consultation Areas (CA).

METHODOLOGY

Following the in-house data collection effort, scientists from Scheda Ecological Associates, Inc. (Scheda) conducted pedestrian field surveys of the SMF sites on September 17-18, 2013 and October 9, 2013 to verify the preliminary data previously obtained and to assess existing ecological conditions present at each site. Using meandering pedestrian and vehicular transects, appropriate habitats within a 50-foot buffer around each SMF site boundary were visually scanned for evidence of listed species as well as general wildlife utilization. Most natural areas (rangeland, upland forests, and wetlands) as well as agricultural lands were considered to be appropriate wildlife habitat. Observations were recorded to characterize vegetative communities present and evaluate the sites' potential to support protected wildlife and floral species.

Scientists from The Wantman Group conducted on-site surveys to determine if areas within or directly adjacent to the proposed pond sites contain jurisdictional wetlands and/or surface waters. All wetlands were identified and characterized according to the USFWS Classification System of Wetlands and Deepwater Habitats of the United States (Cowardin et al., 1979). All identified wetland and surface water boundaries were delineated using handheld GPS. The existing land use/land cover was classified in accordance with FLUCFCS.

For comparison purposes, a rating scale was used for each SMF location reviewed. A rating of "None", "Low", "Medium", or "High" is provided to identify the potential for wetland or protected species involvement associated with the SMF sites. With respect to wetlands, scoring was based on the proportion of the pond's footprint comprised of wetlands: a rating of "None" means 0%; a rating of "Low" is assigned for percentages between 0.10% and 24%; a "Medium" rating is for wetland composition between 25% and 49%; and a "High" rating is assigned when wetland composition is equal to or greater than 50%. Scoring for potential impacts to protected species is based on the type of habitat and its relative condition for supporting wildlife, if particular species were actually observed in the area, and the ease and cost of mitigation if necessary. A rating of "None" means no protected species anticipated; a "Low" rating is for potential but unlikely presence of protected species; a rating of "Medium" is for indication of protected species presence where mitigation is reasonable and possible; and a "High" rating is for indication of protected species presence where mitigation is difficult, costly, or not possible.

Existing land uses were classified in accordance with the SFWMD FLUCFCS and field-verified for accuracy (**Figure 1, Sheets 1-3**).

RESULTS

Based on the literature and database review potential federally listed or federally protected faunal and floral species within the project area include: crested caracara (Caracara cheriway), Florida grasshopper sparrow (Ammodramus savannarum floridanus), Everglade snail kite (Rostrhamus sociabilis plumbeus), wood stork (Mycteria americana), eastern indigo snake (Drymarchon corais couperi),, West Indian manatee (Trichechus manatus), bald eagle (Haliaeetus leucocephalus), Florida bonneted bat (Eumops floridanus) and Okeechobee gourd (Cucurbita okeechobeensis). All of the proposed SMF sites are located within the following USFWS CAs: crested caracara, Florida grasshopper sparrow, Everglade snail kite, Florida bonneted bat, and Okeechobee Gourd.

Potential state listed faunal species in the project area include: Florida burrowing owl (Athene cunicularia floridana), Florida sandhill crane (Grus Canadensis pratensis), little blue heron (Egretta caerulea), limpkin (Aramus guarauna), roseate spoonbill (Platalea ajaja), snowy egret (Egreta thula), southeastern American kestrel (Falco sparverius paulus), tricolored heron (Egretta tricolor), white ibis (Eudocimus albus), gopher frog (Lithobates capito), Florida pine snake (Pituophis melanoleucus mugitus), gopher tortoise (Gopherus polyphemus), American alligator (Alligator mississippiensis), Sherman's fox squirrel (Sciurus niger avicennia), and Florida mouse (Podomys floridanus)..

Potential state listed floral species in the project area include: Catebby lily (*Lilium catesbaei*), lowland loosestrife (*Lythrum flagellare*), Simpson's stopper (*Myrcianthes fragrans*), shell mound prickly pear (*Opuntia stricta*), yellow butterwort (*Pinguicula lutea*), hooded pitcher plant (*Sarracenia minor*), lace-lip ladies tresses (*Spiranthes laciniata*), leafless beaked orchid (*Stenorrhynchos lanceolatus*), inflated wild pine (*Tillandsia balbisiana*), common wild pine (*Tillandsia fasciculata*), soft-leaved wild pine (*Tillandsia valenzuelana*), and redmargin zephyrlily (*Zephyranthes simpsonii*).

All proposed SMF sites are located within the USFWS CA for the crested caracara. Crested caracara surveys conducted during the 2013 nesting season (January – April) for project FPID No. 419344-2-22-01 documented one adult crested caracara, flying over the project corridor, within the limits of this project. However, no nests were observed within the USFWS-defined primary (300 meter) or secondary (1,500 meter)

buffer zones of the project corridor. The FDOT has committed to resurveying the project area prior to construction, and coordinating with the USFWS at that time.

All potential SMF sites fall within the USFWS CA for the Florida grasshopper sparrow. However, no suitable habitat was observed within any of the proposed SMF site locations and no grasshopper sparrows were observed during field survey efforts. Similarly, all SMFs sites are also located with the USFWS CA for the Everglade snail kite. No snail kites were observed during project surveys. No Florida apple snails (*Pomacea paludosa*) or exotic ramshorn apple snails (*Marisa cornuarietis*), which are the primary food sources for the snail kite, were observed within the proposed SMF sites. No large, relatively deep and open marsh habitats, which provide the snail kite's primary foraging habitat, occur in any of the proposed SMF sites. The Taylor Creek Canal, located within the project limits, is accessible to the West Indian manatee. Should any SMF sites be selected that outfall to the canal, the standard manatee conditions for in-water work will be implemented to protect the species, as it will also be implemented for the bridge construction over the Taylor Creek Canal.

Although the project is located within the USFWS Okeechobee gourd CA, no gourd specimens have been documented in Okeechobee County, and the species was not observed during field surveys. If protected plant species are observed within the proposed impact limits during the design phase, coordination with the Florida Department of Agriculture and Consumer Services (FDACS) will be initiated, and efforts will be made prior to construction to allow for seed collection and/or relocation to adjacent habitat or other suitable protected lands.

ALL SMF sites are located within the newly-created CA for the Florida bonneted bat. The Florida bonneted bat has been documented historically in, and continues to have the potential to inhabit, a variety of habitat types including mangroves, earth midden hammocks, pine rockland, wet prairie, tropical hardwoods, hardwood hammock, pine flatwoods, lakes, cypress hammock, scrubby flatwoods, and wetland scrub habitat, as well as man-made and altered areas such as residential and urban areas canals, and developed park land (Federal Register, October 2013). Although the species has been documented in this variety of habitat types, very little is known about the specific habitat requirements of the Florida bonneted bat (Federal Register, October 2013). Currently, the only known Florida bonneted bat roosts are in bat boxes. All SMF sites have limited potential to support the Florida bonneted bat. Following SMF site selection, future field surveys will target the mainline corridor and selected SMF sites for identifying any potential Florida bonneted bat roosts.

The entire project area falls within the core foraging area (CFA) of two known wood stork colonies (Atlas numbers 616047A and 616108). Although no wood storks were observed within the proposed SMF site locations during the recent survey efforts, suitable foraging habitat (i.e., marshes, ditches, canals, open water ponds and forested wetlands) is present within or adjacent to the sites. Any required wetland mitigation is expected similarly compensate for wood stork foraging habitat impacts, and if wetland impacts exceed 5 acres, a wood stork foraging analysis will be conducted to ensure that wetland mitigation adequately offsets wood stork impacts.

Suitable foraging habitat for the Florida sandhill crane is present throughout the project corridor. Recent field surveys did not identify any nests or appropriate nesting habitat within the project area. Several individuals were observed flying over the project area and several were observed foraging within pastures adjacent to the proposed project footprint. Therefore, given the close proximity of additional foraging and nesting habitat surrounding the project area, construction of the SMFs is not likely to affect the Florida sandhill crane.

Field surveys conducted during the PD&E Study identified one individual Sherman's fox squirrel within an alignment that is no longer being considered during this design phase. No Sherman's fox squirrel individuals or nests were identified during recent surveys of the project area. However, foraging and nesting habitat occurs within and adjacent to the project corridor. Given the close proximity of additional foraging and nesting habitat surrounding the project area, construction of the SMFs is not likely to affect the Sherman's fox squirrel.

The bald eagle is no longer listed by the USFWS or FWC but remains protected under the Bald and Golden Eagle Protection Act (BGEPA; 16 U.S.C. 668-668d), as amended, and the Migratory Bird Treaty Act (MBTA; 16 U.S.C. 703-712). In 2011, the FWC conducted a bald eagle nesting season survey in Okeechobee County which identified an active bald eagle nest approximately 3.2 miles from the SR 710 and SR 70 intersection (Nest ID: OK031, FWC Eagle Nest Locator). Given the proximity of the bald eagle nest to the project corridor, human activity in the surrounding area, the uncertainty of nest activity status when project construction is scheduled to commence, and the possibility of new nests being identified by the FWC during future nesting season surveys, the FDOT shall commit to resurveying the project area prior to construction. If any nests within 660-foot protection zone are deemed active, the FDOT will act in accordance with the BGEPA and MBTA.

Based on the findings obtained during corridor and SMF site survey efforts on September 17-18, 2013 and October 9, 2013, the following three (3) state-listed faunal species were observed within or adjacent to the proposed SMF sites: gopher tortoise, snowy egret, and white ibis. No listed floral species were observed.

Suitable gopher tortoise habitat is located throughout the project area. Gopher tortoise burrows, both "potentially occupied burrows" and "abandoned burrows", were identified within the proposed footprints of two (2) SMF sites: 4A and 4D. A total of 13 potentially occupied burrows were identified at the 4A site, another 8 potentially occupied burrows were identified at 4D. Impacts to gopher tortoises, their burrows and habitat, can be mitigated through permitted relocation efforts.

Wading birds such as the limpkin, white ibis, little blue heron, snowy egret, tricolored heron, and roseate spoonbill are not listed as endangered or threatened by the USFWS (although they are protected under the Migratory Bird Treaty Act (MBTA) (16 U.S.C. 703-712), but are listed by the FWC as Species of Special Concern (SSC). Suitable foraging habitat for wading birds is located throughout the proposed project area. Ample wading bird foraging habitat occurs adjacent to and in the immediate vicinity of the project area, therefore construction of the SMF sites is not likely to affect protected wading birds.

Table 1 summarizes the land use / land cover, habitat, and protected species concerns for each SMF site. **Table 1** also summarizes the anticipated wetland and surface water impacts associated with each potential SMF site. **Figure 1** depicts the location of all proposed SMF sites, the surrounding land use / land cover for the SMF alternatives, and the location of all identified wetlands and/or surface waters located within or adjacent to the SMF sites. **Figure 2** depicts the locations of the observed potentially occupied gopher tortoise burrows within the proposed SMF 4A and 4D sites.

SMF Descriptions

<u>SMF 1A – 2.32 acres (Photo 1)</u>

SMF 1A is located approximately 700 feet west of US 441, northwest of the western terminus of NW 13th Street. The SMF site contains the Shrub and Brushland (FLUCFCS 3200) land use / land cover type. No wetlands were observed within this SMF; therefore the wetland rating is "None".

The SMF site is completely overgrown with invasive/nuisance vegetation such as Brazilian pepper (*Schinus terebinthifolius*), air potato (*Dioscorea bulbifera*), cogon grass

(Imperata cylindrica), West Indian marsh grass (Hymenachne amplexicaulis), and other exotic vegetation. Some native species such as cabbage palm (Sabal palmetto) and grape vine (Vitis rotundifolia) are also present. Some depressional areas are present, but the areas are above the natural ground elevation, and will not be claimed jurisdictional by the SFWMD or USACE, and therefore will not require mitigation.

No state or federally listed protected species were previously documented in SMF 1A and none were observed during recent field surveys. Due to the thick coverage of invasive/nuisance vegetation that provide suboptimal habitat for most protected species and the site's proximity to development, this site was given a rating of "Low" for protected species.

SMF 1B – 1.21 acres (Photo 2)

SMF 1B is located approximately 700 feet east of US 441, northeast of the eastern terminus of NW 13th Street. This SMF contains Hardwood - Conifer Mixed (FLUCFCS 4340) and Freshwater Marshes (FLUCFCS 6410) land use / land cover types. An estimated 0.5 acres of wetlands occur within the SMF site, equating to approximately 40% of the total SMF acreage, therefore it was given a wetland rating on "Medium".

The SMF site is comprised of a mix of freshwater marshes and upland forested habitat containing invasive/nuisance vegetation, such as Brazilian pepper, air potato, and others, and native tree species including live oak (*Quercus virginiana*), laurel oak (*Quercus laurifolia*), and cabbage palm. Herbaceous wetland areas are interspersed throughout the forested habitat in the western half of the proposed SMF site.

No state or federally listed protected species were previously documented in SMF 1B and none were observed during recent field surveys. State-protected wading birds and wood storks could forage in the marshes. Coverage by invasive/nuisance vegetation in the forested upland limits potential nesting by crested caracara. Therefore, this site was given a rating of "Low" for protected species.

SMF 1C - 0.88 acres (Photos 3 & 4)

SMF 1C is located approximately 700 feet east of US 441, southeast of the eastern terminus of NW 13th Street. The entire SMF site contains Mixed Wetland Hardwoods (FLUCFCS 6170), therefore it was given a wetland rating of "High".

The entire SMF site contains saturated soils and standing water. The SMF site is comprised mainly of wetland forest vegetation including bald cypress (*Taxodium distichum*), red maple (*Acer rubrum*), swamp fern (*Blechnum serrulatum*), cabbage palm, and Brazilian pepper. Wetland impacts at this site will require compensatory mitigation.

No state or federally listed protected species were previously documented in SMF 1C and none were observed during recent field surveys. State-protected wading birds and wood storks could forage in the forested wetland. Species and canopy coverage is not suitable for crested caracara nesting. Therefore, this site was given a rating of "Low" for protected species.

<u>SMF 2A - 7.84 acres (Photos 5)</u>

SMF 2A is located within a large undeveloped area approximately 800 feet north on NE 15th Street and one mile east of US 441. This SMF contains Improved Pasture (FLUCFCS 2110) and Oak – Cabbage Palm Forest (FLUCFCS 4271) land use / land cover types. No wetlands were observed within this SMF; therefore the wetland rating is "None".

The SMF site consists of live oak, cabbage palm, pasture land, and minimal presence of exotic upland vegetation. No state or federally listed protected species were previously documented in SMF 2A. Crested caracara were observed in close proximity to this site (flying over) and the site contains suitable crested caracara nesting habitat, but no nests were identified in 2013 surveys. This site was given a rating of "Low" for protected species.

SMF 2B - 9.95 acres (Photo 6)

SMF 2B is located to the south of SMF 2A, approximately 300 ft north on NE 15th Street and one mile east of US 441. The entire SMF site contains Improved Pasture (FLUCFCS 2110). No wetlands were observed within this SMF; therefore the wetland rating is "None".

The SMF site consists mainly of pasture land, with a few small patches of slash pine (*Pinus elliotii*), live oak, cabbage palm, and minimal presence of exotic upland vegetation. No state or federally listed protected species were previously documented in SMF 2B. Crested caracara were observed in close proximity to this site (flying over) and the site contains suitable crested caracara nesting habitat, but no nests were identified in 2013. This site was given a rating of "Low" for protected species.

<u>SMF 2C – 10.55 acres (Photos 7 & 8)</u>

SMF 2C is located within a large undeveloped area approximately 1,800 feet east of US 441 and 600 feet north of the Integra roof tile factory. This SMF contains the following land use / land cover classifications: Improved Pasture (FLUCFCS 2110), Oak – Cabbage Palm Forest (FLUCFCS 4271), Mixed Wetland Hardwood (FLUCFCS 6170), and Freshwater Marshes (FLUCFCS 6410). The mixed wetland hardwood occurs over an estimated 0.5 acres of the site. The freshwater marsh wetland occurs over an

estimated 0.2 acres. The combined wetland acreage is less than 10% of the total SMF site acreage, therefore it was given a wetland rating of "Low".

The SMF site consists mainly of live oak, cabbage palm, pasture land and some exotic upland vegetation. Forested wetlands consisting of a mix of exotic and native tree and shrub species occur along the west boundary of this proposed SMF site. A small depressional herbaceous marsh occurs on the east side of the open grassland pasture.

No state or federally listed protected species were previously documented in SMF 2C and none were observed during recent field surveys. The small size of the marsh area will limit foraging by State-listed wading birds and wood storks. The site contains suitable crested caracara nesting habitat, however none were observed in the vicinity during 2013 nesting season surveys. This site was given a rating of "Low" for protected species.

<u>SMF 3A – 3.82 acres (Photo 9)</u>

SMF 3A is located adjacent to and northeast of the SR 70 crossing over the L-63N Canal. The entire SMF site contains Improved Pasture (FLUCFCS 2110). No wetlands were observed within this SMF; therefore the wetland rating is "None".

This SMF site consists mainly of pasture land. The dominant vegetation was made up of various upland grasses with some slash pine and saw palmetto (*Serenoa repens*) scattered throughout. Herbaceous wetlands occur adjacent to the northwest boundary of the proposed SMF site. Impacts to the herbaceous wetlands could require compensatory mitigation. A drainage ditch containing emergent wetland vegetation occurs along the west limit of this proposed SMF site. The SFWMD will claim the ditch as an "Other Surface Waters" (OSW) that will not require mitigation. The USACE may require compensatory mitigation for any impacts to the ditch.

No state or federally listed protected species were previously documented in SMF 3A and none were observed during recent field surveys. The site's proximity to SR 70 likely limits protected species utilization. The site's proximity to adjacent wetlands and surface waters may result in limited utilization by State-listed wading birds and wood storks. The site contains sub-optimal crested caracara nesting habitat. For these reasons, this site was given a rating of "Low" for protected species.

SMF 3B – 3.74 acres (Photo 10)

SMF 3B is located within a large undeveloped area approximately 700 feet north of SR 70 and 900 west of the L-63N Canal. This SMF contains the following land use / land cover classifications: Improved Pasture (FLUCFCS 2110), Unimproved Pasture (FLUCFCS 2120), and Freshwater Marshes (FLUCFCS 6410). The marsh covers an

estimated 0.3 acres, which is less than 10% of the SMF site's total acreage. Therefore, the wetland rating is 'Low".

This SMF site consists mainly of unimproved pastureland. The dominant vegetation was made up of various upland grasses with some scattered slash pine. Much of the site contained saturated soils. The western portion of this SMF site contained a freshwater marsh which was connected to a larger wetland located outside this SMF footprint. Wetland impacts at this site will require compensatory mitigation.

No state or federally listed protected species were previously documented in SMF 3B and none were observed during recent field surveys. The on-site marsh area and site's proximity to adjacent wetlands may result in limited utilization by state-listed wading birds and wood storks. The site contains sub-optimal crested caracara nesting habitat. For these reasons, this site was given a rating of "Low" for protected species.

<u>SMF 3C – 3.78 acres (Photo 11)</u>

SMF 3C is located adjacent to and between NE 4th trail and SR 70, east of NE 34th Avenue. It is situated to the south of an existing retention pond. The entire SMF site contains Hardwood – Conifer Mixed (FLUCFCS 4340) land use / land cover type. No wetlands were observed within this SMF; therefore the wetland rating is "None".

This SMF site consists mainly of a mixed hardwood conifer forest. Dominant vegetation includes live oak, laurel oak, saw palmetto, cabbage palm, Brazilian pepper, and small patches of upland grasses. A drainage ditch dominated by Brazilian pepper occurs along the east limit of this proposed SMF site. The SFWMD will claim the ditch as an OSW and will not require mitigation. The USACE may require compensatory mitigation for any impacts to the ditch.

No state or federally listed protected species were previously documented in SMF 3C and none were observed during recent field surveys. The site's proximity to the adjacent ditch may result in limited utilization by state-listed wading birds and wood storks. The site contains sub-optimal crested caracara nesting habitat. For these reasons, this site was given a rating of "Low" for protected species.

SMF 4A - 7.79 acres (Photos 12 & 20; Figure 2)

SMF 4A is located adjacent to and north of the SR 710 crossing over the L-63N Canal. The SMF site contains Herbaceous Dry Prairie (FLUCFCS 3100) and Hardwood – Conifer Mixed (FLUCFCS 4340) land use / land cover types. No wetlands were observed within this SMF; therefore the wetland rating is "None".

Thirteen (13) potentially occupied gopher tortoise burrows were located within this SMF footprint. A berm consisting of spoil material approximately 10-15 feet high occupies the

entire eastern portion of the site. The berm is sparsely to heavily vegetated with various exotic/invasive weeds and shrubs along with slash pine, Brazilian pepper, and saw palmetto. The remainder of the site consisted of pine flatwoods primarily vegetated by slash pine, saw palmetto, and scattered live oak, with Brazilian pepper scattered along the southern portion near SR 710. Due to the presence and quantity of gopher tortoise burrows at this site, and the associated cost of mitigation (burrow excavation, tortoise relocation, and species-specific permitting), it was given a rating of "Medium" for protected species

<u>SMF 4B – 4.58 acres (Photo 13)</u>

SMF 4B is located directly adjacent to and east of NE 34th Avenue, north of SR 710. This SMF contains the following land use / land cover classifications: Unimproved Pasture (FLUCFCS 2120), Hardwood – Conifer Mixed (FLUCFCS 4340), and Streams and Waterways (FLUCFCS 5100). The Streams and Waterways land use / land cover type represents a drainage ditch that occurs in the north corner of the proposed SMF site. It is classified as a surface water by the State. The ditch covers an estimated 0.1 acres, which is less than 2% of the SMF site's total acreage. Therefore, the wetland rating is 'Low'.

This SMF site consists mainly of a mixed hardwood conifer forest with some unimproved pasture land. Dominant vegetation includes saw palmetto and slash pine, with scattered live oak and cabbage palms. The drainage ditch is dominated by Brazilian pepper. The SFWMD will claim the ditch as an OSW and will not require mitigation. The USACE may require compensatory mitigation for any impacts to the ditch.

No state or federally listed protected species were previously documented in SMF 4B and none were observed during recent field surveys. State-listed wading birds and wood storks may utilize the ditch. The site contains suitable crested caracara nesting habitat, however none were observed in the vicinity during 2013 nesting season surveys. This site was given a rating of "Low" for protected species.

SMF 4C - 3.57 acres (Photo 14)

SMF 4C is located directly adjacent to and north of SR 710, east of NE 34th Avenue. The SMF site contains Unimproved Pasture (FLUCFCS 2120) and Hardwood – Conifer Mixed (FLUCFCS 4340) land use / land cover types. No wetlands were observed within this SMF; therefore the wetland rating is "None".

This SMF site consists mainly of a mixed hardwood conifer forest with some unimproved pasture land. Dominant vegetation includes saw palmetto and slash pine, with scattered live oak and cabbage palms. No state or federally listed protected

species were previously documented in SMF 4C and none were observed during recent field surveys. The site contains suitable crested caracara nesting habitat, however no caracaras were observed in the vicinity during 2013 nesting season surveys. This site was given a rating of "Low" for protected species.

<u>SMF 4D – 8.61 acres (Photos 15, 16, & 20; Figure 2)</u>

SMF 4D is located directly adjacent to (south of) SR 710, between SR 710 and SE 4th Street. It consists primarily of the Hardwood – Conifer Mixed (FLUCFCS 4340) land use / land cover type, but also includes Mixed Use, Low Density Fixed and Mobile Home Units (FLUCFCS 1130) and Fixed Single Family Units, Medium Density (FLUCFCS 1210) land use / land cover. No wetlands were observed within this SMF; therefore the wetland rating is "None".

Eight (8) potentially occupied gopher tortoise burrows were located within this SMF footprint. This site contained many disturbed areas resulting from pedestrian and ATV activity. Slash pine, laurel oak, live oak, cabbage palm, saw palmetto, grapevine, and smilax (*Smilax sp.*) were the dominant vegetative species identified. Due to the presence and quantity of gopher tortoise burrows at this site, and the associated cost of mitigation (burrow excavation, tortoise relocation, and species-specific permitting), it was given a rating of "Medium" for protected species.

<u>SMF 5A – 2.63 acres (Photo 17)</u>

SMF 5A is located north of SR 710, east of the Okeechobee County Agri-Civic Center access road. This SMF contains Hardwood – Conifer Mixed (FLUCFCS 4340) and Mixed Wetland Hardwoods (FLUCFCS 6170) land use/land cover types. The forested wetland area covers an estimated 0.8 acres in the northwest quadrant, which equates to approximate 30% of the SMF site's total acreage. Therefore, the wetland rating is 'Medium'.

The SMF site consisted mainly of slash pines, live oak, saw palmetto, and some exotic upland vegetation. A forested wetland containing a mix of exotic and native tree and shrub species occur on the northwest portion of the proposed SMF site. Wetland impacts at this site will require compensatory mitigation.

No state or federally listed protected species were previously documented in SMF 5A and none were observed during recent field surveys. State-protected wading birds and wood storks could forage in the on-site forested wetland. The site contains sub-optimal crested caracara nesting habitat but no caracaras were observed in the vicinity during 2013 nesting season surveys. Therefore this site was given a rating of "Low" for protected species.

SMF 5B - 2.53 acres (Photo 18)

SMF 5B is located north of SR 710, west of the Okeechobee County Agri-Civic Center access road. This SMF contains Horse Farm (FLUCFCS 2510) and Freshwater Marsh (FLUCFCS 6410) land use/land cover types. The marsh covers an estimated 0.5 acres in the northeast quadrant, which equates to approximate 20% of the SMF site's total acreage. Therefore, the wetland rating is 'Low".

This SMF site consisted mainly of pasture land, along with scattered laurel oaks, cabbage palm, and saw palmetto. An herbaceous wetland occurs in the northeastern portion of the SMF footprint. Wetland impacts at this site will require compensatory mitigation.

No state or federally listed protected species were previously documented in SMF 5B and none were observed during recent field surveys. State-protected wading birds and wood storks could forage in the on-site marsh area. The site contains sub-optimal crested caracara nesting habitat but no caracaras were observed in the vicinity during 2013 nesting season surveys. Therefore this site was given a rating of "Low" for protected species.

SMF 5C – 3.53 acres (Photo 19)

SMF 5C is located directly adjacent to (south of) SR 710, east of the L-63N Canal. It consists entirely of the Hardwood – Conifer Mixed (FLUCFCS 4340) land use / land cover type. No wetlands were observed within this SMF; therefore the wetland rating is "None".

The SMF site consisted mainly of slash pines, live oak, saw palmetto, and some exotic upland vegetation. No state or federally listed protected species were previously documented in SMF 5C and none were observed during recent field surveys. The site contains sub-optimal crested caracara nesting habitat but no caracaras were observed in the vicinity during 2013 nesting season surveys. Therefore this site was given a rating of "Low" for protected species.

CONCLUSIONS AND RECOMMENDATIONS

Wetlands

Based on the results of the preliminary data collection and field reviews, we have determined that nine SMFs (Sites 1A, 2A, 2B, 3A, 3C, 4A, 4C, 4D, and 5C) will have no wetland impacts, four SMFs will have low wetland impacts (Sites 2C, 3B, 4B, and 5B), two SMFs (Sites 1B and 5A) will have medium wetland impacts, and one SMF (Site 1C) will have high wetland impacts. Measures to avoid or minimize wetland and water

quality impacts will be implemented during final pond site design. If selected SMF sites involve wetland impacts, mitigation will be provided through credit purchase at an appropriate mitigation bank such as the Bluefield Ranch Mitigation Bank. Cost-percredit pricing information for the BRMB was unavailable for review. However, based on recent experience with the FDOT's Invitation-to-Bid process, it is anticipated that the actual cost-per-credit will be approximately \$120,000 per credit. An estimated UMAM score of 0.5 per acre (moderate quality score) was assigned to the wetland areas within the proposed SMF sites to provide an estimated per site wetland mitigation cost. These values are provided in **Table 1**. Both wetlands and surface waters were considered as potentially requiring mitigation due to the USACE methods of determining mitigation requirements for waters of the U.S. and wood stork suitable foraging habitat impacts.

Protected Species

Based on results of preliminary data collection and field reviews, we have determined that 14 of the 16 SMF sites (all sites other than 4A and 4D) have low potential protected species involvement. These are due to multiple factors which include, but are not limited to, having suitable crested caracara nesting habitat but no observations of caracaras or nests during recent nesting season surveys, sub-optimal crested caracara nesting habitat, sub-optimal Florida bonneted bat habitat, and/or relatively small-acreage wood stork foraging habitat which may also be used by state-listed wading birds. Due to the presence of potentially-occupied gopher tortoise burrows, SMF sites 4A (with 13 identified burrows) and 4D (with eight identified burrows) have a medium potential for protected species involvement. Access to these sites is readily available, therefore mitigation in the form of burrow excavation and/or gopher tortoise trapping and relocation, with the proper permits from the FWC, is a feasible option to offset impacts. It is estimated that mitigation for gopher tortoise impacts, which includes permitting, burrow excavation, and tortoise relocation, will cost \$18,000 at site 4A and \$15,000 at Site 4D.

<u>RESOURCES</u>

Cowardin, Lewis M., Virginia Carter, Francis C. Golet, and Edward T. LaRoe. 1979. Classification of Wetlands and Deepwater Habitats of the United States, U.S. Fish and Wildlife Service Publication. Washington, D.C., 103 pp.

Humphrey, Stephen R. (Editor). 1992. Rare and Endangered Biota of Florida: Volume 1 Mammals. University Press of Florida. 392 pp.

- Moler, Paul E. (Editor). 1992. Rare and Endangered Biota of Florida: Volume III Amphibians and Reptiles. University Press of Florida.291 pp.
- Myers, Ronald L. and John J. Ewel (Editors). 1990. Ecosystems of Florida. University of Central Florida Press. 765 pp.
- Rodgers Jr., James A., Herbert W. Kale II, and Henry T. Smith. (Editors). 1996. Rare and Endangered Biota of Florida: Volume V Birds.

Table 1. SMF Site Descriptions and Wetlands/Protected Species Involvement.

SMF Site	SMF Acreage	Description	FLUCFCS Code	Soils (NRCS Soil Survey)	Wetland Acreage	Percent Wetland Coverage	Wetland Mitigation Cost*	Wetlands / Surface Water Involvement	Protected Species Involvement/Concerns
1A	2.32	Undeveloped Parcel dominated by exotic vegetation (woody and herbaceous)	3200 - Shrub & Brushland	Immokalee Fine Sand (11)	0	0%	\$0	None	Low
1B	1.21	Undeveloped parcel containing mix of shrub and wooded areas	4340 – Hardwood – Conifer Mixed; 6410 - Freshwater Marsh	Manatee Loamy Fine Sand, Depressional (6)	0.5	40%	\$30,000	Medium	Low
1C	0.88	Forested wetland (mix of exotic and native species); existing small pond near southern limit	6170 - Mixed Wetland Hardwoods	Manatee Loamy Fine Sand, Depressional (6)	0.88	100%	\$52,800	High	Low
2A	7.84	Undeveloped parcel containing mix of open pasture and wooded areas	2110 - Improved Pasture; 4271 - Oak - Cabbage Palm Forest	Immokalee Fine Sand (11), Riviera Fine Sand (9)	0	0%	\$0	None	Low
2B	9.95	Undeveloped parcel containing mix of pasture and wooded areas	2110 - Improved Pasture;	Immokalee Fine Sand (11)	0	0%	\$0	None	Low
2C	10.55	Undeveloped parcel containing mix of pasture and wooded areas	2110 - Improved Pasture; 4271 - Oak - Cabbage Palm Forest; 6170 Mixed Wetland Hardwoods; 6410 - Freshwater Marsh	Basinger Fine Sand (2); Pindea Fine Sand (8); Floridana, Placid, and Okeelanta Soils, Frequently Flooded (19)	0.7	7%	\$42,000	Low	Low
ЗА	3.82	Unimproved pasture with some slash pine and saw palmetto	2110 - Improved Pasture	Immokalee Fine Sand (11)	0	0%	\$0	None	Low
3B	3.74	Unimproved pasture	2120 - Unimproved Pasture; 2110 - Improved Pasture; 6410 - Freshwater Marsh	Immokalee Fine Sand (11); Basinger and Placid Soils, Depressional (3)	0.3	8%	\$18,000	Low	Low
3C	3.78	Undeveloped parcel containing mix of pasture and wooded areas	4340 – Hardwood – Conifer mixed	Immokalee Fine Sand (11); Basinger and Placid Soils, Depressional (3)	0	0%	\$0	None	Low
4A	7.79	Undeveloped parcel containing mix of distrubed herbaceous uplands (spoil berms), palmetto-dominated shrub, and wooded areas	3100 Herbaceous Dry Prairie; 4340 – Hardwood – Conifer mixed	Immokalee Fine Sand (11)	0	0%	\$0	None	Medium
4B	4.58	Undeveloped parcel containing mix of pasture and wooded areas	2120 - Unimproved Pasture; 4340 – Hardwood – Conifer Mixed; 5100 - Streams and Waterways	Immokalee Fine Sand (11); Basinger and Placid Soils, Depressional (3)	0.1	2%	\$6,000	Low	Low
4C	3.57	Undeveloped parcel containing mix of pasture and wooded areas	2120 - Unimproved Pasture; 4340 - Hardwood - Conifer Mixed	Immokalee Fine Sand (11)	0	0%	\$0	None	Low
4D	8.61	Wooded area disturbed by frequent ATV activity adjacent to a medium density residential area	4340 – Hardwood – Conifer Mixed; 1130 - Mixed Use, Low Density Fixed and Mobile Home Units; 1210 - Fixed Single Family Units - Medium Density	Immokalee Fine Sand (11)	0	0%	\$0	None	Medium
5A	2.63	Undeveloped parcel dominated by wooded areas	4340 – Hardwood – Conifer Mixed; 6170 Mixed Wetland Hardwoods	Immokalee Fine Sand (11); Floridana, Placid, and Okeelanta Soils, Frequently Flooded (19)	0.8	30%	\$48,000	Medium	Low
5B	2.53	Unimproved pasture with some laurel oak, cabbage palm, and saw palmetto	2510 – Horse Farm; 6410 - Freshwater Marsh	Immokalee Fine Sand (11)	0.5	20%	\$30,000	Low	Low
5C	3.53	Undeveloped parcel dominated by wooded areas	4340 – Hardwood – Conifer Mixed	Immokalee Fine Sand (11); Floridana, Placid, and Okeelanta Soils, Frequently Flooded (19)	0	0%	\$0	None	Low

^{* =} Approximate wetland mitigation cost assumes moderate wetland quality scores (UMAM = 0.5 per acre) and \$120,000 per credit

NOTES:

None No wetland/surface water impacts; no protected species anticipated to occur based on habitat quality, no observations or records

Low Wetlands/surface waters comprise 1% to 24% of pond footprint; potential but unlikely presence of protected species

 Medium
 Wetlands/surface waters comprise 25% to 49% of pond footprint; indication of species where mitigation is reasonable and possible

 High
 Wetlands/surface waters comprise 50% or more of pond footprint; indication of species where mitigation is difficult, costly, or not possible

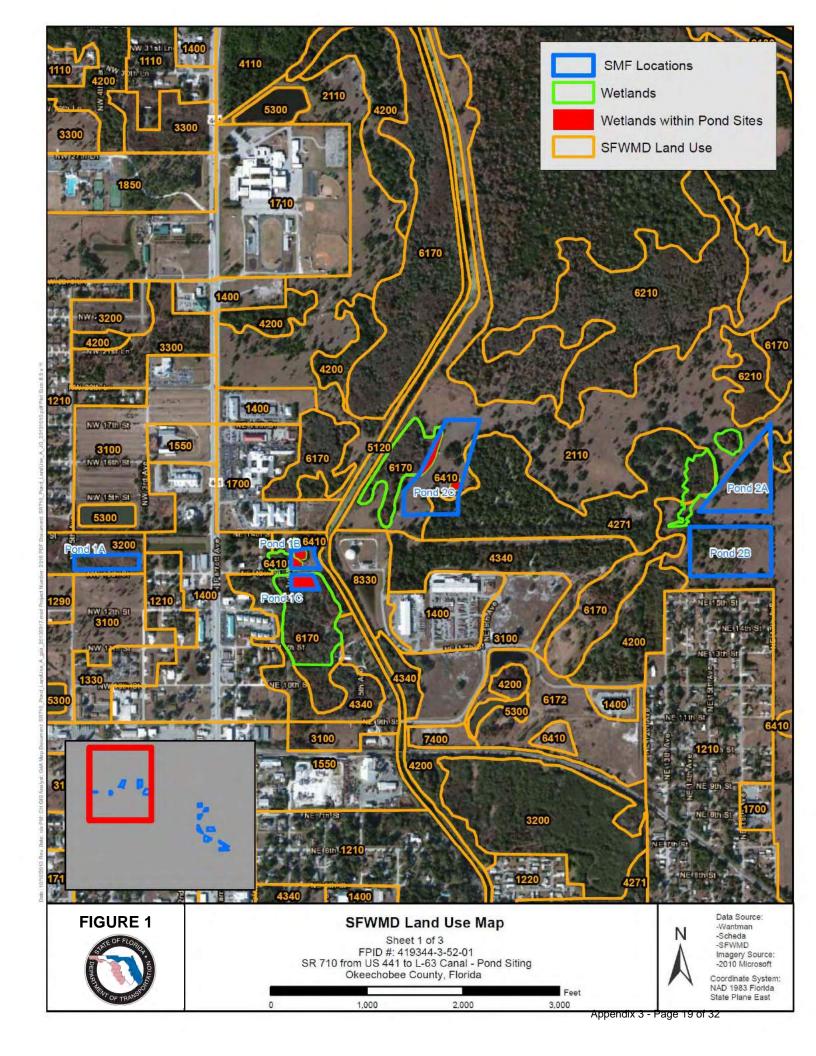




FIGURE 1



SFWMD Land Use Map

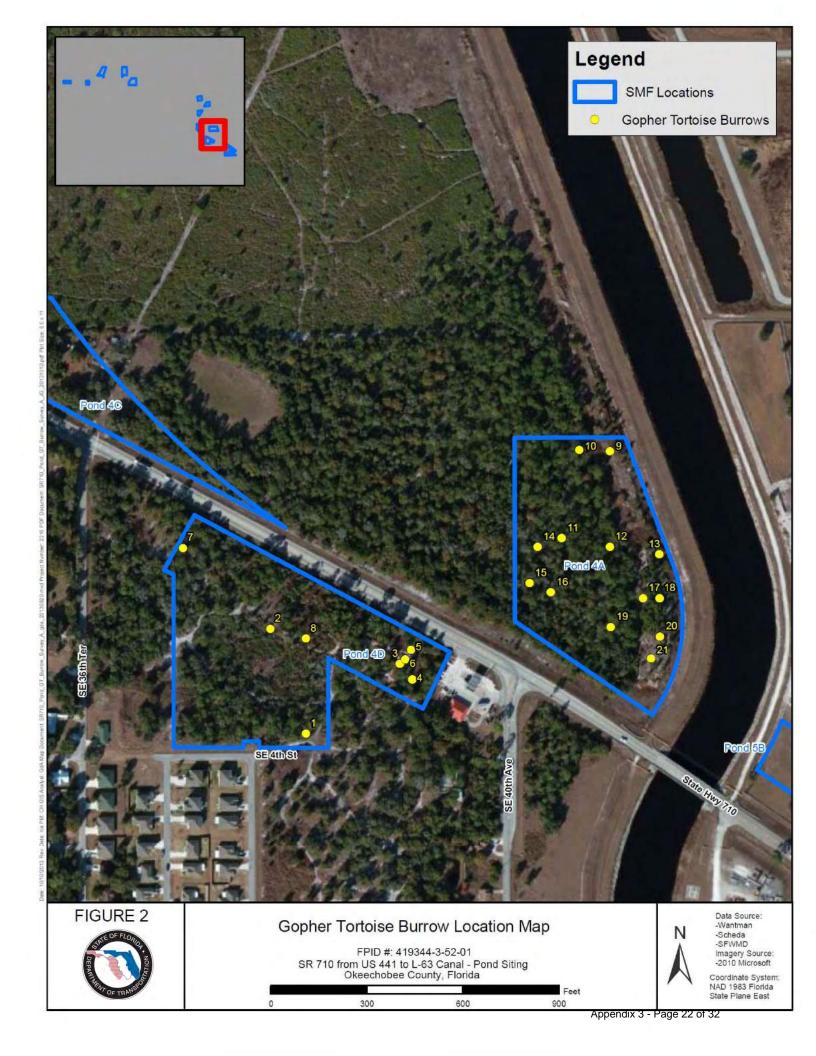
Sheet 3 of 3 FPID #: 419344-3-52-01 SR 710 from US 441 to L-63 Canal - Pond Siting Okeechobee County, Florida

1,000 2,000 3,000

N

Data Source:
-Wantman
-Scheda
-SFWMD
Imagery Source:
-2010 Microsoft

Coordinate System: NAD 1983 Florida State Plane East



Representative Photographs



Photo 1 – Typical view of habitats occurring at proposed SMF 1A site.



Photo 2 – Typical view of habitats occurring at proposed SMF 1B site.



Photo 3 – Typical view of habitats occurring at proposed SMF 1C site.



Photo 4 – Small pond occurring near southern limit of proposed SMF 1C site.



Photo 5 – Typical view of habitats occurring at proposed SMF 2A site.



Photo 6 – Typical view of habitats occurring at proposed SMF 2B site.



Photo 7 – Typical view of habitats occurring at proposed SMF 2C site.



Photo 8 – Typical view of habitats occurring at proposed SMF 2C site.



Photo 9 – Typical view of habitats occurring at proposed SMF 3A site.



Photo 10 – Typical view of habitats occurring at proposed SMF 3B site.



Photo 11 – Typical view of habitats occurring at proposed SMF 3C site.

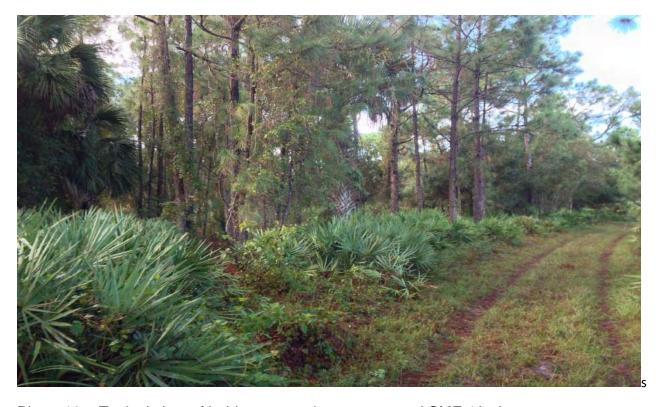


Photo 12 – Typical view of habitats occurring at proposed SMF 4A site.



Photo 13 – Typical view of habitats occurring at proposed SMF 4B site.



Photo 14 - Typical view of habitats occurring at proposed SMF 4C site.



Photo 15 – Typical view of habitats occurring at proposed SMF 4D site.



Photo 16 – Typical view of habitats occurring at proposed SMF 4D site.



Photo 17 – Typical view of habitats occurring at proposed SMF 5A site.



Photo 18 – Typical view of habitats occurring at proposed SMF 5B site.



Photo 19 – Typical view of habitats occurring at proposed SMF 5C site.



Photo 20 – Typical view of a potentially occupied gopher tortoise burrow.

Appendix 4
Draft Level I PSR Contamination Screening
Evaluation Report (CSER) (July 14, 2014-Rev.2) &
Draft Level II Field Screening Report (FSR) Preferred Ponds (January 13, 2017)

July 14, 2014 (Rev. 2)

Wantman Group, Inc. 213 South Dillard St, Suite 210 Winter Garden, Florida 34787

Attn: Mr. Alfredo Rodriguez, PE

Project Manager

RE: Draft Level I PSR Contamination Screening Evaluation Report - Proposed Ponds

SR 710 from US 441 to the L-63 Canal

Okeechobee County, Florida

FPN: 419344-3-32-01

Tierra Project No.: 6511-12-054A

Mr. Rodriguez:

Tierra, Inc. (Tierra) has completed a Level I Pond Siting Contamination Screening Evaluation Report (CSER), dated November 22, 2013 based on the proposed pond alternative locations received in October 2013. Subsequent to receiving updated pond information in March 2014, the report was revised to reflect the changes and dated April 21, 2014.

This report revision incorporates edits made based on comments received from the client and the FDOT in May/June 2014. For reference, a copy of Tierra's Response to Comments Memo, dated July 10, 2014 was submitted along with this revised Draft PSR-CSER.

The information presented herein is intended to provide a risk ranking of all pond sites to support the Pond Siting Report (PSR). The contamination screening evaluation presented herein is based on historical aerial photograph and topographic map reviews, governmental database reviews and site reconnaissance.

Should you have any questions, please contact us at (813) 989-1354.

Respectfully Submitted,

TIERRA, INC.

Clare E. Kramer, PG

Senior Scientist

Donald R. Polanis, PSSC, CGC

Chief Scientist

Executive Summary

Tierra, Inc. (Tierra) has prepared this pond site Contamination Screening Evaluation Report (CSER) for the project referenced above. The information presented is intended to provide a risk ranking of all proposed pond alternatives to support the Pond Siting Report (PSR). The contamination screening evaluation presented herein is based on historical aerial photograph and topographic map reviews, governmental database reviews and site reconnaissance. The Proposed Pond Alternative locations are presented on recent aerial photographs included in **CSER-Appendix A**.

The contamination screening evaluation has resulted in the following risk rankings for the proposed pond alternatives:

Proposed Pond Alternative	Risk Ranking	Comment					
Pond 1A	No	2.32-Acres. Current and historic woodlands					
Pond 1B	Low	1.20-Acres. Risk ranking Low for possible onsite use as water pipeline construction staging area in 1994. Current and historic woodlands with an apiary (bee hives) and open, grassy area					
Pond 1C	No	0.88-Acres. Current and historic woodlands					
Pond 2A – Option 1	No	14.23-Acres. Current and historic pastureland and woodlands					
Pond 2A – Option 2	No	7.93-Acres. Current and historic pastureland and woodlands					
Pond 2A – Option 3	No	6.42-Acres. Current and historic pastureland and woodlands					
Pond 2B – Option 1	No	15.37-Acres. Current and historic pastureland and woodlands					
Pond 2B – Option 2	No	10.00-Acres. Current and historic pastureland and woodlands					
Pond 2B – Option 3	No	7.08-Acres. Current and historic pastureland and woodlands					
Pond 2C – Option 1	No	6.86-Acres. Current and historic pastureland and woodlands					
Pond 2C – Option 2	No	6.14-Acres. Current and historic pastureland and woodlands					
Pond 3A (formerly 3B)	Medium	4.18-Acres. Risk ranking Medium for onsite livestock holding pen. Current pastureland, historic woodlands, wetlands, pastureland and cleared land					
Pond 3B (formerly 3A)	No	2.44-Acres. Current and historic pastureland and wetlands					
Pond 3C Low		3.81-Acres. Risk ranking Low for onsite stormwater pond. Current and historic woodlands					
Pond 4A – Option 1 Low		3.98-Acres. Risk ranking Low for non-adjoining Townstar #40/BP gas station to the southwest. Current woodlands, historic wetland in northeast corner					
Pond 4A – Option 2	Low	3.34-Acres. Risk ranking Low for non-adjoining Townstar #40/BP gas station to the southwest. Current woodlands, historic wetland in northeast corner					
Pond 4B/4C – Option 1	Medium	8.17-Acres. Risk ranking Medium for onsite livestock holding pen. Current and historic woodlands with two (2) sheds, a livestock holding pen and unpaved trails					
Pond 4B – Option 2	No	4.59-Acres. Current and historic woodlands with unpaved trails					
Pond 4D – Option 1	Medium	6.08-Acres. Risk ranking Medium for east adjoining Townstar #40/BP gas station. Current and historic woodlands with unpaved trails/tracks; historic wetlands in northeast corner onsite from 1940 to 1960s. Adjoining operational Townstar #40/BP gas station to the east since 1986; three (3) groundwater monitor wells were installed on Pond 4D in 2007 to assess potential petroleum impacts. The laboratory analytical results did not indicate petroleum contaminants in exceedance of the GCTLs. The highest OVA reading during monitor well installation was one (1) ppm. No soil samples were collected for laboratory analytical testing during this Level I investigation.					

Proposed Pond Alternative	Risk Ranking	Comment
Pond 4D – Option 2	Medium	4.33-Acres. Risk ranking Medium for east adjoining east Townstar #40/BP gas station. Current and historic woodlands with unpaved trails/tracks; historic wetlands in northeast corner onsite from 1940 to 1960s
Pond 5A	No	2.62-Acres. Current and historic woodlands/wetlands/pastureland
Pond 5B	No	2.53-Acres. Pastureland and wetlands associated with north adjacent Paddock Farms (miniature horses)
Pond 5C	Low	3.53-Acres. Risk ranking Low for offsite livestock holding pen, approximately 50 feet south. Current and historic woodlands

For sites ranked "No" or "Low", no additional work is recommended at this time. Should a facility's permitting or regulatory status change between now and the time acquisitions are initiated, additional screening should be conducted.

For the proposed pond sites with risk rankings of "Medium" or "High", Tierra recommends Level II field screening to determine if environmental impacts exist at the preferred pond sites. Regardless of the risk ranking, all ponds sites selected for final design will require Level II field screening. The field screening scope of work should include, at a minimum, soil borings to the proposed depth of the pond and soil sampling for total arsenic. Additional sample analyses may be required based on historical land use of the pond site and surrounding properties. The District Contamination Impact Coordinator should be consulted regarding the field screening scope of work for all final pond sites.

Definitions, Acronyms, and Abbreviations

HAZARDOUS MATERIAL: Any material which has, or, when combined with other materials will have a deleterious effect on people or the environment. As further discussed and defined in Title 42 United States Code (USC), Section 9601, et seq.

HAZARDOUS WASTE: There are 80 pages in the Code of Federal Regulations (CFR) devoted to the definition and identification of Hazardous Waste. Briefly, the CFR defines hazardous waste as a solid waste (could be a liquid) that has not been excluded from regulation and meets the criteria as defined and discussed in Title 40, CFR, Part 261.3, et seq.

CONTAMINATION: The presence of any regulated material / chemical contained within the soil, surface water or groundwater on or adjacent to Department property, or proposed property, that may require assessment, remediation, or special handling, or that has a potential for liability. These materials would include, but not be limited to, those substances normally referred to as petroleum or petroleum products.

SIGNIFICANT CONTAMINATION: The presence of any contamination that would meet the definition of "hazardous materials" or "hazardous waste" and be regulated under CERCLA or RCRA. Petroleum contamination from underground storage tanks is not regulated by CERCLA or RCRA.

AST Aboveground Storage Tank

BLS Below Land Surface

CDV Cattle Dip Vat

CERCLA Comprehensive Environmental Response, Compensation, and Liability Act

De minimis Lacking significance or of minimum importance as to merit disregard

EDR Environmental Data Resources, Inc.

EPA United States Environmental Protection Agency EROS Earth Resource Observation and Science Center

FAC Florida Administrative Code

FDEP Florida Department of Environmental Protection

FDOT Florida Department of Transportation
GCTL Groundwater Clean-up Target Levels
LUST Leaking Underground Storage Tank
NADC Natural Attenuation Default Concentrations

NEPA National Environmental Policy Act

NFA Notice of No Further Action

NGVD National Geodetic Vertical Datum of 1929

NPDES National Pollutant Discharge Elimination System

NRCS National Resource Conservation Service
PD&E Project Development and Environment
RCRA Resource Conservation and Recovery Act

ROW Right-of-Way

SCS Soil Conservation Service SCTL Soil Clean-up Target Levels

SRCO Site Rehabilitation Completion Order
USDA United States Department of Agriculture

USGS United States Geological Survey UST Underground Storage Tank

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1.0 Project Description

The Florida Department of Transportation, District One, is conducting a Project Development and Environmental (PD&E) Study regarding the proposed new road construction (extension to the northwest of existing SR 710) of SR 710 from US 441 to L-63 Canal in Okeechobee County, Florida. The project includes constructing an extension of SR 710 around the northeast side of Okeechobee. The new roadway will have a design speed of 50 mph and will be a high-speed urban four-lane roadway, including a 12-foot multi-use path on one side and five foot sidewalk on the other.

Initially, sixteen (16) Proposed Pond Alternatives were received from the client by email in October 2013. Updated Proposed Pond Alternatives were received from the client in March 2014. There are now a total of twenty-three (23) pond site options identified for evaluation; all are located offsite along or near the proposed new alignment. The project also includes bridge work at the L-63 Canal.

The locations and limits of the pond sites are presented on the Proposed Pond Alternative Location Maps in **CSER-Appendix A**. Also included are the Project Aerial Map Figure 1 (which includes the proposed roadway alignment for SR 710) and the Pond Aerials Figures 12A to 12O, provided by the client and presented in **CSER-Appendix E**.

2.1 Ponds 1A, 1B and 1C

The proposed pond alternatives are all located west of Taylor Creek and north of NW 13th Street in Okeechobee, Florida. Ponds 1B and 1C are both located east of North Parrott Avenue (US Highway 441) and Pond 1A is located west of Parrott Avenue. The specific locations are shown on a recent aerial photographs presented in **CSER-Appendix A** and in **CSER-Appendix E**.

During site reconnaissance, Pond 1A was observed as woodlands; Pond 1B was observed as an open, grassy area with some wooded portions. An apiary (bee nursery) was located onsite near the eastern boundary of Pond 1B. Pond 1C was observed as woodlands. Surrounding properties in the vicinity of Pond 1A include residential neighborhoods approximately 300 feet to the northwest and 150 feet to the southwest. Two manmade ponds were noted approximately 170 feet to the north and 120 feet to the northeast. Developed properties in the surrounding vicinity of Ponds 1B and 1C include Taylor Creek to the east, followed by Okeechobee Utility Authority (water treatment plant constructed about 1994) approximately 120 feet to the east, and Okeechobee Health & Rehabilitation Center approximately 350 feet northwest. The location of the Okeechobee Utility Authority and Okeechobee Health & Rehabilitation Center are indicated on Sheet A-1, Proposed Pond Alternatives Location Map in **CSER-Appendix A**.



Photo 1: View to the north across Pond 1A



Photo 2: View to the north from southeast corner of Pond 1B of onsite bee hives



Photo 3: View to the south from northern boundary of Pond 1C

Historical aerial photographs dated 1940, 1953, 1962, 1970, 1983, 1994, 1999, 2004, 2005, 2006, 2007, 2009, 2010, 2011, and 2012 were reviewed from University of Florida Map & Imagery Library (UF), FDOT Survey & Mapping (FDOT) and Google Earth. A summary of our review is depicted in the table below. Copies of select aerial photographs are included in **CSER-Appendix B**.

Table 1						
Year	Comment	Source				
1940 - 1983	Ponds 1A, 1B, 1C: Undeveloped and wooded land 1962 offsite north: Pond 1A – earthwork/excavation activities are apparent 1970 offsite east: Pond 1B & 1C – Man-made modifications (earthwork) to Taylor Creek	UF, FDOT				
1994 - 2012	Ponds 1A, 1C : Undeveloped and wooded land 1994: Pond 1B – Possible construction staging area for water pipeline installation to offsite east WTP (under construction)	FDOT & Google Earth				

The USGS 7.5-Minute "Taylor Creek SE, Florida" Quadrangle, published in 1983 was reviewed. Pond 1A is shaded white indicating undeveloped or vacant land with a small swamp or marsh located onsite along the central section of the southern boundary. Pond 1B and 1C are shaded white indicating undeveloped or vacant land. Approximate elevation of the land in the area is 25 feet. No structures are depicted onsite. Taylor Creek is depicted to the east of these pond alternatives, but is not labeled on the topographic map. A copy of the topographic map is included in **CSER-Appendix C**.

Regulatory Review

An environmental database search, using Environmental Data Resources, Inc. (EDR) was conducted in October 2013, to identify facilities onsite or within close proximity to the proposed pond alternatives, containing documented or suspected petroleum contamination or other hazardous materials. The regulatory review of federal and state environmental records utilizes an integrated geographic information system database. The search was conducted as a preliminary screening tool to identify facilities that are registered with various county, state, and federal agencies. A copy of the EDR report is included in **CSER-Appendix D**. Supplemental regulatory documentation was reviewed from the EPA's and FDEP's online resources.

Hi-Tek Automotive, an auto repair shop, was not listed in any regulatory reports but was noted to be approximately 500 feet east of Pond 1A. Its location is indicated on Sheet A-1 of **CSER-Appendix 1**.

Risk Ranking

Based on the aerial photographs and regulatory documentation reviewed, Pond 1A and Pond 1C have been historically undeveloped and wooded land. Therefore they are given a risk ranking of "No". Based on the unidentified use of the southeast portion of Pond 1B, as seen in the 1994 aerial photograph and lack of regulatory documentation, Pond 1B is given a potential Risk Ranking of "Low".

2.2 Ponds 2A, 2B and 2C

The proposed pond alternatives are all located generally north of NE 9th Street, east of Taylor Creek and west of the L-63 Canal in Okeechobee, Florida. The specific locations are shown on a recent aerial photographs presented in **CSER-Appendix A** and in **CSER-Appendix E**. During site reconnaissance, Ponds 2A (Options 1, 2 & 3), 2B (Options 1, 2 & 3), and 2C (Options 1 & 2) were observed primarily as pastureland with some wooded areas.



Photo 4: View to the west across Pond 2A from southeastern corner Appendix 4 - Page 10 of 220



Photo 5: View to the south across Pond 2B from northern boundary



Photo 6: View to the northeast across Pond 2C from western boundary

Historical aerial photographs dated 1940, 1953, 1962, 1970, 1983, 1994, 1999, 2004, 2005, 2006, 2007, 2009, 2010, 2011, and 2012 were reviewed from UF, FDOT and Google Earth. A summary of our review is depicted in the table below. Copies of select aerial photographs are included in **CSER-Appendix B**.

	Table 2					
Year	Year Comment					
1940 - 2012	Ponds 2A and 2B: Pastureland/Woodlands Pond 2C: Pastureland/Woodlands/Wetlands	UF, FDOT & Google Earth				

The USGS 7.5-Minute "Taylor Creek SE, Florida" Quadrangle, published in 1983 was reviewed. Ponds 2A, 2B, and 2C are shaded white indicating undeveloped or vacant land. Approximate elevation of the land in the area is 20 to 25 feet. No structures are depicted onsite. Taylor Creek is depicted to the west, and the L-63 Canal is depicted to the east, however both are not labeled. A copy of the topographic map is included in **CSER-Appendix C**.

Regulatory Review

No regulated sites were identified on or within close proximity to the proposed pond alternatives 2A, 2B, and 2C. A copy of the EDR report is included in **CSER-Appendix D**.

Risk Ranking

Based on the historical uses as woodlands and pastureland, Ponds 2A, 2B, and 2C are each given a potential Risk Ranking of "No".

2.3 Ponds 3A, 3B and 3C

The proposed pond alternatives are all located east of NE 32nd Avenue, north and south of SR 70, and west of the L-63 Canal in Okeechobee, Florida. The specific locations are shown on a recent aerial photographs presented in **CSER-Appendix A** and in **CSER-Appendix E**.

During site reconnaissance, Pond 3A (formerly named Pond 3B) was observed to be pastureland with a livestock holding pen (see Photo 8) situated in the southern portion; Pond 3B (formerly named Pond 3A) was observed to be undeveloped land; and Pond 3C was observed as vacant, cleared and wooded land, no signs of soil staining, stressed vegetation, odors or other indications of a potential contamination concern were observed. Pond 3A is adjoined by the L-63 Canal to the east and SR 710 to the south. The Florida Power and Light (FPL) Company service center (Fac. ID 8519987) is located approximately 220 feet southwest of Pond 3C (discussed in following regulatory review). One residence is located approximately 400 feet west of Pond 3C. The FPL facility location is indicated on Sheet A-3, Proposed Pond Alternatives Location Map in CSER-Appendix A.



Photo 7: View to the north across Pond 3B from southern boundary



Photo 8: Livestock holding pen located on Pond 3A



Photo 9: View to the north across Pond 3A from southeastern section



Photo 10: View to the east across Pond 3C from western boundary

Historical aerial photographs dated 1940, 1953, 1962, 1970, 1983, 1994, 1999, 2004, 2005, 2006, 2007, 2009, 2010, 2011, and 2012 were reviewed from UF, FDOT and Google Earth. A summary of our review is depicted in following the table. Copies of select aerial photographs are included in **CSER-Appendix B**.

	Table 3					
Year	Year Comment					
1940 - 1953	Pond 3A, 3B and 3C: Pastureland/Woodlands/Wetlands	UF & FDOT				
1962	Offsite: Pond 3A and 3C adjoined by man-made ditch and unpaved tracks	UF & FDOT				
1970	Offsite: Cleared land (for construction of the L-63 Canal) is apparent to the east of Pond 3A	UF & FDOT				
1983 - 1994	Pond 3A is depicted as cleared land. Pond 3B and 3C appear unchanged. Offsite: the L-63 Canal is apparent to the east of Pond 3A	FDOT & Google Earth				
1999	Pond 3C: a structure with an unpaved parking area is depicted in the southwest Corner Offsite: A man-made stormwater pond is depicted to the north of Pond 3A	Google Earth				
2004	Pond 3C: Southwest corner cleared of structure, possible automobile parking or junk yard	Google Earth				
2005	Pond 3C: Southwest corner is cleared of vehicles, former building footprint is still apparent	Google Earth				
2009 - 2012	Ponds 3A, 3B, 3C: Generally remain the same, undeveloped Pond 3A: Vegetative re-growth is apparent, a cattle pen is noted in the eastern portion of the pond	FDOT & Google Earth				

The USGS 7.5-Minute "Taylor Creek SE, Florida" Quadrangle, published in 1983 was reviewed. Ponds 3A and 3B are depicted with small areas of marsh or swamp. Pond 3C is shaded white, indicating undeveloped or vacant land. Approximate elevation of the land in the area is 25 feet. SR 70 and the L-63 Canal are depicted, but are not labeled. No structures are depicted onsite. A copy of the topographic map is included in **CSER-Appendix C**.

Regulatory Review

One (1) site was identified in close proximity to Pond 3C. The Florida Power & Light Company Service Center (Fac. ID 8519987), 825 N.E. 34th Avenue is located approximately 220 feet west of Pond 3C. This facility was identified on the LUST, AST, UST, FINDS and Tier 2 regulatory databases. According to the EDR report one (1) 3,000-gallon unleaded gasoline AST that was installed in November 2007 is currently maintained at this site. Tierra identified the AST approximately 280 feet southwest of Pond 3C during the site reconnaissance. The FPL facility location is indicated on Sheet A-3, Proposed Pond Alternatives Location Map in **CSER-Appendix A**. A copy of the EDR report is included in **CSER-Appendix D**.

A Contamination Assessment Report (CAR) by Atlanta Testing and Engineering, dated October 5, 1993 included a map which identified one former 5,000-gallon UST to be located approximately 650 feet west of Pond 3C. The report included a map indicating shallow groundwater flow was generally toward the southwest, away from the pond site.

A Site Characterization Screening Letter Report dated December 2012 reveals the former UST was installed in 1974 and situated on the western portion of Florida Power & Light Company Property approximately 530 feet west of the nearest pond, Pond 3C. This UST was first stated to contain gasoline and was later changed to vehicular diesel.

A discharge notification form was submitted to the FDEP in 1992 based on groundwater sample analysis from the UST monitoring wells. The UST was removed in September 1992 in conjunction with source removal of an estimated 784 tons of contaminated soil.

Site screening activities included soil and groundwater sampling (performed by ARCADIS) in November 2012. The laboratory analysis indicated VOC's above applicable GCTL's and SCTL's. According to FDEP the discharge status is currently active and cleanup is ongoing, effective in October 2000. Based on distance from Pond 3C, this facility is not considered a significant contamination concern at this time. Applicable pages from these reports have been included in **CSER-Appendix E**.

Risk Ranking

Based on the current use of Pond 3A as pastureland with an observed livestock holding pen, plus the typical use of herbicides/pesticides associated in these areas, Pond 3A is given a Risk Ranking of "Medium". Based on the historical use of Pond 3B as pastureland and wetlands, it is given a potential risk ranking of "No". Based on the general undeveloped use and that no signs of soil staining, stressed vegetation, odors or other indications of potential contamination conditions were observed on Pond 3C, the former presence of an adjoining unknown structure and possible auto junk yard (noted in the 1999 to 2005 aerials) is not considered a concern. Therefore, Pond 3C is given a potential Risk Ranking of "Low".

2.4 Ponds 4A, 4B, 4C and 4D

The proposed pond alternatives 4A, 4B, 4C and 4D are located west of the L-63 Canal and north and south of the existing SR 710 in Okeechobee, Florida. The specific locations are shown on a recent aerial photographs presented in **CSER-Appendix A** and in **CSER-Appendix E**.

During site reconnaissance, the pond sites 4A (Options 1 & 2), 4B/4C (Option 1), 4B (Option 2) and 4D (Options 1 & 2) were observed as pastureland and woodlands with unpaved trails/tracks throughout. Two (2) gray metal sheds, an abandoned tractor and a livestock holding pen were observed near the central section of the northeastern on Pond 4C. One shed was locked and had a mailbox near the front door. Its use is unknown. The second shed contained several tires, a water well pump and several empty 1-gallon automotive fluid containers. The floor was mainly wood with some areas of bare soil. No obvious soil stains or petroleum odors were noted during the site reconnaissance. An operational retail fuel facility, Town Star #40/BP (Fac. ID 8630309), is located adjoining Pond 4D to the east and is discussed further in the following regulatory review section. The Town Star #40/BP location is indicated on Sheet A-4, Proposed Pond Alternatives Location Map in **CSER-Appendix A**.



Photo 11: View to the north across Pond 4A



Photo 12: View to the south across Pond 4B



Photo 13: Gray metal structure, in central portion of the northeastern boundary on Pond 4C



Photo 14: Livestock holding pen on Pond 4C



Photo 15: Inside of shed on Pond 4C



Photo 16: View to the east across Pond 4C towards an abandoned tractor



Photo 17: View to the south from northern boundary of Pond 4D

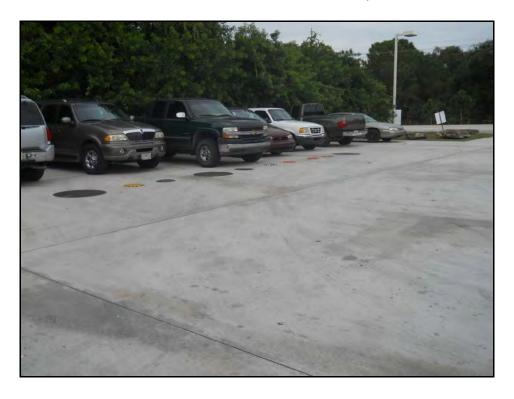


Photo 18: East adjoining Townstar #40/BP gas station tank farm

Historical aerial photographs dated 1940, 1953, 1962, 1970, 1983, 1994, 1999, 2004, 2005, 2006, 2007, 2009, 2010, 2011, and 2012 were reviewed from UF, FDOT and Google Earth. A summary of our review is depicted in the table below. Copies of select aerial photographs are included in **CSER-Appendix B**.

	Table 4						
Year	Comment	Source					
1940 - 1962	Ponds 4A, 4B, 4C and 4D: Pastureland/Woodlands/Wetlands Offsite: SR 710 is present	UF & FDOT					
1970 - 1983	Ponds 4A: possible spoil bank for L-63 Canal construction along the eastern boundary Ponds 4B and 4D: Pastureland/Woodlands Pond 4C: one structure is depicted in the central area Offsite: L-63 canal is apparent to the east of Pond 4A	FDOT					
1994 - 2012	Ponds 4A, 4B, 4C, 4D: Appear generally unchanged and undeveloped Offsite: A retail fuel station adjoins Pond 4D to the east	FDOT & Google Earth					

The USGS 7.5-Minute "Taylor Creek SE, Florida" Quadrangle, published in 1983 was reviewed. Ponds 4A and 4D are shaded white, indicating undeveloped or vacant land. Ponds 4B and 4C are shaded green and white, indicating undeveloped, wooded, or vacant land. Approximate elevation of the land is 25 feet. One structure is depicted on Pond 4C. No structures are depicted on Ponds 4A, 4B or 4D. L-63 Canal and SR 710 are depicted but not labeled. A copy of the topographic map is included in **CSER-Appendix C**.

Regulatory Review

Three (3) sites were identified in EDR's regulatory database report within close proximity to Ponds 4B and 4D. A copy of the EDR report is included in **CSER-Appendix D**.

The Florida Power & Light Company Service Center (Fac. ID 8519987)

This facility is located at 825 NE 34th Avenue located approximately 80 feet northwest of Pond 4B. This site was listed in the EDR report to have one (1) 3,000-gallon unleaded gas AST installed in November 2007, which is currently in service. During the site reconnaissance, the AST was observed and located approximately 170 feet northwest of Pond 4B. No discharge from this AST was identified in regulatory documentation reviewed. The FPL facility location is indicated on Sheet A-3, Proposed Pond Alternatives Location Map in **CSER-Appendix A**.

Additionally, one former 5,000-gallon unleaded gasoline UST was installed in 1974 and removed in 1992. A discharge report was filed on June 25, 1992 for an unleaded gasoline discharge (quantity not specified). A Contamination Assessment Report (CAR) by Atlanta Testing and Engineering, dated October 5, 1993 included a map which depicted the former 5,000-gallon UST location approximately 650 feet northwest of Pond 4B and indicated that shallow groundwater flow was generally toward the southwest, away from the pond site.

Based on its distance, current regulatory status and the reported groundwater flow direction away from the pond alternatives, this facility is not considered to be a potential contamination concern at this time. Applicable pages from these reports have been included in **CSER-Appendix E**.

Town Star #40/BP gas station (Fac. ID 8630309)

This facility is located at 3990 SR 710, adjoining to the east of Pond 4D (approximately 100 feet southwest of Pond 4A). During the site reconnaissance, this facility was identified as an operational Town Star/BP gas station. According to EDRs regulatory database report this facility had three (3) USTs installed in 1986 and removed in 2009. One (1) 22,000-gallon diesel/gasoline fuel UST installed in 2009 remains in-service. A discharge was reported on November 22, 1988. The Town Star #40/BP facility location is indicated on Sheet A-4, Proposed Pond Alternatives Location Map in **CSER-Appendix A**.

A Supplemental Site Assessment Report by Mactec, dated November 21, 2007 indicated three (3) permanent groundwater monitor wells were installed on Pond 4D. These wells are associated with assessment activities at the gas station. Laboratory results collected did not detect analytes above the applicable CTL's. OVA screening of the soils during well installation did not record measurements above 1 ppm. The groundwater flow map indicated the direction towards the northeast on Pond 4D.

A Source Removal Report by Gator Engineering and Aquifer Restoration, Inc. (GEAR), dated September 29, 2009 depicted the three (3) former USTs and the current UST to be located near the western boundary of the Townstar facility (approximately 10 feet east of Pond 4D). Approximately 345.5 tons of impacted soil was removed and disposed offsite during the tank removal. According to the report, laboratory analytical results of confirmation soil samples collected from the excavation were below SCTLs.

Cleanup activities have been completed at the Townstar facility and a SRCO was issued in September 23, 2013. Applicable pages of these reports have been included in **CSER-Appendix E**.

Chevron #47761 (Fac. ID 8512544)

This facility is located at 2768 SR 710 approximately 1,800 feet west of Pond 4B, the nearest pond alternative. Based on distance, this facility is not considered a potential contamination risk to the pond alternative and is not further discussed.

Risk Ranking

Based on the historically undeveloped use and the distance of the Townstar #40/BP gas station to Pond 4A, it is given potential risk ranking of "Low". Based on the historical land use of Pond 4B as undeveloped and wooded land, Pond 4B is given a potential risk ranking of "No". Based on the presence of a livestock holding pen and sheds, plus the typical use of herbicides/pesticides in these areas, Pond 4C is given a potential Risk Ranking of "Medium". Based on the current use of east adjoining property as a retail fuel station with documented historical discharge, Pond 4D has been given a potential Risk Ranking of "Medium".

2.5 Ponds 5A, 5B and 5C

The proposed pond alternatives are all located west of L-63 Canal, 5A and 5B are north of SR 710 and Pond 5C is located south of SR 710 in Okeechobee, Florida. The specific locations are shown on a recent aerial photographs presented in **CSER-Appendix A** and in **CSER-Appendix E**.

During site reconnaissance, the pond sites were observed as woodlands and pastureland. Pond 5B is part of Paddock Farms, a farm for miniature horses. A livestock holding pen was observed approximately 50 feet south of Pond 5C. The livestock holding pen location is indicated on Sheet A-4, Proposed Pond Alternatives Location Map in **CSER-Appendix A**.



Photo 19: View to the north across southern boundary of Pond 5A



Photo 20: View to the northwest across eastern portion of Pond 5B



Photo 21: View to the south across northern corner of Pond 5C

Historical aerial photographs dated 1940, 1953, 1962, 1970, 1983, 1994, 1999, 2004, 2005, 2006, 2007, 2009, 2010, 2011, and 2012 were reviewed from UF, FDOT and Google Earth. A summary of our review is depicted in the table below. Copies of select aerial photographs are included in **CSER-Appendix B**.

Table 5						
Year	Comment	Source				
1940 - 1962	Ponds 5A, 5B and 5C: Pastureland/Woodlands/wetlands Offsite: SR 710 is present	UF, FDOT				
1970 - 1999	Offsite: L-63 Canal is apparent to the west of Pond 5B	FDOT & Google Earth				
2004	Pond 5B: cleared of vegetation and fenced Offsite: A paved access road has been constructed between Pond 5A and 5B	Google Earth				
2005 - 2012	Ponds 5A, 5B, 5C: Pastureland/Woodlands	FDOT & Google Earth				

The USGS 7.5-Minute "Taylor Creek SE, Florida" Quadrangle, published in 1983 was reviewed. Ponds 5A, 5B and 5C are shaded white indicating undeveloped or vacant land. Approximate elevation of the land is 25 feet. No structures are depicted onsite. L-63 Canal and SR 710 are depicted but not labeled. A copy of the topographic map is included in **CSER-Appendix C**.

Regulatory Review

No regulated sites were identified on or within close proximity to the proposed pond alternatives 5A, 5B, and 5C. A copy of the EDR report is included in **CSER-Appendix D**.

Risk Ranking

Based on the historical use as pastureland, woodlands and wetlands, Ponds 5A and 5B are given potential risk rankings of "No". Based on the use of Pond 5C as pastureland/woodlands with a livestock holding pen observed offsite, approximately 50 feet south, Pond 5C is given a potential Risk Ranking of "Low".

3.0 Risk Ranking Summary

This Level I contamination screening evaluation has resulted in the following risk rankings for the proposed pond alternatives:

Proposed Pond Alternative	Risk Ranking	Comment			
Pond 1A	No	2.32-Acres. Current and historic woodlands			
Pond 1B	Low	1.20-Acres. Risk ranking Low for possible onsite use as water pipeline construction staging area in 1994. Current and historic woodlands with an apiary (bee hives) and open, grassy area			
Pond 1C	No	0.88-Acres. Current and historic woodlands			
Pond 2A – Option 1	No	14.23-Acres. Current and historic pastureland and woodlands			
Pond 2A – Option 2	No	7.93-Acres. Current and historic pastureland and woodlands			
Pond 2A – Option 3	No	6.42-Acres. Current and historic pastureland and woodlands			
Pond 2B – Option 1	No	15.37-Acres. Current and historic pastureland and woodlands			
Pond 2B – Option 2	No	10.00-Acres. Current and historic pastureland and woodlands			
Pond 2B – Option 3	No	7.08-Acres. Current and historic pastureland and woodlands			
Pond 2C – Option 1	No	6.86-Acres. Current and historic pastureland and woodlands			
Pond 2C – Option 2	No	6.14-Acres. Current and historic pastureland and woodlands			
Pond 3A (formerly 3B)	Medium	4.18-Acres. Risk ranking Medium for onsite livestock holding pen. Current pastureland, historic woodlands, wetlands, pastureland and cleared land			
Pond 3B (formerly 3A) No		2.44-Acres. Current and historic pastureland and wetlands			
Pond 3C Low		3.81-Acres. Risk ranking Low for onsite stormwater pond. Current and historic woodlands			
Pond 4A – Option 1	Low	3.98-Acres. Risk ranking Low for non-adjoining Townstar #40/BP gas station to the southwest. Current woodlands, historic wetland in northeast corner			
Pond 4A – Option 2	Low	3.34-Acres. Risk ranking Low for non-adjoining Townstar #40/BP gas station to the southwest. Current woodlands, historic wetland in northeast corner			
Pond 4B/4C – Option 1	Medium	8.17-Acres. Risk ranking Medium for onsite livestock holding pen. Current and historic woodlands with two (2) sheds, a livestock holding pen and unpaved trails			
Pond 4B – Option 2	No	4.59-Acres. Current and historic woodlands with unpaved trails			
Pond 4D – Option 1	Medium	6.08-Acres. Risk ranking Medium for east adjoining Townstar #40/BP gas station. Current and historic woodlands with unpaved trails/tracks; historic wetlands in northeast corner onsite from 1940 to 1960s. Adjoining operational Townstar #40/BP gas station to the east since 1986; three (3) groundwater monitor wells were installed on Pond 4D in 2007 to assess potential petroleum impacts. The laboratory analytical results did not indicate petroleum contaminants in exceedance of the GCTLs. The highest OVA reading during monitor well installation was one (1) ppm. No soil samples were collected for laboratory analytical testing during this Level I investigation.			

Proposed Pond Alternative	Risk Ranking	Comment			
Pond 4D – Option 2	A.33-Acres. Risk ranking Medium for Townstar #40/BP gas st Current and historic woodlands with unpaved transport to northeast corner onsite from 19				
Pond 5A	No	2.62-Acres. Current and historic woodlands/wetlands/pastureland			
Pond 5B	No	2.53-Acres. Pastureland and wetlands associated with north adjacent Paddock Farms (miniature horses)			
Pond 5C	Low	3.53-Acres. Risk ranking Low for offsite livestock holding pen, approximately 50 feet south. Current and historic woodlands			

For sites ranked "No" or "Low", no additional work is recommended at this time. Should a facility's permitting or regulatory status change between now and the time acquisitions are initiated, additional screening should be conducted.

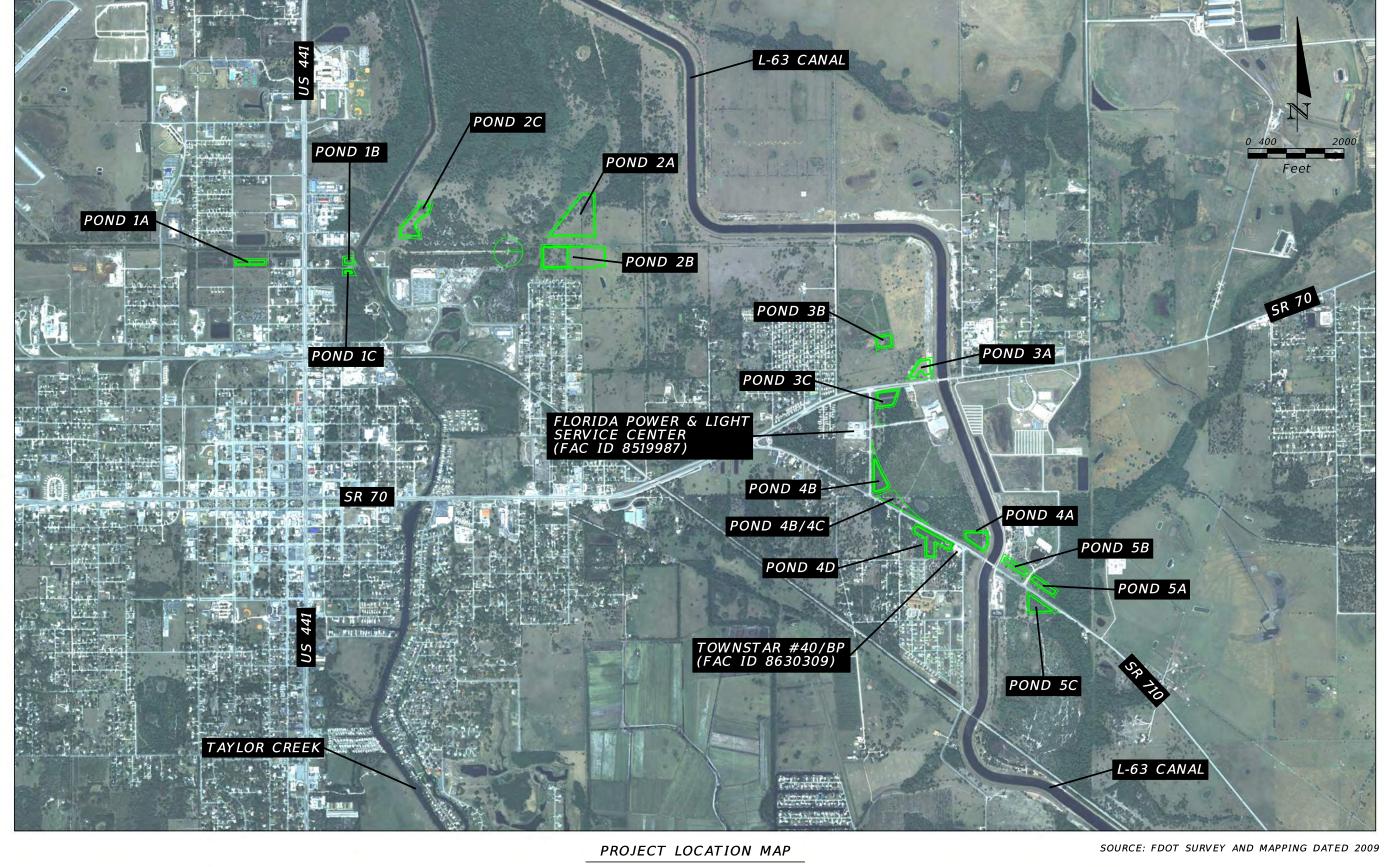
For the proposed pond sites with risk rankings of "Medium" or "High", Tierra recommends Level II field screening to determine if environmental impacts exist at the preferred pond sites. Regardless of the risk ranking, all ponds sites selected for final design will require Level II field screening. The field screening scope of work should include, at a minimum, soil borings to the proposed depth of the pond and soil sampling for total arsenic. Additional sample analyses may be required based on historical land use of the pond site and surrounding properties. The District Contamination Impact Coordinator should be consulted regarding the field screening scope of work for all final pond sites.

4.0 Limitations

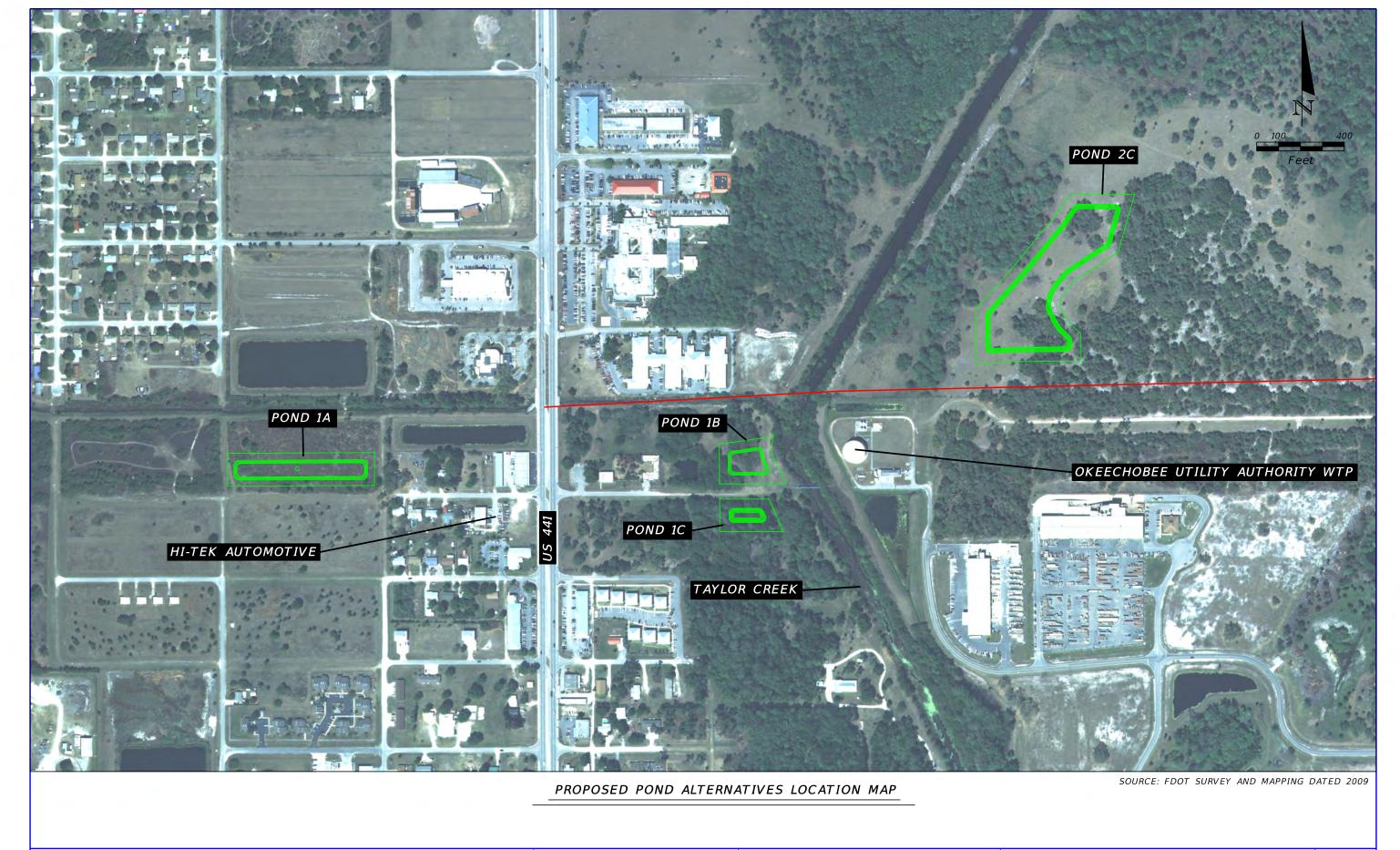
This study was conducted in a manner consistent with the level of care and skill ordinarily exercised by members of the profession currently practicing under similar conditions in the same locale. The results, findings, conclusions and recommendations expressed in this report are based on conditions observed during our course of work and under the scope of work authorized by the client. The information contained in this report is relevant to the date on which this survey was performed, and should not be relied upon to represent conditions at a later date. This report has been prepared on behalf of and exclusively for use by our client for specific application to their project as discussed above. Tierra does not warrant the work of reporting agencies or other third parties supplying information which may have been used in the preparation of this report. No warranty, expressed or implied is made.

CSER-Appendix A

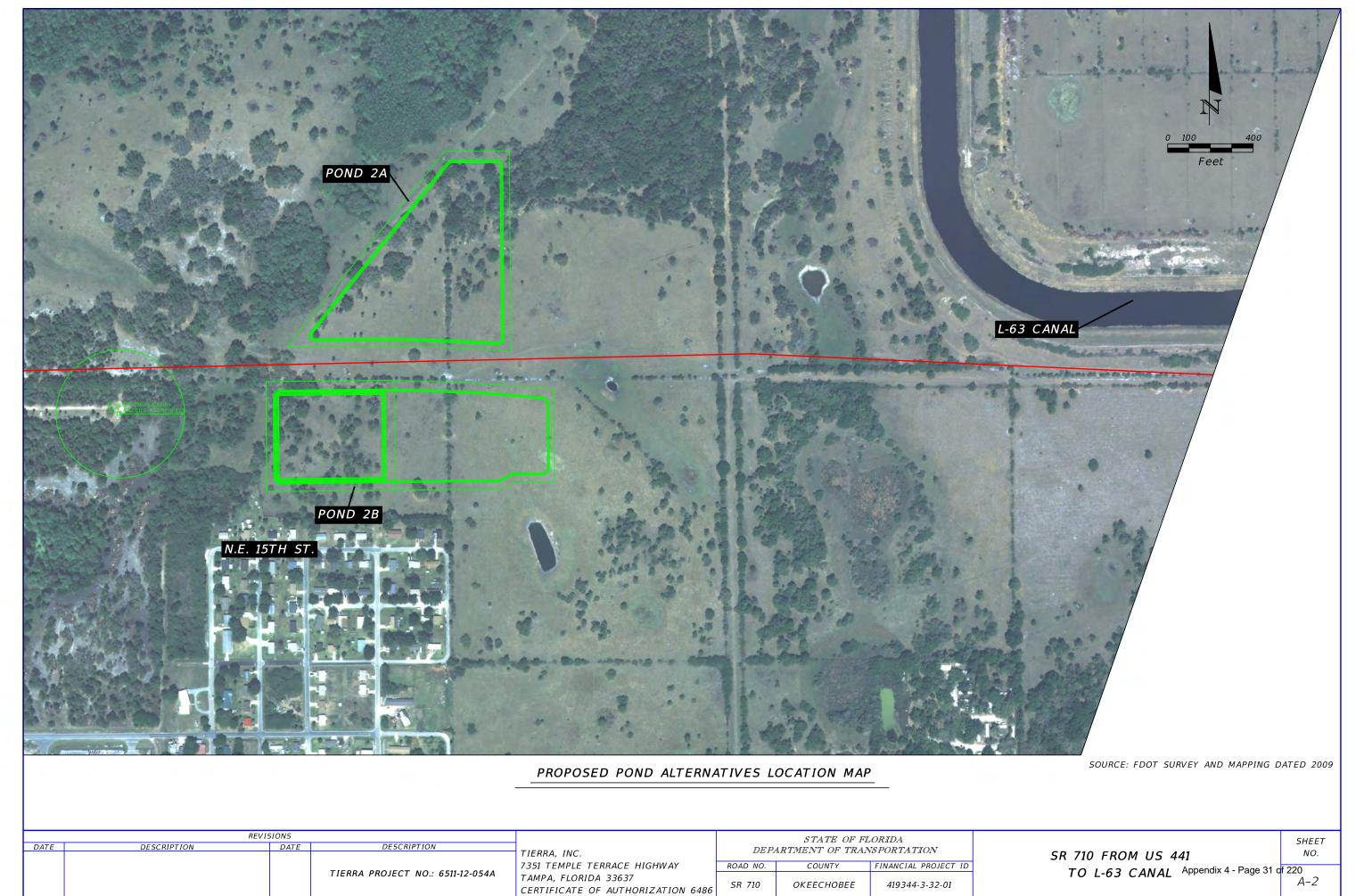
Project Location and Proposed Pond Alternatives Location Maps

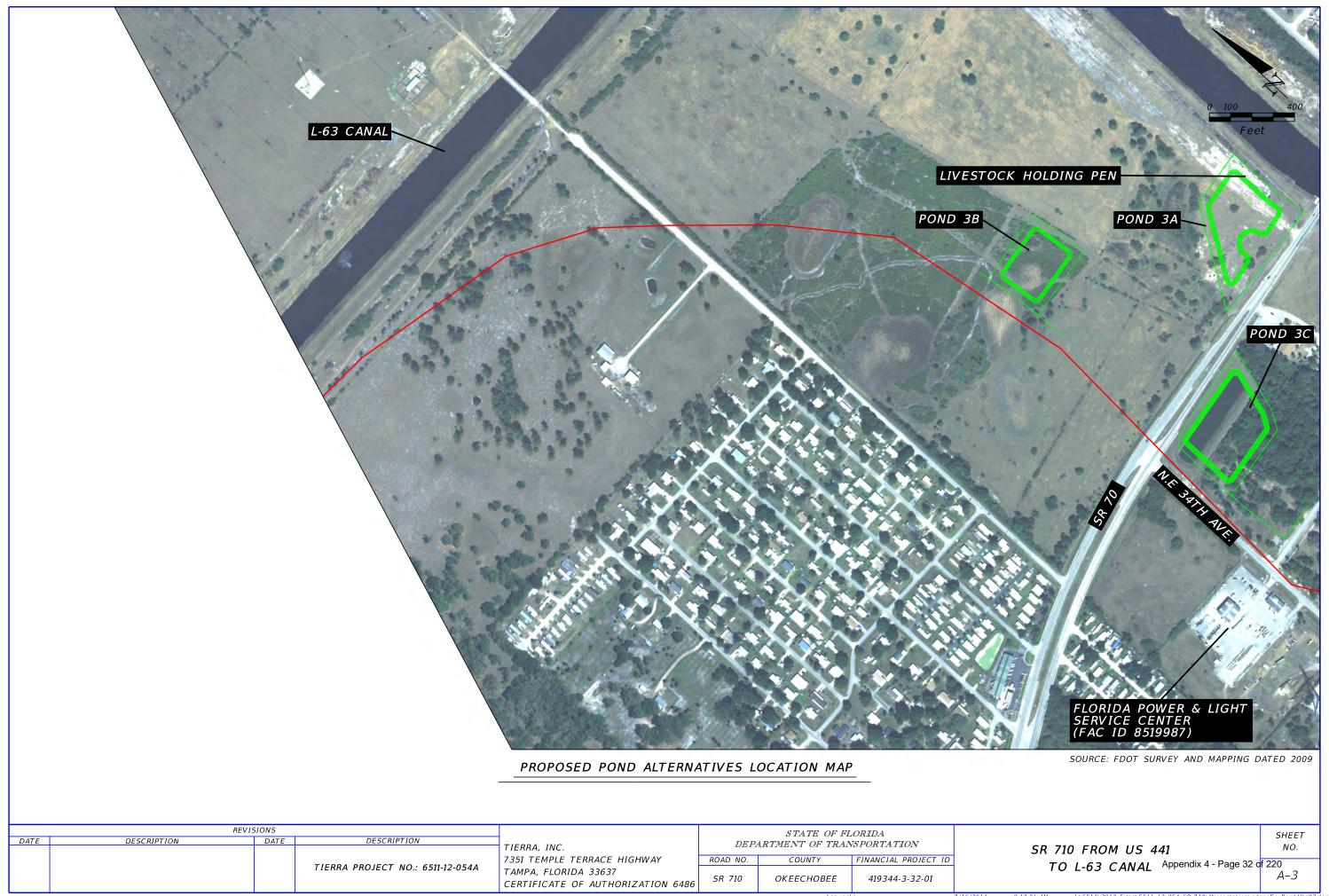


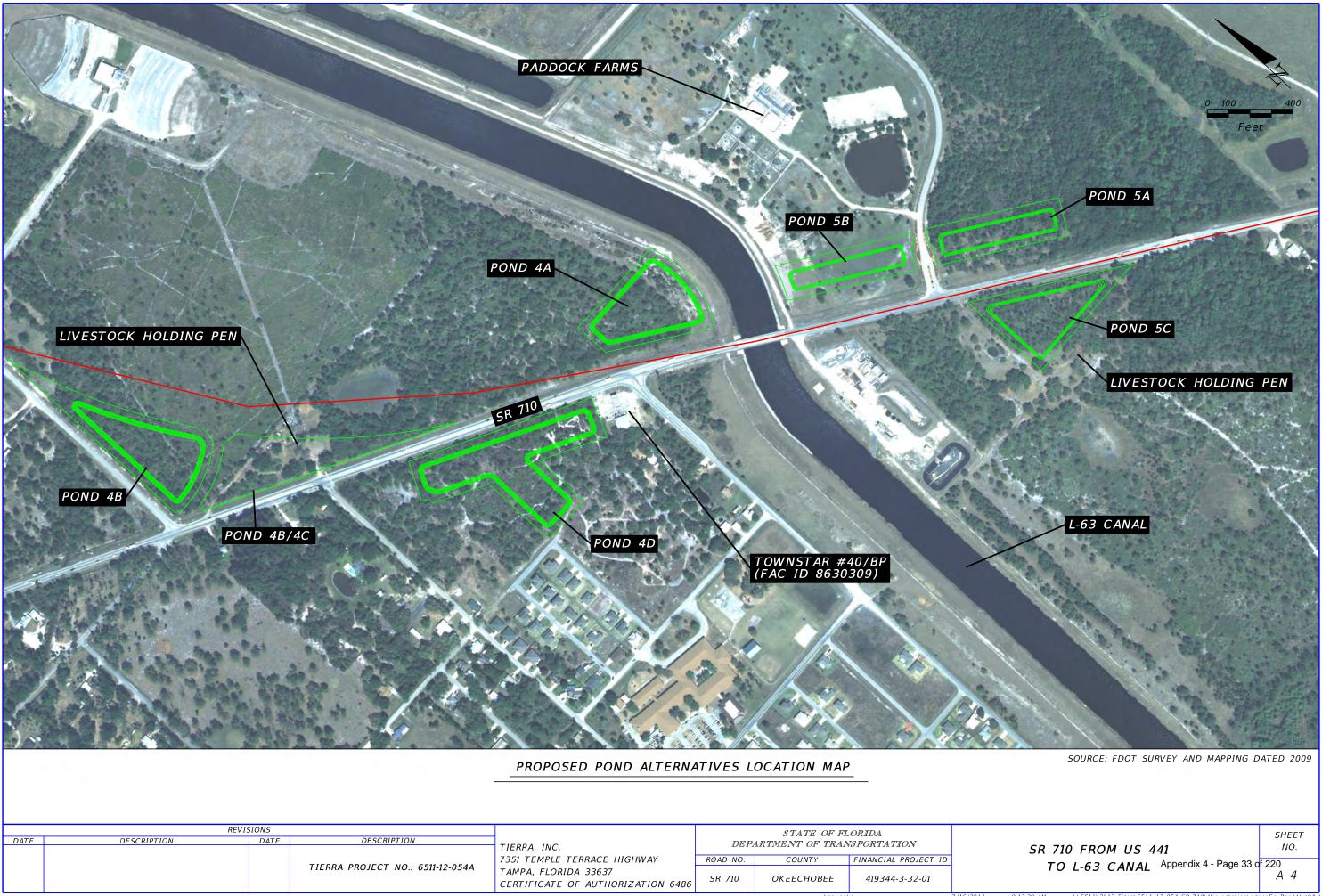
REVISIONS						STATE OF F	LORIDA		SHEET
DATE	DESCRIPTION	DATE	DESCRIPTION	TIERRA, INC.	DEP	ARTMENT OF TRAI		SR 710 FROM US 441	NO.
			TIERRA RROJECT NO. 654142.0544	7351 TEMPLE TERRACE HIGHWAY	ROAD NO.	COUNTY	FINANCIAL PROJECT ID		of 220
			TIERRA PROJECT NO.: 6511-12-054A	TAMPA, FLORIDA 33637 CERTIFICATE OF AUTHORIZATION 6486	SR 710	ОКЕЕСНОВЕЕ	419344-3-32-01	TO L-03 CANAL Appendix 4 Tage 20 0	A



DATE	REVIS DESCRIPTION	DATE	DESCRIPTION	TIERRA, INC.	DEP_{c}	STATE OF FI ARTMENT OF TRAI		SR 710 FROM US 441	SHEET NO.
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			TAMPA, FLORIDA 33637 CERTIFICATE OF AUTHORIZATION 6486	SR 710	ОКЕЕСНОВЕЕ	419344-3-32-01	TO L-03 CANAL Appoint 4 Tage 60 0	A-1	

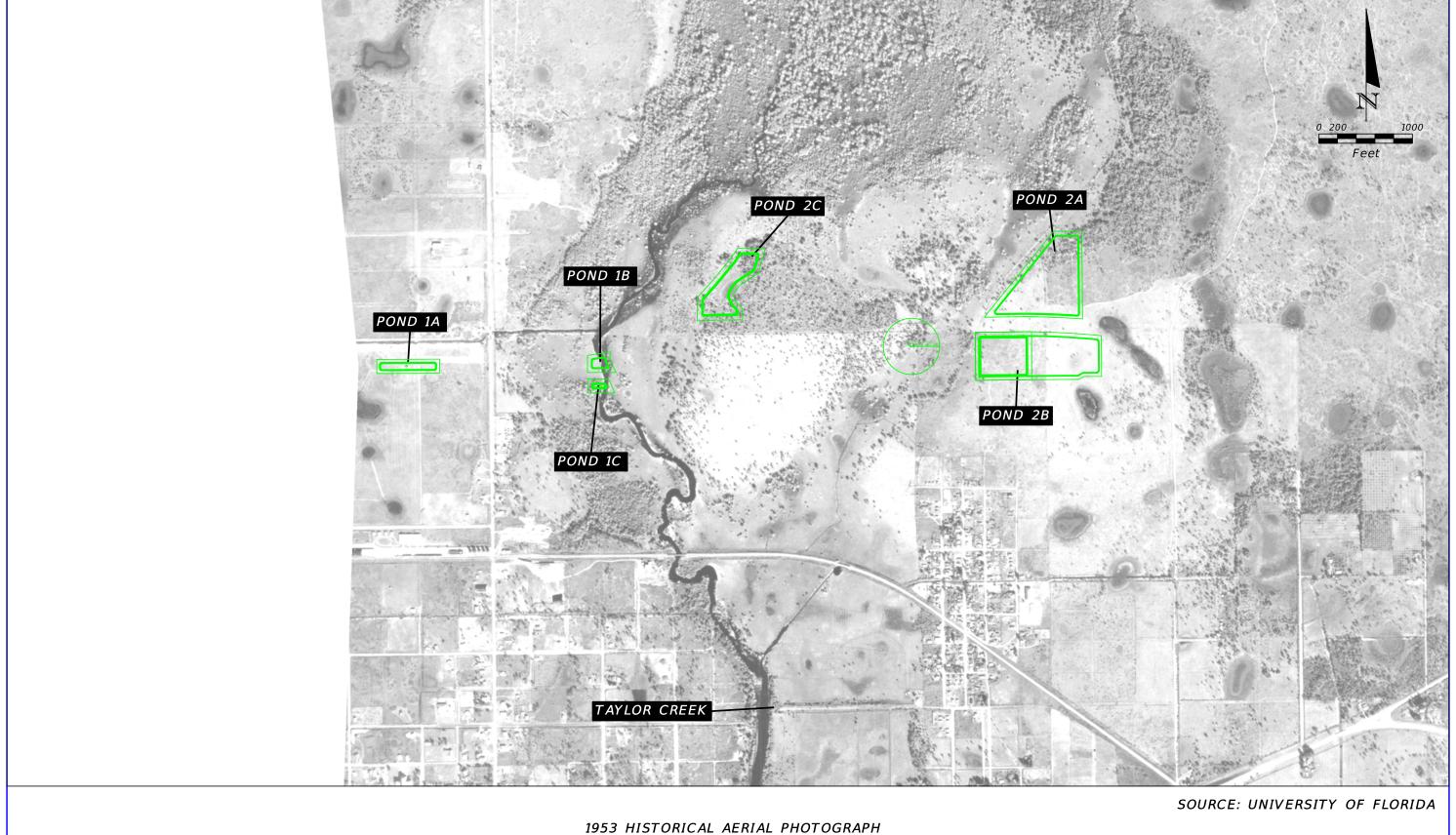




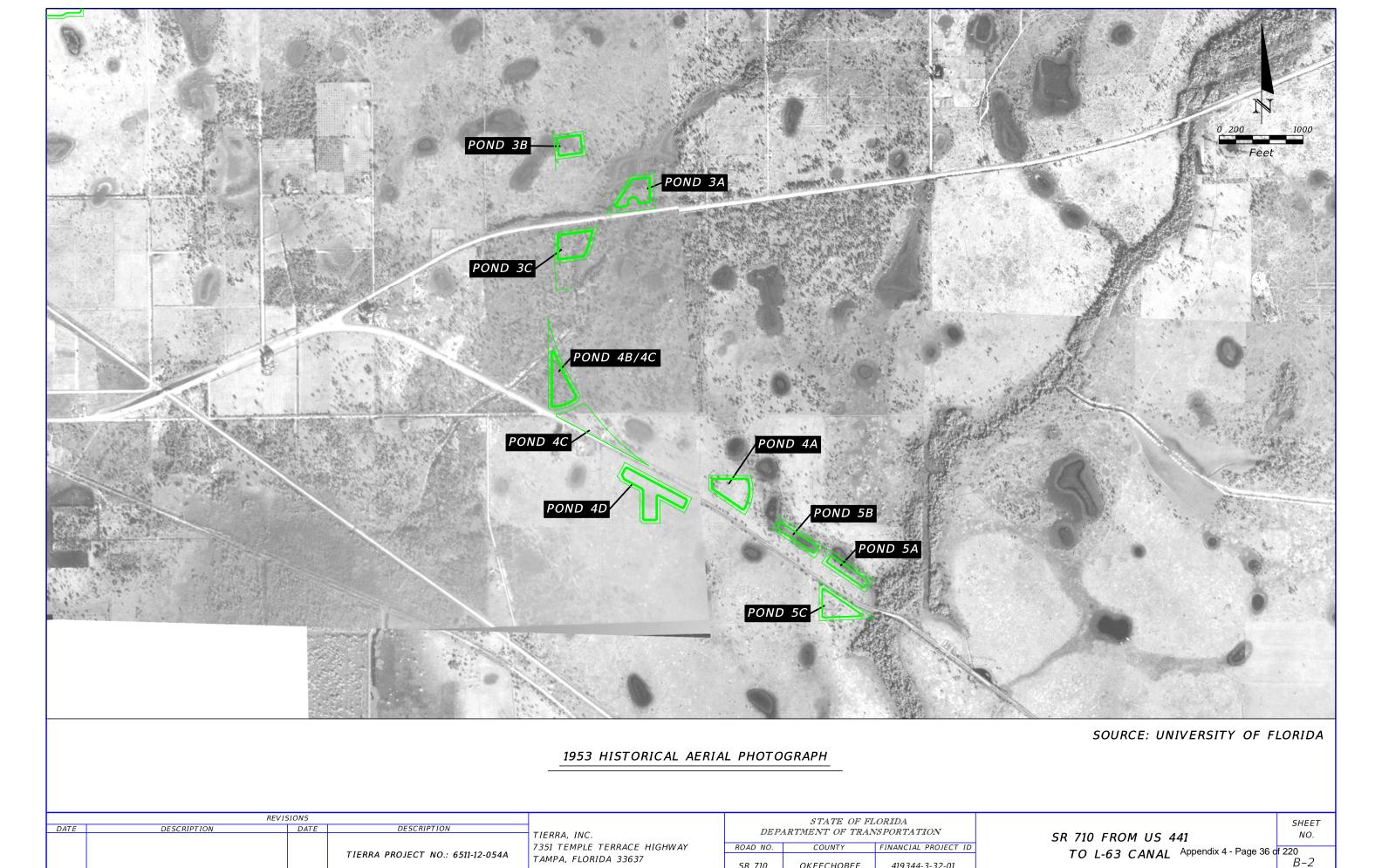


CSER-Appendix B

Historical Aerial Photographs



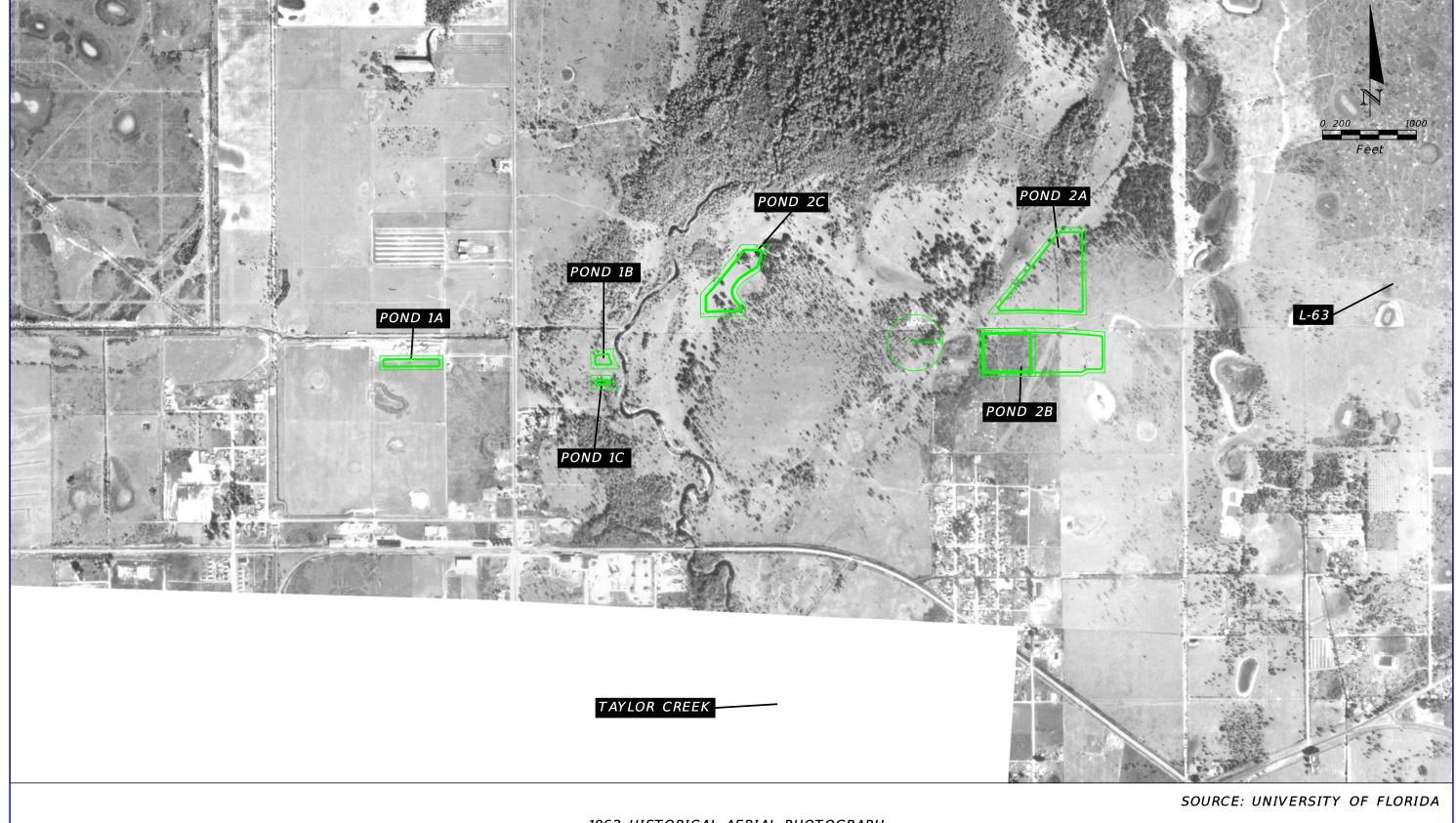
	REVISIONS				STATE OF F	LORIDA		SHEET
DATE	DESCRIPTION DA	<u>DESCRIPTION</u>	TIERRA, INC.	DEPA	RTMENT OF TRAI		SR 710 FROM US 441	NO.
		T15004 000450T NO 054440 0544	7351 TEMPLE TERRACE HIGHWAY	ROAD NO.	COUNTY	FINANCIAL PROJECT ID		220
		TIERRA PROJECT NO.: 6511-12-054A	TAMPA, FLORIDA 33637 CERTIFICATE OF AUTHORIZATION 6486	SR 710	OKEECHOBEE	419344-3-32-01	TO L-03 CANAL Appendix 4 Tage of di	B-1



CERTIFICATE OF AUTHORIZATION 6486

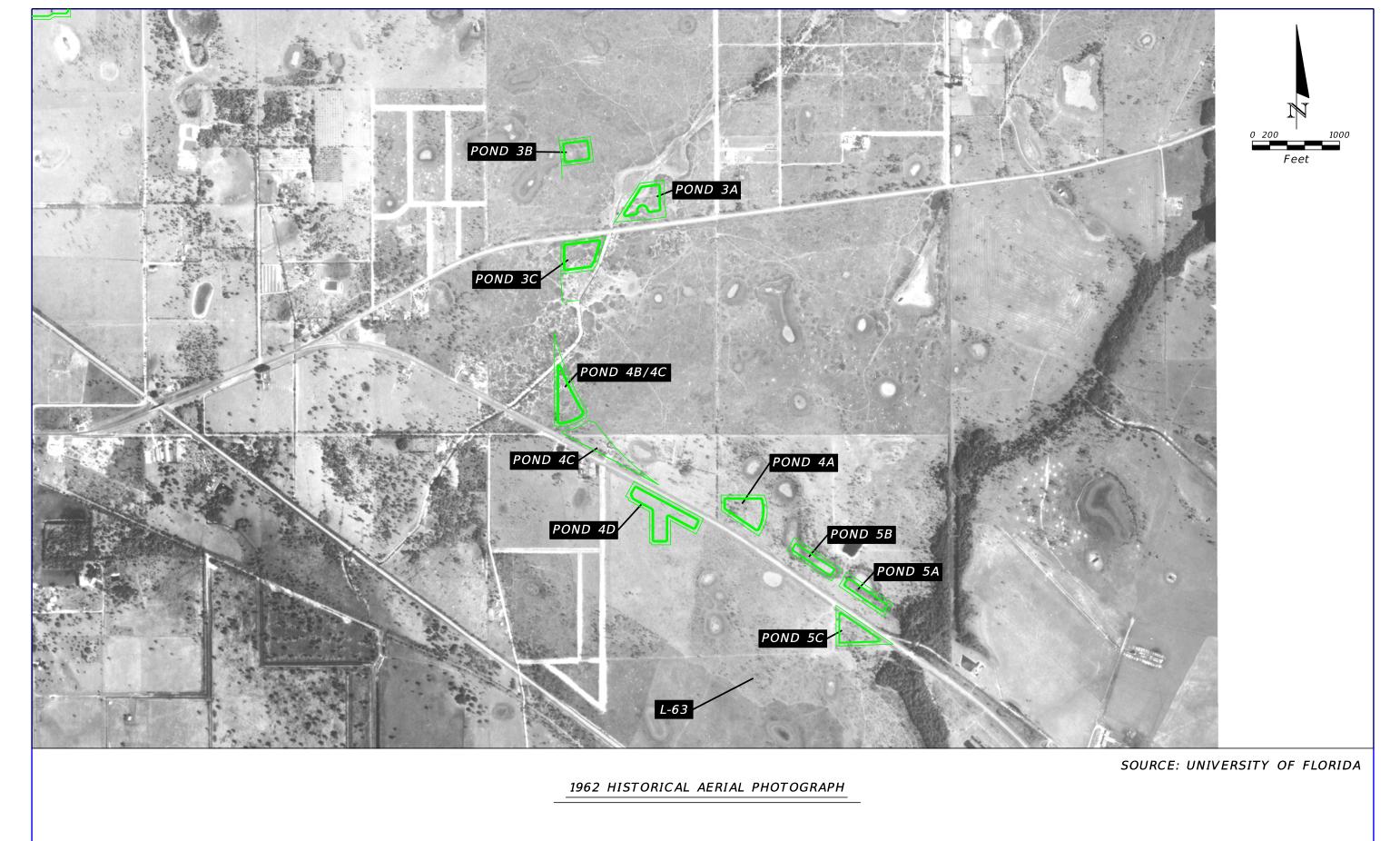
419344-3-32-01

OKEECHOBEE

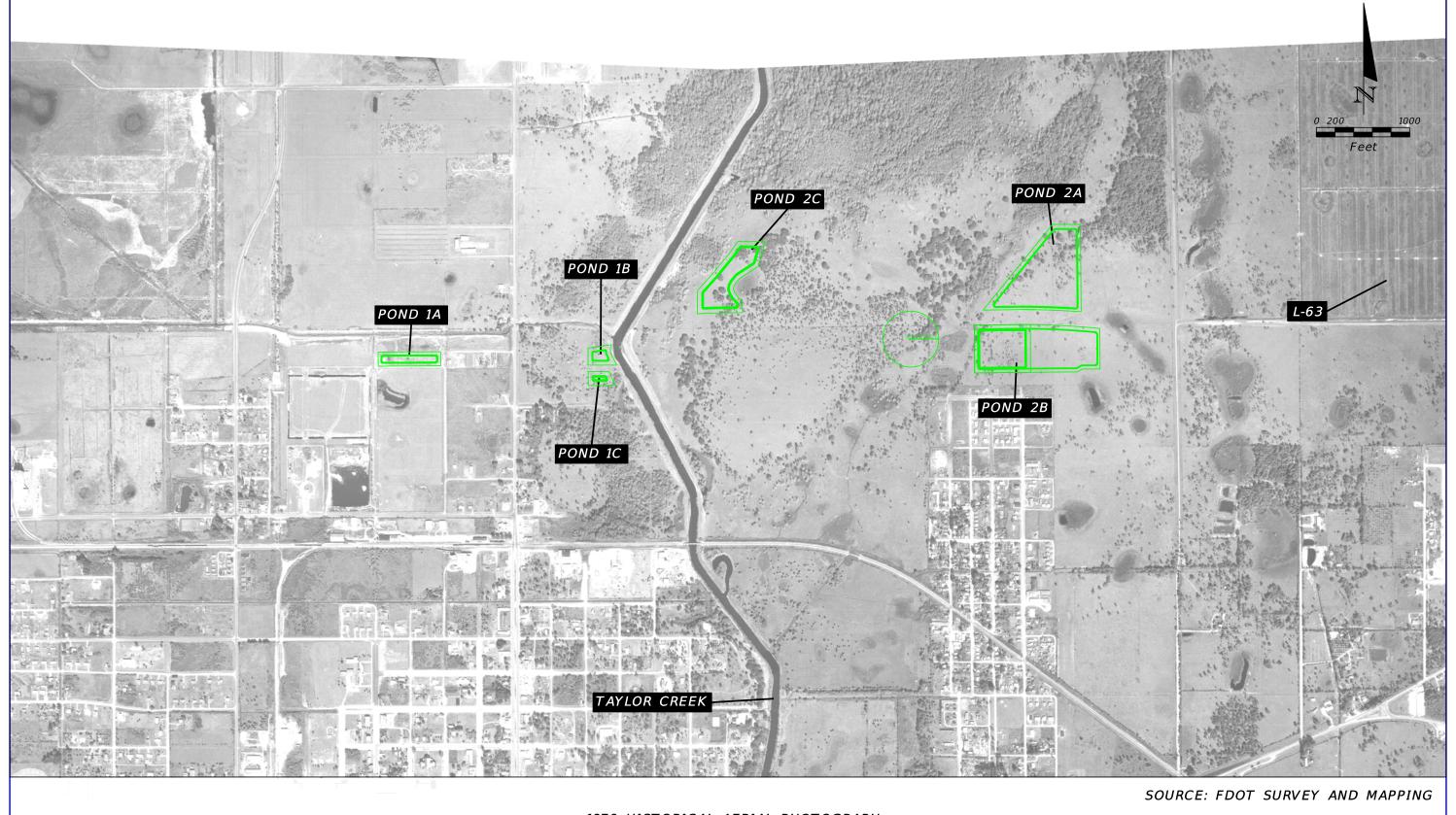


1962 HISTORICAL AERIAL PHOTOGRAPH

	REVI	SIONS				STATE OF FL	LORIDA		SHEET
DATE	DESCRIPTION	DATE	DESCRIPTION	TIERRA, INC.	DEP	ARTMENT OF TRAI	NSPORTATION	SR 710 FROM US 441	NO.
			TIERRA BROJECT NO. CEMAS OF AA	7351 TEMPLE TERRACE HIGHWAY	ROAD NO.	COUNTY	FINANCIAL PROJECT ID		of 220
			TIERRA PROJECT NO.: 6511-12-054A	TAMPA, FLORIDA 33637 CERTIFICATE OF AUTHORIZATION 6486	SR 710	ОКЕЕСНОВЕЕ	419344-3-32-01	TO L-03 CANAL Appointment age of a	B-3

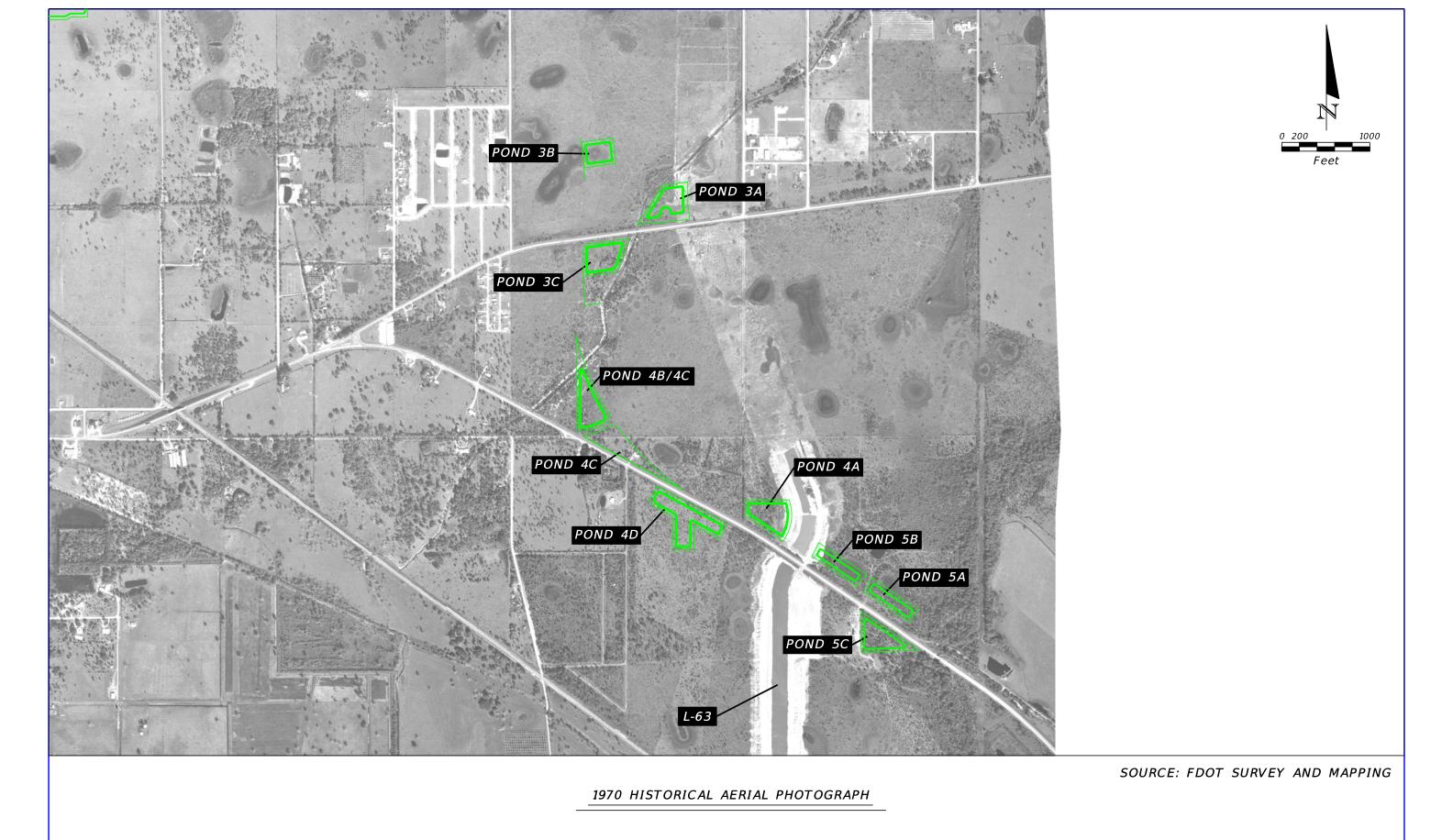


	REVI	SIONS				STATE OF FI	LORIDA		SHEET
DATE	DESCRIPTION	DATE	DESCRIPTION	TIERRA, INC.	DEP_{A}	ARTMENT OF TRAN		SR 710 FROM US 441	NO.
			TIEDDA DDO/50T NO. 0544 12.0544	7351 TEMPLE TERRACE HIGHWAY	ROAD NO.	COUNTY	FINANCIAL PROJECT ID		of 220
			TIERRA PROJECT NO.: 6511-12-054A	TAMPA, FLORIDA 33637 CERTIFICATE OF AUTHORIZATION 6486	SR 710	ОКЕЕСНОВЕЕ	419344-3-32-01	TO L-03 CANAL Appendix 1 rage of C	B-4

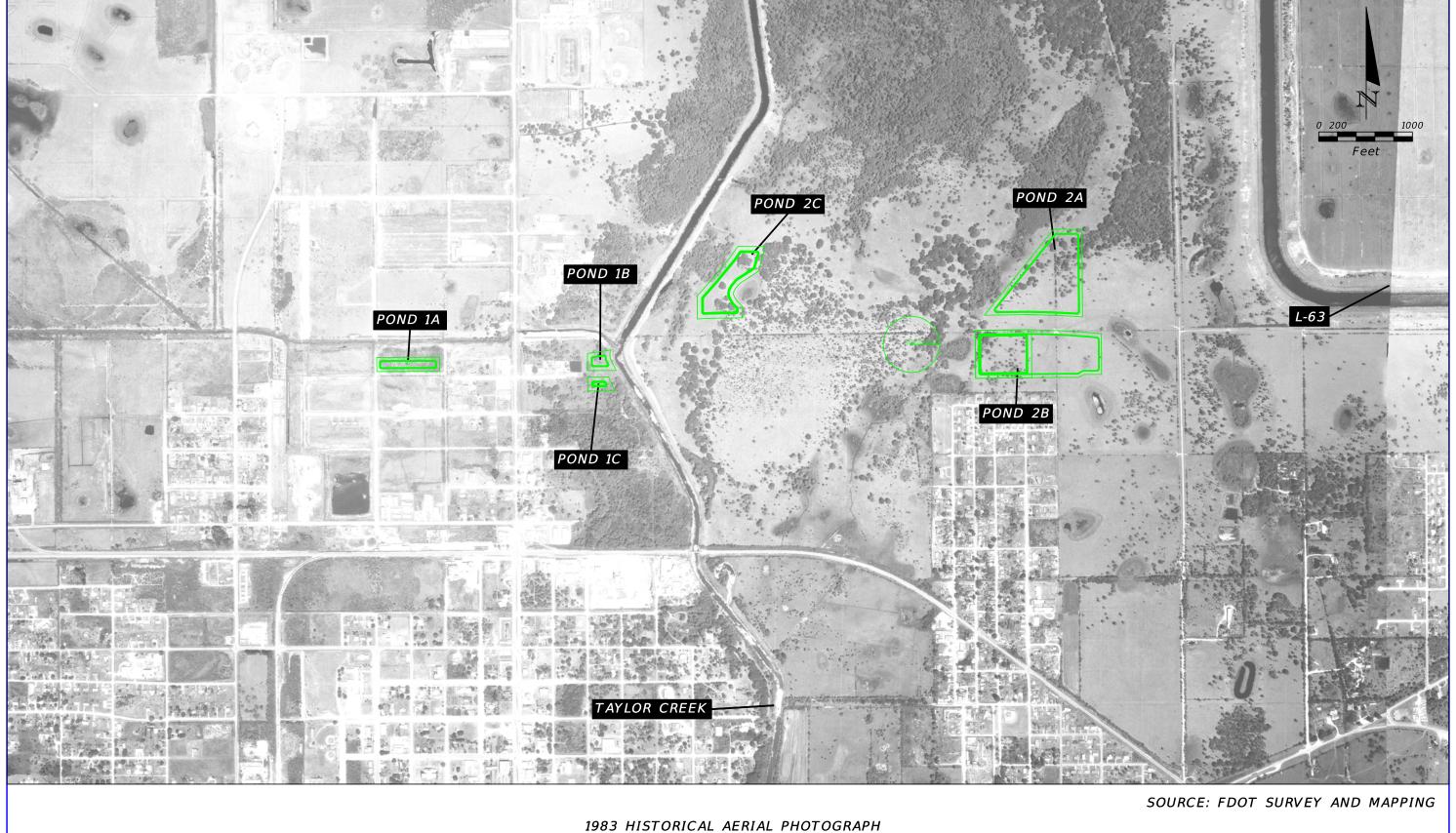


1970 HISTORICAL AERIAL PHOTOGRAPH

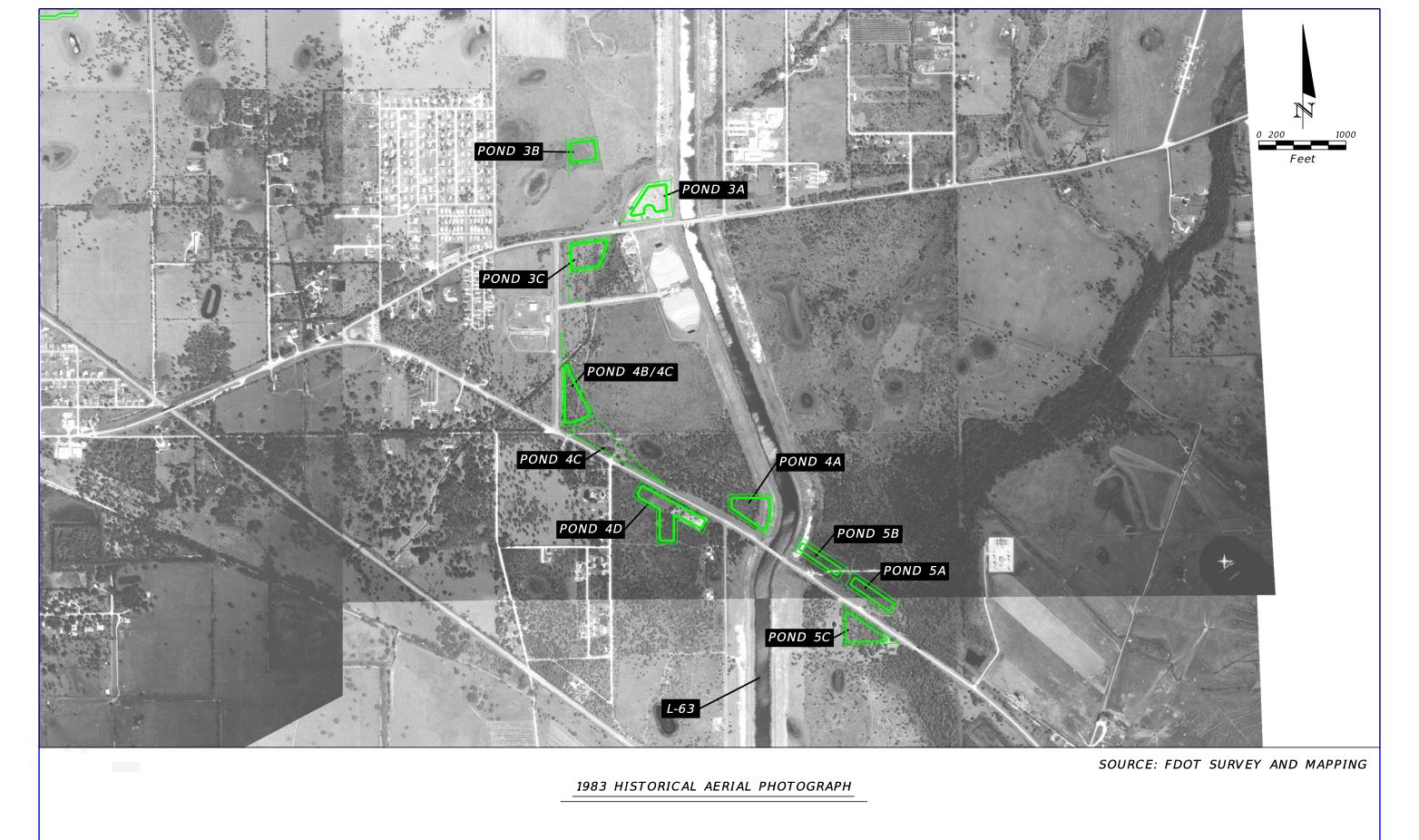
	REVI	SIONS				STATE OF FI	LORIDA		SHEET
DATE	DESCRIPTION	DATE	DESCRIPTION	TIERRA, INC.	DEP_{A}	ARTMENT OF TRAI	NSPORTATION	SR 710 FROM US 441	NO.
			TIEDDA DDO/50T NO. 0544 12.0544	7351 TEMPLE TERRACE HIGHWAY	ROAD NO.	COUNTY	FINANCIAL PROJECT ID		of 220
			TIERRA PROJECT NO.: 6511-12-054A	TAMPA, FLORIDA 33637 CERTIFICATE OF AUTHORIZATION 6486	SR 710	ОКЕЕСНОВЕЕ	419344-3-32-01	TO L-03 CANAL Appointment age of o	B-5



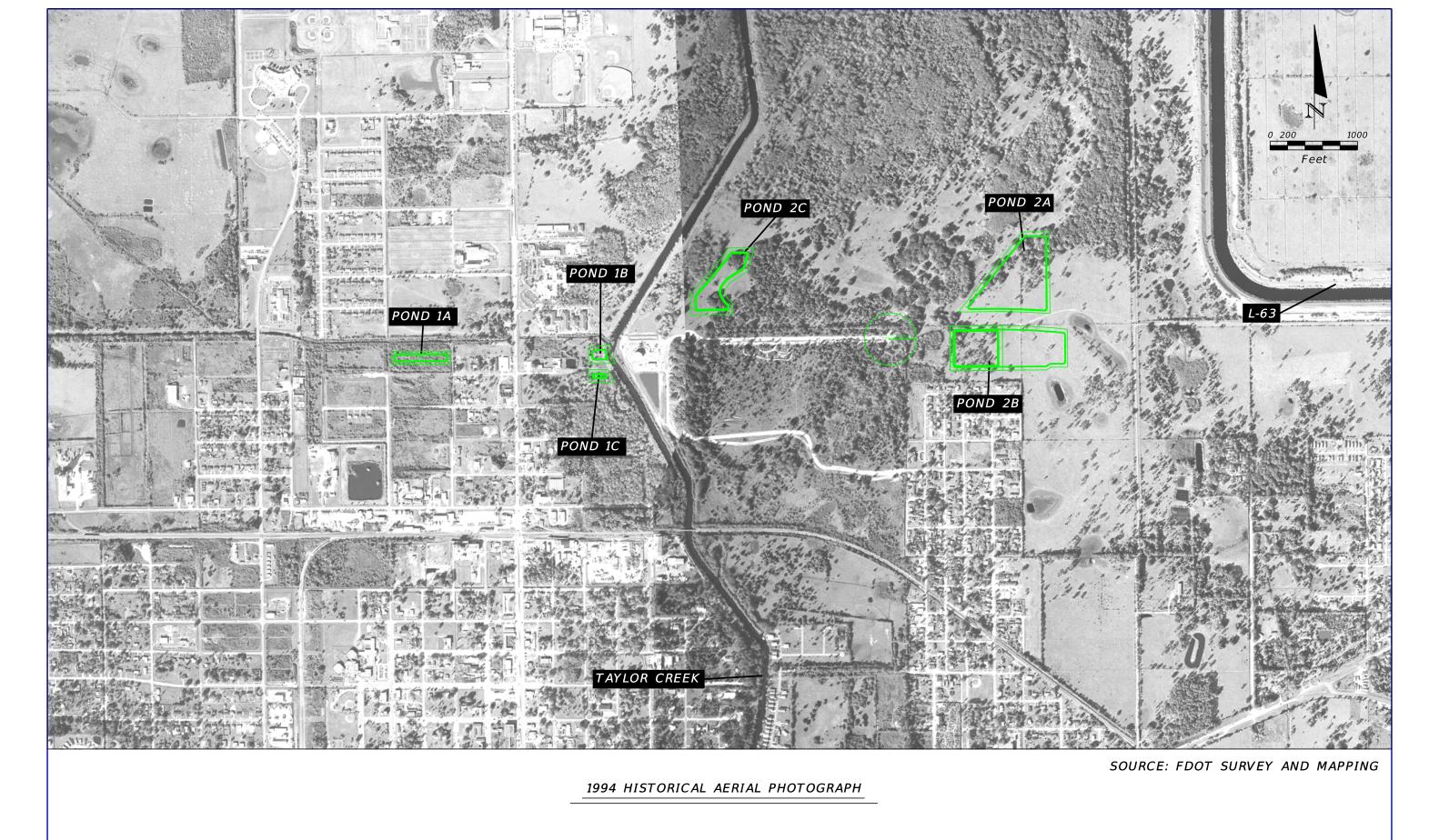
	REV	ISIONS			STATE OF FLORIDA		LORIDA		SHEET
DATE	DESCRIPTION	DATE	DESCRIPTION	TIERRA, INC.	DEP_{A}	ARTMENT OF TRAI		SR 710 FROM US 441	NO.
			T15004 000 150T NO 654440 0544	7351 TEMPLE TERRACE HIGHWAY	ROAD NO.	COUNTY	FINANCIAL PROJECT ID		of 220
			TIERRA PROJECT NO.: 6511-12-054A	TAMPA, FLORIDA 33637 CERTIFICATE OF AUTHORIZATION 6486	SR 710	ОКЕЕСНОВЕЕ	419344-3-32-01	TO L-03 CANAL Appendix 4 Tage 40 C	B-6



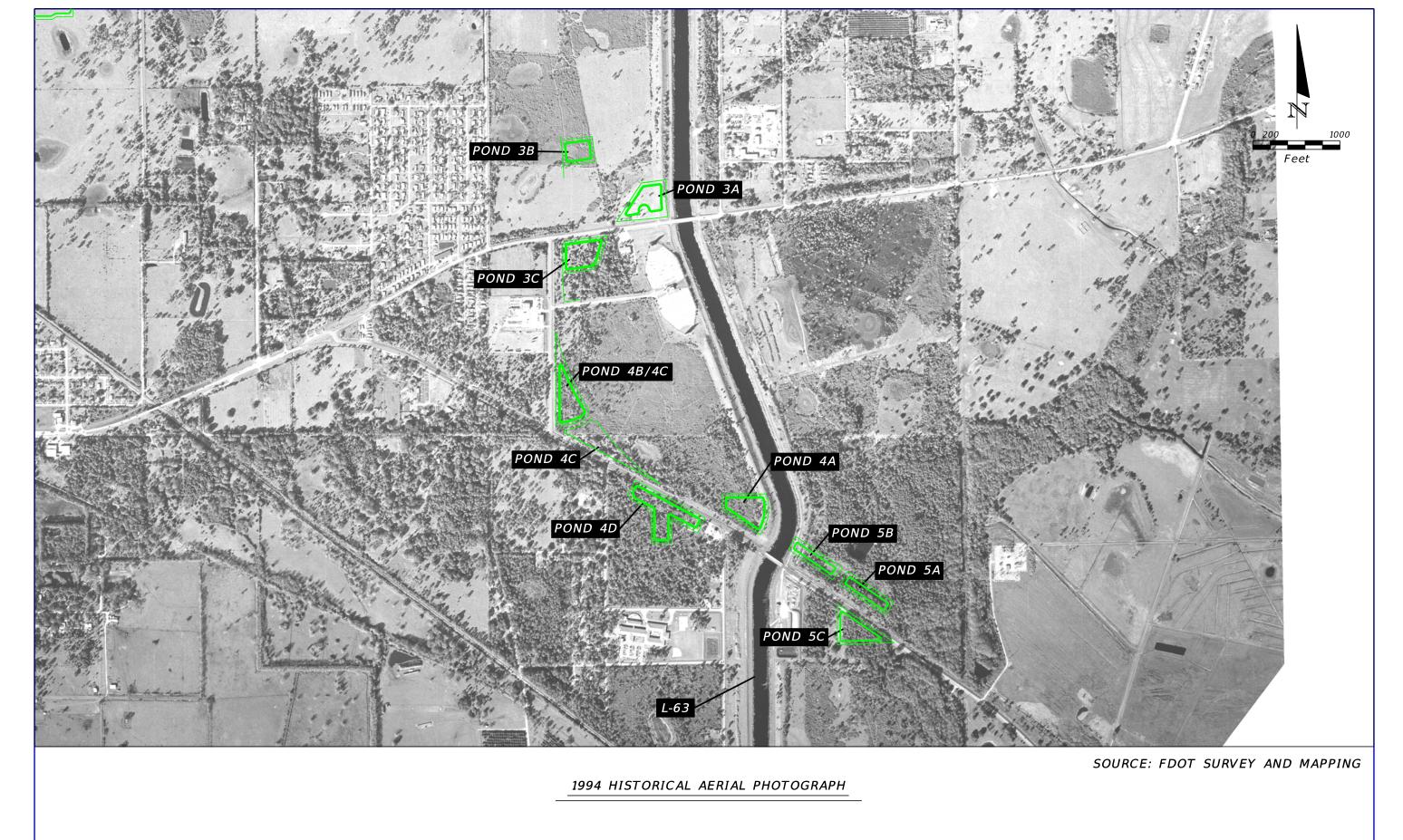
		REVISIONS				STATE OF F	LORIDA		
DATE	DESCRIPTION	DATE	DESCRIPTION	TIERRA, INC.	DEP_{A}	ARTMENT OF TRAI		SR 710 FROM US 441	SHEET NO.
				7351 TEMPLE TERRACE HIGHWAY	ROAD NO.	COUNTY	FINANCIAL PROJECT ID		
			TIERRA PROJECT NO.: 6511-12-054A	TAMPA, FLORIDA 33637 CERTIFICATE OF AUTHORIZATION 6486	SR 710	ОКЕЕСНОВЕЕ	419344-3-32-01	TO L-63 CANAL Appendix 4 - Page 41 c	B-7



	REVISIONS			STATE OF FI	LORIDA		SHEET	
DATE	DESCRIPTION DA	DESCRIPTION	TIERRA, INC.	DEPA	RTMENT OF TRAI		SR 710 FROM US 441	NO.
		TIERRA PROJECT NO. 6544 42 0544	7351 TEMPLE TERRACE HIGHWAY	ROAD NO.	COUNTY	FINANCIAL PROJECT ID		f 220
		TIERRA PROJECT NO.: 6511-12-054A	TAMPA, FLORIDA 33637 CERTIFICATE OF AUTHORIZATION 6486	SR 710	OKEECHOBEE	419344-3-32-01	TO L-03 CANAL Appellance Page 42 9	B-8



	REVI	SIONS				STATE OF FL	LORIDA		SHEET
DATE	DESCRIPTION	DATE	DESCRIPTION	TIERRA, INC.	DEP_{A}	ARTMENT OF TRAI	NSPORTATION	SR 710 FROM US 441	NO.
			TIEDDA DOUEST NO. CEMAS OF AA	7351 TEMPLE TERRACE HIGHWAY	ROAD NO.	COUNTY	FINANCIAL PROJECT ID		of 220
			TIERRA PROJECT NO.: 6511-12-054A	TAMPA, FLORIDA 33637 CERTIFICATE OF AUTHORIZATION 6486	SR 710	ОКЕЕСНОВЕЕ	419344-3-32-01	TO L-03 CANAL Appointment age to 0	B-9



	REVISIONS				STATE OF FI	LORIDA		SHEET
DATE	DESCRIPTION DATE	DESCRIPTION	TIERRA, INC.	DEP	ARTMENT OF TRAN		SR 710 FROM US 441	NO.
		TIEDDA DDO (ECT. NO. CEM 12 05 14	7351 TEMPLE TERRACE HIGHWAY	ROAD NO.	COUNTY	FINANCIAL PROJECT ID		f 220
		TIERRA PROJECT NO.: 6511-12-054A	TAMPA, FLORIDA 33637 CERTIFICATE OF AUTHORIZATION 6486	SR 710	ОКЕЕСНОВЕЕ	419344-3-32-01	TO L-03 CANAL Appoint Fago III	B-10

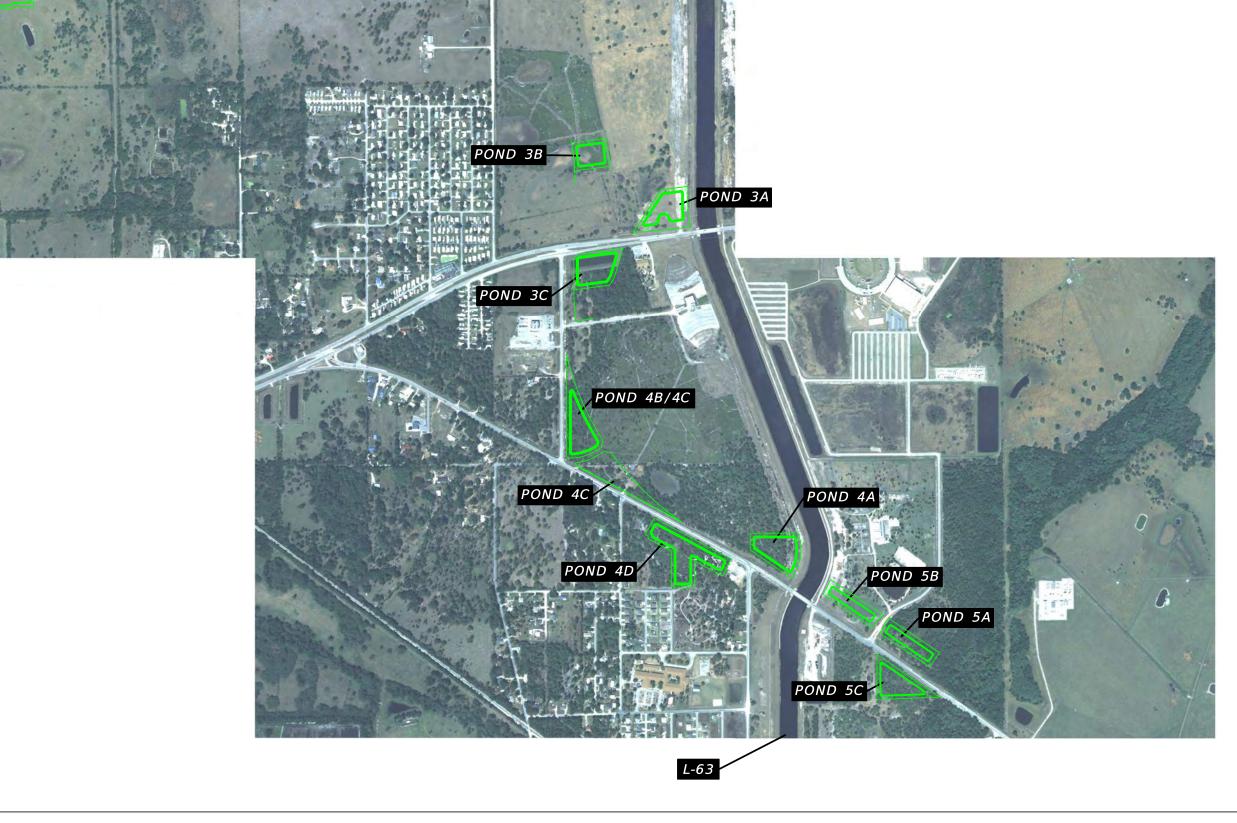


SOURCE: FDOT SURVEY AND MAPPING

2009 HISTORICAL AERIAL PHOTOGRAPH

	REV I.	SIONS				STATE OF F	ORIDA		SHEET
DATE	DESCRIPTION	DATE	DESCRIPTION	TIERRA, INC.	DEPA	RTMENT OF TRAI		SR 710 FROM US 441	NO.
			TIERRA PROJECT NO . CE11 12 OF AA	7351 TEMPLE TERRACE HIGHWAY	ROAD NO.	COUNTY	FINANCIAL PROJECT ID		f 220
			TIERRA PROJECT NO.: 6511-12-054A	TAMPA, FLORIDA 33637 CERTIFICATE OF AUTHORIZATION 6486	SR 710	OKEECHOBEE	419344-3-32-01	TO L-03 CANAL Approximate ago to s	B-11

7/16/2014 9:15:42 AM J:\6.



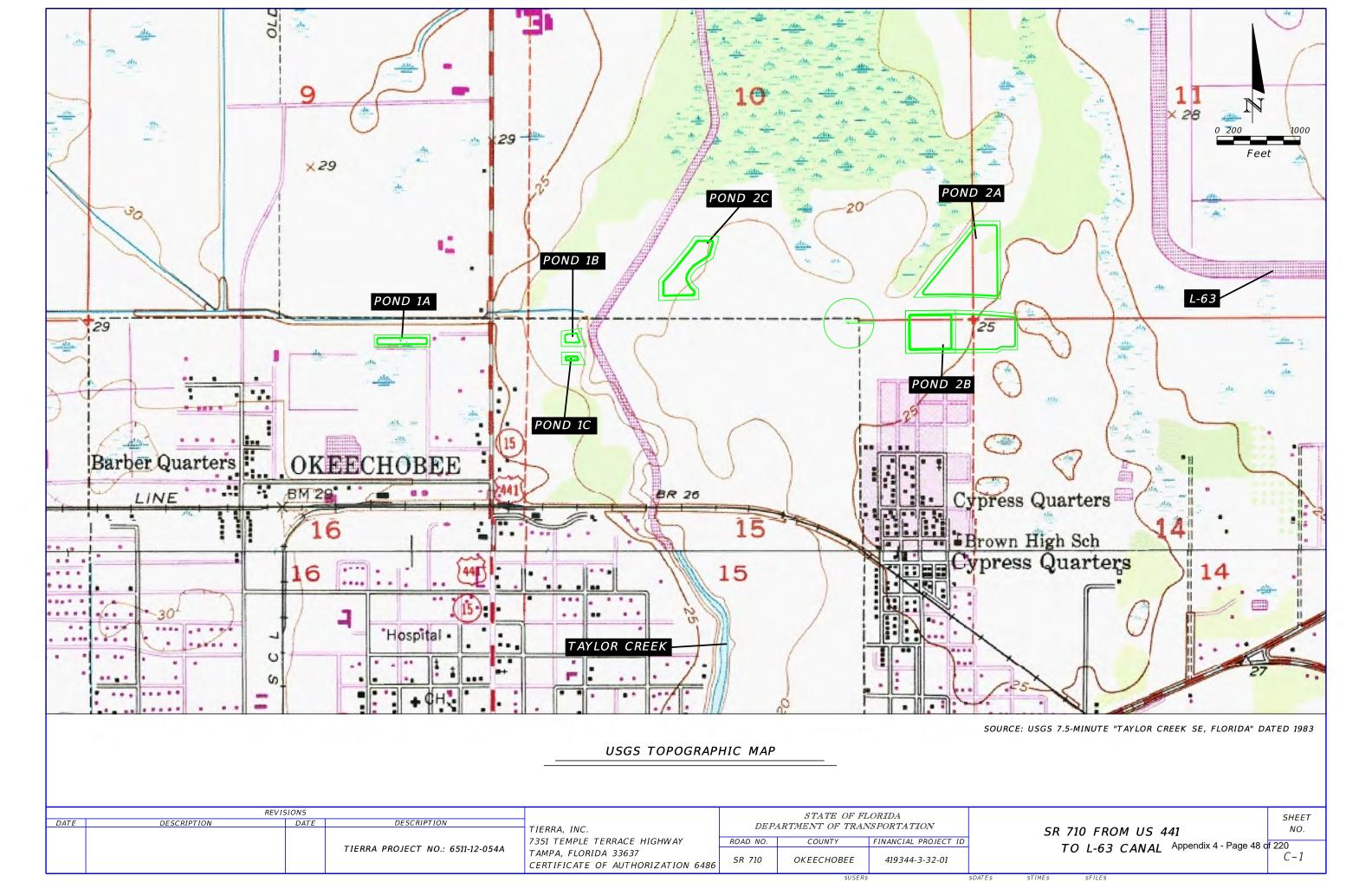
SOURCE: FDOT SURVEY AND MAPPING

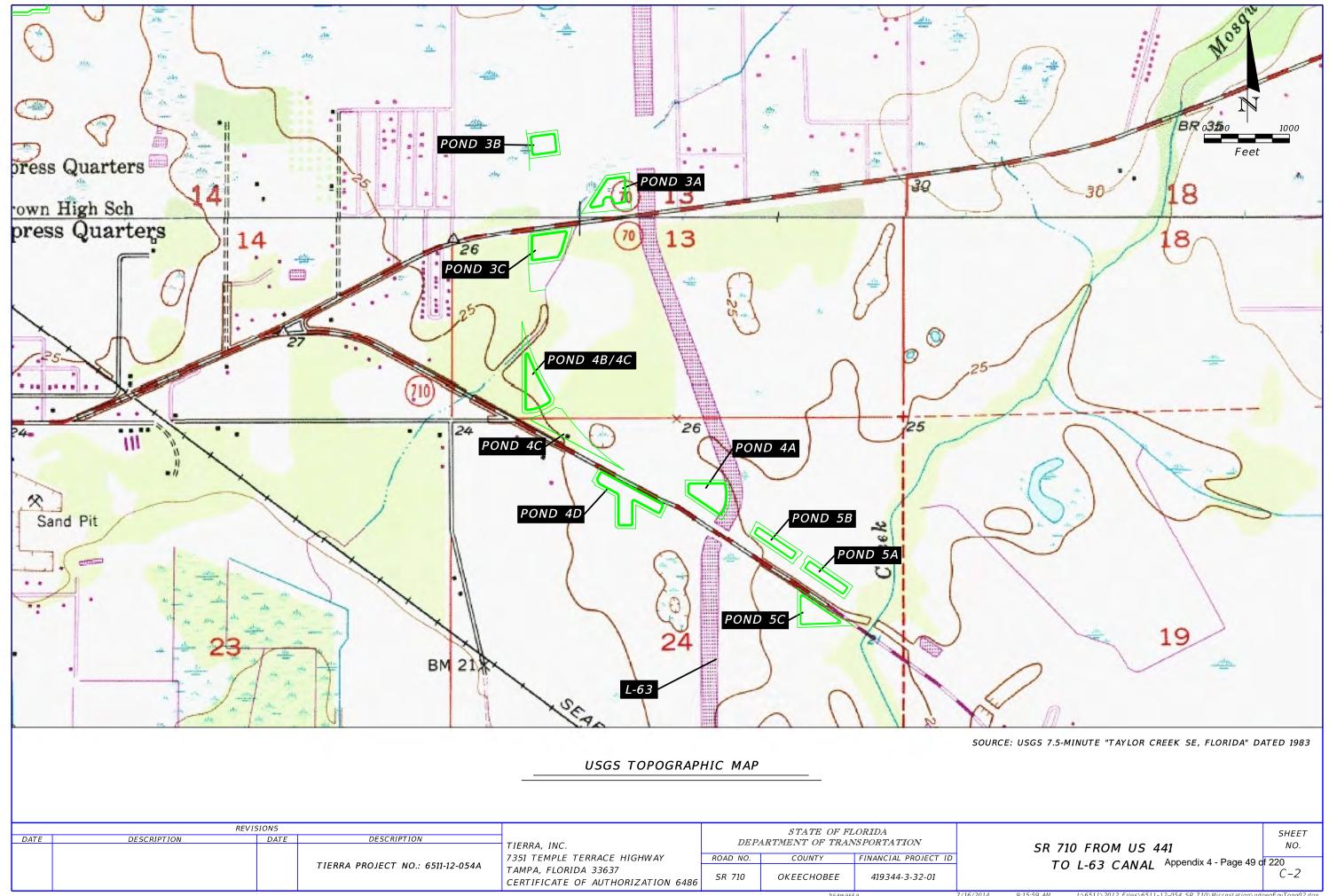
2009 HISTORICAL AERIAL PHOTOGRAPH

	RE	/ISIONS				STATE OF F	LORIDA		
DATE	DESCRIPTION	DATE	DESCRIPTION	TIERRA, INC.	DEP_{ℓ}	ARTMENT OF TRAI	VSPORTATION	SR 710 FROM US 441	SHEET NO.
			TIEDDA DDOUEGT NO. 65# 12.05 14	7351 TEMPLE TERRACE HIGHWAY	ROAD NO.	COUNTY	FINANCIAL PROJECT ID		of 220
			TIERRA PROJECT NO.: 6511-12-054A	TAMPA, FLORIDA 33637 CERTIFICATE OF AUTHORIZATION 6486	SR 710	ОКЕЕСНОВЕЕ	419344-3-32-01	TO L-03 CANAL Appointment rage to a	B-12

CSER-Appendix C

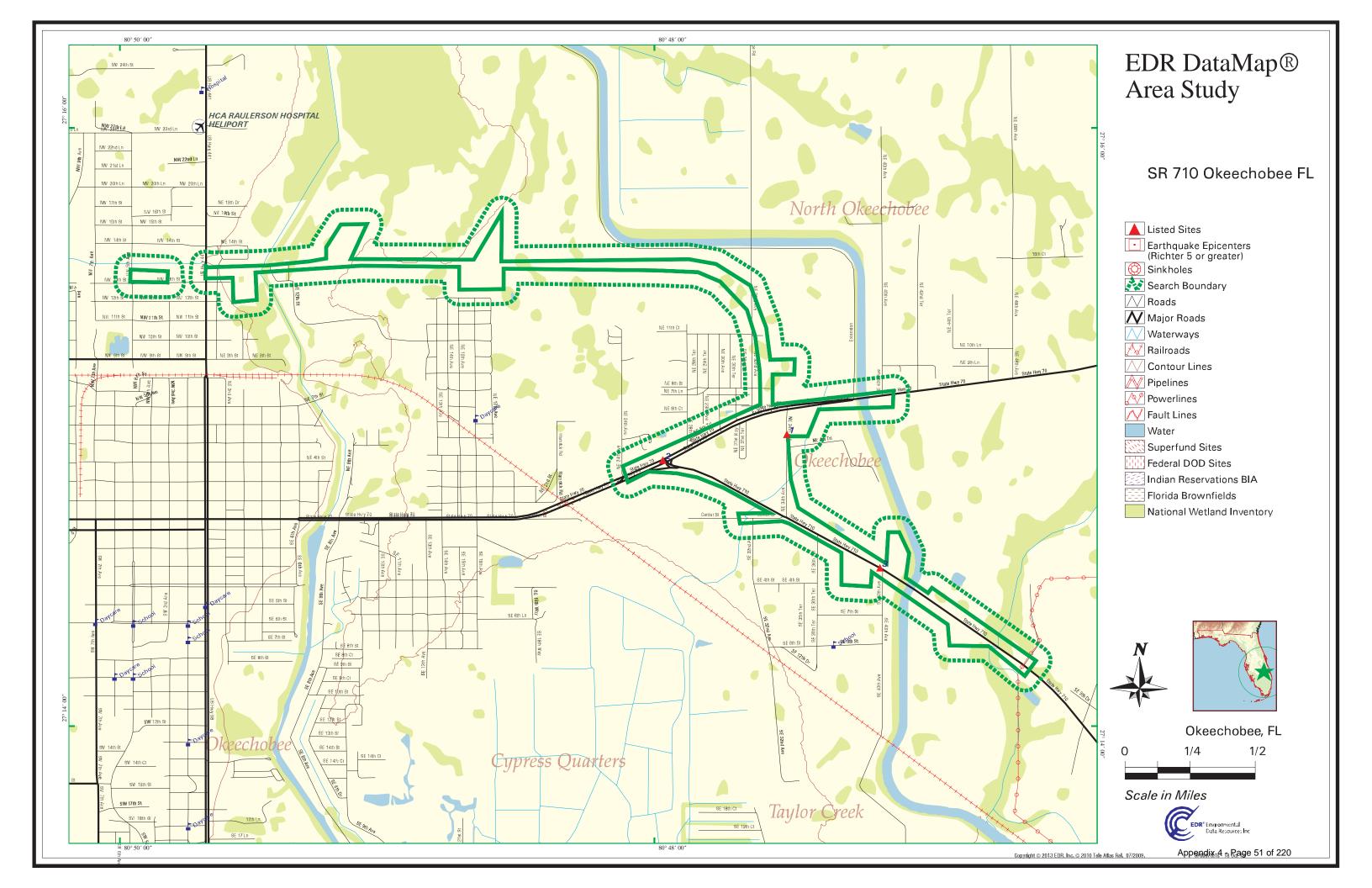
USGS Topographic Map





CSER-Appendix D

EDR® DataMap™ Report

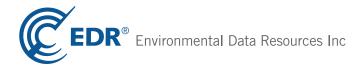


SR 710 Okeechobee FL Okeechobee, FL 34974

Inquiry Number: 3760673.1s

October 18, 2013

EDR DataMap™ Area Study



Thank you for your business. Please contact EDR at 1-800-352-0050 with any questions or comments.

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TARGET PROPERTY INFORMATION

ADDRESS

OKEECHOBEE, FL 34974 OKEECHOBEE, FL 34974

DATABASES WITH NO MAPPED SITES

No mapped sites were found in EDR's search of available ("reasonably ascertainable ") government records within the requested search area for the following databases:

FEDERAL RECORDS

NIDI

NPL	national Phonty List
Proposed NPL	Proposed National Priority List Sites
Delisted NPL	National Priority List Deletions
NPL LIENS	Federal Superfund Liens
	Comprehensive Environmental Response, Compensation, and Liabi
OFDO NEDAD	OFFICIAL Further Demandial Astice Planes

oility Information System

CERC-NFRAP..... CERCLIS No Further Remedial Action Planned

National Priority Liet

LIENS 2..... CERCLA Lien Information CORRACTS..... Corrective Action Report

RCRA-TSDF...... RCRA - Treatment, Storage and Disposal RCRA-LQG..... RCRA - Large Quantity Generators RCRA-SQG..... RCRA - Small Quantity Generators RCRA NonGen / NLR...... RCRA - Non Generators

US ENG CONTROLS..... Engineering Controls Sites List US INST CONTROL..... Sites with Institutional Controls

ERNS..... Emergency Response Notification System

HMIRS..... Hazardous Materials Information Reporting System

DOT OPS..... Incident and Accident Data US CDL..... Clandestine Drug Labs US BROWNFIELDS..... A Listing of Brownfields Sites DOD...... Department of Defense Sites FUDS..... Formerly Used Defense Sites

LUCIS..... Land Use Control Information System CONSENT..... Superfund (CERCLA) Consent Decrees

ROD...... Records Of Decision UMTRA..... Uranium Mill Tailings Sites

DEBRIS REGION 9..... Torres Martinez Reservation Illegal Dump Site Locations

ODI...... Open Dump Inventory US MINES..... Mines Master Index File

TRIS...... Toxic Chemical Release Inventory System

TSCA..... Toxic Substances Control Act

FTTS......FIFRA/ TSCA Tracking System - FIFRA (Federal Insecticide, Fungicide, & Rodenticide

Act)/TSCA (Toxic Substances Control Act)

HIST FTTS...... FIFRA/TSCA Tracking System Administrative Case Listing

SSTS..... Section 7 Tracking Systems

ICIS...... Integrated Compliance Information System

PADS..... PCB Activity Database System MLTS..... Material Licensing Tracking System RADINFO...... Radiation Information Database

RAATS......RCRA Administrative Action Tracking System

RMP..... Risk Management Plans

COAL ASH EPA..... Coal Combustion Residues Surface Impoundments List SCRD DRYCLEANERS...... State Coalition for Remediation of Drycleaners Listing

US HIST CDL..... National Clandestine Laboratory Register PCB TRANSFORMER_____ PCB Transformer Registration Database FEDERAL FACILITY..... Federal Facility Site Information listing US FIN ASSUR..... Financial Assurance Information

EPA WATCH LIST..... EPA WATCH LIST

PRP..... Potentially Responsible Parties 2020 COR ACTION........... 2020 Corrective Action Program List COAL ASH DOE..... Steam-Electric Plant Operation Data FEMA UST..... Underground Storage Tank Listing

LEAD SMELTERS..... Lead Smelter Sites

US AIRS...... Aerometric Information Retrieval System Facility Subsystem

STATE AND LOCAL RECORDS

SHWS......Florida's State-Funded Action Sites SWF/LF..... Solid Waste Facility Database

UIC...... Underground Injection Wells Database Listing

SWRCY..... Recycling Centers

LAST..... Leaking Aboveground Storage Tank Listing

FI Sites List

SPILLS..... Oil and Hazardous Materials Incidents

ENG CONTROLS..... Institutional Controls Registry INST CONTROL..... Institutional Controls RegistryVoluntary Cleanup Sites PRIORITYCLEANERS...... Priority Ranking List DRYCLEANERS...... Drycleaning Facilities

DEDB..... Ethylene Dibromide Database Results

BROWNFIELDS..... Brownfield Areas

NPDES...... Wastewater Facility Regulation Database

AIRS..... Permitted Facilities Listing FL Cattle Dip. Vats..... Cattle Dipping Vats FF TANKS..... Federal Facilities Listing

TRIBAL RECORDS

INDIAN RESERV..... Indian Reservations

INDIAN ODI...... Report on the Status of Open Dumps on Indian Lands INDIAN LUST..... Leaking Underground Storage Tanks on Indian Land INDIAN UST...... Underground Storage Tanks on Indian Land INDIAN VCP...... Voluntary Cleanup Priority Listing

EDR PROPRIETARY RECORDS

EDR MGP..... EDR Proprietary Manufactured Gas Plants EDR US Hist Auto Stat..... EDR Exclusive Historic Gas Stations EDR US Hist Cleaners..... EDR Exclusive Historic Dry Cleaners

SURROUNDING SITES: SEARCH RESULTS

Surrounding sites were identified.

Page numbers and map identification numbers refer to the EDR Radius Map report where detailed data on individual sites can be reviewed.

Sites listed in **bold italics** are in multiple databases.

Unmappable (orphan) sites are not considered in the foregoing analysis.

FEDERAL RECORDS

RCRA-CESQG: RCRAInfo is EPA's comprehensive information system, providing access to data supporting the Resource Conservation and Recovery Act (RCRA) of 1976 and the Hazardous and Solid Waste Amendments (HSWA) of 1984. The database includes selective information on sites which generate, transport, store, treat and/or dispose of hazardous waste as defined by the Resource Conservation and Recovery Act (RCRA). Conditionally exempt small quantity generators (CESQGs) generate less than 100 kg of hazardous waste, or less than 1 kg of acutely hazardous waste per month.

A review of the RCRA-CESQG list, as provided by EDR, and dated 07/11/2013 has revealed that there is 1 RCRA-CESQG site within the searched area.

Site	Address	Map ID	Page
FPL OKEECHOBEE SERVICE CENTER	825 NE 34 AVE	1	5

FINDS: The Facility Index System contains both facility information and "pointers" to other sources of information that contain more detail. These include: RCRIS; Permit Compliance System (PCS); Aerometric Information Retrieval System (AIRS); FATES (FIFRA [Federal Insecticide Fungicide Rodenticide Act] and TSCA Enforcement System, FTTS [FIFRA/TSCA Tracking System]; CERCLIS; DOCKET (Enforcement Docket used to manage and track information on civil judicial enforcement cases for all environmental statutes); Federal Underground Injection Control (FURS); Federal Reporting Data System (FRDS); Surface Impoundments (SIA); TSCA Chemicals in Commerce Information System (CICS); PADS; RCRA-J (medical waste transporters/disposers); TRIS; and TSCA. The source of this database is the U.S. EPA/NTIS.

A review of the FINDS list, as provided by EDR, and dated 03/08/2013 has revealed that there are 3 FINDS sites within the searched area.

Site	Address	Map ID	Page
FPL OKEECHOBEE SERVICE CENTER	825 NE 34 AVE	1	5
FPL OKEECHOBEE SERVICE CENTER	825 NE 34TH AVE	1	7
TOWN STAR # 40	3993 HWY 710 E	3	24

STATE AND LOCAL RECORDS

LUST: The Leaking Underground Storage Tank Incident Reports contain an inventory of reported leaking underground storage tank incidents. The data come from the Department of Environmental Protection's PCTO1--Petroleum Contamination Detail Report.

A review of the LUST list, as provided by EDR, and dated 07/15/2013 has revealed that there are 3 LUST sites within the searched area.

Site	Address	Map ID	Page
FL POWER & LIGHT CO-OKEECHOBE	825 NE 34TH AVE	1	7
Facility-Site Id: 8519987			

Discharge Cleanup Status: RA - RA ONGOING

Site	Address	Map ID	Page
CHEVRON #47761 Facility-Site Id: 8512544	2768 SR 710	2	13
Discharge Cleanup Status: SR	CR - SRCR COMPLETE EQ - CLEANUP NOT REQUIRED		
TOWN STAR #40 Facility-Site Id: 8630309 Discharge Cleanup Status: RA	3990 HWY 710 - RA ONGOING	3	18

UST: The Underground Storage Tank database contains registered USTs. Shortly after the September 11 event, the DEP was instructed to remove the detail about some of the storage tank facilities in the state from their reports. Federal-owned facilities and bulk storage facilities are included in that set.

A review of the UST list, as provided by EDR, and dated 07/15/2013 has revealed that there are 3 UST sites within the searched area.

Site	Address	Map ID	Page
FL POWER & LIGHT CO-OKEECHOBE Facility-Site Id: 8519987	825 NE 34TH AVE	1	7
CHEVRON #47761 Facility-Site Id: 8512544	2768 SR 710	2	13
TOWN STAR #40 Facility-Site Id: 8630309	3990 HWY 710	3	18

AST: Shortly after the Sept 11 event, the DEP was instructed to remove the detail about some of the storage tank facilities in the state from their reports. Federal-owned facilities and bulk storage facilities are included in that set.

A review of the AST list, as provided by EDR, and dated 07/15/2013 has revealed that there is 1 AST site within the searched area.

Site	Address	Map ID	Page
FL POWER & LIGHT CO-OKEECHOBE Facility-Site Id: 8519987	825 NE 34TH AVE	1	7

TIER 2: A listing of facilities which store or manufacture hazardous materials that submit a chemical inventory report.

A review of the TIER 2 list, as provided by EDR, and dated 12/31/2011 has revealed that there is 1 TIER 2 site within the searched area.

Site	Address	Map ID	Page
FLORIDA POWER AND LIGHT - OKEE	825 NORTHEAST 34 AVENUE	1	3

Please refer to the end of the findings report for unmapped orphan sites due to poor or inadequate address information.

MAP FINDINGS SUMMARY

	Database	Total Plotted
FEDERAL DECORDO		
FEDERAL RECORDS		
FEDERAL RECORDS	NPL Proposed NPL Delisted NPL NPL LIENS CERCLIS CERC-NFRAP LIENS 2 CORRACTS RCRA-TSDF RCRA-LQG RCRA-SQG RCRA-CESQG RCRA NonGen / NLR US ENG CONTROLS US INST CONTROL ERNS HMIRS DOT OPS US CDL US BROWNFIELDS DOD FUDS LUCIS CONSENT ROD UMTRA DEBRIS REGION 9 ODI US MINES TRIS TSCA FTTS HIST FTTS SSTS ICIS PADS MLTS RADINFO FINDS RAATS RMP COAL ASH EPA SCRD DRYCLEANERS	000000000000000000000000000000000000000
	US HIST CDL PCB TRANSFORMER FEDERAL FACILITY	0 0 0
	US FIN ASSUR EPA WATCH LIST	0 0

MAP FINDINGS SUMMARY

	Database	Total Plotted
	PRP 2020 COR ACTION COAL ASH DOE FEMA UST LEAD SMELTERS US AIRS	0 0 0 0 0
STATE AND LOCAL RECOR	DS	
	SHWS SWF/LF UIC SWRCY LUST UST LAST AST FI Sites SPILLS ENG CONTROLS INST CONTROL VCP PRIORITYCLEANERS DEDB BROWNFIELDS NPDES AIRS TIER 2 FL Cattle Dip. Vats FF TANKS	0 0 0 0 3 3 3 0 1 0 0 0 0 0 0 0 0 0 0
TRIBAL RECORDS		
	INDIAN RESERV INDIAN ODI INDIAN LUST INDIAN UST INDIAN VCP	0 0 0 0
EDR PROPRIETARY RECOR	RDS	
	EDR MGP EDR US Hist Auto Stat EDR US Hist Cleaners	0 0 0

NOTES:

Sites may be listed in more than one database

1

rection EDR ID Number

FLORIDA POWER AND LIGHT - OKEECHOBEE SERVICE CENTER 825 NORTHEAST 34 AVENUE OKEECHOBEE, FL 34972 TIER 2 S109615339 N/A

EPA ID Number

Database(s)

TIER 2:

Year: 2011 3990915 Facility Id: Not reported Active Date: Inactive Date: Not reported Sale Pending: Not reported Original Date: Not reported PLOT Source: Not reported 27.25052 Latitude: -80.792920 Longitude: LEPC District: Not reported Counties: Not reported SERC: Not reported Program Level: Not reported PRIME: Not reported SIC Code: Not reported SIC Code 2: Not reported NAICS Code: Not reported Last Modified Date: 11/12/2012 11/09/2012 First Submit Date:

Data Submitted By: Florida Division of Emergency Management

Company Name: FLORIDA POWER AND LIGHT

Comments: Not reported

Contact1 Name: PAT COYLE

Contact1 Type: Tier II Emergency 24 Hour Contact

Contact1 EMail: Not reported
Contact1 Telephone: 800-741-2650
Contact2 Name: PAT COYLE

Contact2 Type: Tier II Emergency Contact

Contact2 EMail: Not reported
Contact2 Telephone: 561-722-4486
Contact3 Name: PAT COYLE

Contact3 Type: Tier II Secondary 24 Hour Contact

Contact3 EMail: Not reported
Contact3 Telephone: 561-722-4486
Contact4 Name: JEFF WADE

Contact4 Type: Tier II Secondary Contact

Contact4 EMail:
Contact4 Telephone:
954-599-0317
Contact5 Name:
Not reported
Contact5 Type:
Not reported
Contact5 EMail:
Not reported
Not reported
Not reported
Not reported
Not reported

Chemical Code: Not reported Chemical Name: Not reported Not reported Chemical State: Location Name: Not reported Not reported Container Code: Pressure Code: Not reported Temperature Code: Not reported Not reported Average Quantity: Maximum Quantity: Not reported

rection EDR ID Number

FLORIDA POWER AND LIGHT - OKEECHOBEE SERVICE CENTER (Continued)

S109615339

EPA ID Number

Database(s)

Days On Site: Not reported

Year: Not reported Facility Id: Not reported Active Date: Not reported Inactive Date: Not reported Sale Pending: False Original Date: Not reported PLOT Source: Not reported Latitude: 27.250520 -80.792920 Longitude:

LEPC District: 7

Counties: Polk,Okeechobee,Highlands,Hardee,DeSoto,

 SERC:
 36108

 Program Level:
 Not reported

 PRIME:
 72

 SIC Code:
 4911

 SIC Code 2:
 Not reported

 NAICS Code:
 221122

Other Chemical Data:

Mixture Percent:

Report Year: 2008 Tier 2 Report ID: 106083 Chemical ID: 318057 8006619 CAS Number: Chemical Name: **GASOLINE** Chemical Date: 6/2/2009 Average Amount: 3 Maximum Amount: 9600 Location ID: 519133 Chemical State: Liquid False Mixture:

Containter: A - ABOVE GROUND TANK
Pressure: 1 - AMBIENT PRESSURE
Temperature: 4 - AMBIENT TEMPERATURE

100.00

Average Amount: 3
Maximum Amount: 9600
Days on Site: 365
Site Plan: True
Site Plan Document: Not reported

Private Location: Not reported False

Location: SEE ENCLOSED DIAGRAM

 Report Year:
 2008

 Tier 2 Report ID:
 106083

 Chemical ID:
 318056

 CAS Number:
 68476346

Chemical Name: DIESEL FUEL OIL (HIGH SULFUR)

Chemical Date: 6/2/2009
Average Amount: 4
Maximum Amount: 14800
Location ID: 519132
Chemical State: LIQUID
Mixture: True
Mixture Percent: .00

Containter: A - ABOVE GROUND TANK

ection EDR ID Number

Database(s) EPA ID Number

FLORIDA POWER AND LIGHT - OKEECHOBEE SERVICE CENTER (Continued)

S109615339

Pressure: 1 - AMBIENT PRESSURE Temperature: 4 - AMBIENT TEMPERATURE

Average Amount: 4

Maximum Amount: 14800

Days on Site: 365

Site Plan: True

Site Plan Document: Not reported

Private Location: False

Location: SEE ENCLOSED DIAGRAM

Company Info:

Company Name: FLORIDA POWER AND LIGHT
Company Address: 2455 PORT WEST BOULEVARD
Company City,St,Zip: WEST PALM BEACH, FL 33407

Company Phone: 561-845-3344
Company Fax: Not reported
Company Email: Not reported
FEI Number: 590247775
Comany Contact Name: DAN RAWSON
Cmpny Contact Phone: 561-845-3344

Reduced Fees: False
Exempt Fees: False
Electronic Filing: True
Employee: Not re

Employee: Not reported Comments: Not reported

Contact:

Contact ID: 30478

Contact Type: Tier II Emergency Contact

Contact Name: JEFF WADE

Contact Title: ENVIRONMENTAL COORDINATOR

Contact Phone: 954-599-0317 Contact 24Hr Phone: 561-616-1702

Contact ID: 30479

Contact Type: Tier II Secondary Contact

Contact Name: PAT COYLE
Contact Title: FLEET SUPERVISOR
Contact Phone: 561-722-4486

Contact Phone: 561-722-4486 Contact 24Hr Phone: 561-616-1702

1 FPL OKEECHOBEE SERVICE CENTER 825 NE 34 AVE OKEECHOBEE, FL RCRA-CESQG 1004682782 FINDS FLD000733881

RCRA-CESQG:

Date form received by agency: 02/08/1996

Facility name: FPL OKEECHOBEE SERVICE CENTER

Facility address: 825 NE 34TH AVE

OKEECHOBEE, FL 349743540

EPA ID: FLD000733881 Mailing address: PO BOX 78768

WEST PALM BEACH, FL 33407-0768

Map ID Direction Distance

Distance (ft.)Site Database(s) EPA ID Number

FPL OKEECHOBEE SERVICE CENTER (Continued)

1004682782

EDR ID Number

Contact: CHARLES D HENDERSON

Contact address: PO BOX 078768

WEST PALM BEACH, FL 33407

Contact country: US

Contact telephone: 4076976930 Contact email: Not reported

EPA Region: 04

Classification: Conditionally Exempt Small Quantity Generator

Description: Handler: generates 100 kg or less of hazardous waste per calendar

month, and accumulates 1000 kg or less of hazardous waste at any time; or generates 1 kg or less of acutely hazardous waste per calendar month, and accumulates at any time: 1 kg or less of acutely hazardous waste; or 100 kg or less of any residue or contaminated soil, waste or other debris resulting from the cleanup of a spill, into or on any land or water, of acutely hazardous waste; or generates 100 kg or less of any residue or contaminated soil, waste or other debris resulting from the cleanup of a spill, into or on any land or water, of acutely hazardous waste during any calendar month, and accumulates at any time: 1 kg or less of acutely hazardous waste; or 100 kg or less of any residue or contaminated soil, waste or other debris resulting from

the cleanup of a spill, into or on any land or water, of acutely

hazardous waste

Owner/Operator Summary:

Owner/operator name: CHARLES HENDERSON

Owner/operator address: PO BOX 78768

WEST PALM BEACH, FL 33407

Owner/operator country: US

Owner/operator telephone: Not reported Legal status: Private
Owner/Operator Type: Owner
Owner/Op start date: 10/18/1996
Owner/Op end date: Not reported

Owner/operator name: HENDERSON CHARLES

Owner/operator address: PO BOX 78768

WEST PALM BEACH, FL 33407

Owner/operator country: US

Owner/operator telephone: Not reported Legal status: Private Owner/Operator Type: Owner Owner/Op start date: 10/18/1996 Owner/Op end date: Not reported

Handler Activities Summary:

U.S. importer of hazardous waste: No Mixed waste (haz. and radioactive): No Recycler of hazardous waste: No Transporter of hazardous waste: No Treater, storer or disposer of HW: No Underground injection activity: No On-site burner exemption: No Furnace exemption: No Used oil fuel burner: No Used oil processor: No User oil refiner: No

ection EDR ID Number

Database(s) EPA ID Number

FPL OKEECHOBEE SERVICE CENTER (Continued)

1004682782

Used oil fuel marketer to burner: No
Used oil Specification marketer: No
Used oil transfer facility: No
Used oil transporter: No

Hazardous Waste Summary:

Waste code: D001

Waste name: IGNITABLE HAZARDOUS WASTES ARE THOSE WASTES WHICH HAVE A FLASHPOINT OF

LESS THAN 140 DEGREES FAHRENHEIT AS DETERMINED BY A PENSKY-MARTENS CLOSED CUP FLASH POINT TESTER. ANOTHER METHOD OF DETERMINING THE FLASH POINT OF A WASTE IS TO REVIEW THE MATERIAL SAFETY DATA SHEET, WHICH CAN BE OBTAINED FROM THE MANUFACTURER OR DISTRIBUTOR OF THE MATERIAL. LACQUER THINNER IS AN EXAMPLE OF A COMMONLY USED SOLVENT

WHICH WOULD BE CONSIDERED AS IGNITABLE HAZARDOUS WASTE.

Violation Status: No violations found

FINDS:

Registry ID: 110008320110

Environmental Interest/Information System

RCRAInfo is a national information system that supports the Resource Conservation and Recovery Act (RCRA) program through the tracking of events and activities related to facilities that generate, transport, and treat, store, or dispose of hazardous waste. RCRAInfo allows RCRA

program staff to track the notification, permit, compliance, and

corrective action activities required under RCRA.

1 FPL OKEECHOBEE SERVICE CENTER 825 NE 34TH AVE OKEECHOBEE, FL FINDS 1011437914 N/A

FINDS:

Registry ID: 110035623769

Environmental Interest/Information System

Florida Environmental System Today Application (FIESTA) Data Maintenance (FDM) system maintains entity, environmental interest and

affiliation data for the State of Florida.

1 FL POWER & LIGHT CO-OKEECHOBE SRVC CTR 825 NE 34TH AVE OKEECHOBEE, FL 34972 LUST U002313644 UST N/A

AST

LUST:

Region: STATE
Facility Id: 8519987
Facility Status: OPEN

Facility Type: C - Fuel user/Non-retail

Facility Phone: (772)223-4255

Facility Cleanup Rank: 4370

District: Southeast District

irection EDR ID Number

FL POWER & LIGHT CO-OKEECHOBE SRVC CTR (Continued)

U002313644

EPA ID Number

Database(s)

Lat/Long (dms): 27 14 52.6124 / 80 47 41.9811

Section: 013 37S Township: 35E Range: Not reported Feature: UNVR Method: Datum: 0 Score: 45 Score Effective Date: 10/03/2011 Score When Ranked: 36

 Operator:
 PAT COYLE

 Name Update:
 05/14/2002

 Address Update:
 02/28/2008

Petroleum Cleanup PCT Facility Score:

Facility Cleanup Status:

Contact:

Contact Company:

Contact Address:

Contact City/State/Zip:

ONGO - ONGOING

ANDREW DAUGHERTY

FL POWER & LIGHT CO

7200 NW 4TH ST

PLANTATION, FL 33317

Phone: (954)581-3014

 Bad Address Ind:
 N

 State:
 FL

 Zip:
 34972

 Score:
 45

Score Effective Date: 2011-10-03 00:00:00

Related Party ID: 27028

Primary RP Role: ACCOUNT OWNER

RP Begin Date: 04/26/1994
RP Zip: Not reported
RP Extension: Not reported

Discharge Cleanup Summary:

Discharge Date: 06/25/1992 PCT Discharge Combined: Not reported

Cleanup Required: R - CLEANUP REQUIRED
Discharge Cleanup Status: RA - RA ONGOING

Disch Cleanup Status Date: 08/26/2008
Cleanup Work Status: INACTIVE

Information Source: I - PLIRP (INSURANCE)

Other Source Description:

Eligibility Indicator:

Site Manager:

Site Mgr End Date:

Not reported

E - ELIGIBLE

PERRY_H

04/23/2013

Tank Office: PCTM6 - PETROLEUM CLEANUP TEAM 6

Petroleum Cleanup Program Eligibility:

Facility ID: 8519987
Discharge Date: 25-Jun-1992
Pct Discharge Combined With: Not reported

Cleanup Required: R - CLEANUP REQUIRED Discharge Cleanup Status: RA - RA ONGOING

Disch Cleanup Status Date: 08/26/2008
Cleanup Work Status: INACTIVE

Information Source: I - PLIRP (INSURANCE)

Other Source Description: Not reported Application Received Date: 7/7/1992

Cleanup Program: P - PETROLEUM LIABILITY AND RESTORATION INSURANCE PROGRAM

rection EDR ID Number

FL POWER & LIGHT CO-OKEECHOBE SRVC CTR (Continued)

U002313644

EPA ID Number

Database(s)

Eligibility Status: 1/27/1993
Elig Status Date: 1/27/1993
Letter Of Intent Date: 07/07/1992
Redetermined: No
Inspection Date: 07/21/1992
Site Manager: PERRY_H
Site Mgr End Date: 04/23/2013

Tank Office: PCTM6 - PETROLEUM CLEANUP TEAM 6

Deductible Amount: 500
Deductible Paid To Date: 500
Co-Pay Amount: 0
Co-Pay Paid To Date: 0
Cap Amount: 1200000

Contaminated Media:

Discharge Date: 06/25/1992
Pct Discharge Combined With: Not reported

Cleanup Required: R - CLEANUP REQUIRED Discharge Cleanup Status: RA - RA ONGOING

Disch Cleanup Status Date: 08/26/2008 Cleanup Work Status: INACTIVE

Information Source: I - PLIRP (INSURANCE)

Other Source Description:

Elig Indicator:

Site Manager:

Site Mgr End Date:

Not reported

E - ELIGIBLE

PERRY_H

04/23/2013

Tank Office: PCTM6 - PETROLEUM CLEANUP TEAM

Contaminated Drinking Wells: 0
Contaminated Monitoring Well: Yes
Contaminated Soil: No
Contaminated Surface Water: No
Contaminated Ground Water: Yes

Pollutant: B - UNLEADED GAS

Pollutant Other Description: Not reported Gallons Discharged: Not reported

Task Information:

District: SED
Facility ID: 8519987
Facility Status: OPEN

Facility Type: C - Fuel user/Non-retail -

County: OKEECHOBEE

County ID: 47
Cleanup Eligibility Status: E

Source Effective Date: Not reported Discharge Date: 06-25-1992

Cleanup Required: R - CLEANUP REQUIRED Discharge Cleanup Status: RA - RA ONGOING

Disch Cleanup Status Date: 08-26-2008

SRC Action Type:

SRC Submit Date: Not reported SRC Review Date: Not reported

SRC Completion Status:

SRC Issue Date:

SRC Comment:

Cleanup Work Status:

Site Mgr:

Site Mgr End Date:

Not reported

INACTIVE

PERRY_H

04-23-2013

Map ID Direction Distance

Distance (ft.)Site Database(s) EPA ID Number

FL POWER & LIGHT CO-OKEECHOBE SRVC CTR (Continued)

U002313644

EDR ID Number

Tank Office: PCTM6 - Team 6

SR Task ID: 35916
SR Cleanup Responsible: SR Funding Eligibility Type: -

SR Actual Cost:

SR Completion Date:

SR Payment Date:

SR Oral Date:

SR Written Date:

Not reported

Not reported

Not reported

Not reported

SR Soil Removal: Y

SR Free Product Removal: Not reported

SR Soil Tonnage Removed: 784

SR Soil Treatment:

SR Other Treatment:

SR Alternate Proc Received Date:
SR Alternate Procedure Status:

SR Alternate Procedure Status:

Not reported
SR Alternate Procedure Status Date: Not reported
SR Alternate Procedure Comments:
Not reported
SA Task ID:

Not reported
35917

SA Cleanup Responsible: - SA Funding Eligibility Type: -

SA Actual Cost:

SA Completion Date:

SA Payment Date:

RAP Task ID:

Not reported

Not reported

67618

RAP Cleanup Responsible ID: RAP Funding Eligibility Type:

RAP Actual Cost: Not reported
RAP Completion Date: Not reported
RAP Payment Date: Not reported
RAP Last Order Approved: Not reported
RA Task ID: 75630

RA Cleanup Responsible: RA Funding Eligibility Type: -

RA Years to Complete: Not reported RA Actual Cost: Not reported

Click here for Florida Oculus:

UST:

Facility Id: 8519987 Facility Status: OPEN

Type Description: Fuel user/Non-retail Facility Phone: (772) 223-4255
Region: STATE
Positioning Method: UNVR

Lat/Long (dms): 27 14 42 / 80 47 44

Owner:

Owner Id: 27028

Owner Name: FL POWER & LIGHT CO
Owner Address: 7200 NW 4TH ST

Owner Address 2: ATTN: ANDREW DAUGHERTY
Owner City,St,Zip: PLANTATION, FL 33317
Owner Contact: ANDREW DAUGHERTY

Owner Phone: (954) 581-3014

Distance
Distance (ft.)Site Database(s) EPA ID Number

FL POWER & LIGHT CO-OKEECHOBE SRVC CTR (Continued)

U002313644

EDR ID Number

Tank Info:

Tank ld:

Status: Removed
Status Date: 31-DEC-1992
Install Date: 01-JUN-1974
Substance: Vehicular diesel
Content Description: Vehicular Diesel

Gallons: 5000 Vessel Indicator: TANK

Tank Location: UNDERGROUND

DEP Contractor: No

Click here for Florida Oculus:

AST:

Facility ID: 8519987 Facility Status: OPEN

Type Description: Fuel user/Non-retail Facility Phone: (772) 223-4255

DEP Contractor Own: No

Region: STATE Positioning Method: UNVR

Lat/Long (dms): 27 14 42 / 80 47 44

Owner:

Owner Id: 27028

Owner Name: FL POWER & LIGHT CO
Owner Address: 7200 NW 4TH ST

Owner Address 2: ATTN: ANDREW DAUGHERTY
Owner City,St,Zip: PLANTATION, FL 33317
Owner Contact: ANDREW DAUGHERTY

Owner Phone: (954) 581-3014

Tank Id: 2
Status: Removed
Status Date: Removed
Install Date: Not reported
Substance: Vehicular diesel
Content Description: Vehicular Diesel

Gallons: 1000

Tank Location: ABOVEGROUND

Tank Id: 3
Status: Removed
Status Date: Removed
Install Date: Not reported
Substance: Unleaded gas
Content Description: Unleaded Gas

Gallons: 280

Tank Location: ABOVEGROUND

Tank Id: 4

Status: In service
Status Date: In service
Install Date: 01-NOV-2007

Map ID
Direction
Distance

Distance (ft.)Site Database(s) EPA ID Number

FL POWER & LIGHT CO-OKEECHOBE SRVC CTR (Continued)

U002313644

EDR ID Number

Substance: Unleaded gas Content Description: Unleaded Gas

Gallons: 3000

Tank Location: ABOVEGROUND

Construction:

Tank ld:

Construction Category: Primary Construction

Construction Description: Stee

Tank ld: 4

Construction Category: Secondary Containment

Construction Description: Double wall

Tank ld:

Construction Category: Overfill/Spill

Construction Description: Spill containment bucket

Tank ld:

Construction Category: Overfill/Spill

Construction Description: Level gauges/alarms

Tank Id:

Construction Category: Miscellaneous Attributes

Construction Description: Compartmented

Monitoring:

Tank ID:

Monitoring Description: Monitor dbl wall tank space

Tank ID:

Monitoring Description: Visual inspection of ASTs

Tank ID:

Monitoring Description: Continuous electronic sensing

Tank ID: 4

Monitoring Description: External piping monitoring

Piping:

Tank ID:

Piping Category: Miscellaneous Attributes
Piping Description: Abv, no soil contact

Tank ID: 4

Piping Category: Miscellaneous Attributes
Piping Description: Suction piping system

Tank ID: 4

Piping Category: Primary Construction
Piping Description: Steel/galvanized metal

Tank Id: 5
Status: Deleted
Status Date: Deleted
Install Date: 01-NOV-2007

Map ID Direction Distance Distance (ft.)Site

rection EDR ID Number (stance)

FL POWER & LIGHT CO-OKEECHOBE SRVC CTR (Continued)

U002313644

EPA ID Number

Database(s)

Substance: Vehicular diesel Content Description: Vehicular Diesel

Gallons: 1500

Tank Location: ABOVEGROUND

Click here for Florida Oculus:

2 CHEVRON #47761 LUST U001363551 2768 SR 710 UST N/A OKEECHOBEE, FL 34974

LUST:

Region: STATE
Facility Id: 8512544
Facility Status: CLOSED
Facility Type: A - Retail Station
Facility Phone: (863)763-4522
Facility Cleanup Rank: Not reported
District: Southeast District

Lat/Long (dms): 27 14 46.2312 / 80 47 57.672

Section: Not reported
Township: Not reported
Range: Not reported
Feature: Not reported
Method: UNVR
Datum: 0
Score: 71

Score Effective Date: 02/23/2000
Score When Ranked: Not reported

Operator: DOUGLAS,ROY MALCOLM

Name Update: Not reported Address Update: Not reported

Discharge Cleanup Summary:

Discharge Date: 06/01/1992
PCT Discharge Combined: Not reported

Cleanup Required: R - CLEANUP REQUIRED Discharge Cleanup Status: SRCR - SRCR COMPLETE

Disch Cleanup Status Date: 12/27/2002 Cleanup Work Status: COMPLETED

Information Source: A - ABANDONED TANK RESTORATION

Other Source Description:

Eligibility Indicator:

Site Manager:

Site Mgr End Date:

Not reported

E - ELIGIBLE

ALLEN_T

01/06/2003

Tank Office: PCTM6 - PETROLEUM CLEANUP TEAM 6

Discharge Date: 12/27/1988
PCT Discharge Combined: Not reported

Cleanup Required: N - NO CLEANUP REQUIRED
Discharge Cleanup Status: NREQ - CLEANUP NOT REQUIRED

Disch Cleanup Status Date: 09/18/2001
Cleanup Work Status: COMPLETED
Information Source: E - EDI
Other Source Description: Not reported
Eligibility Indicator: I - INELIGIBLE
Site Manager: ALLEN_T
Site Mgr End Date: 01/06/2003

Map ID Direction Distance

Distance (ft.)Site Database(s) **EPA ID Number**

CHEVRON #47761 (Continued)

U001363551

EDR ID Number

Tank Office: PCTM6 - PETROLEUM CLEANUP TEAM 6

Petroleum Cleanup Program Eligibility:

Facility ID: 8512544 Discharge Date: 01-Jun-1992 Pct Discharge Combined With: Not reported

R - CLEANUP REQUIRED Cleanup Required: Discharge Cleanup Status: SRCR - SRCR COMPLETE

Disch Cleanup Status Date: 12/27/2002 Cleanup Work Status: **COMPLETED**

Information Source: A - ABANDONED TANK RESTORATION

Other Source Description: Not reported 6/12/1992 Application Received Date:

A - ABANDONED TANK RESTORATION PROGRAM Cleanup Program:

Eligibility Status: 8/19/1992 Elig Status Date: 8/19/1992 Letter Of Intent Date: Not reported Redetermined: No

Inspection Date: 06/10/1992 Site Manager: ALLEN_T

Site Mgr End Date: Tank Office: PCTM6 - PETROLEUM CLEANUP TEAM 6

01/06/2003

Deductible Amount: 500 Deductible Paid To Date: 500 Co-Pay Amount: 0 Co-Pay Paid To Date:

Cap Amount: Not reported

Contaminated Media:

Discharge Date: 06/01/1992 Pct Discharge Combined With: Not reported

R - CLEANUP REQUIRED Cleanup Required: Discharge Cleanup Status: SRCR - SRCR COMPLETE

Disch Cleanup Status Date: 12/27/2002 Cleanup Work Status: **COMPLETED**

A - ABANDONED TANK RESTORATION Information Source:

Other Source Description: Not reported E - ELIGIBLE Eliq Indicator: Site Manager: ALLEN_T Site Mgr End Date: 01/06/2003

PCTM6 - PETROLEUM CLEANUP TEAM Tank Office:

Contaminated Drinking Wells: Not reported Contaminated Monitoring Well: Not reported Contaminated Soil: Not reported Not reported Contaminated Surface Water: Not reported Contaminated Ground Water: B - UNLEADED GAS Pollutant:

Pollutant Other Description: Not reported Gallons Discharged: Not reported Discharge Date: 12/27/1988 Pct Discharge Combined With: Not reported

Cleanup Required: N - NO CLEANUP REQUIRED Discharge Cleanup Status: NREQ - CLEANUP NOT REQUIRED

Disch Cleanup Status Date: 09/18/2001 Cleanup Work Status: COMPLETED Information Source: E - EDI Not reported Other Source Description: Elig Indicator: I - INELIGIBLE Map ID Direction Distance

Distance (ft.)Site Database(s) EPA ID Number

CHEVRON #47761 (Continued)

U001363551

EDR ID Number

Site Manager: ALLEN_T Site Mgr End Date: 01/06/2003

Tank Office: PCTM6 - PETROLEUM CLEANUP TEAM

Contaminated Drinking Wells: 6
Contaminated Monitoring Well: Yes
Contaminated Soil: No
Contaminated Surface Water: No
Contaminated Ground Water: Yes

Pollutant: A - LEADED GAS
Pollutant Other Description: Not reported
Gallons Discharged: Not reported
Discharge Date: 12/27/1988

Pct Discharge Combined With:
Cleanup Required:
Discharge Cleanup Status:

Not reported
N - NO CLEANUP REQUIRED
NREQ - CLEANUP NOT REQUIRED

Disch Cleanup Status Date: 09/18/2001
Cleanup Work Status: COMPLETED
Information Source: E - EDI
Other Source Description: Not reported
Elig Indicator: I - INELIGIBLE
Site Manager: ALLEN_T
Site Mgr End Date: 01/06/2003

Tank Office: PCTM6 - PETROLEUM CLEANUP TEAM

Contaminated Drinking Wells: 6
Contaminated Monitoring Well: Yes
Contaminated Soil: No
Contaminated Surface Water: No
Contaminated Ground Water: Yes

Pollutant: B - UNLEADED GAS

Pollutant Other Description: Not reported Gallons Discharged: Not reported

Task Information:

District: SED
Facility ID: 8512544
Facility Status: CLOSED
Facility Type: A - Retail Station -

County: OKEECHOBEE

County ID: 47
Cleanup Eligibility Status: E

Source Effective Date: 12-27-2002 Discharge Date: 06-01-1992

Cleanup Required: R - CLEANUP REQUIRED
Discharge Cleanup Status: SRCR - SRCR COMPLETE

Disch Cleanup Status Date: 12-27-2002

SRC Action Type: SRCR - SITE REHABILITATION COMPLETION REPORT

SRC Submit Date: 10-15-2002 SRC Review Date: 10-21-2002 A - APPROVED SRC Completion Status: SRC Issue Date: 12-27-2002 SRC Comment: Not reported Cleanup Work Status: COMPLETED Site Mgr: ALLEN_T Site Mgr End Date: 01-06-2003 Tank Office: PCTM6 - Team 6 SR Task ID: Not reported

SR Cleanup Responsible: SR Funding Eligibility Type: -

Map ID Direction Distance Distance (ft.)Site

stance

CHEVRON #47761 (Continued)

U001363551

Database(s)

EDR ID Number

EPA ID Number

SR Actual Cost: Not reported SR Completion Date: Not reported SR Payment Date: Not reported SR Oral Date: Not reported SR Written Date: Not reported SR Soil Removal: Not reported SR Free Product Removal: Not reported Not reported SR Soil Tonnage Removed: SR Soil Treatment: Not reported SR Other Treatment: Not reported Not reported SR Alternate Proc Received Date: Not reported SR Alternate Procedure Status: SR Alternate Procedure Status Date: Not reported SR Alternate Procedure Comments: Not reported SA Task ID: 36117

SA Cleanup Responsible: SA Funding Eligibility Type: -

SA Actual Cost:

SA Completion Date:

SA Payment Date:

RAP Task ID:

RAP Cleanup Responsible ID:

Not reported
Not reported
36118
ST - STATE

RAP Funding Eligibility Type:

RAP Actual Cost:

RAP Completion Date:

RAP Payment Date:

RAP Last Order Approved:

RA Task ID:

RA Cleanup Responsible:

Not reported
Not reported
Str - STATE

RA Funding Eligibility Type: - RA Years to Complete: 0

RA Actual Cost:

District:

Facility ID:

Racility Status:

Not reported
SED
8512544
CLOSED

Facility Type: A - Retail Station - County: OKEECHOBEE

County ID: 47
Cleanup Eligibility Status: I

Source Effective Date: Not reported Discharge Date: 12-27-1988

Cleanup Required: N - NO CLEANUP REQUIRED
Discharge Cleanup Status: NREQ - CLEANUP NOT REQUIRED

Disch Cleanup Status Date: 09-18-2001

SRC Action Type:

SRC Submit Date: Not reported SRC Review Date: Not reported

SRC Completion Status:

SRC Issue Date:

SRC Comment:

Cleanup Work Status:

Site Mgr:

Site Mgr End Date:

Tank Office:

Not reported

COMPLETED

ALLEN_T

01-06-2003

PCTM6 - Team 6

SR Task ID: 36120 SR Cleanup Responsible: ST - STATE

SR Funding Eligibility Type: -

Map ID Direction Distance Distance (ft.)Site

ection EDR ID Number

Database(s) EPA ID Number

CHEVRON #47761 (Continued)

U001363551

SR Actual Cost: Not reported Not reported SR Completion Date: SR Payment Date: Not reported SR Oral Date: Not reported SR Written Date: Not reported Not reported SR Soil Removal: Not reported SR Free Product Removal: SR Soil Tonnage Removed: Not reported SR Soil Treatment: Not reported SR Other Treatment: Not reported SR Alternate Proc Received Date: Not reported Not reported SR Alternate Procedure Status: SR Alternate Procedure Status Date: Not reported SR Alternate Procedure Comments: Not reported SA Task ID: 36121 SA Cleanup Responsible: ST - STATE

SA Funding Eligibility Type: -

SA Actual Cost:

SA Completion Date:

SA Payment Date:

RAP Task ID:

Not reported

Not reported

Not reported

36122

RAP Cleanup Responsible ID: ST - STATE

RAP Funding Eligibility Type:

RAP Actual Cost:

RAP Completion Date:

RAP Payment Date:

RAP Last Order Approved:

RATask ID:

RAP Cleanup Responsible:

Not reported

Not reported

Not reported

ST - STATE

RA Funding Eligibility Type:

RA Years to Complete: Not reported RA Actual Cost: Not reported

Click here for Florida Oculus:

UST:

Facility Id: 8512544
Facility Status: CLOSED
Type Description: Retail Station
Facility Phone: (863) 763-4522
Region: STATE
Positioning Method: UNVR

Lat/Long (dms): 27 14 47 / 80 48 47

Owner Records Not Found for this facility id:

Tank Info:

Tank Id:

Status: Removed
Status Date: 31-MAY-1990
Install Date: 01-JUL-1963
Substance: Unleaded gas
Content Description: Unleaded Gas
Gallons: 1000

Vessel Indicator: TANK

Tank Location: UNDERGROUND

DEP Contractor: No

Map ID Direction Distance

Distance (ft.)Site Database(s) **EPA ID Number**

CHEVRON #47761 (Continued)

U001363551

EDR ID Number

Tank Id: 2 Status: Removed Status Date: 31-MAY-1990 Install Date: 01-JUL-1975 Substance: Leaded gas

Leaded Gas Content Description: Gallons: 3000 **TANK** Vessel Indicator:

Tank Location: **UNDERGROUND**

DEP Contractor: No

Tank Id: 3

Status: Removed Status Date: 31-MAY-1990 01-JUL-1982 Install Date: Substance: Unleaded gas Unleaded Gas Content Description:

2000 Gallons: Vessel Indicator: **TANK**

UNDERGROUND Tank Location:

DEP Contractor: No

Tank Id:

Status: Removed Status Date: 31-MAY-1990 Install Date: 01-JUL-1982 Substance: Vehicular diesel Content Description: Vehicular Diesel

Gallons: 2000 Vessel Indicator: **TANK**

Tank Location: **UNDERGROUND**

DEP Contractor: No

Click here for Florida Oculus:

TOWN STAR #40 3 3990 HWY 710 OKEECHOBEE, FL 34974

U004138146 LUST UST N/A

LUST:

Region: STATE Facility Id: 8630309 Facility Status: **OPEN**

Facility Type: A - Retail Station Facility Phone: (863)763-0907

Facility Cleanup Rank: 3987

Southeast District District: Lat/Long (dms): 27 14 27.2 / 80 47 17.8

Section: Not reported Township: Not reported Not reported Range: Feature: UST'S Method: AGPS Datum: Score: 36 Score Effective Date: 05/24/2012

Score When Ranked: 41 Map ID Direction Distance Distance (ft.)Site

Virection EDR ID Number

TOWN STAR #40 (Continued) U004138146

Database(s)

EPA ID Number

Operator: ROSEMARY HERRON

 Name Update:
 07/29/2009

 Address Update:
 07/29/2009

Petroleum Cleanup PCT Facility Score:

Facility Cleanup Status: ONGO - ONGOING Contact: JOHN TIFFANY

Contact Company: TIME SAVER FOOD STORES
Contact Address: 2178 RESERVE PARK TRACE
Contact City/State/Zip: PORT SAINT LUCIE, FL 34986

Phone: (772)466-8585

Bad Address Ind: N State: FL

Zip: 34974, 3516

Score: 36

Score Effective Date: 2012-05-24 00:00:00

Related Party ID: 54445

Primary RP Role: ACCOUNT OWNER

RP Begin Date: 07/10/2003
RP Zip: Not reported
RP Extension: Not reported

Discharge Cleanup Summary:

Discharge Date: 11/22/1988
PCT Discharge Combined: Not reported

Cleanup Required: R - CLEANUP REQUIRED Discharge Cleanup Status: RA - RA ONGOING

Disch Cleanup Status Date: 11/02/2009
Cleanup Work Status: INACTIVE
Information Source: E - EDI
Other Source Description: Not reported
Eligibility Indicator: E - ELIGIBLE
Site Manager: PERRY_H
Site Mgr End Date: Not reported

Tank Office: PCTM6 - PETROLEUM CLEANUP TEAM 6

Petroleum Cleanup Program Eligibility:

Facility ID: 8630309
Discharge Date: 22-Nov-1988
Pct Discharge Combined With: Not reported

Cleanup Required: R - CLEANUP REQUIRED Discharge Cleanup Status: RA - RA ONGOING

Disch Cleanup Status Date: 11/02/2009
Cleanup Work Status: INACTIVE
Information Source: E - EDI
Other Source Description: Not reported
Application Received Date: 12/30/1988

Cleanup Program: E - EARLY DETECTION INCENTIVE

Eligibility Status: 8/30/1990
Elig Status Date: 8/30/1990
Letter Of Intent Date: Not reported
Redetermined: No

Inspection Date: 07/25/1990
Site Manager: PERRY_H
Site Mgr End Date: Not reported

Tank Office: PCTM6 - PETROLEUM CLEANUP TEAM 6

Deductible Amount: Not reported

Deductible Paid To Date: 0

Map ID Direction Distance

Distance (ft.)Site Database(s) EPA ID Number

TOWN STAR #40 (Continued)

· ·

EDR ID Number

U004138146

Co-Pay Amount: Not reported

Co-Pay Paid To Date:

Cap Amount: Not reported

Contaminated Media:

Discharge Date: 11/22/1988
Pct Discharge Combined With: Not reported

Cleanup Required: R - CLEANUP REQUIRED Discharge Cleanup Status: RA - RA ONGOING

Disch Cleanup Status Date: 11/02/2009
Cleanup Work Status: INACTIVE
Information Source: E - EDI
Other Source Description: Not reported
Elig Indicator: E - ELIGIBLE
Site Manager: PERRY_H
Site Mgr End Date: Not reported

Tank Office: PCTM6 - PETROLEUM CLEANUP TEAM

Contaminated Drinking Wells: 0
Contaminated Monitoring Well: Yes
Contaminated Soil: No
Contaminated Surface Water: No
Contaminated Ground Water: No

Pollutant: Y - UNKNOWN/NOT REPORTED

Pollutant Other Description: Not reported Gallons Discharged: Not reported

Task Information:

District: SED
Facility ID: 8630309
Facility Status: OPEN

Facility Type: A - Retail Station - OKEECHOBEE

County ID: 47
Cleanup Eligibility Status: E

Source Effective Date: Not reported Discharge Date: 11-22-1988

Cleanup Required: R - CLEANUP REQUIRED Discharge Cleanup Status: RA - RA ONGOING

Disch Cleanup Status Date: 11-02-2009

SRC Action Type:

SRC Submit Date: Not reported SRC Review Date: Not reported

SRC Completion Status: -

SRC Issue Date:

SRC Comment:

Cleanup Work Status:

Site Mgr:

Site Mgr End Date:

Tank Office:

SR Task ID:

Not reported

INACTIVE

PERRY_H

Not reported

PCTM6 - Team 6

36042

SR Task ID: 36042 SR Cleanup Responsible: ST - STATE

SR Funding Eligibility Type:

SR Actual Cost:

SR Completion Date:

SR Payment Date:

SR Oral Date:

SR Written Date:

Not reported

Map ID Direction Distance Distance (ft.)Site

EDR ID Number

Database(s) **EPA ID Number**

U004138146

TOWN STAR #40 (Continued)

SR Free Product Removal: Not reported Not reported SR Soil Tonnage Removed: SR Soil Treatment: Not reported SR Other Treatment: Not reported SR Alternate Proc Received Date: Not reported SR Alternate Procedure Status: Not reported SR Alternate Procedure Status Date: Not reported SR Alternate Procedure Comments: Not reported 36043 SA Task ID: SA Cleanup Responsible: ST - STATE

SA Funding Eligibility Type:

SA Actual Cost: Not reported SA Completion Date: Not reported SA Payment Date: Not reported RAP Task ID: 36044 RAP Cleanup Responsible ID: ST - STATE

RAP Funding Eligibility Type:

RAP Actual Cost: Not reported **RAP Completion Date:** Not reported **RAP Payment Date:** Not reported RAP Last Order Approved: Not reported RA Task ID: 36045 ST - STATE RA Cleanup Responsible:

RA Funding Eligibility Type:

RA Years to Complete: Not reported **RA Actual Cost:** Not reported

Click here for Florida Oculus:

UST:

8630309 Facility Id: Facility Status: OPEN Type Description: Retail Station Facility Phone: (863) 763-0907 STATE Region:

AGPS Positioning Method:

Lat/Long (dms): 27 14 27.1999999 / 80 47 17.8000000

Owner:

Owner Id: 54445

Owner Name: TIME SAVER FOOD STORES Owner Address: 2178 RESERVE PARK TRACE

Owner Address 2: ATTN: JOHN TIFFANY

Owner City, St, Zip: PORT SAINT LUCIE, FL 34986

Owner Contact: JOHN TIFFANY Owner Phone: (772) 466-8585

Tank Info:

Tank Id:

Status: Removed Status Date: 29-JUL-2009 Install Date: 01-MAY-1986 Substance: Unleaded gas Content Description: **Unleaded Gas** 10000 Gallons:

Vessel Indicator: **TANK**

UNDERGROUND Tank Location:

Map ID
Direction
Distance

Distance (ft.)Site Database(s) EPA ID Number

TOWN STAR #40 (Continued)

U004138146

EDR ID Number

DEP Contractor: No

Tank Id: 2

Status: Removed
Status Date: 29-JUL-2009
Install Date: 01-MAY-1986
Substance: Unleaded gas
Content Description: Unleaded Gas
Gallons: 10000
Vessel Indicator: TANK

Tank Location: UNDERGROUND

DEP Contractor: No

Tank ld: 3

Status: Removed
Status Date: 29-JUL-2009
Install Date: 01-MAY-1986
Substance: Vehicular diesel
Content Description: Vehicular Diesel

Gallons: 10000 Vessel Indicator: TANK

Tank Location: UNDERGROUND

DEP Contractor: No

Tank ld: 4

Status: In service
Status Date: 01-AUG-2009
Install Date: 01-JUL-2009
Substance: Vehicular diesel
Content Description: Vehicular Diesel

Gallons: 22000 Vessel Indicator: TANK

Tank Location: UNDERGROUND

DEP Contractor: No

Construction:

Tank Id:

Construction Category: Primary Construction

Construction Description: Fiberglass

Tank ld: 4

Construction Category: Overfill/Spill
Construction Description: Ball check valve

Tank Id:

Construction Category: Overfill/Spill

Construction Description: Spill containment bucket

Tank Id: 4

Construction Category: Overfill/Spill Construction Description: Flow shut-Off

Tank ld:

Construction Category: Overfill/Spill Construction Description: Tight fill

Tank Id:

Construction Category: Overfill/Spill

Map ID Direction Distance

Distance (ft.)Site Database(s) **EPA ID Number**

TOWN STAR #40 (Continued)

U004138146

EDR ID Number

Construction Description: Level gauges/alarms

Tank Id:

Construction Category: Secondary Containment

Construction Description: Double wall

Tank Id:

Miscellaneous Attributes Construction Category:

Construction Description: Compartmented

Monitoring:

Tank ID:

Monitoring Description: Monitor dbl wall tank space

Tank ID:

Monitoring Description: Mechanical line leak detector

Tank ID:

Monitoring Description: Monitor dbl wall pipe space

Tank ID:

Monitoring Description: Continuous electronic sensing

Tank ID:

Monitoring Description: Electronic monitor pipe sumps

Tank ID:

Monitoring Description: Visual inspect dispenser liners

Piping:

Tank ID:

Piping Category: Secondary Containment

Piping Description: Double wall

Tank ID:

Piping Category: Miscellaneous Attributes

Piping Description: Dispenser liners

Tank ID:

Primary Construction Piping Category:

Piping Description: Fiberglass

Tank ID:

Piping Category: Miscellaneous Attributes Piping Description: Pressurized piping system

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MAP FINDINGS

Map ID
Direction
Distance

Distance (ft.)Site Database(s) EPA ID Number

3 TOWN STAR # 40 3993 HWY 710 E OKEECHOBEE, FL FINDS 1012070869 N/A

EDR ID Number

FINDS:

Registry ID: 110038370367

Environmental Interest/Information System

US National Pollutant Discharge Elimination System (NPDES) module of the Compliance Information System (ICIS) tracks surface water permits issued under the Clean Water Act. Under NPDES, all facilities that discharge pollutants from any point source into waters of the United States are required to obtain a permit. The permit will likely contain limits on what can be discharged, impose monitoring and reporting requirements, and include other provisions to ensure that the discharge does not adversely affect water quality.

PCS (Permit Compliance System) is a computerized management information system that contains data on National Pollutant Discharge Elimination System (NPDES) permit holding facilities. PCS tracks the permit, compliance, and enforcement status of NPDES facilities.

Count: 72 records ORPHAN SUMMARY

City	EDR ID	Site Name	Site Address	Zip	Database(s)
BUCKHEAD RIDGE	S109418011	BUCKHEAD RIDGE PUMP STATION S-129	SR 78	34974	AIRS
BUCKHEAD RIDGE	S101264716	SOUTH FL WATER MGMT DIST S-127	P S S-127 L-48 @BUCKHEAD RIDGE	34974	LUST, LAST, AST
LAKEPORT	S108634871	SOUTH FLORIDA WATER MANAGEMENT DISTRICT - PUMP STATION S- 12	JUNCTION L-49 AND LAKE OKEECHOBEE (SR 78 7MI NORTH	34974	TIER 2
OKEECHOBEE	S108978858	OKEECHOBEE COUNTY FIRE RESCUE #4	1199 NORTHEAST 168TH STREET	34972	AST, TIER 2
OKEECHOBEE	1010500312	TOWNS OF OKEECHOBEE	NW 23RD LN		FINDS
OKEECHOBEE	A100359004	OKEECHOBEE ACHIEVEMENT ACADEMY	1000 NW 34TH ST	34972	AST
OKEECHOBEE	S102848128	PRIMROSE RV PARK	US 441 SOUTH		NPDES
OKEECHOBEE	1012049922	SUPERIOR WATER WORKS, INC.	4072 HWY 441 N	34972	SSTS
OKEECHOBEE	S107714788	BELLSOUTH TELECOMMUNICATIONS - E6093	26800 HIGHWAY 441 NORTH	34972	TIER 2
OKEECHOBEE	S102848106	BLUE CYPRESS WWTF	13801 S.R. 441 S.E.		NPDES
OKEECHOBEE	S103616416	MCARTHUR FARMS DAIRY BARNS 1 & 2	HIGHWAY 441 NORTH		NPDES
OKEECHOBEE	U004053726	MCARTHUR FARMS INC - BARN 1	18116 HWY 441 N	34972	AST
OKEECHOBEE	S109352831	BUREAU OF INDIAN AFFAIRS-BRIGHTON	RT 6 BOX 666		FF TANKS
OKEECHOBEE	1008157577	SR 70 - SLOPE STABILIZATION	SR 70 /CSX OVERPASS -OKEECHOBE		FINDS
OKEECHOBEE	1011437516	THE ESTATES AT OKEECHOBEE PINES	SR 70 WEST OF BERMAN ROAD		FINDS
OKEECHOBEE	1015908899	DOLLAR GENERAL OKEECHOBEE	1620 HIGHWAY 70 W		FINDS
OKEECHOBEE	S104492290	PINE RIDGE PARK	SR 70		NPDES
OKEECHOBEE	1014388955	TIRE KINGDOM LLC #955	1595 HIGHWAY 70 E	34972	RCRA NonGen / NLR
OKEECHOBEE	U001352545	HITCHING POST-BRIGHTON SEMINOLE	HWY 721 S	34974	UST
OKEECHOBEE	1014468614	SEMINOLE TRIBE OF FLORIDA	RT 721A/RED BARN ROAD	34974	RCRA-CESQG
OKEECHOBEE	S108787777	E-1G20	SR 78 TO CR 78B		NPDES
OKEECHOBEE	U001363571	PARRISH SEPTIC TANK INC	HWY 78 W	34974	UST
OKEECHOBEE	S102848105	BIG "O" CAMPGROUND	SR 78 WEST OF SR 441		NPDES
OKEECHOBEE	S113426883	HHD CULVERT 7,9 & TAYLOR CREEK CULVERT ADANDONMENT	900 HWY 78 W		NPDES
OKEECHOBEE	S111443947	BUCKHEAD RIDGE MOSQUITO CONTROL DISTRICT	30052 HIGHWAY 78 WEST		NPDES
OKEECHOBEE	S102848116	OKEE-TANTI REC AREA	SR 78, 7.6 MI SW OF OKEECHOBEE		NPDES
OKEECHOBEE	U001363546	OKEECHOBEE COUNTY AIRPORT	RT 8 BOX 510 HWY 98N	34972	UST
OKEECHOBEE	S108516481	MILKING R DAIRY	6300 HIGHWAY 98 NORTH		NPDES
OKEECHOBEE	1011436696	OKEECHOBEE, CITY OF - COMMERCE CENTER	APPROX. 1250 W OF US 441 ON NE 9TH ST		FINDS
OKEECHOBEE	1008156964	CITY OF OKEECHOBEE COMMERCE CE	APPROX. 1250' W OF US 441 ON N		FINDS
OKEECHOBEE	1012091239	CANE FIELDS SITE	BIA HWY 1305 AND RED BARN ROAD	34974	US BROWNFIELDS, FINDS
OKEECHOBEE	S108634844	SOUTH FLORIDA WATER MANAGEMENT DISTRICT - OKEECHOBEE	1000 NORTH EAST 40 TH AVENUE	34972	TIER 2
OKEECHOBEE	S103616415	MCARTHUR FARMS DAIRY - BARN 4	U.S. HIGHWAY 441		NPDES
OKEECHOBEE	1012240141	SOUTH FLORIDA WATER MANAGEMENT DISTRICT	2780 SE HWY 441	34974	FINDS, US AIRS
OKEECHOBEE	S107936806	PUMP STATION S-133	2780 SE HWY 441	34974	AIRS
OKEECHOBEE	S102848135	VILLA MARGARET	4648 US HWY 441N		NPDES
OKEECHOBEE	1011406635	OKEECHOBEE NEW EVERGLADES SCHOOL	3 MI.EAST OF CITY OF OKEE.		FINDS
OKEECHOBEE	S102848118	OKEECHOBEE CORRECTIONAL WWTF	9 MILES NORTH OF OKEECHOBEE		NPDES
OKEECHOBEE	1011403233	OKEECHOBEE CORRECTIONAL WWTF	9 MILES NORTH OF OKEECHOBEE		FINDS
OKEECHOBEE	1007994023	OKEECHOBEE UTILITY AUTHORITY GWTP	1200 N.E.12TH ST.		FINDS

Count: 72 records ORPHAN SUMMARY

City	EDR ID	Site Name	Site Address	Zip	Database(s)
OKEECHOBEE	1011833496	OKEECHOBEE UTILITY AUTHORITY GWTP	1200 N.E.12TH ST.	34974	RMP
OKEECHOBEE	S107723813	SOUTHEAST MILK - OKEECHOBEE SUPPLY	1005 WEST NORTH PARK STREET	34972	TIER 2
OKEECHOBEE		SOUTH FL WATER MGMT DIST-S 72	C-40 NW HWY 78-20 MI FROM OKEE		UST
OKEECHOBEE		DR FRED BROWN CHILDREN'S HEALTH CENTER	NWC OF NW 20TH LN & US-441		NPDES
OKEECHOBEE		BOWLEGS PASTURE SITE	WEST OF BIA HWY 283	34974	US BROWNFIELDS, FINDS
OKEECHOBEE		SOUTH FL WATER MGMT DIST-LYKES BROS WWTR PAST	S SIDE C-39A CANAL, 10 MILES E HWY 27	34974	,
OKEECHOBEE	S111310925	APPLEBEES	SR-70		NPDES
OKEECHOBEE	S112805034	GLADES BUCKHEAD RIDGE RESORT	670 STATE ROAD 78B	34974	SWF/LF
OKEECHOBEE	S102846708	LAKEPORT MOTEL AND RESTAURANT WWTP	11700 E STATE ROAD 78 NE		NPDES
OKEECHOBEE	1012216316	FLORIDA GAS TRANSMISSION COMPANY	STATE HIGHWAY 70	34974	FINDS, US AIRS
OKEECHOBEE	S109996282	VENTURE INN	3095 E STATE ROAD 60		NPDES
OKEECHOBEE	1014694113	OKEECHOBEE LANDFILL CELLS 33-3	UNKNOWN		FINDS
OKEECHOBEE		OKEECHOBEE COUNTY SCHOOL - OKE	UNKNOWN		FINDS
OKEECHOBEE		LAKE OKEECHOBEE S-65ESTRUCTURE	UNKNOWN		FINDS
OKEECHOBEE		OKEECHOBEE ASPHALT AND READY M	UNKNOWN		FINDS
OKEECHOBEE	1014690796	OKEECHOBEE LANDFILL FLARE COMP	UNKNOWN		FINDS
OKEECHOBEE		OKEECHOBEE CONTRACTOR YARD	UNKNOWN		FINDS
OKEECHOBEE		OKEECHOBEE DRIVERS ED LOT IMPROVEMENTS	UNKNOWN		FINDS
OKEECHOBEE	1004458180	OKEECHOBEE COUNTY SCHOOL DISTRICT	1090 SOUTH WEST 5TH AVENUE	34974	FTTS, HIST FTTS, FINDS
OKEECHOBEE - NEG SOD	S113388221	SOUTHEAST MILK - OKEECHOBEE SUPPLY	1005 WEST NORTH PARK STREET -NEG SODNEG SOD- 2008		TIER 2
OKEECHOBEE COUNTY		CYPRESS ENERGY LP	STATE ROAD ROUTE 98		UIC
UNICORP	S108634881	SOUTH FLORIDA WATER MANAGEMENT DISTRICT -	US 441 WEST SIDE 7 MILE NORTH OF STATE ROAD 76(BEH	34974	TIER 2
		PUMP STATION S-135			
UNICORP	S111751167		US 441 (WEST SIDE) 7 MILE NORTH OF SR 76 (BEHIND J&S FISH	34974	TIER 2
		PUMP STATION S-135	CA		
UNICORP	S108634882	SOUTH FLORIDA WATER MANAGEMENT DISTRICT -	57005 ALLIGATOR ALLEY (APPROX. 25 MI. W OF US 27)	34974	TIER 2
		PUMP STATION S-140			
UNICORP	S111751159	SOUTH FLORIDA WATER MANAGEMENT - LYKES	CANAL C39A SOUTH OF STATE ROAD 70 - 21 MILES WEST OF US	34974	TIER 2
		BROTHERS	HIGH		
UNICORP	S113388213	SOUTH FLORIDA WATER MANAGEMENT DISTRICT -	US HIGHWAY 441 - 7 MILE NORTH OF STATE ROAD 76BEHIND J	34974	TIER 2
		PUMP STATION S-135	AND S		
UNICORP	S113388212	SOUTH FLORIDA WATER MANAGEMENT DISTRICT -	US HIGHWAY 27 - 5 MILES NORTH OF PALM BEACH / BROWARD	34974	TIER 2
		PUMP STATION G - 3	COUNTY		
UNICORP	S108634891	SOUTH FLORIDA WATER MANAGEMENT DISTRICT -	SIX MILE SOUTH STATE 880, (SOUTHERN TIP OF 1 WEST)	34974	TIER 2
		PUMP STATION G 310			
UNICORP	S108634892	SOUTH FLORIDA WATER MANAGEMENT DISTRICT -	SIX MILES SOUTH OF STATE ROAD 880(SOUTHERN TIP OF	34974	TIER 2
		PUMP STATION G 310			
UNICORP	S108634893	SOUTH FLORIDA WATER MANAGEMENT DISTRICT -	THREE NORTH EAST OF US 27(PALM BEACH/BROWARD COUNT	34974	TIER 2
		PUMP STATION G-335			
UNICORP	S111751164	SOUTH FLORIDA WATER MANAGEMENT DISTRICT -	THREE MILES NORTHEAST OF US 27 (PALM BEACH/BROWARD COUNTY	34974	TIER 2
		PUMP STATION G-335	LI		
UNICORP	S108634899	SOUTH FLORIDA WATER MANAGEMENT DISTRICT -	ON US 27, 5 MILE NORTH OF PALM BEACH/BROWARD CO. LINE	34974	TIER 2
		PUMP STATION G - 3			

To maintain currency of the following federal and state databases, EDR contacts the appropriate governmental agency on a monthly or quarterly basis, as required.

Number of Days to Update: Provides confirmation that EDR is reporting records that have been updated within 90 days from the date the government agency made the information available to the public.

FEDERAL RECORDS

NPL: National Priority List

National Priorities List (Superfund). The NPL is a subset of CERCLIS and identifies over 1,200 sites for priority cleanup under the Superfund Program. NPL sites may encompass relatively large areas. As such, EDR provides polygon coverage for over 1,000 NPL site boundaries produced by EPA's Environmental Photographic Interpretation Center (EPIC) and regional EPA offices.

Date of Government Version: 04/26/2013 Date Data Arrived at EDR: 05/09/2013 Date Made Active in Reports: 07/10/2013

Number of Days to Update: 62

Source: EPA Telephone: N/A

Last EDR Contact: 10/11/2013

Next Scheduled EDR Contact: 01/20/2014 Data Release Frequency: Quarterly

NPL Site Boundaries

Sources:

EPA's Environmental Photographic Interpretation Center (EPIC)

Telephone: 202-564-7333

EPA Region 1 EPA Region 6

Telephone 617-918-1143 Telephone: 214-655-6659

EPA Region 3 EPA Region 7

Telephone 215-814-5418 Telephone: 913-551-7247

EPA Region 4 **EPA Region 8**

Telephone 404-562-8033 Telephone: 303-312-6774

EPA Region 9 EPA Region 5

Telephone 312-886-6686 Telephone: 415-947-4246

EPA Region 10

Telephone 206-553-8665

Proposed NPL: Proposed National Priority List Sites

A site that has been proposed for listing on the National Priorities List through the issuance of a proposed rule in the Federal Register. EPA then accepts public comments on the site, responds to the comments, and places on the NPL those sites that continue to meet the requirements for listing.

Date of Government Version: 04/26/2013 Date Data Arrived at EDR: 05/09/2013

Date Made Active in Reports: 07/10/2013

Number of Days to Update: 62

Source: EPA Telephone: N/A

Last EDR Contact: 10/11/2013

Next Scheduled EDR Contact: 01/20/2014 Data Release Frequency: Quarterly

DELISTED NPL: National Priority List Deletions

The National Oil and Hazardous Substances Pollution Contingency Plan (NCP) establishes the criteria that the EPA uses to delete sites from the NPL. In accordance with 40 CFR 300.425.(e), sites may be deleted from the NPL where no further response is appropriate.

Date of Government Version: 04/26/2013 Date Data Arrived at EDR: 05/09/2013

Date Made Active in Reports: 07/10/2013

Number of Days to Update: 62

Source: EPA Telephone: N/A

Last EDR Contact: 10/11/2013

Next Scheduled EDR Contact: 01/20/2014 Data Release Frequency: Quarterly

NPL LIENS: Federal Superfund Liens

Federal Superfund Liens. Under the authority granted the USEPA by CERCLA of 1980, the USEPA has the authority to file liens against real property in order to recover remedial action expenditures or when the property owner received notification of potential liability. USEPA compiles a listing of filed notices of Superfund Liens.

Date of Government Version: 10/15/1991 Date Data Arrived at EDR: 02/02/1994 Date Made Active in Reports: 03/30/1994

Number of Days to Update: 56

Source: EPA

Telephone: 202-564-4267 Last EDR Contact: 08/15/2011

Next Scheduled EDR Contact: 11/28/2011 Data Release Frequency: No Update Planned

CERCLIS: Comprehensive Environmental Response, Compensation, and Liability Information System

CERCLIS contains data on potentially hazardous waste sites that have been reported to the USEPA by states, municipalities, private companies and private persons, pursuant to Section 103 of the Comprehensive Environmental Response, Compensation, and Liability Act (CERCLA). CERCLIS contains sites which are either proposed to or on the National Priorities List (NPL) and sites which are in the screening and assessment phase for possible inclusion on the NPL.

Date of Government Version: 04/26/2013 Date Data Arrived at EDR: 05/29/2013 Date Made Active in Reports: 08/09/2013

Number of Days to Update: 72

Source: EPA

Telephone: 703-412-9810 Last EDR Contact: 10/18/2013

Next Scheduled EDR Contact: 12/09/2013 Data Release Frequency: Quarterly

CERCLIS-NFRAP: CERCLIS No Further Remedial Action Planned

Archived sites are sites that have been removed and archived from the inventory of CERCLIS sites. Archived status indicates that, to the best of EPA's knowledge, assessment at a site has been completed and that EPA has determined no further steps will be taken to list this site on the National Priorities List (NPL), unless information indicates this decision was not appropriate or other considerations require a recommendation for listing at a later time. This decision does not necessarily mean that there is no hazard associated with a given site; it only means that, based upon available information, the location is not judged to be a potential NPL site.

Date of Government Version: 04/26/2013 Date Data Arrived at EDR: 05/29/2013 Date Made Active in Reports: 08/09/2013

Number of Days to Update: 72

Source: EPA

Telephone: 703-412-9810 Last EDR Contact: 10/18/2013

Next Scheduled EDR Contact: 12/09/2013 Data Release Frequency: Quarterly

LIENS 2: CERCLA Lien Information

A Federal CERCLA ('Superfund') lien can exist by operation of law at any site or property at which EPA has spent Superfund monies. These monies are spent to investigate and address releases and threatened releases of contamination. CERCLIS provides information as to the identity of these sites and properties.

Date of Government Version: 02/06/2013 Date Data Arrived at EDR: 04/25/2013 Date Made Active in Reports: 05/10/2013

Number of Days to Update: 15

Source: Environmental Protection Agency

Telephone: 202-564-6023 Last EDR Contact: 07/24/2013

Next Scheduled EDR Contact: 11/11/2013 Data Release Frequency: Varies

CORRACTS: Corrective Action Report

CORRACTS identifies hazardous waste handlers with RCRA corrective action activity.

Date of Government Version: 07/11/2013 Date Data Arrived at EDR: 08/08/2013 Date Made Active in Reports: 09/13/2013

Number of Days to Update: 36

Source: EPA

Telephone: 800-424-9346 Last EDR Contact: 10/02/2013

Next Scheduled EDR Contact: 01/13/2014 Data Release Frequency: Quarterly

RCRA-TSDF: RCRA - Treatment, Storage and Disposal

RCRAInfo is EPA's comprehensive information system, providing access to data supporting the Resource Conservation and Recovery Act (RCRA) of 1976 and the Hazardous and Solid Waste Amendments (HSWA) of 1984. The database includes selective information on sites which generate, transport, store, treat and/or dispose of hazardous waste as defined by the Resource Conservation and Recovery Act (RCRA). Transporters are individuals or entities that move hazardous waste from the generator offsite to a facility that can recycle, treat, store, or dispose of the waste. TSDFs treat, store, or dispose of the waste.

Date of Government Version: 07/11/2013 Date Data Arrived at EDR: 08/08/2013 Date Made Active in Reports: 09/13/2013

Number of Days to Update: 36

Source: Environmental Protection Agency

Telephone: (404) 562-8651 Last EDR Contact: 10/02/2013

Next Scheduled EDR Contact: 01/13/2014 Data Release Frequency: Quarterly

RCRA-LQG: RCRA - Large Quantity Generators

RCRAInfo is EPA's comprehensive information system, providing access to data supporting the Resource Conservation and Recovery Act (RCRA) of 1976 and the Hazardous and Solid Waste Amendments (HSWA) of 1984. The database includes selective information on sites which generate, transport, store, treat and/or dispose of hazardous waste as defined by the Resource Conservation and Recovery Act (RCRA). Large quantity generators (LQGs) generate over 1,000 kilograms (kg) of hazardous waste, or over 1 kg of acutely hazardous waste per month.

Date of Government Version: 07/11/2013 Date Data Arrived at EDR: 08/08/2013 Date Made Active in Reports: 09/13/2013

Number of Days to Update: 36

Source: Environmental Protection Agency

Telephone: (404) 562-8651 Last EDR Contact: 10/02/2013

Next Scheduled EDR Contact: 01/13/2014 Data Release Frequency: Quarterly

RCRA-SQG: RCRA - Small Quantity Generators

RCRAInfo is EPA's comprehensive information system, providing access to data supporting the Resource Conservation and Recovery Act (RCRA) of 1976 and the Hazardous and Solid Waste Amendments (HSWA) of 1984. The database includes selective information on sites which generate, transport, store, treat and/or dispose of hazardous waste as defined by the Resource Conservation and Recovery Act (RCRA). Small quantity generators (SQGs) generate between 100 kg and 1,000 kg of hazardous waste per month.

Date of Government Version: 07/11/2013 Date Data Arrived at EDR: 08/08/2013 Date Made Active in Reports: 09/13/2013

Number of Days to Update: 36

Source: Environmental Protection Agency Telephone: (404) 562-8651

Last EDR Contact: 10/02/2013

Next Scheduled EDR Contact: 01/13/2014 Data Release Frequency: Quarterly

RCRA-CESQG: RCRA - Conditionally Exempt Small Quantity Generators

RCRAInfo is EPA's comprehensive information system, providing access to data supporting the Resource Conservation and Recovery Act (RCRA) of 1976 and the Hazardous and Solid Waste Amendments (HSWA) of 1984. The database includes selective information on sites which generate, transport, store, treat and/or dispose of hazardous waste as defined by the Resource Conservation and Recovery Act (RCRA). Conditionally exempt small quantity generators (CESQGs) generate less than 100 kg of hazardous waste, or less than 1 kg of acutely hazardous waste per month.

Date of Government Version: 07/11/2013 Date Data Arrived at EDR: 08/08/2013 Date Made Active in Reports: 09/13/2013

Number of Days to Update: 36

Source: Environmental Protection Agency

Telephone: (404) 562-8651 Last EDR Contact: 10/02/2013

Next Scheduled EDR Contact: 01/13/2014 Data Release Frequency: Varies

RCRA NonGen / NLR: RCRA - Non Generators

RCRAInfo is EPA's comprehensive information system, providing access to data supporting the Resource Conservation and Recovery Act (RCRA) of 1976 and the Hazardous and Solid Waste Amendments (HSWA) of 1984. The database includes selective information on sites which generate, transport, store, treat and/or dispose of hazardous waste as defined by the Resource Conservation and Recovery Act (RCRA). Non-Generators do not presently generate hazardous waste.

Date of Government Version: 07/11/2013 Date Data Arrived at EDR: 08/08/2013 Date Made Active in Reports: 09/13/2013

Number of Days to Update: 36

Source: Environmental Protection Agency

Telephone: (404) 562-8651 Last EDR Contact: 10/02/2013

Next Scheduled EDR Contact: 01/13/2014 Data Release Frequency: Varies

US ENG CONTROLS: Engineering Controls Sites List

A listing of sites with engineering controls in place. Engineering controls include various forms of caps, building foundations, liners, and treatment methods to create pathway elimination for regulated substances to enter environmental media or effect human health.

Date of Government Version: 06/17/2013 Date Data Arrived at EDR: 06/21/2013 Date Made Active in Reports: 10/03/2013 Number of Days to Update: 104

Source: Environmental Protection Agency Telephone: 703-603-0695 Last EDR Contact: 09/10/2013

Next Scheduled EDR Contact: 12/23/2013 Data Release Frequency: Varies

US INST CONTROL: Sites with Institutional Controls

A listing of sites with institutional controls in place. Institutional controls include administrative measures, such as groundwater use restrictions, construction restrictions, property use restrictions, and post remediation care requirements intended to prevent exposure to contaminants remaining on site. Deed restrictions are generally required as part of the institutional controls.

Date of Government Version: 06/17/2013 Date Data Arrived at EDR: 06/21/2013 Date Made Active in Reports: 10/03/2013

Source: Environmental Protection Agency Telephone: 703-603-0695 Last EDR Contact: 09/10/2013

Number of Days to Update: 104

Next Scheduled EDR Contact: 12/23/2013 Data Release Frequency: Varies

ERNS: Emergency Response Notification System

Emergency Response Notification System. ERNS records and stores information on reported releases of oil and hazardous substances.

Date of Government Version: 12/31/2012 Date Data Arrived at EDR: 01/17/2013 Date Made Active in Reports: 02/15/2013 Source: National Response Center, United States Coast Guard

Telephone: 202-267-2180 Last EDR Contact: 10/01/2013

Number of Days to Update: 29

Next Scheduled EDR Contact: 01/13/2014 Data Release Frequency: Annually

HMIRS: Hazardous Materials Information Reporting System

Hazardous Materials Incident Report System. HMIRS contains hazardous material spill incidents reported to DOT.

Date of Government Version: 12/31/2012

Source: U.S. Department of Transportation

Date Data Arrived at EDR: 01/03/2013 Date Made Active in Reports: 02/27/2013

Telephone: 202-366-4555 Last EDR Contact: 10/01/2013

Number of Days to Update: 55

Next Scheduled EDR Contact: 01/13/2014 Data Release Frequency: Annually

DOT OPS: Incident and Accident Data

Department of Transporation, Office of Pipeline Safety Incident and Accident data.

Date of Government Version: 07/31/2012 Date Data Arrived at EDR: 08/07/2012 Date Made Active in Reports: 09/18/2012 Source: Department of Transporation, Office of Pipeline Safety

Number of Days to Update: 42

Last EDR Contact: 08/05/2013

Telephone: 202-366-4595

Next Scheduled EDR Contact: 11/18/2013 Data Release Frequency: Varies

US CDL: Clandestine Drug Labs

A listing of clandestine drug lab locations. The U.S. Department of Justice ("the Department") provides this web site as a public service. It contains addresses of some locations where law enforcement agencies reported they found chemicals or other items that indicated the presence of either clandestine drug laboratories or dumpsites. In most cases, the source of the entries is not the Department, and the Department has not verified the entry and does not guarantee its accuracy. Members of the public must verify the accuracy of all entries by, for example, contacting local law enforcement and local health departments.

Date of Government Version: 08/06/2013 Date Data Arrived at EDR: 09/11/2013 Date Made Active in Reports: 10/03/2013

Number of Days to Update: 22

Source: Drug Enforcement Administration

Telephone: 202-307-1000 Last EDR Contact: 09/04/2013

Next Scheduled EDR Contact: 12/16/2013 Data Release Frequency: Quarterly

US BROWNFIELDS: A Listing of Brownfields Sites

Brownfields are real property, the expansion, redevelopment, or reuse of which may be complicated by the presence or potential presence of a hazardous substance, pollutant, or contaminant. Cleaning up and reinvesting in these properties takes development pressures off of undeveloped, open land, and both improves and protects the environment. Assessment, Cleanup and Redevelopment Exchange System (ACRES) stores information reported by EPA Brownfields grant recipients on brownfields properties assessed or cleaned up with grant funding as well as information on Targeted Brownfields Assessments performed by EPA Regions. A listing of ACRES Brownfield sites is obtained from Cleanups in My Community. Cleanups in My Community provides information on Brownfields properties for which information is reported back to EPA, as well as areas served by Brownfields grant programs.

Date of Government Version: 06/24/2013 Date Data Arrived at EDR: 06/25/2013 Date Made Active in Reports: 08/09/2013

Number of Days to Update: 45

Source: Environmental Protection Agency

Telephone: 202-566-2777 Last EDR Contact: 09/24/2013

Next Scheduled EDR Contact: 01/08/2014 Data Release Frequency: Semi-Annually

DOD: Department of Defense Sites

This data set consists of federally owned or administered lands, administered by the Department of Defense, that have any area equal to or greater than 640 acres of the United States, Puerto Rico, and the U.S. Virgin Islands.

Date of Government Version: 12/31/2005 Date Data Arrived at EDR: 11/10/2006 Date Made Active in Reports: 01/11/2007

Number of Days to Update: 62

Source: USGS Telephone: 888-275-8747 Last EDR Contact: 10/18/2013

Next Scheduled EDR Contact: 01/27/2014 Data Release Frequency: Semi-Annually

FUDS: Formerly Used Defense Sites

The listing includes locations of Formerly Used Defense Sites properties where the US Army Corps of Engineers is actively working or will take necessary cleanup actions.

Date of Government Version: 12/31/2011 Date Data Arrived at EDR: 02/26/2013 Date Made Active in Reports: 03/13/2013

Number of Days to Update: 15

Source: U.S. Army Corps of Engineers

Telephone: 202-528-4285 Last EDR Contact: 09/10/2013

Next Scheduled EDR Contact: 12/23/2013 Data Release Frequency: Varies

LUCIS: Land Use Control Information System

LUCIS contains records of land use control information pertaining to the former Navy Base Realignment and Closure properties.

Date of Government Version: 12/09/2005 Date Data Arrived at EDR: 12/11/2006 Date Made Active in Reports: 01/11/2007

Number of Days to Update: 31

Source: Department of the Navy Telephone: 843-820-7326 Last EDR Contact: 08/15/2013

Next Scheduled EDR Contact: 09/02/2013 Data Release Frequency: Varies

CONSENT: Superfund (CERCLA) Consent Decrees

Major legal settlements that establish responsibility and standards for cleanup at NPL (Superfund) sites. Released periodically by United States District Courts after settlement by parties to litigation matters.

Date of Government Version: 06/30/2013 Date Data Arrived at EDR: 08/07/2013 Date Made Active in Reports: 10/03/2013

Number of Days to Update: 57

Source: Department of Justice, Consent Decree Library

Telephone: Varies

Last EDR Contact: 09/30/2013

Next Scheduled EDR Contact: 01/13/2014 Data Release Frequency: Varies

ROD: Records Of Decision

Record of Decision. ROD documents mandate a permanent remedy at an NPL (Superfund) site containing technical and health information to aid in the cleanup.

Date of Government Version: 12/18/2012 Date Data Arrived at EDR: 03/13/2013 Date Made Active in Reports: 04/12/2013

Number of Days to Update: 30

Source: EPA

Telephone: 703-416-0223 Last EDR Contact: 09/13/2013

Next Scheduled EDR Contact: 12/23/2013 Data Release Frequency: Annually

UMTRA: Uranium Mill Tailings Sites

Uranium ore was mined by private companies for federal government use in national defense programs. When the mills shut down, large piles of the sand-like material (mill tailings) remain after uranium has been extracted from the ore. Levels of human exposure to radioactive materials from the piles are low; however, in some cases tailings were used as construction materials before the potential health hazards of the tailings were recognized.

Date of Government Version: 09/14/2010
Date Data Arrived at EDR: 10/07/2011
Date Made Active in Reports: 03/01/2012

Number of Days to Update: 146

Source: Department of Energy Telephone: 505-845-0011 Last EDR Contact: 05/28/2013

Next Scheduled EDR Contact: 09/09/2013 Data Release Frequency: Varies

DEBRIS REGION 9: Torres Martinez Reservation Illegal Dump Site Locations

A listing of illegal dump sites location on the Torres Martinez Indian Reservation located in eastern Riverside County and northern Imperial County, California.

Date of Government Version: 01/12/2009 Date Data Arrived at EDR: 05/07/2009 Date Made Active in Reports: 09/21/2009

Number of Days to Update: 137

Source: EPA, Region 9 Telephone: 415-947-4219 Last EDR Contact: 07/26/2013

Next Scheduled EDR Contact: 11/11/2013
Data Release Frequency: No Update Planned

ODI: Open Dump Inventory

An open dump is defined as a disposal facility that does not comply with one or more of the Part 257 or Part 258 Subtitle D Criteria.

Date of Government Version: 06/30/1985 Date Data Arrived at EDR: 08/09/2004 Date Made Active in Reports: 09/17/2004

Number of Days to Update: 39

Source: Environmental Protection Agency

Telephone: 800-424-9346 Last EDR Contact: 06/09/2004 Next Scheduled EDR Contact: N/A

Data Release Frequency: No Update Planned

US MINES: Mines Master Index File

Contains all mine identification numbers issued for mines active or opened since 1971. The data also includes violation information.

Date of Government Version: 08/01/2013 Date Data Arrived at EDR: 09/05/2013 Date Made Active in Reports: 10/03/2013

Number of Days to Update: 28

Source: Department of Labor, Mine Safety and Health Administration

Telephone: 303-231-5959 Last EDR Contact: 09/05/2013

Next Scheduled EDR Contact: 12/16/2013 Data Release Frequency: Semi-Annually

TRIS: Toxic Chemical Release Inventory System

Toxic Release Inventory System. TRIS identifies facilities which release toxic chemicals to the air, water and land in reportable quantities under SARA Title III Section 313.

Date of Government Version: 12/31/2011 Date Data Arrived at EDR: 07/31/2013 Date Made Active in Reports: 09/13/2013

Number of Days to Update: 44

Source: EPA

Telephone: 202-566-0250 Last EDR Contact: 08/30/2013

Next Scheduled EDR Contact: 12/09/2013 Data Release Frequency: Annually

TSCA: Toxic Substances Control Act

Toxic Substances Control Act. TSCA identifies manufacturers and importers of chemical substances included on the TSCA Chemical Substance Inventory list. It includes data on the production volume of these substances by plant site.

Date of Government Version: 12/31/2006 Date Data Arrived at EDR: 09/29/2010 Date Made Active in Reports: 12/02/2010

Number of Days to Update: 64

Source: EPA

Telephone: 202-260-5521 Last EDR Contact: 09/24/2013

Next Scheduled EDR Contact: 01/08/2014 Data Release Frequency: Every 4 Years

FTTS: FIFRA/ TSCA Tracking System - FIFRA (Federal Insecticide, Fungicide, & Rodenticide Act)/TSCA (Toxic Substances Control Act) FTTS tracks administrative cases and pesticide enforcement actions and compliance activities related to FIFRA, TSCA and EPCRA (Emergency Planning and Community Right-to-Know Act). To maintain currency, EDR contacts the Agency on a quarterly basis.

Date of Government Version: 04/09/2009 Date Data Arrived at EDR: 04/16/2009 Date Made Active in Reports: 05/11/2009

Number of Days to Update: 25

Source: EPA/Office of Prevention, Pesticides and Toxic Substances

Telephone: 202-566-1667 Last EDR Contact: 08/22/2013

Next Scheduled EDR Contact: 12/09/2013 Data Release Frequency: Quarterly

FTTS INSP: FIFRA/ TSCA Tracking System - FIFRA (Federal Insecticide, Fungicide, & Rodenticide Act)/TSCA (Toxic Substances Control Act)
A listing of FIFRA/TSCA Tracking System (FTTS) inspections and enforcements.

Date of Government Version: 04/09/2009 Date Data Arrived at EDR: 04/16/2009 Date Made Active in Reports: 05/11/2009

Number of Days to Update: 25

Source: EPA

Telephone: 202-566-1667 Last EDR Contact: 08/22/2013

Next Scheduled EDR Contact: 12/09/2013 Data Release Frequency: Quarterly

HIST FTTS: FIFRA/TSCA Tracking System Administrative Case Listing

A complete administrative case listing from the FIFRA/TSCA Tracking System (FTTS) for all ten EPA regions. The information was obtained from the National Compliance Database (NCDB). NCDB supports the implementation of FIFRA (Federal Insecticide, Fungicide, and Rodenticide Act) and TSCA (Toxic Substances Control Act). Some EPA regions are now closing out records. Because of that, and the fact that some EPA regions are not providing EPA Headquarters with updated records, it was decided to create a HIST FTTS database. It included records that may not be included in the newer FTTS database updates. This database is no longer updated.

Date of Government Version: 10/19/2006 Date Data Arrived at EDR: 03/01/2007 Date Made Active in Reports: 04/10/2007

Number of Days to Update: 40

Source: Environmental Protection Agency

Telephone: 202-564-2501 Last EDR Contact: 12/17/2007

Next Scheduled EDR Contact: 03/17/2008 Data Release Frequency: No Update Planned

HIST FTTS INSP: FIFRA/TSCA Tracking System Inspection & Enforcement Case Listing

A complete inspection and enforcement case listing from the FIFRA/TSCA Tracking System (FTTS) for all ten EPA regions. The information was obtained from the National Compliance Database (NCDB). NCDB supports the implementation of FIFRA (Federal Insecticide, Fungicide, and Rodenticide Act) and TSCA (Toxic Substances Control Act). Some EPA regions are now closing out records. Because of that, and the fact that some EPA regions are not providing EPA Headquarters with updated records, it was decided to create a HIST FTTS database. It included records that may not be included in the newer FTTS database updates. This database is no longer updated.

Date of Government Version: 10/19/2006 Date Data Arrived at EDR: 03/01/2007 Date Made Active in Reports: 04/10/2007

Number of Days to Update: 40

Source: Environmental Protection Agency

Telephone: 202-564-2501 Last EDR Contact: 12/17/2008

Next Scheduled EDR Contact: 03/17/2008 Data Release Frequency: No Update Planned

SSTS: Section 7 Tracking Systems

Section 7 of the Federal Insecticide, Fungicide and Rodenticide Act, as amended (92 Stat. 829) requires all registered pesticide-producing establishments to submit a report to the Environmental Protection Agency by March 1st each year. Each establishment must report the types and amounts of pesticides, active ingredients and devices being produced, and those having been produced and sold or distributed in the past year.

Date of Government Version: 12/31/2009 Date Data Arrived at EDR: 12/10/2010 Date Made Active in Reports: 02/25/2011

Number of Days to Update: 77

Source: EPA

Telephone: 202-564-4203 Last EDR Contact: 07/24/2013

Next Scheduled EDR Contact: 11/11/2013 Data Release Frequency: Annually

ICIS: Integrated Compliance Information System

The Integrated Compliance Information System (ICIS) supports the information needs of the national enforcement and compliance program as well as the unique needs of the National Pollutant Discharge Elimination System (NPDES) program

Date of Government Version: 07/20/2011 Date Data Arrived at EDR: 11/10/2011 Date Made Active in Reports: 01/10/2012

Number of Days to Update: 61

Source: Environmental Protection Agency

Telephone: 202-564-5088 Last EDR Contact: 10/09/2014

Next Scheduled EDR Contact: 01/27/2014 Data Release Frequency: Quarterly

PADS: PCB Activity Database System

PCB Activity Database. PADS Identifies generators, transporters, commercial storers and/or brokers and disposers of PCB's who are required to notify the EPA of such activities.

Date of Government Version: 11/01/2012 Date Data Arrived at EDR: 01/16/2013 Date Made Active in Reports: 05/10/2013

Number of Days to Update: 114

Source: EPA

Telephone: 202-566-0500 Last EDR Contact: 10/18/2013

Next Scheduled EDR Contact: 01/27/2014 Data Release Frequency: Annually

MLTS: Material Licensing Tracking System

MLTS is maintained by the Nuclear Regulatory Commission and contains a list of approximately 8,100 sites which possess or use radioactive materials and which are subject to NRC licensing requirements. To maintain currency, EDR contacts the Agency on a quarterly basis.

Date of Government Version: 03/14/2013 Date Data Arrived at EDR: 03/20/2013 Date Made Active in Reports: 07/10/2013

Number of Days to Update: 112

Source: Nuclear Regulatory Commission

Telephone: 301-415-7169 Last EDR Contact: 09/10/2013

Next Scheduled EDR Contact: 12/23/2013 Data Release Frequency: Quarterly

RADINFO: Radiation Information Database

The Radiation Information Database (RADINFO) contains information about facilities that are regulated by U.S. Environmental Protection Agency (EPA) regulations for radiation and radioactivity.

Date of Government Version: 04/09/2013 Date Data Arrived at EDR: 04/11/2013 Date Made Active in Reports: 05/10/2013

Number of Days to Update: 29

Source: Environmental Protection Agency

Telephone: 202-343-9775 Last EDR Contact: 10/09/2013

Next Scheduled EDR Contact: 01/20/2014 Data Release Frequency: Quarterly

FINDS: Facility Index System/Facility Registry System

Facility Index System. FINDS contains both facility information and 'pointers' to other sources that contain more detail. EDR includes the following FINDS databases in this report: PCS (Permit Compliance System), AIRS (Aerometric Information Retrieval System), DOCKET (Enforcement Docket used to manage and track information on civil judicial enforcement cases for all environmental statutes), FURS (Federal Underground Injection Control), C-DOCKET (Criminal Docket System used to track criminal enforcement actions for all environmental statutes), FFIS (Federal Facilities Information System), STATE (State Environmental Laws and Statutes), and PADS (PCB Activity Data System).

Date of Government Version: 03/08/2013 Date Data Arrived at EDR: 03/21/2013 Date Made Active in Reports: 07/10/2013

Number of Days to Update: 111

Source: EPA

Telephone: (404) 562-9900 Last EDR Contact: 09/11/2013

Next Scheduled EDR Contact: 12/23/2013 Data Release Frequency: Quarterly

RAATS: RCRA Administrative Action Tracking System

RCRA Administration Action Tracking System. RAATS contains records based on enforcement actions issued under RCRA pertaining to major violators and includes administrative and civil actions brought by the EPA. For administration actions after September 30, 1995, data entry in the RAATS database was discontinued. EPA will retain a copy of the database for historical records. It was necessary to terminate RAATS because a decrease in agency resources made it impossible to continue to update the information contained in the database.

Date of Government Version: 04/17/1995 Date Data Arrived at EDR: 07/03/1995 Date Made Active in Reports: 08/07/1995

Number of Days to Update: 35

Source: EPA

Telephone: 202-564-4104 Last EDR Contact: 06/02/2008

Next Scheduled EDR Contact: 09/01/2008 Data Release Frequency: No Update Planned

RMP: Risk Management Plans

When Congress passed the Clean Air Act Amendments of 1990, it required EPA to publish regulations and guidance for chemical accident prevention at facilities using extremely hazardous substances. The Risk Management Program Rule (RMP Rule) was written to implement Section 112(r) of these amendments. The rule, which built upon existing industry codes and standards, requires companies of all sizes that use certain flammable and toxic substances to develop a Risk Management Program, which includes a(n): Hazard assessment that details the potential effects of an accidental release, an accident history of the last five years, and an evaluation of worst-case and alternative accidental releases; Prevention program that includes safety precautions and maintenance, monitoring, and employee training measures; and Emergency response program that spells out emergency health care, employee training measures and procedures for informing the public and response agencies (e.g the fire department) should an accident occur.

Date of Government Version: 05/08/2012 Date Data Arrived at EDR: 05/25/2012 Date Made Active in Reports: 07/10/2012

Number of Days to Update: 46

Source: Environmental Protection Agency

Telephone: 202-564-8600 Last EDR Contact: 07/24/2013

Next Scheduled EDR Contact: 11/11/2013 Data Release Frequency: Varies

BRS: Biennial Reporting System

The Biennial Reporting System is a national system administered by the EPA that collects data on the generation and management of hazardous waste. BRS captures detailed data from two groups: Large Quantity Generators (LQG) and Treatment, Storage, and Disposal Facilities.

Date of Government Version: 12/31/2011 Date Data Arrived at EDR: 02/26/2013 Date Made Active in Reports: 04/19/2013

Number of Days to Update: 52

Source: EPA/NTIS Telephone: 800-424-9346 Last EDR Contact: 08/26/2013

Next Scheduled EDR Contact: 12/09/2013 Data Release Frequency: Biennially

COAL ASH EPA: Coal Combustion Residues Surface Impoundments List

A listing of coal combustion residues surface impoundments with high hazard potential ratings.

Date of Government Version: 08/17/2010 Date Data Arrived at EDR: 01/03/2011 Date Made Active in Reports: 03/21/2011

Number of Days to Update: 77

Source: Environmental Protection Agency

Telephone: N/A

Last EDR Contact: 09/13/2013

Next Scheduled EDR Contact: 12/23/2013 Data Release Frequency: Varies

FEDERAL FACILITY: Federal Facility Site Information listing

A listing of National Priority List (NPL) and Base Realignment and Closure (BRAC) sites found in the Comprehensive Environmental Response, Compensation and Liability Information System (CERCLIS) Database where EPA Federal Facilities Restoration and Reuse Office is involved in cleanup activities.

Date of Government Version: 07/31/2012 Date Data Arrived at EDR: 10/09/2012 Date Made Active in Reports: 12/20/2012

Number of Days to Update: 72

Source: Environmental Protection Agency

Telephone: 703-603-8704 Last EDR Contact: 10/11/2013

Next Scheduled EDR Contact: 01/20/2014 Data Release Frequency: Varies

LEAD SMELTER 1: Lead Smelter Sites

A listing of former lead smelter site locations.

Date of Government Version: 01/29/2013 Date Data Arrived at EDR: 02/14/2013 Date Made Active in Reports: 02/27/2013

Number of Days to Update: 13

Source: Environmental Protection Agency

Telephone: 703-603-8787 Last EDR Contact: 09/24/2013

Next Scheduled EDR Contact: 01/20/2014 Data Release Frequency: Varies

LEAD SMELTER 2: Lead Smelter Sites

A list of several hundred sites in the U.S. where secondary lead smelting was done from 1931and 1964. These sites

may pose a threat to public health through ingestion or inhalation of contaminated soil or dust

Date of Government Version: 04/05/2001 Date Data Arrived at EDR: 10/27/2010 Date Made Active in Reports: 12/02/2010

Number of Days to Update: 36

Source: American Journal of Public Health

Telephone: 703-305-6451 Last EDR Contact: 12/02/2009 Next Scheduled EDR Contact: N/A

Data Release Frequency: No Update Planned

FEMA UST: Underground Storage Tank Listing

A listing of all FEMA owned underground storage tanks.

Date of Government Version: 01/01/2010 Date Data Arrived at EDR: 02/16/2010 Date Made Active in Reports: 04/12/2010

Number of Days to Update: 55

Source: FEMA

Telephone: 202-646-5797 Last EDR Contact: 10/17/2013

Next Scheduled EDR Contact: 01/27/2014 Data Release Frequency: Varies

COAL ASH DOE: Sleam-Electric Plan Operation Data

A listing of power plants that store ash in surface ponds.

Date of Government Version: 12/31/2005 Date Data Arrived at EDR: 08/07/2009 Date Made Active in Reports: 10/22/2009

Number of Days to Update: 76

Source: Department of Energy Telephone: 202-586-8719 Last EDR Contact: 10/15/2013

Next Scheduled EDR Contact: 01/27/2014 Data Release Frequency: Varies

PCB TRANSFORMER: PCB Transformer Registration Database

The database of PCB transformer registrations that includes all PCB registration submittals.

Date of Government Version: 02/01/2011 Date Data Arrived at EDR: 10/19/2011 Date Made Active in Reports: 01/10/2012

Number of Days to Update: 83

Source: Environmental Protection Agency

Telephone: 202-566-0517 Last EDR Contact: 08/02/2013

Next Scheduled EDR Contact: 11/11/2013 Data Release Frequency: Varies

US HIST CDL: National Clandestine Laboratory Register

A listing of clandestine drug lab locations. The U.S. Department of Justice ("the Department") provides this web site as a public service. It contains addresses of some locations where law enforcement agencies reported they found chemicals or other items that indicated the presence of either clandestine drug laboratories or dumpsites. In most cases, the source of the entries is not the Department, and the Department has not verified the entry and does not guarantee its accuracy. Members of the public must verify the accuracy of all entries by, for example, contacting local law enforcement and local health departments.

Date of Government Version: 09/01/2007 Date Data Arrived at EDR: 11/19/2008 Date Made Active in Reports: 03/30/2009

Number of Days to Update: 131

Source: Drug Enforcement Administration

Telephone: 202-307-1000 Last EDR Contact: 03/23/2009

Next Scheduled EDR Contact: 06/22/2009 Data Release Frequency: No Update Planned

US FIN ASSUR: Financial Assurance Information

All owners and operators of facilities that treat, store, or dispose of hazardous waste are required to provide proof that they will have sufficient funds to pay for the clean up, closure, and post-closure care of their facilities.

Date of Government Version: 03/04/2013 Date Data Arrived at EDR: 03/15/2013 Date Made Active in Reports: 05/10/2013

Number of Days to Update: 56

Source: Environmental Protection Agency

Telephone: 202-566-1917 Last EDR Contact: 09/27/2013

Next Scheduled EDR Contact: 12/02/2013 Data Release Frequency: Quarterly

EPA WATCH LIST: EPA WATCH LIST

EPA maintains a "Watch List" to facilitate dialogue between EPA, state and local environmental agencies on enforcement matters relating to facilities with alleged violations identified as either significant or high priority. Being on the Watch List does not mean that the facility has actually violated the law only that an investigation by EPA or a state or local environmental agency has led those organizations to allege that an unproven violation has in fact occurred. Being on the Watch List does not represent a higher level of concern regarding the alleged violations that were detected, but instead indicates cases requiring additional dialogue between EPA, state and local agencies - primarily because of the length of time the alleged violation has gone unaddressed or unresolved.

Date of Government Version: 06/30/2013 Date Data Arrived at EDR: 08/13/2013 Date Made Active in Reports: 09/13/2013

Number of Days to Update: 31

Source: Environmental Protection Agency

Telephone: 617-520-3000 Last EDR Contact: 08/07/2013

Next Scheduled EDR Contact: 11/25/2013

Data Release Frequency: Quarterly

US AIRS (AFS): Aerometric Information Retrieval System Facility Subsystem (AFS)

The database is a sub-system of Aerometric Information Retrieval System (AIRS). AFS contains compliance data on air pollution point sources regulated by the U.S. EPA and/or state and local air regulatory agencies. This information comes from source reports by various stationary sources of air pollution, such as electric power plants, steel mills, factories, and universities, and provides information about the air pollutants they produce. Action, air program, air program pollutant, and general level plant data. It is used to track emissions and compliance data from industrial plants.

Date of Government Version: 01/23/2013 Date Data Arrived at EDR: 01/30/2013 Date Made Active in Reports: 05/10/2013

Number of Days to Update: 100

Source: EPA

Telephone: 202-564-5962 Last EDR Contact: 09/30/2013

Next Scheduled EDR Contact: 01/13/2014 Data Release Frequency: Annually

SCRD DRYCLEANERS: State Coalition for Remediation of Drycleaners Listing

The State Coalition for Remediation of Drycleaners was established in 1998, with support from the U.S. EPA Office of Superfund Remediation and Technology Innovation. It is comprised of representatives of states with established drycleaner remediation programs. Currently the member states are Alabama, Connecticut, Florida, Illinois, Kansas, Minnesota, Missouri, North Carolina, Oregon, South Carolina, Tennessee, Texas, and Wisconsin.

Date of Government Version: 03/07/2011 Date Data Arrived at EDR: 03/09/2011 Date Made Active in Reports: 05/02/2011

Number of Days to Update: 54

Source: Environmental Protection Agency

Telephone: 615-532-8599

Last EDR Contact: 08/01/2013

Next Scheduled EDR Contact: 11/04/2013

Data Release Frequency: Varies

2020 COR ACTION: 2020 Corrective Action Program List

The EPA has set ambitious goals for the RCRA Corrective Action program by creating the 2020 Corrective Action Universe. This RCRA cleanup baseline includes facilities expected to need corrective action. The 2020 universe contains a wide variety of sites. Some properties are heavily contaminated while others were contaminated but have since been cleaned up. Still others have not been fully investigated yet, and may require little or no remediation. Inclusion in the 2020 Universe does not necessarily imply failure on the part of a facility to meet its RCRA obligations.

Date of Government Version: 11/11/2011 Date Data Arrived at EDR: 05/18/2012 Date Made Active in Reports: 05/25/2012

Number of Days to Update: 7

Source: Environmental Protection Agency

Telephone: 703-308-4044 Last EDR Contact: 08/16/2013

Next Scheduled EDR Contact: 11/25/2013 Data Release Frequency: Varies

PRP: Potentially Responsible Parties

A listing of verified Potentially Responsible Parties

Date of Government Version: 04/15/2013 Date Data Arrived at EDR: 07/03/2013 Date Made Active in Reports: 09/13/2013

Number of Days to Update: 72

Source: EPA

Telephone: 202-564-6023 Last EDR Contact: 10/04/2013

Next Scheduled EDR Contact: 01/13/2014 Data Release Frequency: Quarterly

US AIRS MINOR: Air Facility System Data A listing of minor source facilities.

Date of Government Version: 01/23/2013
Date Data Arrived at EDR: 01/30/2013
Date Made Active in Reports: 05/10/2013
Number of Days to Lindate: 100

Number of Days to Update: 100

Source: EPA

Telephone: 202-564-5962 Last EDR Contact: 09/30/2013

Next Scheduled EDR Contact: 01/13/2014 Data Release Frequency: Annually

STATE AND LOCAL RECORDS

SHWS: Florida's State-Funded Action Sites

State Hazardous Waste Sites. State hazardous waste site records are the states' equivalent to CERCLIS. These sites may or may not already be listed on the federal CERCLIS list. Priority sites planned for cleanup using state funds (state equivalent of Superfund) are identified along with sites where cleanup will be paid for by potentially responsible parties. Available information varies by state.

Date of Government Version: 07/24/2013 Date Data Arrived at EDR: 08/27/2013 Date Made Active in Reports: 10/02/2013

Number of Days to Update: 36

Source: Department of Environmental Protection

Telephone: 850-488-0190 Last EDR Contact: 08/27/2013

Next Scheduled EDR Contact: 12/09/2013 Data Release Frequency: Semi-Annually

SWF/LF: Solid Waste Facility Database

Solid Waste Facilities/Landfill Sites. SWF/LF type records typically contain an inventory of solid waste disposal facilities or landfills in a particular state. Depending on the state, these may be active or inactive facilities or open dumps that failed to meet RCRA Subtitle D Section 4004 criteria for solid waste landfills or disposal sites.

Date of Government Version: 07/22/2013 Date Data Arrived at EDR: 07/22/2013 Date Made Active in Reports: 08/12/2013

Number of Days to Update: 21

Source: Department of Environmental Protection

Telephone: 850-922-7121 Last EDR Contact: 07/22/2013

Next Scheduled EDR Contact: 11/04/2013 Data Release Frequency: Semi-Annually

UIC: Underground Injection Wells Database Listing

A listing of Class I wells. Class I wells are used to inject hazardous waste, nonhazardous waste, or municipal waste below the lowermost USDW.

Date of Government Version: 07/29/2013 Date Data Arrived at EDR: 07/30/2013 Date Made Active in Reports: 08/22/2013

Number of Days to Update: 23

Source: Department of Environmental Protection

Telephone: 850-245-8655 Last EDR Contact: 07/26/2013

Next Scheduled EDR Contact: 11/11/2013

Data Release Frequency: Varies

SWRCY: Recycling Centers

A listing of recycling centers located in the state of Florida.

Date of Government Version: 12/31/2011 Date Data Arrived at EDR: 11/13/2012 Date Made Active in Reports: 12/05/2012

Number of Days to Update: 22

Source: Department of Environmental Protection

Telephone: 850-245-8718 Last EDR Contact: 07/26/2013

Next Scheduled EDR Contact: 11/04/2013 Data Release Frequency: Varies

LUST: Petroleum Contamination Detail Report

Leaking Underground Storage Tank Incident Reports. LUST records contain an inventory of reported leaking underground storage tank incidents. Not all states maintain these records, and the information stored varies by state.

Date of Government Version: 07/15/2013 Date Data Arrived at EDR: 08/05/2013 Date Made Active in Reports: 08/08/2013

Number of Days to Update: 3

Source: Department of Environmental Protection

Telephone: 850-245-8839 Last EDR Contact: 08/05/2013

Next Scheduled EDR Contact: 11/18/2013 Data Release Frequency: Quarterly

UST: Storage Tank Facility Information

Registered Underground Storage Tanks. UST's are regulated under Subtitle I of the Resource Conservation and Recovery Act (RCRA) and must be registered with the state department responsible for administering the UST program. Available information varies by state program.

Date of Government Version: 07/15/2013 Date Data Arrived at EDR: 08/05/2013 Date Made Active in Reports: 10/03/2013

Number of Days to Update: 59

Source: Department of Environmental Protection

Telephone: 850-245-8839 Last EDR Contact: 08/05/2013

Next Scheduled EDR Contact: 11/18/2013 Data Release Frequency: Quarterly

LAST: Leaking Aboveground Storage Tank Listing

A statewide listing of leaking aboveground storage tank site locations.

Date of Government Version: 09/05/2013 Date Data Arrived at EDR: 09/05/2013 Date Made Active in Reports: 10/02/2013

Number of Days to Update: 27

Source: Department of Environmental Protection

Telephone: 850-245-8799 Last EDR Contact: 08/15/2013

Next Scheduled EDR Contact: 11/18/2013 Data Release Frequency: Varies

AST: Storage Tank Facility Information Registered Aboveground Storage Tanks.

Date of Government Version: 07/15/2013 Date Data Arrived at EDR: 08/05/2013 Date Made Active in Reports: 10/03/2013

Number of Days to Update: 59

Source: Department of Environmental Protection

Telephone: 850-245-8839 Last EDR Contact: 08/05/2013

Next Scheduled EDR Contact: 11/18/2013 Data Release Frequency: Quarterly

FL SITES: Sites List

This summary status report was developed from a number of lists including the Eckhardt list, the Moffit list, the EPA Hazardous Waste Sites list, EPA's Emergency & Remedial Response information System list (RCRA Section 3012) & existing department lists such as the obsolete uncontrolled Hazardous Waste Sites list. This list is no longer updated.

Date of Government Version: 12/31/1989 Date Data Arrived at EDR: 05/09/1994 Date Made Active in Reports: 08/04/1994

Number of Days to Update: 87

Source: Department of Environmental Protection

Telephone: 850-245-8705 Last EDR Contact: 03/24/1994 Next Scheduled EDR Contact: N/A

Data Release Frequency: No Update Planned

SPILLS: Oil and Hazardous Materials Incidents

Statewide oil and hazardous materials inland incidents.

Date of Government Version: 07/17/2013 Date Data Arrived at EDR: 07/18/2013 Date Made Active in Reports: 08/12/2013

Number of Days to Update: 25

Source: Department of Environmental Protection

Telephone: 850-245-2010 Last EDR Contact: 10/09/2013

Next Scheduled EDR Contact: 01/27/2014 Data Release Frequency: Semi-Annually

ENG CONTROLS: Institutional Controls Registry

The registry is a database of all contaminated sites in the state of Florida which are subject to engineering controls. Engineering Controls encompass a variety of engineered remedies to contain and/or reduce contamination, and/or physical barriers intended to limit access to property. ECs include fences, signs, guards, landfill caps, provision of potable water, slurry walls, sheet pile (vertical caps), pumping and treatment of groundwater, monitoring wells, and vapor extraction systems.

Date of Government Version: 07/01/2013 Date Data Arrived at EDR: 07/08/2013 Date Made Active in Reports: 08/09/2013

Number of Days to Update: 32

Source: Department of Environmental Protection

Telephone: 850-245-8927 Last EDR Contact: 10/08/2013

Next Scheduled EDR Contact: 01/20/2014 Data Release Frequency: Semi-Annually

Inst Control: Institutional Controls Registry

The registry is a database of all contaminated sites in the state of Florida which are subject to institutional and engineering controls.

Date of Government Version: 07/01/2013 Date Data Arrived at EDR: 07/08/2013 Date Made Active in Reports: 08/09/2013

Number of Days to Update: 32

Source: Department of Environmental Protection

Telephone: 850-245-8927 Last EDR Contact: 10/08/2013

Next Scheduled EDR Contact: 01/20/2014 Data Release Frequency: Semi-Annually

VCP: Voluntary Cleanup Sites

Listing of closed and active voluntary cleanup sites.

Date of Government Version: 06/27/2013 Date Data Arrived at EDR: 07/08/2013 Date Made Active in Reports: 08/09/2013

Number of Days to Update: 32

Source: Department of Environmental Protection

Telephone: 850-245-8705 Last EDR Contact: 10/10/2013

Next Scheduled EDR Contact: 12/09/2013

Data Release Frequency: Varies

PRIORITYCLEANERS: Priority Ranking List

The Florida Legislature has established a state-funded program to cleanup properties that are contaminated as a result of the operations of a drycleaning facility.

Date of Government Version: 07/01/2013 Date Data Arrived at EDR: 08/19/2013 Date Made Active in Reports: 10/02/2013

Number of Days to Update: 44

Source: Department of Environmental Protection

Telephone: 850-245-8927 Last EDR Contact: 08/19/2013

Next Scheduled EDR Contact: 12/02/2013 Data Release Frequency: Varies

DRYCLEANERS: Drycleaning Facilities

The Drycleaners database, maintained by the Department of Environmental Protection, provides information about permitted dry cleaner facilities.

Date of Government Version: 07/15/2013 Date Data Arrived at EDR: 07/30/2013 Date Made Active in Reports: 08/09/2013

Number of Days to Update: 10

Source: Department of Environmental Protection

Telephone: 850-245-8927 Last EDR Contact: 07/30/2013

Next Scheduled EDR Contact: 11/11/2013 Data Release Frequency: Semi-Annually

DEDB: Ethylene Dibromide Database Results

Ethylene dibromide (EDB), a soil fumigant, that has been detected in drinking water wells. The amount found exceeds the maximum contaminant level as stated in Chapter 62-550 or 520. It is a potential threat to public health when present in drinking water.

Date of Government Version: 07/15/2013 Date Data Arrived at EDR: 07/16/2013 Date Made Active in Reports: 08/09/2013

Number of Days to Update: 24

Source: Department of Environmental Protection

Telephone: 850-245-8335 Last EDR Contact: 09/23/2013

Next Scheduled EDR Contact: 01/08/2014

Data Release Frequency: Varies

BROWNFIELDS: Brownfield Areas

Brownfields are abandoned, idled, or underused industrial and commercial facilities where expansion or redevelopment is complicated by real or perceived environmental contamination. Florida's Brownfields Redevelopment Acti primary goals are to reduce health and environmental hazards on existing commercial and industrial sites that are abandoned or underused due to these hazards and create financial and regulatory incentives to encourage voluntary cleanup and redevelopment of sites.

Date of Government Version: 07/08/2013 Date Data Arrived at EDR: 07/08/2013 Date Made Active in Reports: 08/07/2013

Number of Days to Update: 30

Source: Department of Environmental Protection

Telephone: 850-245-8927 Last EDR Contact: 10/08/2013

Next Scheduled EDR Contact: 01/20/2014 Data Release Frequency: Semi-Annually

WASTEWATER: Wastewater Facility Regulation Database

Domestic and industrial wastewater facilities.

Date of Government Version: 08/02/2013 Date Data Arrived at EDR: 08/14/2013 Date Made Active in Reports: 10/01/2013

Number of Days to Update: 48

Source: Department of Environmental Protection

Telephone: 850-245-8600 Last EDR Contact: 08/14/2013

Next Scheduled EDR Contact: 11/25/2013 Data Release Frequency: Quarterly

AIRS: Permitted Facilities Listing

A listing of Air Resources Management permits.

Date of Government Version: 07/31/2013 Date Data Arrived at EDR: 08/01/2013 Date Made Active in Reports: 08/09/2013

Number of Days to Update: 8

Source: Department of Environmental Protection

Telephone: 850-921-9558 Last EDR Contact: 07/31/2013

Next Scheduled EDR Contact: 11/18/2013

Data Release Frequency: Varies

TIER 2: Tier 2 Facility Listing

A listing of facilities which store or manufacture hazardous materials that submit a chemical inventory report.

Date of Government Version: 12/31/2011 Date Data Arrived at EDR: 04/03/2013 Date Made Active in Reports: 04/23/2013

Number of Days to Update: 20

Source: Department of Environmental Protection

Telephone: 850-413-9970 Last EDR Contact: 09/16/2013

Next Scheduled EDR Contact: 12/30/2013 Data Release Frequency: Varies

FL Cattle Dip. Vats: Cattle Dipping Vats

From the 1910's through the 1950's, these vats were filled with an arsenic solution for the control and eradication of the cattle fever tick. Other pesticides, such as DDT, were also widely used. By State law, all cattle, horses, mules, goats, and other susceptible animals were required to be dipped every 14 days. Under certain circumstances, the arsenic and other pesticides remaining at the site may present an environmental or public health hazard.

Date of Government Version: 02/04/2005 Date Data Arrived at EDR: 06/29/2007 Date Made Active in Reports: 07/11/2007

Number of Days to Update: 12

Source: Department of Environmental Protection

Telephone: 850-488-3601 Last EDR Contact: 10/09/2013

Next Scheduled EDR Contact: 01/27/2014 Data Release Frequency: No Update Planned

FF TANKS: Federal Facilities Listing

A listing of federal facilities with storage tanks.

Date of Government Version: 06/26/2013 Date Data Arrived at EDR: 07/01/2013 Date Made Active in Reports: 08/07/2013

Number of Days to Update: 37

Source: Department of Environmental Protection

Telephone: 850-245-8250 Last EDR Contact: 10/09/2013

Next Scheduled EDR Contact: 01/27/2014 Data Release Frequency: Quarterly

TRIBAL RECORDS

INDIAN RESERV: Indian Reservations

This map layer portrays Indian administered lands of the United States that have any area equal to or greater

than 640 acres.

Date of Government Version: 12/31/2005 Date Data Arrived at EDR: 12/08/2006 Date Made Active in Reports: 01/11/2007

Number of Days to Update: 34

Source: USGS

Telephone: 202-208-3710 Last EDR Contact: 10/18/2013

Next Scheduled EDR Contact: 01/27/2014 Data Release Frequency: Semi-Annually

INDIAN ODI: Report on the Status of Open Dumps on Indian Lands

Location of open dumps on Indian land.

Date of Government Version: 12/31/1998 Date Data Arrived at EDR: 12/03/2007 Date Made Active in Reports: 01/24/2008

Number of Days to Update: 52

Source: Environmental Protection Agency

Telephone: 703-308-8245 Last EDR Contact: 07/31/2013

Next Scheduled EDR Contact: 11/18/2013

Data Release Frequency: Varies

INDIAN LUST R8: Leaking Underground Storage Tanks on Indian Land

LUSTs on Indian land in Colorado, Montana, North Dakota, South Dakota, Utah and Wyoming.

Date of Government Version: 08/27/2012 Date Data Arrived at EDR: 08/28/2012 Date Made Active in Reports: 10/16/2012

Number of Days to Update: 49

Source: EPA Region 8 Telephone: 303-312-6271 Last EDR Contact: 07/24/2013

Next Scheduled EDR Contact: 11/11/2013 Data Release Frequency: Quarterly

INDIAN LUST R7: Leaking Underground Storage Tanks on Indian Land

LUSTs on Indian land in Iowa, Kansas, and Nebraska

Date of Government Version: 12/31/2012 Date Data Arrived at EDR: 02/28/2013 Date Made Active in Reports: 04/12/2013

Number of Days to Update: 43

Source: EPA Region 7 Telephone: 913-551-7003 Last EDR Contact: 07/24/2013

Next Scheduled EDR Contact: 11/11/2013 Data Release Frequency: Varies

INDIAN LUST R4: Leaking Underground Storage Tanks on Indian Land LUSTs on Indian land in Florida, Mississippi and North Carolina.

Date of Government Version: 02/06/2013 Date Data Arrived at EDR: 02/08/2013 Date Made Active in Reports: 04/12/2013

Number of Days to Update: 63

Source: EPA Region 4 Telephone: 404-562-8677 Last EDR Contact: 07/24/2013

Next Scheduled EDR Contact: 11/11/2013 Data Release Frequency: Semi-Annually

INDIAN LUST R1: Leaking Underground Storage Tanks on Indian Land A listing of leaking underground storage tank locations on Indian Land.

Date of Government Version: 09/28/2012 Date Data Arrived at EDR: 11/01/2012 Date Made Active in Reports: 04/12/2013

Number of Days to Update: 162

Source: EPA Region 1 Telephone: 617-918-1313 Last EDR Contact: 08/02/2013

Next Scheduled EDR Contact: 11/11/2013 Data Release Frequency: Varies

INDIAN LUST R9: Leaking Underground Storage Tanks on Indian Land LUSTs on Indian land in Arizona, California, New Mexico and Nevada

Date of Government Version: 03/01/2013 Date Data Arrived at EDR: 03/01/2013 Date Made Active in Reports: 04/12/2013

Number of Days to Update: 42

Source: Environmental Protection Agency

Telephone: 415-972-3372 Last EDR Contact: 07/24/2013

Next Scheduled EDR Contact: 11/11/2013 Data Release Frequency: Quarterly

INDIAN LUST R10: Leaking Underground Storage Tanks on Indian Land LUSTs on Indian land in Alaska, Idaho, Oregon and Washington.

Date of Government Version: 02/05/2013 Date Data Arrived at EDR: 02/06/2013 Date Made Active in Reports: 04/12/2013

Number of Days to Update: 65

Source: EPA Region 10 Telephone: 206-553-2857 Last EDR Contact: 07/24/2013

Next Scheduled EDR Contact: 11/11/2013 Data Release Frequency: Quarterly

INDIAN LUST R6: Leaking Underground Storage Tanks on Indian Land

LUSTs on Indian land in New Mexico and Oklahoma.

Date of Government Version: 09/12/2011 Date Data Arrived at EDR: 09/13/2011 Date Made Active in Reports: 11/11/2011

Number of Days to Update: 59

Source: EPA Region 6 Telephone: 214-665-6597 Last EDR Contact: 07/24/2013

Next Scheduled EDR Contact: 11/11/2013 Data Release Frequency: Varies

INDIAN UST R1: Underground Storage Tanks on Indian Land

The Indian Underground Storage Tank (UST) database provides information about underground storage tanks on Indian land in EPA Region 1 (Connecticut, Maine, Massachusetts, New Hampshire, Rhode Island, Vermont and ten Tribal Nations).

Date of Government Version: 09/28/2012 Date Data Arrived at EDR: 11/07/2012 Date Made Active in Reports: 04/12/2013

Number of Days to Update: 156

Source: EPA, Region 1 Telephone: 617-918-1313 Last EDR Contact: 08/02/2013

Next Scheduled EDR Contact: 11/11/2013 Data Release Frequency: Varies

INDIAN UST R4: Underground Storage Tanks on Indian Land

The Indian Underground Storage Tank (UST) database provides information about underground storage tanks on Indian land in EPA Region 4 (Alabama, Florida, Georgia, Kentucky, Mississippi, North Carolina, South Carolina, Tennessee and Tribal Nations)

Date of Government Version: 02/06/2013 Date Data Arrived at EDR: 02/08/2013 Date Made Active in Reports: 04/12/2013

Number of Days to Update: 63

Source: EPA Region 4 Telephone: 404-562-9424 Last EDR Contact: 07/24/2013

Next Scheduled EDR Contact: 11/11/2013 Data Release Frequency: Semi-Annually

INDIAN UST R5: Underground Storage Tanks on Indian Land

The Indian Underground Storage Tank (UST) database provides information about underground storage tanks on Indian land in EPA Region 5 (Michigan, Minnesota and Wisconsin and Tribal Nations).

Date of Government Version: 08/02/2012 Date Data Arrived at EDR: 08/03/2012 Date Made Active in Reports: 11/05/2012

Number of Days to Update: 94

Source: EPA Region 5 Telephone: 312-886-6136 Last EDR Contact: 07/24/2013

Next Scheduled EDR Contact: 11/11/2013 Data Release Frequency: Varies

INDIAN UST R6: Underground Storage Tanks on Indian Land

The Indian Underground Storage Tank (UST) database provides information about underground storage tanks on Indian land in EPA Region 6 (Louisiana, Arkansas, Oklahoma, New Mexico, Texas and 65 Tribes).

Date of Government Version: 05/10/2011 Date Data Arrived at EDR: 05/11/2011 Date Made Active in Reports: 06/14/2011

Number of Days to Update: 34

Source: EPA Region 6 Telephone: 214-665-7591 Last EDR Contact: 07/24/2013

Next Scheduled EDR Contact: 11/11/2013 Data Release Frequency: Semi-Annually

INDIAN UST R7: Underground Storage Tanks on Indian Land

The Indian Underground Storage Tank (UST) database provides information about underground storage tanks on Indian land in EPA Region 7 (Iowa, Kansas, Missouri, Nebraska, and 9 Tribal Nations).

Date of Government Version: 12/31/2012 Date Data Arrived at EDR: 02/28/2013 Date Made Active in Reports: 04/12/2013

Number of Days to Update: 43

Source: EPA Region 7 Telephone: 913-551-7003 Last EDR Contact: 07/24/2013

Next Scheduled EDR Contact: 11/11/2013 Data Release Frequency: Varies

INDIAN UST R8: Underground Storage Tanks on Indian Land

The Indian Underground Storage Tank (UST) database provides information about underground storage tanks on Indian land in EPA Region 8 (Colorado, Montana, North Dakota, South Dakota, Utah, Wyoming and 27 Tribal Nations).

Date of Government Version: 08/27/2012 Date Data Arrived at EDR: 08/28/2012 Date Made Active in Reports: 10/16/2012

Number of Days to Update: 49

Source: EPA Region 8 Telephone: 303-312-6137 Last EDR Contact: 07/24/2013

Next Scheduled EDR Contact: 11/11/2013 Data Release Frequency: Quarterly

INDIAN UST R9: Underground Storage Tanks on Indian Land

The Indian Underground Storage Tank (UST) database provides information about underground storage tanks on Indian land in EPA Region 9 (Arizona, California, Hawaii, Nevada, the Pacific Islands, and Tribal Nations).

Date of Government Version: 02/21/2013 Date Data Arrived at EDR: 02/26/2013 Date Made Active in Reports: 04/12/2013

Number of Days to Update: 45

Source: EPA Region 9 Telephone: 415-972-3368 Last EDR Contact: 07/24/2013

Next Scheduled EDR Contact: 11/11/2013
Data Release Frequency: Quarterly

INDIAN UST R10: Underground Storage Tanks on Indian Land

The Indian Underground Storage Tank (UST) database provides information about underground storage tanks on Indian land in EPA Region 10 (Alaska, Idaho, Oregon, Washington, and Tribal Nations).

Date of Government Version: 02/05/2013 Date Data Arrived at EDR: 02/06/2013 Date Made Active in Reports: 04/12/2013

Number of Days to Update: 65

Source: EPA Region 10 Telephone: 206-553-2857 Last EDR Contact: 07/24/2013

Next Scheduled EDR Contact: 11/11/2013 Data Release Frequency: Quarterly

INDIAN VCP R1: Voluntary Cleanup Priority Listing

A listing of voluntary cleanup priority sites located on Indian Land located in Region 1.

Date of Government Version: 09/28/2012 Date Data Arrived at EDR: 10/02/2012 Date Made Active in Reports: 10/16/2012

Number of Days to Update: 14

Source: EPA, Region 1 Telephone: 617-918-1102 Last EDR Contact: 10/01/2013

Next Scheduled EDR Contact: 01/13/2014 Data Release Frequency: Varies

INDIAN VCP R7: Voluntary Cleanup Priority Lisitng

A listing of voluntary cleanup priority sites located on Indian Land located in Region 7.

Date of Government Version: 03/20/2008 Date Data Arrived at EDR: 04/22/2008 Date Made Active in Reports: 05/19/2008 Source: EPA, Region 7 Telephone: 913-551-7365 Last EDR Contact: 04/20/2009

Number of Days to Update: 27

Next Scheduled EDR Contact: 07/20/2009

Data Release Frequency: Varies

EDR PROPRIETARY RECORDS

EDR MGP: EDR Proprietary Manufactured Gas Plants

The EDR Proprietary Manufactured Gas Plant Database includes records of coal gas plants (manufactured gas plants) compiled by EDR's researchers. Manufactured gas sites were used in the United States from the 1800's to 1950's to produce a gas that could be distributed and used as fuel. These plants used whale oil, rosin, coal, or a mixture of coal, oil, and water that also produced a significant amount of waste. Many of the byproducts of the gas production, such as coal tar (oily waste containing volatile and non-volatile chemicals), sludges, oils and other compounds are potentially hazardous to human health and the environment. The byproduct from this process was frequently disposed of directly at the plant site and can remain or spread slowly, serving as a continuous source of soil and groundwater contamination.

Date of Government Version: N/A Source: EDR, Inc. Date Data Arrived at EDR: N/A Telephone: N/A Date Made Active in Reports: N/A Last EDR Contact: N/A

Number of Days to Update: N/A Next Scheduled EDR Contact: N/A

Data Release Frequency: No Update Planned

EDR US Hist Auto Stat: EDR Exclusive Historic Gas Stations

EDR has searched selected national collections of business directories and has collected listings of potential gas station/filling station/service station sites that were available to EDR researchers. EDR's review was limited to those categories of sources that might, in EDR's opinion, include gas station/filling station/service station establishments. The categories reviewed included, but were not limited to gas, gas station, gasoline station, filling station, auto, automobile repair, auto service station, service station, etc. This database falls within a category of information EDR classifies as "High Risk Historical Records", or HRHR. EDR's HRHR effort presents unique and sometimes proprietary data about past sites and operations that typically create environmental concerns, but may not show up in current government records searches.

Date of Government Version: N/A Source: EDR, Inc. Date Data Arrived at EDR: N/A Telephone: N/A Date Made Active in Reports: N/A Last EDR Contact: N/A

Number of Days to Update: N/A Next Scheduled EDR Contact: N/A Data Release Frequency: Varies

EDR US Hist Cleaners: EDR Exclusive Historic Dry Cleaners

EDR has searched selected national collections of business directories and has collected listings of potential dry cleaner sites that were available to EDR researchers. EDR's review was limited to those categories of sources that might, in EDR's opinion, include dry cleaning establishments. The categories reviewed included, but were not limited to dry cleaners, cleaners, laundry, laundromat, cleaning/laundry, wash & dry etc. This database falls within a category of information EDR classifies as "High Risk Historical Records", or HRHR. EDR's HRHR effort presents unique and sometimes proprietary data about past sites and operations that typically create environmental concerns, but may not show up in current government records searches.

Date of Government Version: N/A Source: EDR, Inc. Date Data Arrived at EDR: N/A Telephone: N/A Last EDR Contact: N/A Date Made Active in Reports: N/A

Number of Days to Update: N/A Next Scheduled EDR Contact: N/A Data Release Frequency: Varies

EDR US Hist Cleaners: EDR Proprietary Historic Dry Cleaners - Cole

Date of Government Version: N/A

Date Data Arrived at EDR: N/A

Date Made Active in Reports: N/A

Last EDR Contact: N/A

Number of Days to Update: N/A

Next Scheduled EDR Contact: N/A

Data Release Frequency: Varies

EDR US Hist Auto Stat: EDR Proprietary Historic Gas Stations - Cole

Date of Government Version: N/A

Date Data Arrived at EDR: N/A

Date Made Active in Reports: N/A

Last EDR Contact: N/A

Number of Days to Update: N/A Next Scheduled EDR Contact: N/A Data Release Frequency: Varies

COUNTY RECORDS

ALACHUA COUNTY:

Facility List

List of all regulated facilities in Alachua County.

Date of Government Version: 04/01/2013 Date Data Arrived at EDR: 04/03/2013 Date Made Active in Reports: 04/23/2013

Number of Days to Update: 20

Source: Alachua County Environmental Protection Department

Telephone: 352-264-6800 Last EDR Contact: 09/30/2013

Next Scheduled EDR Contact: 01/13/2014 Data Release Frequency: Annually

BROWARD COUNTY:

Aboveground Storage Tanks

Aboveground storage tank locations in Broward County.

Date of Government Version: 06/05/2013 Date Data Arrived at EDR: 06/12/2013 Date Made Active in Reports: 08/06/2013

Number of Days to Update: 55

Source: Broward County Environmental Protection Department

Telephone: 954-818-7509 Last EDR Contact: 09/06/2013

Next Scheduled EDR Contact: 12/16/2013 Data Release Frequency: Varies

Underground Storage Tanks

All known regulated storage tanks within Broward County, including those tanks that have been closed

Date of Government Version: 06/05/2013 Date Data Arrived at EDR: 06/12/2013 Date Made Active in Reports: 08/06/2013

Number of Days to Update: 55

Source: Broward County Environmental Protection Department

Telephone: 954-818-7509 Last EDR Contact: 06/12/2013

Next Scheduled EDR Contact: 12/16/2013 Data Release Frequency: Annually

HILLSBOROUGH COUNTY:

HILLSBOROUGH CO LF

Hillsborough county landfill sites.

Date of Government Version: 06/01/2010 Date Data Arrived at EDR: 01/18/2012 Date Made Active in Reports: 02/21/2012

Number of Days to Update: 34

Source: Hillsborough County Environmental Protection Commission

Telephone: 813-627-2600 Last EDR Contact: 10/09/2013

Next Scheduled EDR Contact: 01/27/2014 Data Release Frequency: Varies

MIAMI-DADE COUNTY:

Air Permit Sites

Facilities that release or have a potential to release pollutants.

Date of Government Version: 09/04/2013 Date Data Arrived at EDR: 09/04/2013 Date Made Active in Reports: 10/02/2013

Number of Days to Update: 28

Source: Department of Environmental Resources Management

Telephone: 305-372-6755 Last EDR Contact: 09/04/2013

Next Scheduled EDR Contact: 12/16/2013 Data Release Frequency: Semi-Annually

Marine Facilities Operating Permit

What is this permit used for? Miami-Dade County Ordinance 89-104 and Section 24-18 of the Code of Miami-Dade County require the following types of marine facilities to obtain annual operating permits from DERM: All recreational boat docking facilities with ten (10) or more boat slips, moorings, davit spaces, and vessel tie-up spaces.

All boat storage facilities contiguous to tidal waters in Miami-Dade County with ten (10) or more dry storage spaces including boatyards and boat manufacturing facilities.

Date of Government Version: 09/04/2013 Date Data Arrived at EDR: 09/04/2013 Date Made Active in Reports: 10/02/2013

Number of Days to Update: 28

Source: DERM

Telephone: 305-372-3576 Last EDR Contact: 09/04/2013

Next Scheduled EDR Contact: 12/16/2013 Data Release Frequency: Quarterly

Maimi River Enforcement

The Miami River Enforcement database files were created for facilities and in some instances vessels that were inspected by a workgroup within the Department that was identified as the Miami River Enforcement Group. The files do not all necessarily reflect enforcement cases and some were created for locations that were permitted by other Sections within the Department.

Date of Government Version: 06/05/2013 Date Data Arrived at EDR: 06/06/2013 Date Made Active in Reports: 08/06/2013

Number of Days to Update: 61

Source: DERM

Telephone: 305-372-3576 Last EDR Contact: 09/03/2013

Next Scheduled EDR Contact: 12/16/2013 Data Release Frequency: Quarterly

Industrial Waste Permit Sites

Facilities that either generate more than 25,000 of wastewater per day to sanitary sewers or are pre-defined by EPA.

Date of Government Version: 09/04/2013 Date Data Arrived at EDR: 09/04/2013 Date Made Active in Reports: 10/02/2013

Number of Days to Update: 28

Source: Department of Environmental Resources Management

Telephone: 305-372-6700 Last EDR Contact: 09/04/2013

Next Scheduled EDR Contact: 12/16/2013 Data Release Frequency: Semi-Annually

Enforcement Case Tracking System Sites

Enforcement cases monitored by the Dade County Department of Environmental Resources Management.

Date of Government Version: 09/04/2013 Date Data Arrived at EDR: 09/04/2013 Date Made Active in Reports: 10/02/2013

Number of Days to Update: 28

Source: Department of Environmental Resources Management

Telephone: 305-372-6755 Last EDR Contact: 09/04/2013

Next Scheduled EDR Contact: 12/16/2013 Data Release Frequency: Semi-Annually

Fuel Spills Cases

DERM documents fuel spills of sites that are not in a state program.

Date of Government Version: 01/08/2009 Date Data Arrived at EDR: 01/13/2009 Date Made Active in Reports: 02/05/2009

Number of Days to Update: 23

Source: Department of Environmental Resources Management

Telephone: 305-372-6755 Last EDR Contact: 09/03/2013

Next Scheduled EDR Contact: 12/16/2013 Data Release Frequency: Semi-Annually

Storage Tanks

A listing of aboveground and underground storage tank site locations.

Date of Government Version: 09/04/2013 Date Data Arrived at EDR: 09/04/2013 Date Made Active in Reports: 10/02/2013

Number of Days to Update: 28

Source: Department of Environmental Resource Management

Telephone: 305-372-6700 Last EDR Contact: 09/04/2013

Next Scheduled EDR Contact: 12/16/2013 Data Release Frequency: Semi-Annually

PALM BEACH COUNTY:

PALM BEACH CO. LF

Palm Beach County Inventory of Solid Waste Sites.

Date of Government Version: 09/01/2011 Date Data Arrived at EDR: 09/20/2011 Date Made Active in Reports: 10/10/2011

Number of Days to Update: 20

Source: Palm Beach County Solid Waste Authority

Telephone: 561-640-4000 Last EDR Contact: 09/16/2013

Next Scheduled EDR Contact: 12/30/2013

Data Release Frequency: Varies

OTHER DATABASE(S)

Depending on the geographic area covered by this report, the data provided in these specialty databases may or may not be complete. For example, the existence of wetlands information data in a specific report does not mean that all wetlands in the area covered by the report are included. Moreover, the absence of any reported wetlands information does not necessarily mean that wetlands do not exist in the area covered by the report.

CT MANIFEST: Hazardous Waste Manifest Data

Facility and manifest data. Manifest is a document that lists and tracks hazardous waste from the generator through transporters to a tsd facility.

Date of Government Version: 07/30/2013 Date Data Arrived at EDR: 08/19/2013 Date Made Active in Reports: 10/03/2013

Number of Days to Update: 45

Source: Department of Energy & Environmental Protection

Telephone: 860-424-3375 Last EDR Contact: 08/19/2013

Next Scheduled EDR Contact: 12/02/2013 Data Release Frequency: Annually

NJ MANIFEST: Manifest Information

Hazardous waste manifest information.

Date of Government Version: 12/31/2011 Date Data Arrived at EDR: 07/19/2012 Date Made Active in Reports: 08/28/2012

Number of Days to Update: 40

Source: Department of Environmental Protection

Telephone: N/A

Last EDR Contact: 10/18/2013

Next Scheduled EDR Contact: 01/27/2014 Data Release Frequency: Annually

NY MANIFEST: Facility and Manifest Data

Manifest is a document that lists and tracks hazardous waste from the generator through transporters to a TSD facility.

Date of Government Version: 08/01/2013 Date Data Arrived at EDR: 08/07/2013 Date Made Active in Reports: 09/10/2013

Number of Days to Update: 34

Source: Department of Environmental Conservation

Telephone: 518-402-8651 Last EDR Contact: 08/07/2013

Next Scheduled EDR Contact: 11/18/2013 Data Release Frequency: Annually

GOVERNMENT RECORDS SEARCHED / DATA CURRENCY TRACKING

PA MANIFEST: Manifest Information

Hazardous waste manifest information.

Date of Government Version: 12/31/2012 Date Data Arrived at EDR: 07/24/2013 Date Made Active in Reports: 08/19/2013

Number of Days to Update: 26

Source: Department of Environmental Protection

Telephone: 717-783-8990 Last EDR Contact: 07/18/2013

Next Scheduled EDR Contact: 11/04/2013 Data Release Frequency: Annually

RI MANIFEST: Manifest information

Hazardous waste manifest information

Date of Government Version: 12/31/2012 Date Data Arrived at EDR: 06/21/2013 Date Made Active in Reports: 08/05/2013

Number of Days to Update: 45

Source: Department of Environmental Management

Telephone: 401-222-2797 Last EDR Contact: 08/23/2013

Next Scheduled EDR Contact: 12/09/2013 Data Release Frequency: Annually

WI MANIFEST: Manifest Information

Hazardous waste manifest information.

Date of Government Version: 12/31/2012 Date Data Arrived at EDR: 08/09/2013 Date Made Active in Reports: 09/27/2013

Number of Days to Update: 49

Source: Department of Natural Resources

Telephone: N/A

Last EDR Contact: 09/16/2013

Next Scheduled EDR Contact: 12/30/2013 Data Release Frequency: Annually

Oil/Gas Pipelines: This data was obtained by EDR from the USGS in 1994. It is referred to by USGS as GeoData Digital Line Graphs from 1:100,000-Scale Maps. It was extracted from the transportation category including some oil, but primarily gas pipelines.

Sensitive Receptors: There are individuals deemed sensitive receptors due to their fragile immune systems and special sensitivity to environmental discharges. These sensitive receptors typically include the elderly, the sick, and children. While the location of all sensitive receptors cannot be determined, EDR indicates those buildings and facilities - schools, daycares, hospitals, medical centers, and nursing homes - where individuals who are sensitive receptors are likely to be located.

AHA Hospitals:

Source: American Hospital Association, Inc.

Telephone: 312-280-5991

The database includes a listing of hospitals based on the American Hospital Association's annual survey of hospitals.

Medical Centers: Provider of Services Listing

Source: Centers for Medicare & Medicaid Services

Telephone: 410-786-3000

A listing of hospitals with Medicare provider number, produced by Centers of Medicare & Medicaid Services,

a federal agency within the U.S. Department of Health and Human Services.

Nursing Homes

Source: National Institutes of Health

Telephone: 301-594-6248

Information on Medicare and Medicaid certified nursing homes in the United States.

Public Schools

Source: National Center for Education Statistics

Telephone: 202-502-7300

The National Center for Education Statistics' primary database on elementary

and secondary public education in the United States. It is a comprehensive, annual, national statistical database of all public elementary and secondary schools and school districts, which contains data that are

comparable across all states.

Private Schools

Source: National Center for Education Statistics

Telephone: 202-502-7300

The National Center for Education Statistics' primary database on private school locations in the United States.

Daycare Centers: Department of Children & Families

Source: Provider Information Telephone: 850-488-4900

GOVERNMENT RECORDS SEARCHED / DATA CURRENCY TRACKING

Flood Zone Data: This data, available in select counties across the country, was obtained by EDR in 2003 & 2011 from the Federal Emergency Management Agency (FEMA). Data depicts 100-year and 500-year flood zones as defined by FEMA.

NWI: National Wetlands Inventory. This data, available in select counties across the country, was obtained by EDR in 2002 and 2005 from the U.S. Fish and Wildlife Service.

State Wetlands Data: Wetlands Inventory Source: Department of Environmental Protection

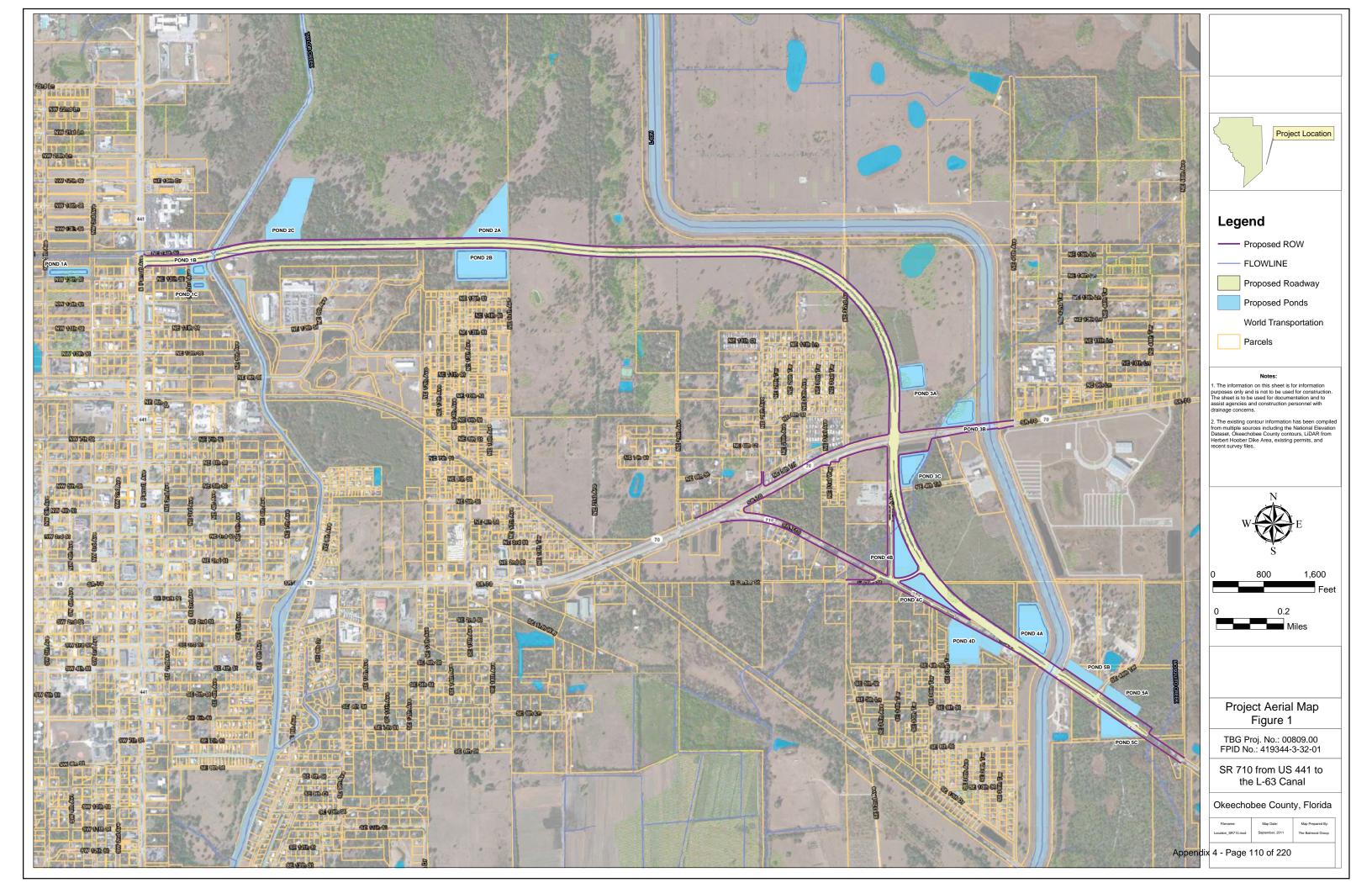
Telephone: 850-245-8238

STREET AND ADDRESS INFORMATION

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CSER-Appendix E

Supplemental Information



















SR 710 from US 441 to the L-63N Canal

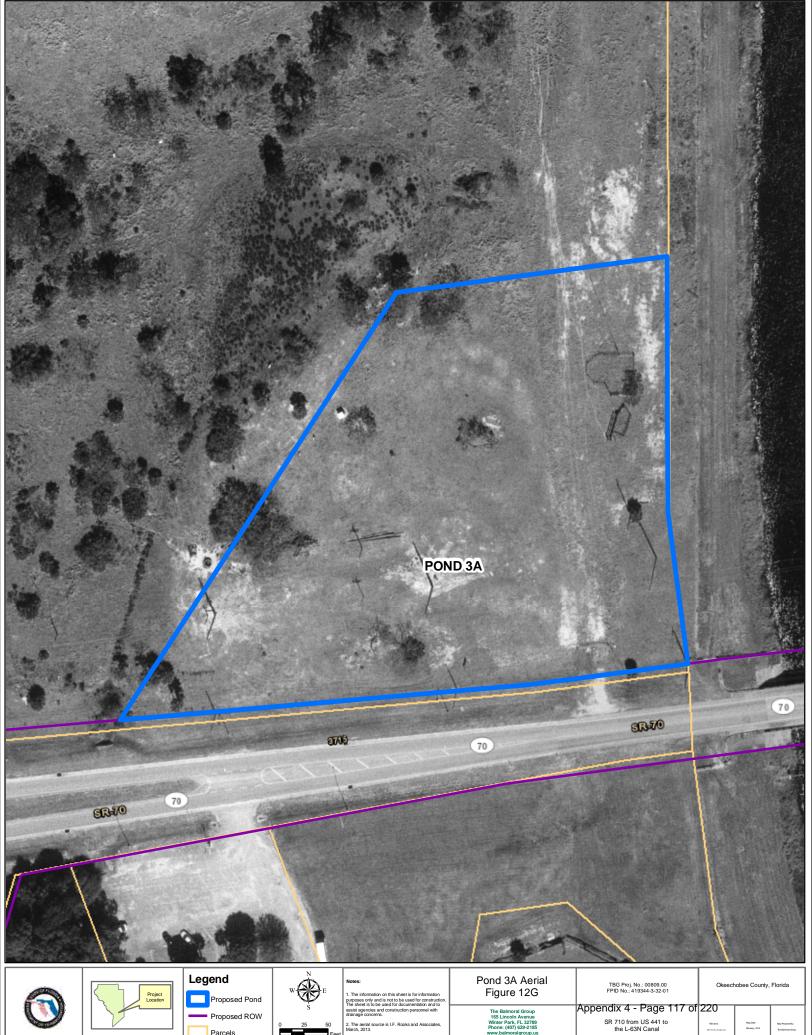








The aerial source is I.F. Rooks and Associates, March, 2013.









Parcels

2. The aerial source is I.F. Rooks and Associates, March, 2013.



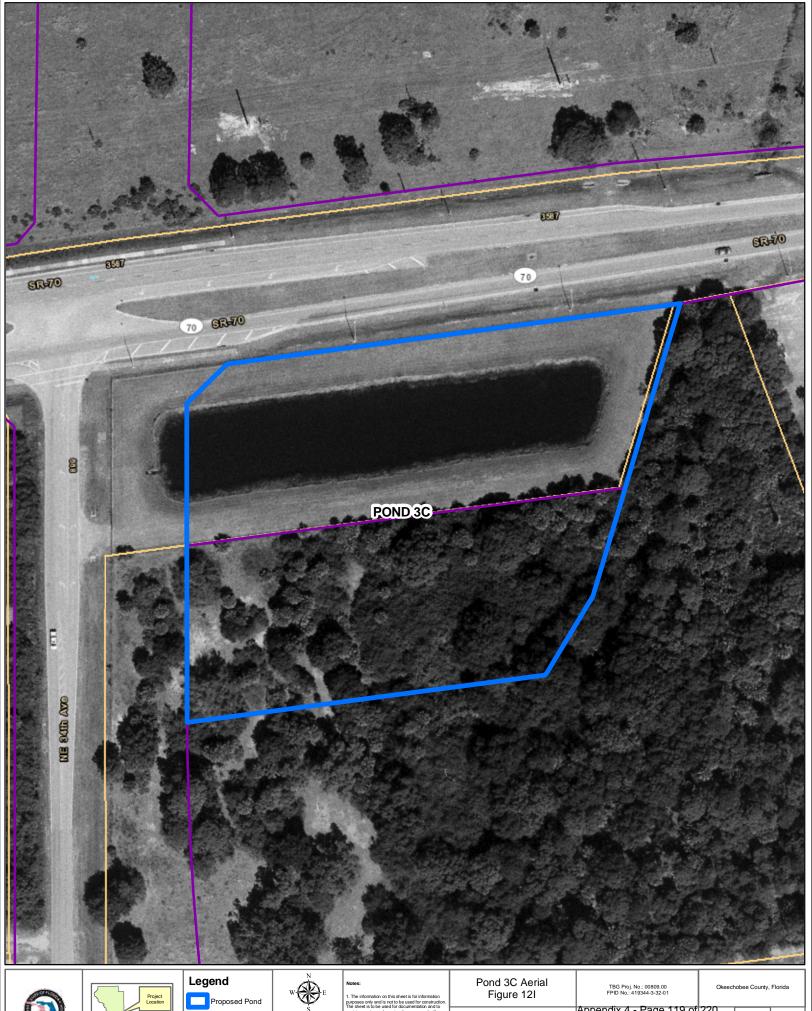








SR 710 from US 441 to the L-63N Canal







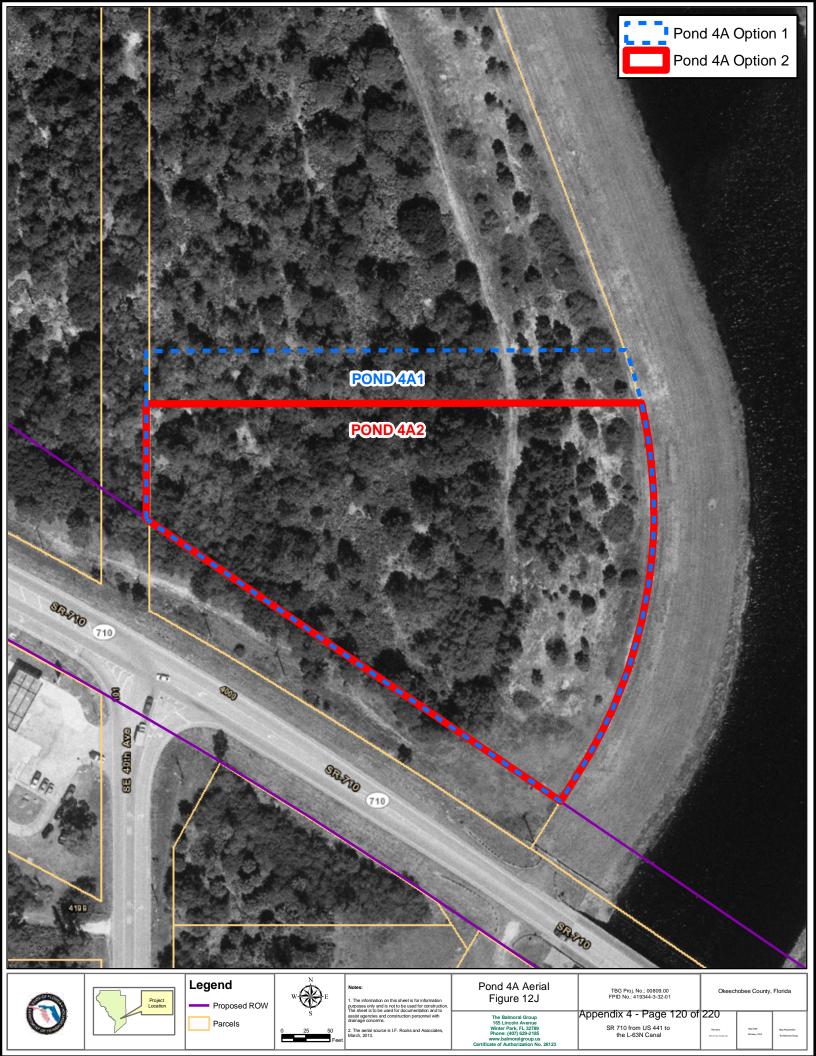


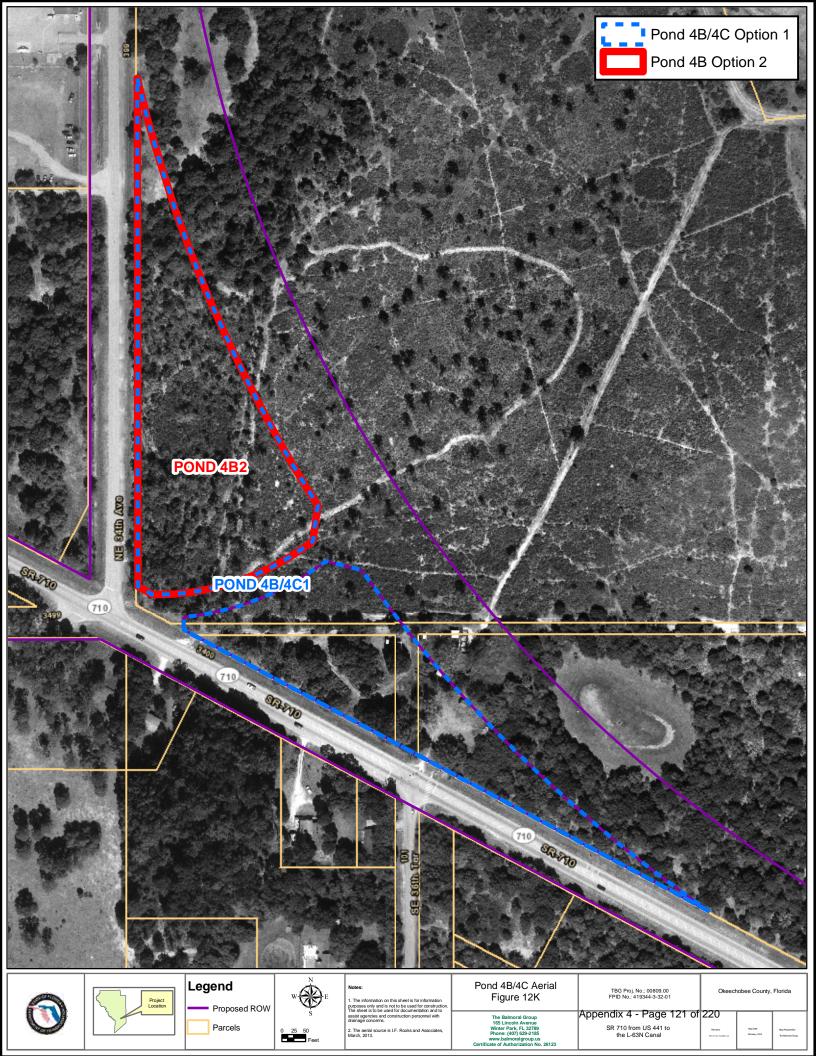


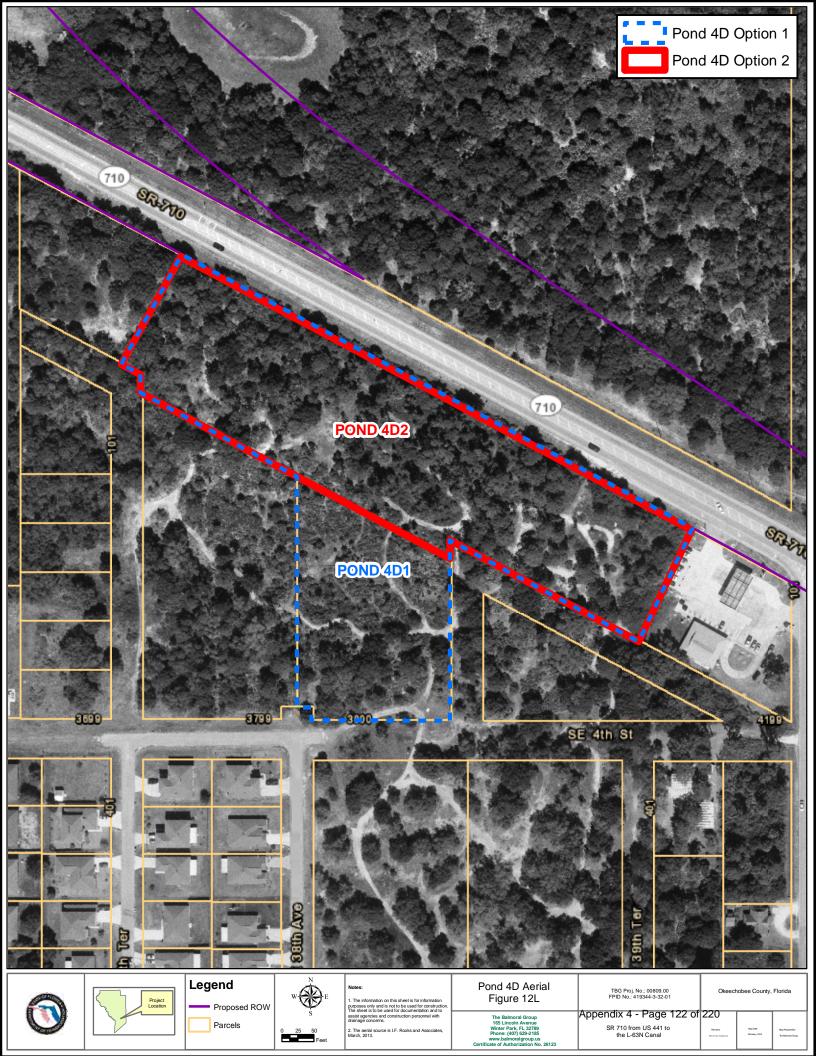
The information on this sheet is for information purposes only and is not to be used for construction. The sheet is to be used for documentation and to assist agencies and construction personnel with drainage concerns.

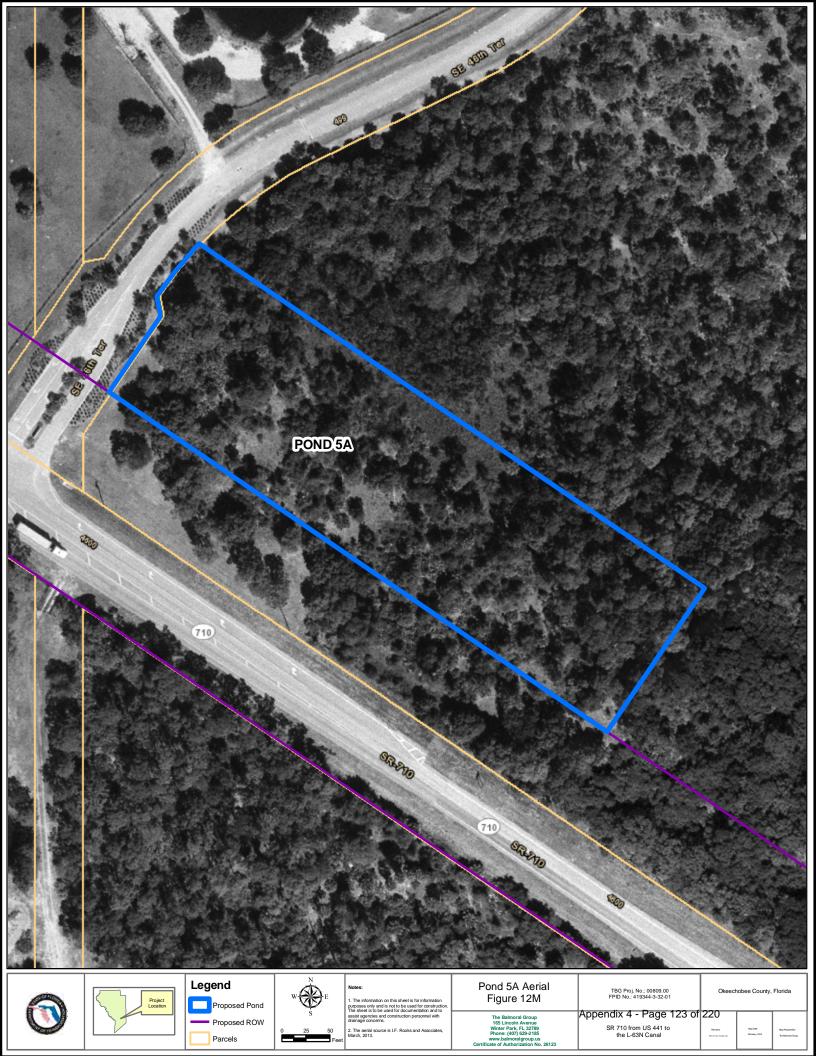
SR 710 from US 441 to the L-63N Canal

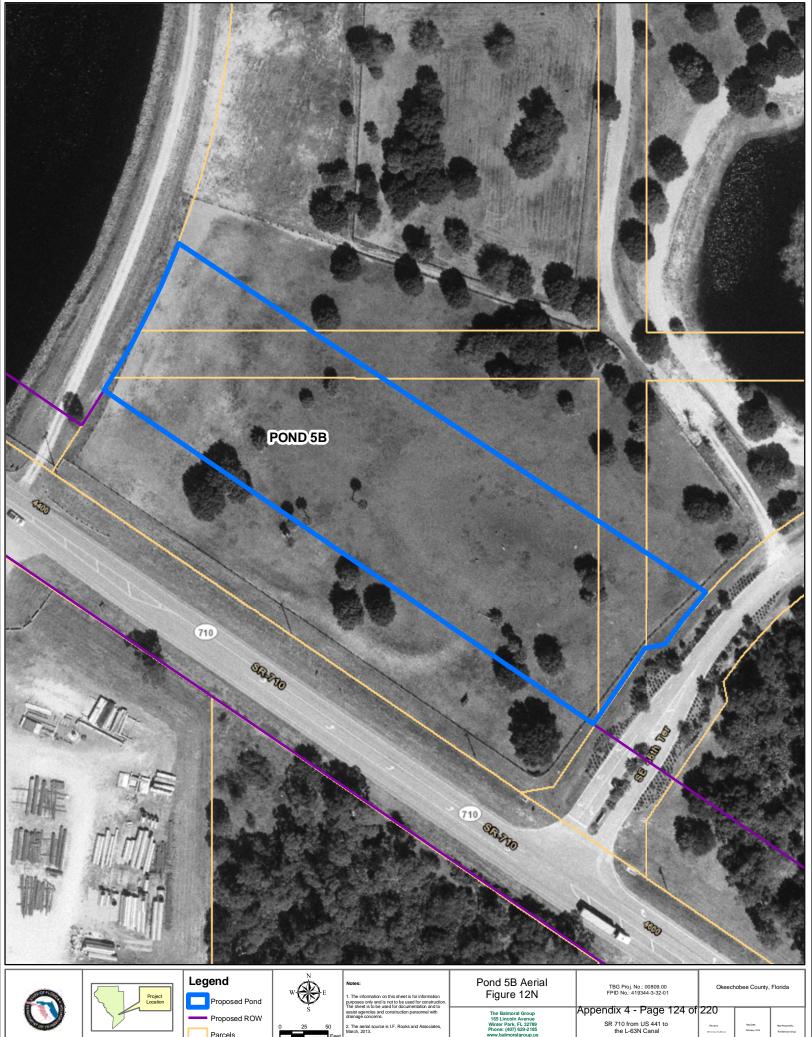
Appendix 4 - Page 119 of 220









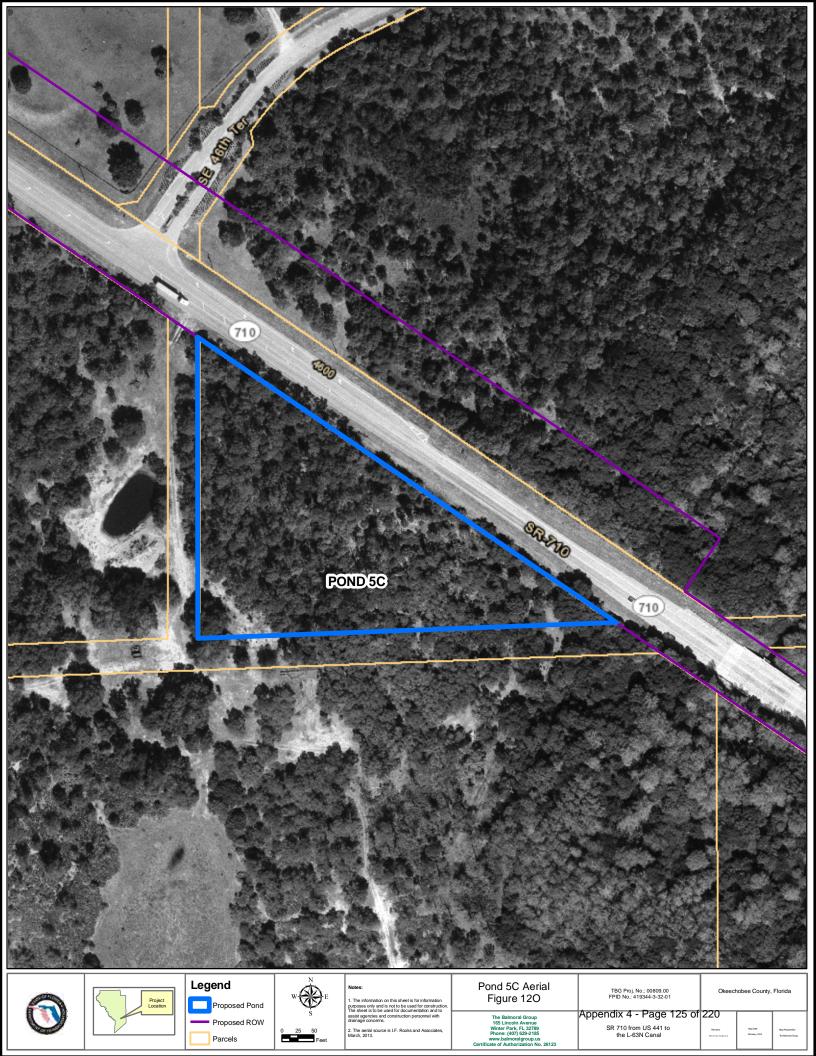








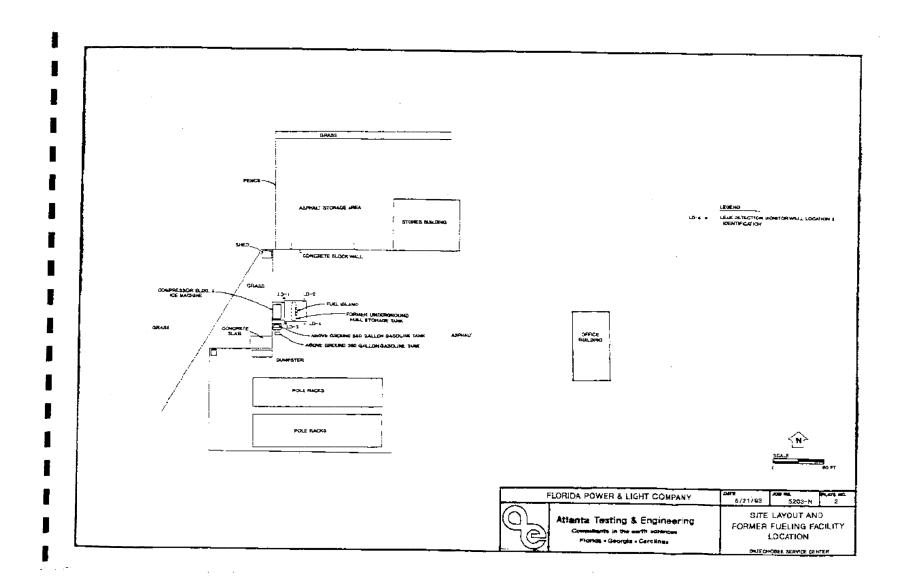
The aerial source is I.F. Rooks and Associates, March, 2013.

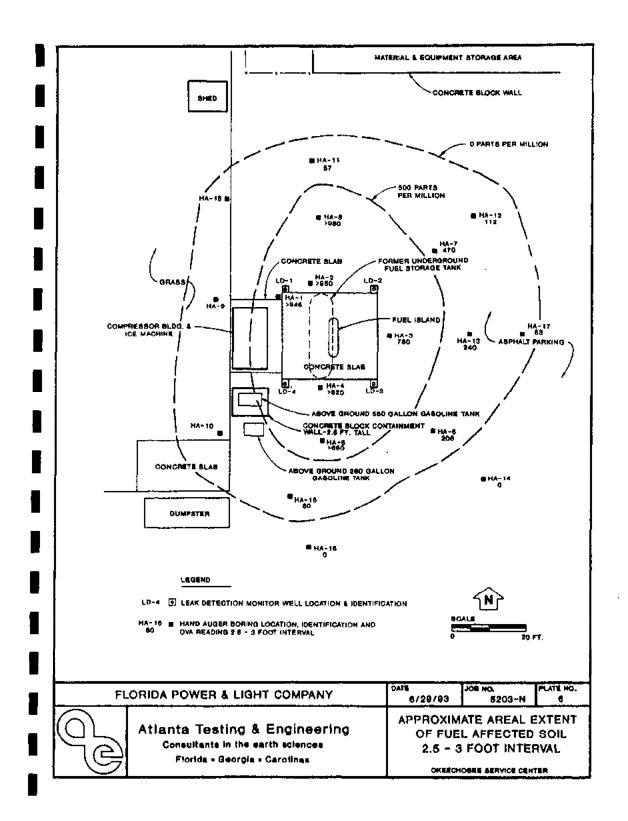


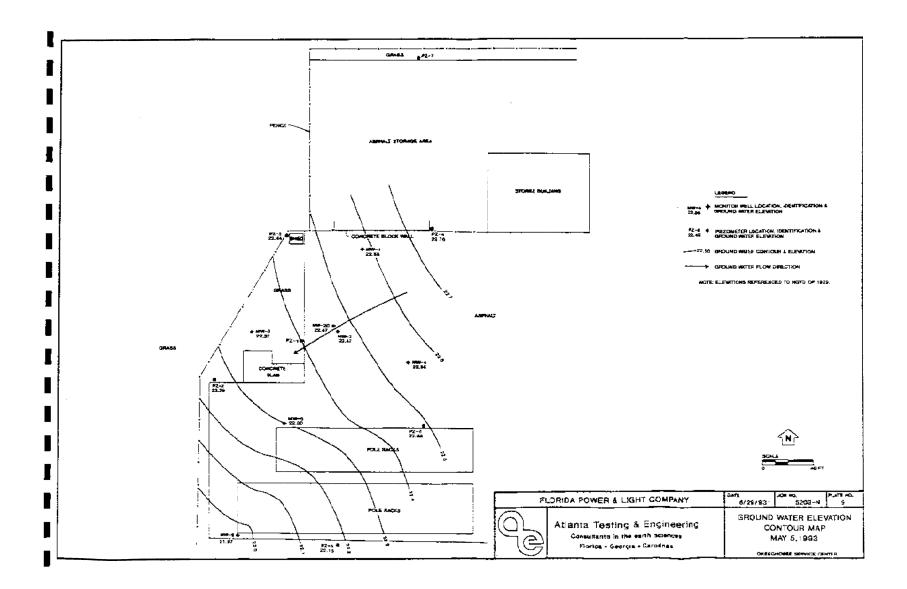
SRb710bPondbAreas FPIDb19344-3-32-01

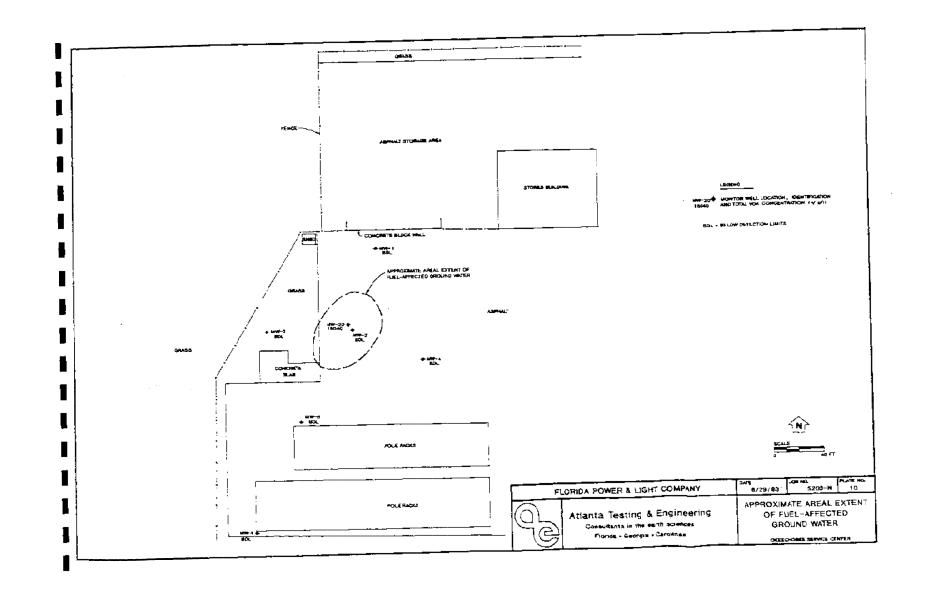
PondbD	Areak(ac.)
1A	2.32
1B	1.20
1C	0.88
2As∙sOptions1	14.23
2As-sOptions2	7.93
2As-sOptions3	6.42
2B-Options1	15.37
2B-Options2	10.00
2B-Options	7.08
2C-Options1	6.86
2C-Options2	6.14
3A	4.18
3B	2.44
3C	3.81
4A-Options1	3.98
4A-Options2	3.34
4B/4Cs-sOptions1	8.17
4Bs-sOptions2	4.59
4Ds-sOptions1	6.08
4Ds-sOptions2	4.33
5A	2.62
5B	2.53
5C	3.53

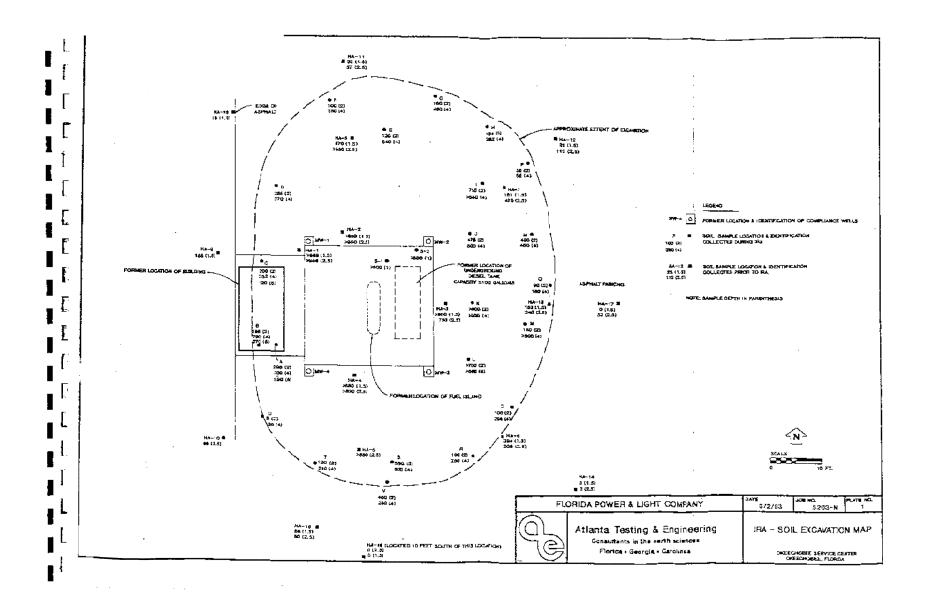
Florida Power and Light Co. (FPL) (Fac. ID 8519987) Contamination Assessment Report 1993











Townstar #40/BP gas station (Fac. ID 8630309) Source Removal Report 2009

1.0 SITE DESCRIPTION

Gator Engineering & Aquifer Restoration, Inc. (GEAR), on behalf of TimeSaver Properties, Inc. (Timesaver) has recently completed Limited Source Removal Initiative (LSRI) activities in conjunction with Underground Storage Tank (UST) upgrade activities at the Townstar #40 facility (Site).

The Site is located at 3993 Highway 710 East in Okeechobee, Okeechobee County, Florida and is in the Pre-Approval program (PAP) (FDEP FAC ID No. 47/8630309) with a priority score of 42. The site location is illustrated on Figure 1, USGS Topographical Map. The facility layout is depicted on Figure 2, Site Plan.

2.0 HISTORICAL ACTIVITIES

According to the OCULUS database, a discharge was reported on December 30, 1988 based upon laboratory results collected on November 22, 1988. No discharge reporting form was available for review. However, the EDI program application listed the cause and type of discharge as "unknown".

The site owners retained MACTEC as the remediation contractor and on October 27, 2006, MACTEC submitted the first of two Supplemental Site Assessment Reports (SSARs). During the field work portion of the assessment, MACTEC oversaw the advancement of eight (8) soil borings (via DPT), the installation and subsequent sampling of five (5) additional on-site monitoring wells and the collection of three (3) soil samples. As a result of this assessment, MACTEC recommended the installation of three (3) additional wells to the west of the subject property (off-site wells).

On November 21, 2007, MACTEC submitted the second SSAR. This report document the installation of the three (3) off-site wells and an additional round of groundwater sampling. The report concluded that there were no vadose zone impacts at the sampling locations and that the groundwater impacts were contained on-site. Based on these results, MACTEC recommended that the site be placed in a NAM program. The site owner then selected GEAR to perform the monitoring and move the site to closure.

In the first quarter of 2008, GEAR submitted a pre-approval proposal to the FDEP to conduct the first year of NAM monitoring. However, due to a lack of available funding, this work order was not implemented.

According to the FDEP Bureau of Petroleum Storage Systems website (STCM Database), the current facility layout contains three (3) 10,000 gallon underground storage tanks (USTs) that were installed in May 1986. Timesaver is the storage tank owner and is conducting the required 2009 upgrades to the USTs and product piping under the LSRI. GEAR submitted an LSRI proposal for this site on February 17, 2009. However, the proposal lacked sufficient soil exploration to substantiate evidence of a soil source for the LSRI. Therefore, Timesaver requested GEAR to conduct a soil investigation in the exclusion zone.

Therefore, Timesavers' contractor Wilson's petroleum (Wilson's) sawcut areas around the USTs and GEAR's field technician reported that the highest organic vapor concentrations were encountered in the trench near the center of the USTs and that the top of the water table was located at approximately 7.0 feet bls. Therefore, GEAR's technician was instructed to collect one (1) soil sample from this location for

Source Removal Report Timesaver #40 3993 Highway 710 East, Okeechobee Facility ID No. 8630309 GEAR Project No. 07-0040-1 Page 2

laboratory analysis. The collected soil sample was analyzed by EPA methods 8260 (BTEX + MTBE), 8270 (PAHs) and by laboratory method FL-PRO (TRPH). The laboratory results indicated the presence of impacted soils at concentrations that exceeded their applicable Chapter 62-777 Soil Cleanup Target Levels (SCTLs) and therefore, the LSRI work order was approved for up to 600 tons of contaminated soil. These results also further supported the need for dewatering effluent treatment.

3.0 NPDES PERMITING

Due to an average water table depth of approximately seven (7) feet below land surface (ft bls), dewatering was required to conduct the replacement of the existing UST system. In order to discharge the dewatering effluent to the storm sewer system, TimeSaver was required to obtain a National Pollutant Discharge Elimination System (NPDES) permit.

Therefore, on December 23, 2008, GEAR mobilized to the site to complete the required groundwater sampling to obtain the NPDES permit for the Townstar #40 facility. One (1) groundwater sample was collected from Monitoring Well MW-10. Monitoring Well MW-10 was chosen based upon its proximity to the tank farm, accessibility and history of contamination. All groundwater sampling was conducted in accordance with FDEP Standard Operating Procedure DEP-SOP-001/01.

The groundwater samples collected were appropriately preserved and forwarded to a NELAP certified and FDEP-approved laboratory for analyses. The groundwater samples were analyzed for Benzene, Naphthalene, Total Organic Carbon, flardness, Alkalinity, for Hexavalent Chromium, and for total recoverable Mercury, Cadmium, Copper, Lead, Zine, and Chromium. The turbidity and pH of the samples were determined in the field.

The laboratory analytical results revealed that all tested parameters met the FDEP screening values for surface water discharge to fresh waters described in FAC Chapter 62-621.300(1), Table 4.

Since the results of the groundwater analyses met the screening parameters, the discharge of groundwater from this location was authorized under the *Generic Permit for Discharges from Petroleum Contaminated Sites* FAC Chapter 62-621.300(1) as long as proper treatment of the dewatering effluent was provided. See **Attachment A** for the NPDES permit approval letter.

4.0 SOURCE REMOVAL ACTIVITIES

The source removal activities consisted of dewatering and the excavation of impacted soils that were located above and below the water table. The site activities were conducted from July 13th, 2009 (date of the pre-burn sample) through July 30th, 2009 (final soil loadout). TimeSaver's petroleum installation contractor (Wilson's Petroleum) then continued with UST installation activities. The activities that GEAR observed are detailed below.

4.1 Source Removal - Dewatering System

On July 13th, 2009, GFAR personnel mobilized to the subject site to collect a "pre-burn" sample to facilitate soil disposal. Wilson's Petroleum was on-site removing the old dispensers when GEAR arrived on-site. After the pre-burn sample was collected, GEAR's technician transported the sample to the laboratory for analysis.

On July 24th, 2009, GEAR personnel returned to the subject site to perform soil screening activities as the concrete over the USTs was being removed. When GEAR arrived, Wilson's was removing the remaining USTs. After the tanks were removed, GEAR began mapping out a grid pattern for soil sampling. At each

Source Removal Report Timesaver ##40 3993 Highway 710 East, Okecchobee Facility ID No. 8630109 GEAR Project No. 07-0040-1

Page 3

point on the grid (illustrated on **Figure 3**, *Area of Excavation*), GEAR's technician advanced a soil boring to an approximate depth of six (6) feet below land surface (ft-bls). The technician then collected soil samples at two (2) foot intervals from each boring for analysis of organic vapors utilizing an organic vapor analyzer (OVA) equipped with a photo ionization detector (PID). After the OVA readings were completed, GEAR's technician left the site. Based on this analysis, GEAR concluded that there was approximately 259 cubic yards (363 tons) of impacted soils based on an OVA of 35 ppm from grid area 8 (See Figure 3 and field notes from July 24, 2009 for details).

Also on July 24th, 2009, GEAR personnel oversaw the connection of the "sparge barge" to the dewatering system and collected the first effluent sample from the dewatering treatment system. After collecting the sample, GEAR's technician transported the collected sample to Genapure Laboratories of Boca Raton, Florida. The collected sample was laboratory analyzed by EPA methods 8260 (BTEX + MTBE + Naphthalene) and 6010 (Lead). After receiving the analytical results demonstrating the systems' ability to remediate the dewatering effluent, the dewatering activities began on July 25th, 2009 and continued until July 28th, 2009.

In order to comply with the NPDES permit, GEAR sampled the dewatering effluent daily. The collected groundwater samples were analyzed by EPA Methods 8260 (BTEX + MTBE + Naphthalenc), and 6010 (Lead). A total of three (3) effluent grab samples (1 for start-up, and 2 daily) were obtained for the Daily Monitor Reports (DMR) completed for each day as per NPDES requirements. The sample results are presented in Table 1 Effluent Analytical Summary – VOCs and Metals, and Table 2 Effluent Analytical Summary – PAHs and TRPHs. The field notes and calibration documentation are presented in Attachment B. The complete laboratory analytical report and chain of custody documentation are presented in Attachment C. The DMRs for the Generic Permit are provided in Attachment D. It should be noted that there was no sample collected on July 27, 2009. The sample was scheduled to be collected during the afternoon. However, due to problems with the dewatering pump, there was not enough water extracted from the ground to collect a sample.

The treated groundwater water was discharged into the storm water swale located adjacent to Highway 710 East as illustrated on **Figure 2**. The water infiltrated back into the ground within 50 feet of that location

4.2 Source Removal - Soil Excavation

After the water table had been sufficiently depressed, GEAR provided soil segregating and confirmatory sampling activities during the tank upgrade activities. These activities were conducted on July 27th, 2009 through July 28th, 2009. Prior to starting work each day, GEAR attended a tailgate safety meeting conducted by Wilson. GEAR used an OVA response of 35 ppm as the threshold for determining what soils were clean and what soils need disposal. Soils that were either dug from the locations were previous impacted soils were encountered (See Figure 3 *Area of Soil Excavation*) or registered an OVA reading of greater than 35 ppm were placed in one pile while "clean" soils were placed in another pile. At the time an estimated 500 – 600 tons were stockpiled.

After the UST area was excavated, GEAR personnel returned on July 30th, 2009 to oversec the soil load out. Due to the low readings, the soil pile was re-screened to ensure that only impacted soils were removed. It should be noted that some of the OVA readings that were collected during this re-screening were below 35 ppm. GEAR attributes this to the aeration effect and still believes that the removed soils were impacted. The impacted soils (greater than 35 ppm) were then loaded into trucks, manifested and transported to Waste Management's Okeechobec Landfill for proper disposal. According to the manifests and weigh tickets, 345.5 tons were excavated from the UST area and removed from the site for proper disposal. The Non-Hazardous Waste Manifests and Weigh Tickets are provided in **Attachment B**.

Page 4

Source Removal Report Timesaver #40 3993 Highway 710 East, Okeechobee Facility ID No. 8630309 GEAR Project No. 07-0040-1

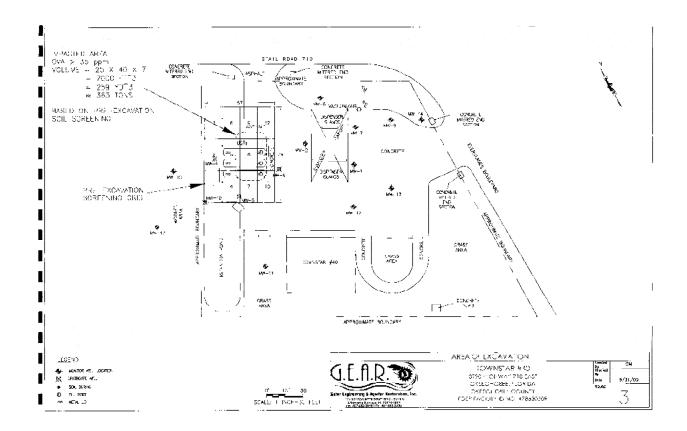
After the impacted soils were excavated and the pit was expanded to accommodate the new USTs, GEAR personnel collected four (4) sidewall samples (north, east, south and west) and one (1) tank pit bottom soil sample. The samples were collected from a depth of approximately 5 ft bls. The collected soil samples were analyzed by EPA Method 8260 (BTEX + MTBE), EPA Method 8310 (PAHs), and by laboratory method FL-PRO (TRPH). The sampling locations are illustrated on Figure 4 Area of Excavation with New Tank location. The analytical results are provided in Table 3 Soil Analytical Summary - VOCs and Metals, Table 4 Soil Analytical Summary - Non-Carcinogenic PAHs and Table 5 Soil Analytical Summary - Carcinogenic PAHs. The complete laboratory analytical report is provided in Attachment C.

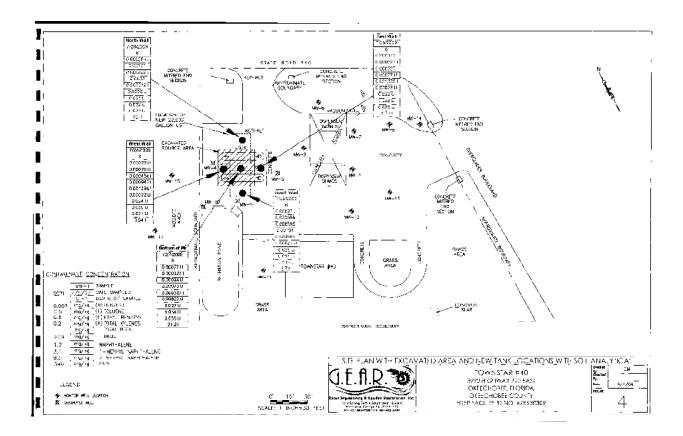
As the laboratory results indicate, there were no petroleum related hydrocarbon constituents detected in the samples collected from the bottom of the pit, or the north, south east or west side walls that exceeded their respective Chapter 62-777 SCTLs for leachability or Residential Direct Exposure.

5.0 CONCLUSIONS AND RECOMMENDATIONS

The laboratory analytical results indicated that no impacted soils remain either in or adjacent to the excavated area. Additionally, the latest groundwater assessment results (collected by MACTEC in October 2007) did not reveal any exceedances of the Chapter 62-777 Groundwater Cleanup Target Levels (GCTLs) in any of the site's monitor wells except for MW-5, MW-12 and MW-14. In those wells, low levels of benzene (3.1 µg/L in MW-6 and 7.5 µg/L in MW-4) and MTBE (55 µg/L in MW-12 and 38 µg/L in MW-14) were detected. Based on these low groundwater contaminant concentrations, and the large amount of soil and groundwater that was either treated and/or removed during the upgrade activities, GEAR recommends that a Site Rehabilitation Completion Order (SRCO) be issued for the site.

Source Removal Report Timesaver #40 3993 Highway 710 East, Okeechobee Facility ID No. 8630309 GFAR Project No. 07-0040-1 Page 5





Townstar #40/BP gas station (Fac. ID 8630309) Supplemental Site Assessment Report 2007



DUPLICATE

engineering and constructing a better tomorrow

RECEIVED BY

November 21, 2007

NOV 26 2007 TEAM 5

Mr. Ian K. Tiang Florida Department of Environmental Protection Bureau of Petroleum Storage Systems 2600 Blair Stone Road, MS 4585 Tallahassec, Florida 32399-2400

SUBJECT:

Supplemental Site Assessment Report

Townstar 40

3393 State Road 710 E, Okeechobee, Okeechobee County, Florida

Priority Score: 41

FDEP Facility ID No. 47/8630309 Work Order: 2007-95-W59048 TREALINE ED PROPERTION OF THE 23 TEAM 5

Dear Mr. Tiang:

MACTEC Engineering and Consulting Inc. (MACTEC) is pleased to submit this Supplemental Site Assessment Report for the Townstar 40 site in Okeechobee, Florida (Figure 1). This report summarizes the site assessment activities conducted at the referenced location and serves as the final deliverable for Work Order: 2007-95-W59048.

SITE BACKGROUND

MACTEC submitted a Supplemental Site Assessment Report on October 25, 2006. The report concluded that Methyl Tertiary Butyl Ether (MTBE), Benzene and Xylenes were present in groundwater above Groundwater Contamination Target Level (GCTL). Since the contaminants plume were not completely established, MACTEC recommended the installation of off site monitoring wells at the adjacent property to the west. MACTEC also recommended re-sampling monitoring well MW-14 since the concentration of Benzene and MTBE were detected in the above the GCTL which was inconsistent with values obtained in the surrounding monitoring wells during the groundwater assessment.

In a letter dated December 27, 2006, the Bureau of Petroleum Storage Systems (BPSS) reviewed the Supplemental Site Assessment Report dated October 25, 2006 and the Response to Comment Letter dated November 21, 2006. The report including the addendum was acceptable and demonstrated that the work

MACTEC Engineering and Consulting, Inc.

4150 N. John Young Parkway • Orlando, Fl. 32804:2620 • Phone: 407-522,7570 • 407.522,7576

www.mactec.com

outlined in Work Order #2006-95-W13495 was satisfactory performed. The BPSS agreed with the recommendations to collect confirmatory groundwater samples from monitoring well MW-14 and also to install additional monitoring wells to the west of monitoring well MW-10 to delincate the horizontal extent of groundwater contaminations.

SUMMARY OF CURRENT SITE ASSESSMENT ACTIVITIES

Monitoring Well Installation

On October 12, 2007 MACTEC's subcontractor, Preferred Drilling, installed three shallow monitoring wells (MW-15 through MW-17) using a drill rig equipped with a hollow stem auger (Figure 2). Monitoring well MW-16 was installed to an approximate depth of 13 feet below land surface (bls). Monitoring wells MW-15 and MW-17 were installed to an approximate depth of 14 feet bls.

The wells were constructed of 10 feet of 2 inch diameter 0.010-inch slotted PVC screen and five feet of 2-inch PVC risers. The borehole diameter was 8 inches. A 20/30 silica sand filter pack was placed in the annular space between the well screen and the borehole and was extended to a height of approximately 1.5 feet bis at each location. The remaining space was grouted with Portland cement to approximately 0.5 bis. Each monitoring well was capped with a flush mount casing, set in a two-foot by two-foot by six-inch concrete pad. All casings were secured with a two-inch "expando-cap". Table 1 summarizes the well construction data and Appendix A includes the monitoring well construction logs. The monitoring wells were developed using a centrifugal/peristaltic pump until the extracted groundwater was clear of sediment,

The soil boring was continuously screened every two feet using an OVA to the water table. OVA soil screening is a State of Florida Department of Environmental Protection (FDEP) approved screening method for detecting the presence of hydrocarbons in soils. Headspace analyses were conducted on the soil samples in general accordance with the guidelines set forth in Chapter 62-770, Florida Administrative Code (F.A.C.). The headspace analysis was performed by half filling two clear 16-ounce glass jar with soil, covering the jars with aluminum foil, and allowing a minimum period of five minutes for volatile organic vapors to collect in the headspace above the soil in the jar. A charcoal filter was used to assist in distinguishing vapors between petroleum and methane. The net measurement (unfiltered minus filtered) is an indication of the presence of hydrocarbon vapors in the soil sample. Table 2 summarized the OVA

results. A pre-burn/disposal sample was collected and was placed on ice and transported to Southern Research Laboratory in Orlando, Florida. The sample was analyzed for BTEX/MTBE by USEPA Method 8021, TRPHs by FL-PRO, Arsenic, Cadmium, Lead and Chromium. The laboratory result of pre-burn soil analysis is attached in Appendix B. The soil cuttings and development water were drummed. The drums will be properly disposed of by Greenleaf Treatment Corp. The manifest will be forwarded following drum disposal.

Groundwater Quality Assessment

On October 16, 2007, MACTEC personnel collected groundwater samples from monitoring wells MW-1, MW-5, MW-6, MW-7, MW-10, MW-12, and MW-14 through MW-17. The sampling event was conducted in accordance with the Petroleum Cleanup Preapproval Program Standard Operating Procedures. During purging, stabilization parameters (pH, temperature, conductivity, turbidity, and dissolved oxygen) were measured until stabilized. Copies of the Groundwater Sampling Logs and calibration information are included in Appendix C.

Groundwater samples were placed on ice and transported to Southern Research Laboratory in Orlando, Florida. The samples were analyzed for BTEX/MTBE by USEPA Method 8021, PAHs by USEPA Method 8310 and TRPHs by FL-PRO.

Groundwater Flow Direction

Depth-to-groundwater measurements were collected on October 16, 2007 from monitoring wells MW-1 through MW-17 to evaluate the groundwater flow direction in the upper zone of the surficial aquifer. Groundwater elevations were measured in the wells using an electronic measuring tape to an accuracy of 0.01 feet (Table 3). Based on the water level data, the groundwater flow direction was toward the water (Figure 3).

Analytical Results

Based on groundwater laboratory analytical results, some petroleum contaminants were detected above the Chapter 62-777, Florida Administrative Code (F.A.C.) GCTLs. The following parameters and respective concentrations were detected above the laboratory detection limits.

Sample from MW-1

- > Total Xylenes was estimated at 0.5 μg/l below GCTL of 20 μg/l
- > MTBE was detected at 4.5 μg/l below GCTL of 20 μg/l

Sample from MW-5

> No parameters were detected above laboratory detection limits.

Sample from MW-6

- Benzene was detected at 3.1 μg/l which exceeds the GCTL of 1 μg/l.
- > Total Xylone was estimated at 1.7 μg/l below GCTL of 20 μg/l.
- > MTBE was detected at 17 μg/l below GCTL of 20 μg/l
- TRPH was detected at 0.8 mg/l below GCTL of 5 mg/l

Sample from MW-7

- Benzene was estimated at 0.5 μg/l below GCTL of 1 μg/l.
- Total Xylene was detected at 3.1 μg/l below GCTL of 20 μg/l.
- \gg MTBE was detected at 8.1 µg/l below GCTL of 20 µg/l
- Naphthalene was estimated at 0.88 μg/l below GCTL of 14 μg/l.

Sample from MW-10

No parameters were detected above laboratory detection limits.

Sample from MW-12

ightharpoonup MTBE was detected at 55 µg/l which exceeds the GCTL of 20 µg/l

Sample from MW-14

- Benzene was detected at 7.5 μg/l which exceeds the GCTL of 1 μg/l
- > MTBE was detected at 38 μg/l which exceeds the GCTL of 20 μg/l

Sample from MW-15

> No parameters were detected above laboratory detection limits.

Sample from MW-16

Townstar #40-Okeechahee, Florida Supplemental Site Assessment Report

No parameters were detected above laboratory detection limits.

Sample from MW-17

> No parameters were detected above laboratory detection limits.

A summary of groundwater analytical data is presented in Table 4. Laboratory analytical data is presented as Appendix B.

CONCLUSIONS AND RECOMMENDATIONS

No parameters were detected above the laboratory detection limits in monitor wells MW-15, MW-16, and MW-17. Based on these analytical results, MACTEC concludes that the extent of contamination has been delineated on the western portion of the site. In addition, the adjacent property to the west has not been impacted by the release at the Townstar #40 facility.

The monitoring wells exhibiting elevated concentrations were within the interior of the site, with the exception of MW-14. Contaminants of concern (7.5 µg/L for Benzene and 38 µg/L MTBE) were confirmed above the GCTLs in the monitoring well MW-14. However, these concentrations were below the Natural Attenuation Default Concentrations of 100 µg/L and 200 µg/L as provided in Table V of Chapter 62-777. MACTEC recommends conducting a Natural Attenuation Monitoring Plan for this site based on the recent analytical results.

CLOSING

MACTEC appreciates the opportunity to provide these services and submit this data to Florida Department of Environmental Protection, Protection Cleanup Section, on behalf of TimeSaver Food Stores, LLC. Should you have any questions concerning the contents of this report, please do not hesitate to contact us at (407) 522-7570.

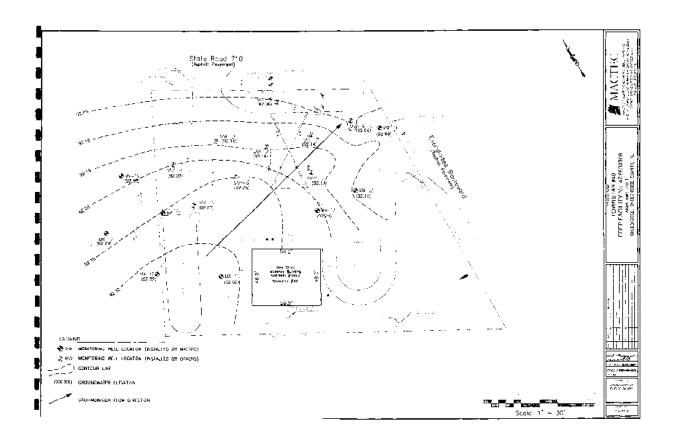
Sincerely,

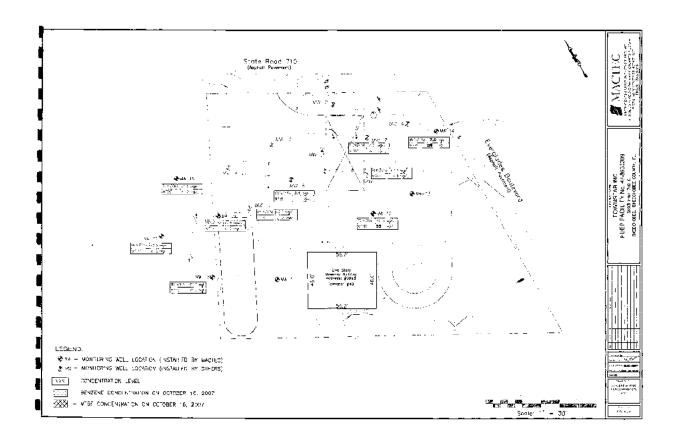
MACTEC Engineering and Consulting Inc.

Angeliare King
for Mahesh Krishnamoorthy with Jerminion"

5

Florman Blackbarn; Principal Engineer





January 13, 2017

Wantman Group, Inc. 213 South Dillard St, Suite 210 Winter Garden, Florida 34787

Attn: Mr. Alfredo Rodriguez, PE

Project Manager

RE: DRAFT Level II Field Screening Report (FSR) – Preferred Ponds

SR 710 from US 441 to the L-63 Canal

Okeechobee County, Florida

FPN: 419344-3-32-01

Tierra Project No.: 6511-12-054A

Mr. Rodriguez:

Tierra, Inc. (Tierra) has prepared this Level II Soil and Groundwater Field Screening Report (FSR) for your use as part of the design submittal documents. This report provides results of Level II field screening activities completed at the Preferred Pond locations for the project referenced above.

The Final Level I PSR-CSER for Proposed Ponds dated August 18, 2014 identified the following risk rankings for the selected Preferred Pond sites: Pond 1B "Low", Pond 2A-Option 1 "Low", Pond 3B "No", Pond 4B-Option 2 "No", and Pond 5A "No". Tierra received notification of the Preferred Pond sites in September 2016. The Level II Scope of Services was reviewed and approved by Mr. Jeffery James, DCIC on November 21, 2016.

Should you have any questions, please contact our office at (813) 989-1354.

Respectfully Submitted,

TIERRA, INC.

Clare E. Kramer, PG Senior Scientist Donald R. Polanis, CGC, PSSC Chief Scientist

DRAFT Level II Field Screening Report – Preferred Ponds

SR 710 from US 441 to the L-63 Canal Okeechobee County, Florida

FDOT District I FPN: 419344-3-32-01

Prepared for:

Wantman Group, Inc. 2910 Maguire Road, Suite 2008 Ocoee, Florida 34761

Prepared by:

Tierra, Inc.7351 Temple Terrace Highway
Tampa, Florida 33637

Tierra Project No.: 6511-12-054A

January 13, 2017

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1.0	INTRODUCTION	1
2.0	SCOPE AND METHODOLOGY	2
3.0	FINDINGS	3
4.0	CONCLUSIONS	3
5.0	RECOMMENDATIONS	4
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Appendix A

Sheet 1 – Project Location Map Sheet 2 – Sample Location Map

Appendix B

Table 1 – Soil Analytical Summary Table 2 – GPS Coordinates

Appendix C

Laboratory Analytical Report

Appendix D

Soil Boring Logs

1.0 INTRODUCTION

The Florida Department of Transportation, District One, is conducting a Project Development and Environmental (PD&E) Study regarding the proposed new road construction (extension to the northwest of existing SR 710) of SR 710 from US 441 to L-63 Canal in Okeechobee County, Florida. The project includes constructing an extension of SR 710 around the northeast side of Okeechobee. The new roadway will have a design speed of 50 mph and will be a high-speed urban four-lane roadway, including a 12-foot multi-use path on one side and five foot sidewalk on the other. A Project Location Map is presented on Sheet A-1 in **Appendix A**.

Initially, sixteen (16) Proposed Pond Alternatives were received from the client by email in October 2013. Updated Proposed Pond Alternatives were received from the client in March 2014. A total of twenty-three (23) pond site options were evaluated and the Final Level I PSR-CSER dated August 18, 2014 was submitted to the FDOT. Additionally, Regional Pond 2D was evaluated and a Tech Memo was prepared (as an addendum to the CSER) and dated May 12, 2015. The final pond locations were received by email from the client on September 29, 2016

This report provides Level II soil field screening results for five (5) Preferred Pond sites identified in the 2014 Final Level I PSR-CSER for the Proposed Ponds. The Level II contamination screening evaluation has resulted in the Post-Level II risk rankings for the final pond locations:

Risk Ranking Summary					
Preferred Pond	Pre-Level II Risk Rank	Post-Level II Risk Rank			
Pond 1B	LOW	NO			

1.20-Acres. Located west of Taylor Creek, east of North Parrott Avenue (US Highway 441), and north of NW 13th Street.

Use as construction staging area in 1994. Current and historic woodlands with an apiary (bee hives).

Level II field screening did not indicate arsenic contamination in the tested locations.

Undesirable buried debris was not encountered in the borings completed during Level II field activities.

Preferred Pond	Pre-Level II Risk Rank	Post-Level II Risk Rank		
Pond 2A – Option 1	LOW	NO		

14.23-Acres. Located north of NE 9th Street, east of Taylor Creek, and west of the L-63 Canal. Current and historic pastureland and woodlands.

Level II field screening did not indicate arsenic contamination in the tested locations.

Undesirable buried debris was not encountered in the borings completed during Level II field activities.

Preferred Pond	Pre-Level II Risk Rank	Post-Level II Risk Rank		
Pond 3B	NO	NO		

2.44-Acres. Located east of NE 32nd Avenue, north and south of SR 70, and west of the L-63 Canal. Current and historic pastureland and wetlands.

Level II field screening did not indicate arsenic contamination in the tested locations.

Undesirable buried debris was not encountered in the borings completed during Level II field activities.

Preferred Pond	Pre-Level II Risk Rank	Post-Level II Risk Rank		
Pond 4B – Option 2	NO	NO		

4.59-Acres. Located west of the L-63 Canal, and north of the existing SR 710. Current and historic woodlands with unpaved trails.

Level II field screening did not indicate arsenic contamination in the tested locations.

Undesirable buried debris was not encountered in the borings completed during Level II field activities.

 Preferred Pond
 Pre-Level II Risk Rank
 Post-Level II Risk Rank

 Pond 5A
 NO
 NO

2.62-Acres. Located west of L-63 Canal, and north of SR 710. Current and historic woodlands/wetlands/pastureland.

Level II field screening did not indicate arsenic contamination in the tested locations.

Undesirable buried debris was not encountered in the borings completed during Level II field activities.

Testing for arsenic in soils at each pond location is required to identify areas of elevated arsenic levels (above the SCTLs), to establish proper management techniques and to determine disposal options of impacted soils. If sites were to receive a risk ranking of "Medium" or "High", Tierra would recommend further Level II testing by the Contamination Assessment and Remediation (CAR) contractor, if required by the DCIC.

For sites post-ranked "No" or "Low", no additional work is recommended at this time. Should a facility's permitting or regulatory status change between now and the time acquisitions are initiated, additional screening should be conducted.

2.0 SCOPE AND METHODOLOGY

The field screening activities at the Preferred Pond sites were conducted in December 2016 and were based on the site specific Level II Scope of Services that included the number of soil samples, boring locations, and analysis testing, reviewed and approved by the DCIC in November 2016, prior to initiating the field activities.

Arsenic based pesticides and herbicides were historically used for vegetation and weed control on farmland such as citrus groves and/or row crops. Based on the current and historical presence of row crops and/or citrus groves at the pond locations, Level II soil screening activities were performed to provide information on the presence or absence of the tested contaminant at the specified sample locations. The sample locations are indicated on the Sample Location Map presented on Sheets A-2 and A-3 in **Appendix A.**

Equipment decontamination, sample collection, field documentation, sample custody, and laboratory analyses were performed in general accordance with the latest version of the "Florida Department of Environmental Protection (FDEP) Standard Operating Procedures (SOP) for Field Activities." All field services were conducted and overseen by Tierra personnel.

All samples collected for analytical testing were stored in ice and shipped under COC to a Florida certified NELAP environmental laboratory (Pace Analytical Services, LLC – Laboratory Certification ID# E83079). The full laboratory analytical report is included in **Appendix C**.

The methodology of the Level II field screening activities at the Preferred Pond sites identified for this project, are described below.

Boring Installation and Soil Sampling

Utilizing a stainless-steel hand auger, a total of twenty-two (22) auger borings were completed within the designed pond boundaries at five (5) Preferred Pond site locations. Each boring was advanced to a maximum depth of 10 feet below land surface (BLS) or to the groundwater water-table, to visually check for buried debris.

Four (4) soil samples were collected from 0 to 2 feet BLS at each pond site. A total of twenty (20) soil samples were sent for laboratory analysis of *Arsenic by EPA Method 6010*.

Groundwater sampling and analysis at the Preferred Ponds sites was not scoped for this project based on the typical screening protocols (lack of evidence to suggest impact to the groundwater) and approval by the FDOT District One DCIC, Mr. Jeffery James. The potential for contamination impact to the groundwater was not considered to be a concern in this locale and therefore groundwater sampling was not warranted.

3.0 FINDINGS

Tierra analyzed the data collected to determine whether levels of target analytes exceeded the FDEPs Soil Cleanup Target Levels (SCTL) contained in Chapter 62-777 FAC. The results of the laboratory analysis were compared to the SCTL for both Residential and Commercial/Industrial Direct Exposure (RDE and C/IDE) limits.

The sample locations at the Preferred Pond sites are illustrated on the Sample Location Map presented in **Appendix A**. The Soil Analytical Summary is presented in Table 1 of **Appendix B**. GPS Coordinates for the SBs were recorded and are tabulated in Table 2 of **Appendix B**. The full laboratory report and copy of the COC are included in **Appendix C**. Field notes describing the soil lithology; any buried debris or petroleum odors were documented on Soil Boring Logs and copies are included in **Appendix D**.

Soil Sampling and Analysis

Twenty (20) soil samples (SB-1 through SB-20) were collected between 0 and 2 feet BLS and analyzed for *Arsenic by EPA Method 6010*. The laboratory results indicate:

- None of the 20 samples analyzed were detected in exceedance of the RDE (2.1 mg/kg) or CIDE (12 mg/kg) SCTLs.
- Low levels of Arsenic were detected between the PQL and MDL, in SB-8 (0.39 mg/kg), SB-12 (0.38 mg/kg), and SB-13 (0.45 mg/kg); and above the MDL in SB-10 (0.69 mg/kg). However, all are below the SCTLs.

Visual Observations

The groundwater table was encountered at 4 to 5 feet depths in each of the borings completed.

A small amount of discarded material was encountered in borings SB-13, SB-13A, SB-14, and SB-14A located in the central area of the southern portion of Pond 4B-Option 2. Fragments of glass and pieces of metal rods where noted from 0 to 2 feet depth in these boring locations.

4.0 CONCLUSIONS

Based on the methodology and findings discussed in this report, Level II field screening indicates that contaminants of concern within the soils in the tested locations have not been identified.

- Arsenic was not detected in exceedance of the RDE (2.1 mg/kg) or CIDE (12 mg/kg) SCTLs in the 20 samples analyzed.
- Groundwater samples were not collected for laboratory analysis.
- No undesirable buried debris or petroleum odors were encountered in the borings completed during Level II field screening activities.
- In Pond 4B-Option 2, de minimis amounts of discarded material was observed from 0 to 1 feet depth in borings SB-13, SB-13A, SB-14, and SB-14A.

5.0 RECOMMENDATIONS

For sites ranked "No" or "Low", no additional work is recommended at this time. Should a facility's permitting or regulatory status change between now and the time acquisitions are initiated, additional screening should be conducted.

Testing for arsenic in soils at each pond location is required to identify areas of elevated arsenic levels (above the SCTLs), to establish proper management techniques and to determine disposal options of impacted soils.

- Soils that are identified to contain less than 2.1 mg/kg total arsenic RDE SCTL are unrestricted in the reuse and placement.
- The material observed in the southern portion of Pond 4B-Option 2 is not considered to be a contamination concern but should be removed and properly disposed of prior to construction activities.

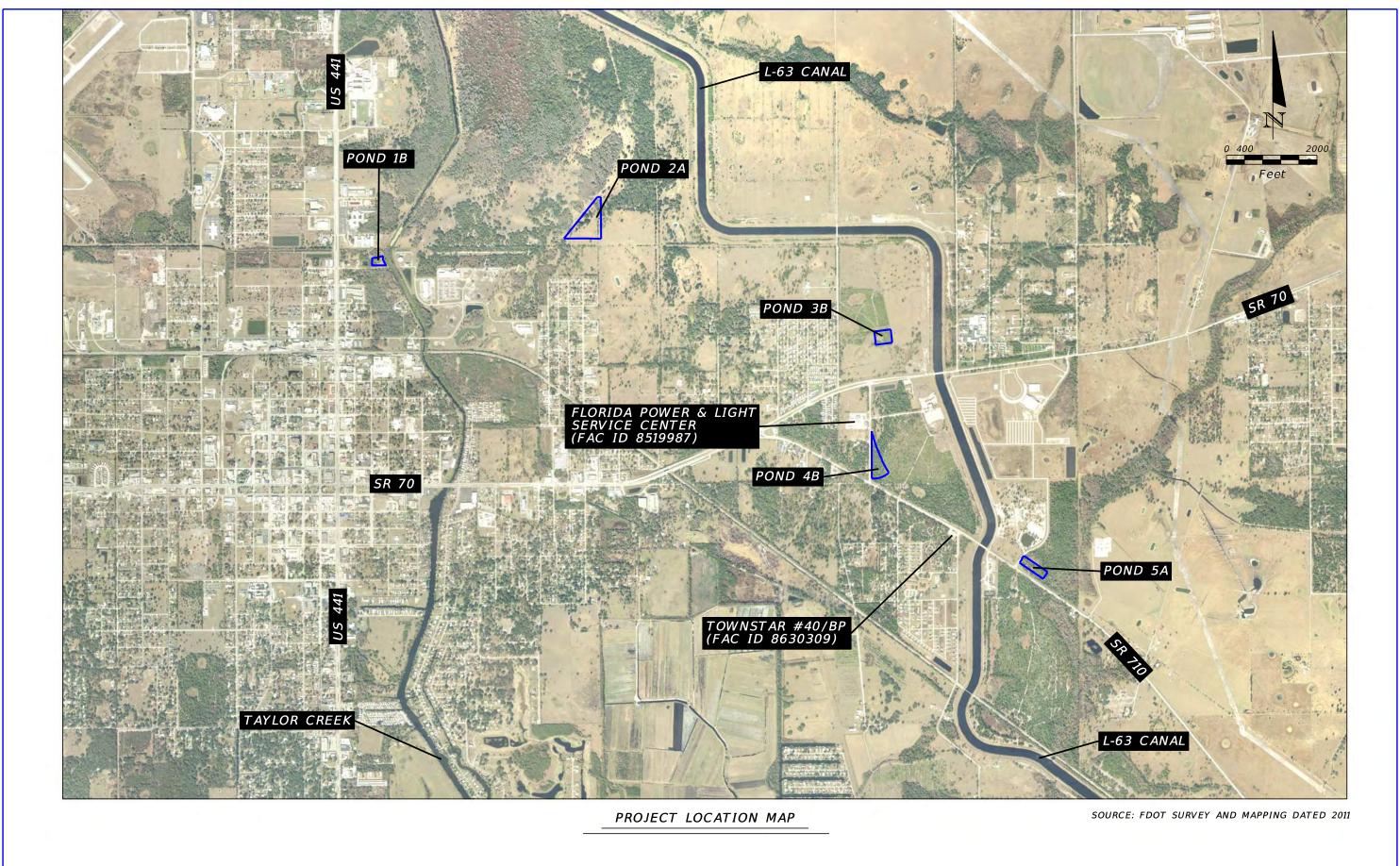
No additional assessment is recommended.

6.0 LIMITATIONS

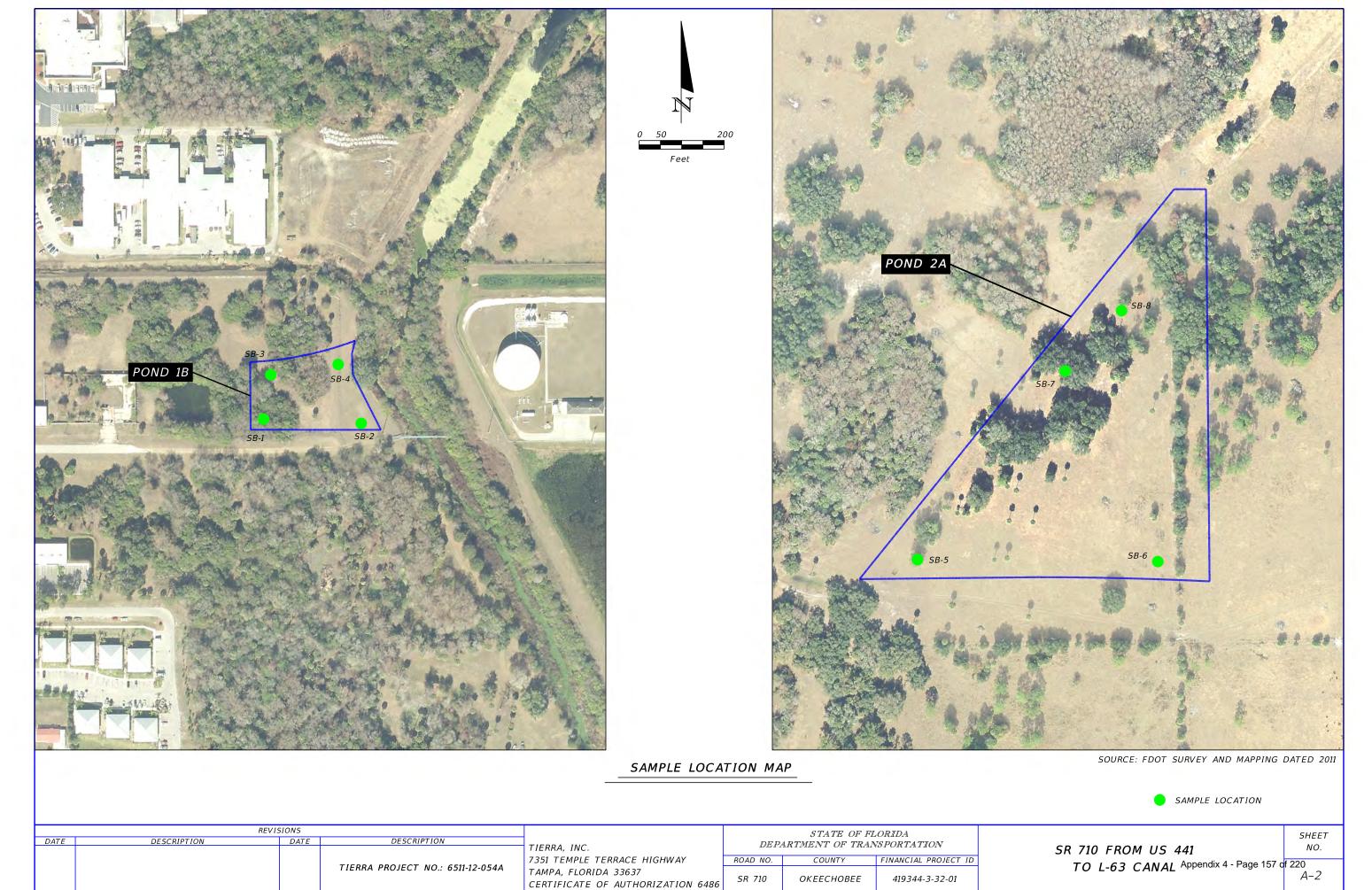
This study was conducted in a manner consistent with the level of care and skill ordinarily exercised by members of the profession currently practicing under similar conditions in the same locale. The results, findings, conclusions and recommendations expressed in this report are based on conditions observed during our course of work and under the scope of work authorized by the client. This report provides analytical results for a limited number of sample locations and should not be used to represent an assessment, but rather a Level II field screening that identifies the presence or absence of a tested contaminant. The information contained in this report is relevant to the date on which this survey was performed, and should not be relied upon to represent conditions at a later date. This report has been prepared on behalf of and exclusively for use by our client for specific application to their project as discussed above. Contractors or consultants reviewing this report must draw their own conclusions regarding further investigation or remediation deemed necessary. Tierra does not warrant the work of reporting agencies, laboratories or other third parties supplying information which may have been used in the preparation of this report. No warranty, expressed or implied is made.

Appendix A

Sheet 1 – Project Location Map Sheet 2 – Sample Location Map



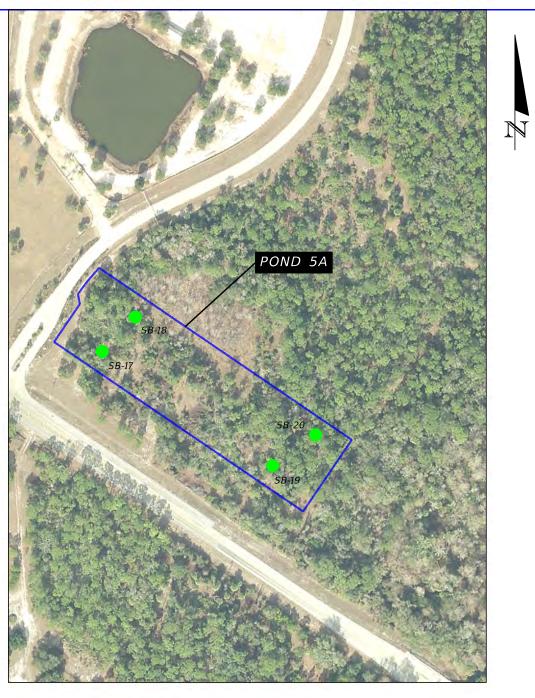
	REVISIONS			STATE OF FL	ORIDA		SHEET	
DATE	DESCRIPTION DATE	DESCRIPTION	DEDA DTWENT OF TRANSPORTATION		DEPARTMENT OF TRANSPORTATION			
			TIERRA, INC.	10121-1	antibalita or incar	STORIATION	SR 710 FROM US 441	NO.
			7351 TEMPLE TERRACE HIGHWAY	ROAD NO.	COUNTY	FINANCIAL PROJECT ID		
		TIERRA PROJECT NO.: 6511-12-054A	I ====================================				TO L-63 CANAL Appendix 4 - Page 156 of	1220
		71EMMA 7 NOSECT NO.: 0511-12-054A	TAMPA, FLORIDA 33637	CD 710	OKEECHOREE	410244222201	TO LOS CAMAL	$\Delta - 1$
			CERTIFICATE OF AUTHORIZATION 6486	SR 710	OKEECHOBEE	419344-3-32-01		/ 1 2
			CERTIFICATE OF AUTHORIZATION 6486					



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SAMPLE LOCATION MAP

SOURCE: FDOT SURVEY AND MAPPING DATED 2011

SAMPLE LOCATION

	REVISIONS					STATE OF FI	LORIDA		SHEET
DATE	DESCRIPTION	DATE	DESCRIPTION	TIERRA, INC.	DEPARTMENT OF TRANSPORTATION		SR 710 FROM US 441	NO.	
				7351 TEMPLE TERRACE HIGHWAY ROAD NO. COUNTY FINANCIAL PROJECT ID			f 220		
			TIERRA PROJECT NO.: 6511-12-054A TAMPA, FLORIDA 33637 CERTIFICATE OF AUTHORIZAT	TAMPA, FLORIDA 33637 CERTIFICATE OF AUTHORIZATION 6486	SR 710	OKEECHOBEE	419344-3-32-01	TO L-03 CANAL Appendix 1 rage 100 0	A-3

Appendix B

Table 1 – Soil Analytical Summary
Table 2 – GPS Coordinates

TABLE 1 – SOIL ANALYTICAL SUMMARY

TIERRA PROJECT NO: 6511-12-054A

	EPA METHOD 6010 (mg/kg)			
Pond Name	Sample ID	Sample Depth	Date Collected	Arsenic
	Reside	ntial Direct Exposu	re SCTL (mg/kg) $ ightarrow$	2.1
	Commercial/Indus	strial Direct Exposu	re SCTL (mg/kg) $ ightarrow$	12.0
		Leachabil	ity SCTL (mg/kg) \rightarrow	SPLP
Pond 1B	SB-1	0-2 feet	12/6/16	0.35 U
Pond 1B	SB-2	0-2 feet	12/6/16	0.30 U
Pond 1B	SB-3	0-2 feet	12/6/16	0.35 U
Pond 1B	SB-4	0-2 feet	12/6/16	0.30 U
Pond 2A-Option 1	SB-5	0-2 feet	12/6/16	0.28 U
Pond 2A-Option 1	SB-6	0-2 feet	12/6/16	0.27 U
Pond 2A-Option 1	SB-7	0-2 feet	12/6/16	0.36 U
Pond 2A-Option 1	SB-8	0-2 feet	12/6/16	0.39 I
Pond 3B	SB-9	0-2 feet	12/6/16	0.32 U
Pond 3B	SB-10	0-2 feet	12/6/16	0.69
Pond 3B	SB-11	0-2 feet	12/6/16	0.27 U
Pond 3B	SB-12	0-2 feet	12/6/16	0.38 I
Pond 4B-Option 2	SB-13	0-2 feet	12/6/16	0.45 I
Pond 4B-Option 2	SB-14	0-2 feet	12/6/16	0.29 U
Pond 4B-Option 2	SB-15	0-2 feet	12/6/16	0.32 U
Pond 4B-Option 2	SB-16	0-2 feet	12/6/16	0.27 U
Pond 5A	SB-17	0-2 feet	12/6/16	0.27 U
Pond 5A	SB-18	0-2 feet	12/6/16	0.29 U
Pond 5A	SB-19	0-2 feet	12/6/16	0.31 U
Pond 5A	SB-20	0-2 feet	12/6/16	0.31 U

NOTES:

mg/kg = milligrams per kilogram
SCTL = Soil Cleanup Target Level per Ch. 62-777, F.A.C.
U = Analyte not detected above noted concentration

I = Analyte detected between PQL and MDL; see lab report

BOLD concentration exceeds MDL

Highlighted concentration exceeds SCTL

TABLE 2 - GPS COORDINATES FOR BORINGS

TIERRA PROJECT NO: 6511-12-054A

Pond Name	Boring No.	Latitude	Longitude
Pond 1B	SB-1	27.2571243	-80.8274177
Pond 1B	SB-2	27.2570954	-80.8267112
Pond 1B	SB-3	27.2574110	-80.8273652
Pond 1B	SB-4	27.2574774	-80.8268771
Pond 2A-Option 1	SB-5	27.2587891	-80.8140458
Pond 2A-Option 1	SB-6	27.2587737	-80.8123055
Pond 2A-Option 1	SB-7	27.2600076	-80.8129738
Pond 2A-Option 1	SB-8	27.2603979	-80.8125652
Pond 3B	SB-9	27.2524804	-80.7929520
Pond 3B	SB-10	27.2527881	-80.7925552
Pond 3B	SB-11	27.2529194	-80.7930908
Pond 3B	SB-12	27.2530302	-80.7923218
Pond 4B-Option 2	SB-13	27.2446320	-80.7933240
Pond 4B-Option 2	SB-13A	27.2446640	-80.7933160
Pond 4B-Option 2	SB-14	27.2446950	-80.7932720
Pond 4B-Option 2	SB-14A	27.2446610	-80.7931670
Pond 4B-Option 2	SB-15	27.2456123	-80.7932164
Pond 4B-Option 2	SB-16	27.2462946	-80.7933328
Pond 5A	SB-17	27.2388684	-80.7832076
Pond 5A	SB-18	27.2390651	-80.7829964
Pond 5A	SB-19	27.2382126	-80.7821163
Pond 5A	SB-20	27.2383891	-80.7818402

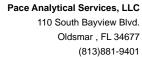
NOTES: Geographic Coordinate System: GCS_WGS_84
Geodetic Datum: D_WGS_84

Geodetic Datum: D_WGS_84
Prime Meridian: Greenwich
Angular Unit: Degree

The World Geodetic System 1984 (WGS84) is the reference coordinate system used by the Global Positioning System (GPS). WGS 84 was established in 1984 and last revised in 2004. The latitude and longitude of a point are reported in the Decimal Degrees format.

Appendix C

Laboratory Analytical Report





December 22, 2016

Clare Kramer Tierra, Inc. 7351 Temple Terrace Highway Tampa, FL 33637

RE: Project: SR710 Ponds- 6511-12054A

Pace Project No.: 35281680

Dear Clare Kramer:

Enclosed are the analytical results for sample(s) received by the laboratory on December 07, 2016. The results relate only to the samples included in this report. Results reported herein conform to the most current, applicable TNI/NELAC standards and the laboratory's Quality Assurance Manual, where applicable, unless otherwise noted in the body of the report.

If you have any questions concerning this report, please feel free to contact me.

Sincerely,

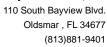
Lori Palmer lori.palmer@pacelabs.com

SA Palmer

Project Manager

Enclosures







CERTIFICATIONS

Project: SR710 Ponds- 6511-12054A

Pace Project No.: 35281680

Ormond Beach Certification IDs

8 East Tower Circle, Ormond Beach, FL 32174

Alabama Certification #: 41320 Connecticut Certification #: PH-0216

Delaware Certification: FL NELAC Reciprocity

Florida Certification #: E83079 Georgia Certification #: 955

Guam Certification: FL NELAC Reciprocity Hawaii Certification: FL NELAC Reciprocity

Illinois Certification #: 200068

Indiana Certification: FL NELAC Reciprocity

Kansas Certification #: E-10383

Louisiana Certification #: FL NELAC Reciprocity Louisiana Environmental Certificate #: 05007

Maryland Certification: #346 Michigan Certification #: 9911

Mississippi Certification: FL NELAC Reciprocity

Missouri Certification #: 236 Montana Certification #: Cert 0074 Nebraska Certification: NE-OS-28-14

Nevada Certification: FL NELAC Reciprocity

New York Certification #: 11608

North Carolina Environmental Certificate #: 667

North Carolina Certification #: 12710
Oklahoma Certification #: D9947
Pennsylvania Certification #: 68-00547
Puerto Rico Certification #: FL01264
South Carolina Certification: #96042001
Tennessee Certification #: TN02974
Texas Certification: FL NELAC Reciprocity

US Virgin Islands Certification: FL NELAC Reciprocity Virginia Environmental Certification #: 460165

Wyoming Certification: FL NELAC Reciprocity

West Virginia Certification #: 9962C Wisconsin Certification #: 399079670

Wyoming (EPA Region 8): FL NELAC Reciprocity

REPORT OF LABORATORY ANALYSIS



SAMPLE SUMMARY

Project: SR710 Ponds- 6511-12054A

Pace Project No.: 35281680

Lab ID	Sample ID	Matrix	Date Collected	Date Received
35281680001	SB-1	Solid	12/06/16 11:56	12/07/16 12:07
35281680002	SB-2	Solid	12/06/16 12:10	12/07/16 12:07
35281680003	SB-3	Solid	12/06/16 12:23	12/07/16 12:07
35281680004	SB-4	Solid	12/06/16 12:40	12/07/16 12:07
35281680005	SB-5	Solid	12/06/16 13:25	12/07/16 12:07
35281680006	SB-6	Solid	12/06/16 13:40	12/07/16 12:07
35281680007	SB-7	Solid	12/06/16 13:56	12/07/16 12:07
35281680008	SB-8	Solid	12/06/16 14:08	12/07/16 12:07
35281680009	SB-9	Solid	12/06/16 14:36	12/07/16 12:07
35281680010	SB-10	Solid	12/06/16 14:47	12/07/16 12:07
35281680011	SB-11	Solid	12/06/16 14:58	12/07/16 12:07
35281680012	SB-12	Solid	12/06/16 15:11	12/07/16 12:07
35281680013	SB-13	Solid	12/07/16 08:12	12/07/16 12:07
35281680014	SB-14	Solid	12/07/16 08:36	12/07/16 12:07
35281680015	SB-15	Solid	12/07/16 08:50	12/07/16 12:07
35281680016	SB-16	Solid	12/07/16 09:12	12/07/16 12:07
35281680017	SB-17	Solid	12/07/16 09:32	12/07/16 12:07
35281680018	SB-18	Solid	12/07/16 09:47	12/07/16 12:07
35281680019	SB-19	Solid	12/07/16 10:01	12/07/16 12:07
35281680020	SB-20	Solid	12/07/16 10:17	12/07/16 12:07

REPORT OF LABORATORY ANALYSIS



SAMPLE ANALYTE COUNT

Project: SR710 Ponds- 6511-12054A

Pace Project No.: 35281680

Lab ID	Sample ID	Method	Analysts	Analytes Reported	Laboratory
35281680001	SB-1	EPA 6010		1	PASI-O
		ASTM D2974-87	DRC	1	PASI-O
35281680002	SB-2	EPA 6010	JTJ	1	PASI-O
		ASTM D2974-87	DRC	1	PASI-O
35281680003	SB-3	EPA 6010	JTJ	1	PASI-O
		ASTM D2974-87	DRC	1	PASI-O
5281680004	SB-4	EPA 6010	JTJ	1	PASI-O
		ASTM D2974-87	DRC	1	PASI-O
5281680005	SB-5	EPA 6010	JTJ	1	PASI-O
		ASTM D2974-87	DRC	1	PASI-O
5281680006	SB-6	EPA 6010	JTJ	1	PASI-O
		ASTM D2974-87	DRC	1	PASI-O
5281680007	SB-7	EPA 6010	JTJ	1	PASI-O
		ASTM D2974-87	DRC	1	PASI-O
5281680008	SB-8	EPA 6010	JTJ	1	PASI-O
		ASTM D2974-87	DRC	1	PASI-O
5281680009	SB-9	EPA 6010	JTJ	1	PASI-O
		ASTM D2974-87	DRC	1	PASI-O
5281680010	SB-10	EPA 6010	JTJ	1	PASI-O
		ASTM D2974-87	DRC	1	PASI-O
5281680011	SB-11	EPA 6010	JTJ	1	PASI-O
		ASTM D2974-87	DRC	1	PASI-O
5281680012	SB-12	EPA 6010	JTJ	1	PASI-O
		ASTM D2974-87	DRC	1	PASI-O
5281680013	SB-13	EPA 6010	JTJ	1	PASI-O
		ASTM D2974-87	DRC	1	PASI-O
5281680014	SB-14	EPA 6010	JTJ	1	PASI-O
		ASTM D2974-87	DRC	1	PASI-O
5281680015	SB-15	EPA 6010	JTJ	1	PASI-O
		ASTM D2974-87	DRC	1	PASI-O
5281680016	SB-16	EPA 6010	JTJ	1	PASI-O
		ASTM D2974-87	DRC	1	PASI-O
5281680017	SB-17	EPA 6010	JTJ	1	PASI-O
		ASTM D2974-87	DRC	1	PASI-O
35281680018	SB-18	EPA 6010	JTJ	1	PASI-O
		ASTM D2974-87	DRC	1	PASI-O
35281680019	SB-19	EPA 6010	JTJ	1	PASI-O

REPORT OF LABORATORY ANALYSIS

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SAMPLE ANALYTE COUNT

Project: SR710 Ponds- 6511-12054A

Pace Project No.: 35281680

Lab ID	Sample ID	Method	Analysts	Analytes Reported	Laboratory
		ASTM D2974-87	DRC	1	PASI-O
35281680020	SB-20	EPA 6010	JTJ	1	PASI-O
		ASTM D2974-87	DRC	1	PASI-O



ANALYTICAL RESULTS

Project: SR710 Ponds- 6511-12054A

Pace Project No.: 35281680

Date: 12/22/2016 04:12 PM

Sample: SB-1 Lab ID: 35281680001 Collected: 12/06/16 11:56 Received: 12/07/16 12:07 Matrix: Solid

Parameters	Results	Units	PQL	MDL	DF	Prepared	Analyzed	CAS No.	Qual
6010 MET ICP	Analytical	Method: EPA	6010 Prepara	ation Meth	od: EP/	A 3050			
Arsenic	0.35 U	mg/kg	0.70	0.35	1	12/14/16 06:50	12/17/16 01:33	7440-38-2	
Percent Moisture	Analytical	Method: AST	M D2974-87						
Percent Moisture	16.1	%	0.10	0.10	1		12/14/16 11:00		



ANALYTICAL RESULTS

Project: SR710 Ponds- 6511-12054A

Pace Project No.: 35281680

Date: 12/22/2016 04:12 PM

Sample: SB-2 Lab ID: 35281680002 Collected: 12/06/16 12:10 Received: 12/07/16 12:07 Matrix: Solid

Parameters	Results	Units	PQL	MDL	DF	Prepared	Analyzed	CAS No.	Qual
6010 MET ICP	Analytical	Method: EPA	A 6010 Prepara	ation Meth	od: EP	A 3050			
Arsenic	0.30 U	mg/kg	0.60	0.30	1	12/14/16 06:50	12/17/16 01:51	7440-38-2	
Percent Moisture	Analytical	Method: AST	M D2974-87						
Percent Moisture	2.3	%	0.10	0.10	1		12/14/16 11:00		



ANALYTICAL RESULTS

Project: SR710 Ponds- 6511-12054A

Pace Project No.: 35281680

Date: 12/22/2016 04:12 PM

Sample: SB-3 Lab ID: 35281680003 Collected: 12/06/16 12:23 Received: 12/07/16 12:07 Matrix: Solid

Parameters	Results	Units	PQL	MDL	DF	Prepared	Analyzed	CAS No.	Qual
6010 MET ICP	Analytical	Method: EPA	A 6010 Prepara	ation Meth	od: EP	A 3050			
Arsenic	0.35 U	mg/kg	0.69	0.35	1	12/14/16 06:50	12/17/16 01:55	7440-38-2	
Percent Moisture	Analytical	Method: AST	M D2974-87						
Percent Moisture	11.4	%	0.10	0.10	1		12/14/16 11:00		J(D6)



ANALYTICAL RESULTS

Project: SR710 Ponds- 6511-12054A

Pace Project No.: 35281680

Date: 12/22/2016 04:12 PM

Sample: SB-4 Lab ID: 35281680004 Collected: 12/06/16 12:40 Received: 12/07/16 12:07 Matrix: Solid

Parameters	Results	Units	PQL	MDL	DF	Prepared	Analyzed	CAS No.	Qual
6010 MET ICP	Analytical	Method: EPA	6010 Prepar	ation Meth	od: EP	A 3050			
Arsenic	0.30 U	mg/kg	0.61	0.30	1	12/14/16 06:50	12/17/16 02:00	7440-38-2	
Percent Moisture	Analytical	Method: AST	M D2974-87						
Percent Moisture	5.0	%	0.10	0.10	1		12/14/16 11:01		



ANALYTICAL RESULTS

Project: SR710 Ponds- 6511-12054A

Pace Project No.: 35281680

Date: 12/22/2016 04:12 PM

Sample: SB-5 Lab ID: 35281680005 Collected: 12/06/16 13:25 Received: 12/07/16 12:07 Matrix: Solid

Parameters	Results	Units	PQL	MDL	DF	Prepared	Analyzed	CAS No.	Qual
6010 MET ICP	Analytical	Method: EPA	6010 Prepara	ation Meth	od: EP/	A 3050			
Arsenic	0.28 U	mg/kg	0.57	0.28	1	12/14/16 06:50	12/17/16 02:04	7440-38-2	
Percent Moisture	Analytical	Method: AST	M D2974-87						
Percent Moisture	6.6	%	0.10	0.10	1		12/14/16 11:01		

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ANALYTICAL RESULTS

Project: SR710 Ponds- 6511-12054A

Pace Project No.: 35281680

Date: 12/22/2016 04:12 PM

Sample: SB-6 Lab ID: 35281680006 Collected: 12/06/16 13:40 Received: 12/07/16 12:07 Matrix: Solid

Parameters	Results	Units	PQL	MDL	DF	Prepared	Analyzed	CAS No.	Qual
6010 MET ICP	Analytical	Method: EPA	6010 Prepara	ation Meth	od: EP/	A 3050			
Arsenic	0.27 U	mg/kg	0.54	0.27	1	12/14/16 06:50	12/17/16 02:18	7440-38-2	
Percent Moisture	Analytical	Method: AST	M D2974-87						
Percent Moisture	3.4	%	0.10	0.10	1		12/14/16 11:01		



ANALYTICAL RESULTS

Project: SR710 Ponds- 6511-12054A

Pace Project No.: 35281680

Date: 12/22/2016 04:12 PM

Sample: SB-7 Lab ID: 35281680007 Collected: 12/06/16 13:56 Received: 12/07/16 12:07 Matrix: Solid

Parameters	Results	Units	PQL _	MDL	DF	Prepared	Analyzed	CAS No.	Qual
6010 MET ICP	Analytical	Method: EPA	6010 Prepara	ation Metho	od: EP	A 3050			
Arsenic	0.36 U	mg/kg	0.71	0.36	1	12/14/16 06:50	12/17/16 02:22	7440-38-2	
Percent Moisture	Analytical	Method: AST	M D2974-87						
Percent Moisture	18.1	%	0.10	0.10	1		12/14/16 11:01		



ANALYTICAL RESULTS

Project: SR710 Ponds- 6511-12054A

Pace Project No.: 35281680

Date: 12/22/2016 04:12 PM

Sample: SB-8 Lab ID: 35281680008 Collected: 12/06/16 14:08 Received: 12/07/16 12:07 Matrix: Solid

Parameters	Results	Units	PQL	MDL	DF	Prepared	Analyzed	CAS No.	Qual
6010 MET ICP	Analytical	Method: EPA	6010 Prepar	ation Meth	od: EP	A 3050			
Arsenic	0.39 I	mg/kg	0.60	0.30	1	12/14/16 06:50	12/17/16 02:27	7440-38-2	
Percent Moisture	Analytical	Method: AST	M D2974-87						
Percent Moisture	9.9	%	0.10	0.10	1		12/14/16 11:01		



ANALYTICAL RESULTS

Project: SR710 Ponds- 6511-12054A

Pace Project No.: 35281680

Date: 12/22/2016 04:12 PM

Sample: SB-9 Lab ID: 35281680009 Collected: 12/06/16 14:36 Received: 12/07/16 12:07 Matrix: Solid

Parameters	Results	Units	PQL	MDL	DF	Prepared	Analyzed	CAS No.	Qual
6010 MET ICP	Analytical	Method: EPA	6010 Prepara	ation Meth	od: EP	A 3050			
Arsenic	0.32 U	mg/kg	0.64	0.32	1	12/14/16 06:50	12/17/16 02:31	7440-38-2	
Percent Moisture	Analytical	Method: AST	M D2974-87						
Percent Moisture	8.7	%	0.10	0.10	1		12/14/16 11:01		



ANALYTICAL RESULTS

Project: SR710 Ponds- 6511-12054A

Pace Project No.: 35281680

Date: 12/22/2016 04:12 PM

Sample: SB-10 Lab ID: 35281680010 Collected: 12/06/16 14:47 Received: 12/07/16 12:07 Matrix: Solid

Parameters	Results	Units	PQL	MDL	DF	Prepared	Analyzed	CAS No.	Qual
6010 MET ICP	Analytical	Method: EPA	6010 Prepar	ation Meth	od: EP	A 3050			
Arsenic	0.69	mg/kg	0.54	0.27	1	12/14/16 06:50	12/17/16 02:36	7440-38-2	
Percent Moisture	Analytical	Method: AST	M D2974-87						
Percent Moisture	15.5	%	0.10	0.10	1		12/14/16 11:01		



ANALYTICAL RESULTS

Project: SR710 Ponds- 6511-12054A

Pace Project No.: 35281680

Date: 12/22/2016 04:12 PM

Sample: SB-11 Lab ID: 35281680011 Collected: 12/06/16 14:58 Received: 12/07/16 12:07 Matrix: Solid

Parameters	Results	Units	PQL	MDL	DF	Prepared	Analyzed	CAS No.	Qual
6010 MET ICP	Analytical	Method: EPA	6010 Prepar	ation Meth	od: EP	A 3050			
Arsenic	0.27 U	mg/kg	0.53	0.27	1	12/14/16 06:50	12/17/16 02:40	7440-38-2	
Percent Moisture	Analytical	Method: AST	M D2974-87						
Percent Moisture	10.4	%	0.10	0.10	1		12/14/16 11:01		



ANALYTICAL RESULTS

Project: SR710 Ponds- 6511-12054A

Pace Project No.: 35281680

Date: 12/22/2016 04:12 PM

Sample: SB-12 Lab ID: 35281680012 Collected: 12/06/16 15:11 Received: 12/07/16 12:07 Matrix: Solid

Parameters	Results	Units	PQL	MDL	DF	Prepared	Analyzed	CAS No.	Qual
6010 MET ICP	Analytical	Method: EPA	6010 Prepar	ation Meth	od: EP	A 3050			
Arsenic	0.38 I	mg/kg	0.71	0.35	1	12/14/16 06:50	12/17/16 02:45	7440-38-2	
Percent Moisture	Analytical	Method: AST	M D2974-87						
Percent Moisture	27.1	%	0.10	0.10	1		12/14/16 11:01		





ANALYTICAL RESULTS

Project: SR710 Ponds- 6511-12054A

Pace Project No.: 35281680

Date: 12/22/2016 04:12 PM

Sample: SB-13 Lab ID: 35281680013 Collected: 12/07/16 08:12 Received: 12/07/16 12:07 Matrix: Solid

Parameters	Results	Units	PQL	MDL	DF	Prepared	Analyzed	CAS No.	Qual
6010 MET ICP	Analytical	Method: EPA	6010 Prepara	ation Meth	od: EP/	A 3050			
Arsenic	0.45 I	mg/kg	0.57	0.29	1	12/14/16 06:50	12/17/16 02:49	7440-38-2	
Percent Moisture	Analytical	Method: AST	M D2974-87						
Percent Moisture	5.7	%	0.10	0.10	1		12/14/16 11:02		



ANALYTICAL RESULTS

Project: SR710 Ponds- 6511-12054A

Pace Project No.: 35281680

Date: 12/22/2016 04:12 PM

Sample: SB-14 Lab ID: 35281680014 Collected: 12/07/16 08:36 Received: 12/07/16 12:07 Matrix: Solid

Parameters	Results	Units	PQL	MDL	DF	Prepared	Analyzed	CAS No.	Qual
6010 MET ICP	Analytical	Method: EPA	6010 Prepar	ation Meth	od: EP	A 3050			
Arsenic	0.29 U	mg/kg	0.59	0.29	1	12/14/16 06:50	12/17/16 02:54	7440-38-2	
Percent Moisture	Analytical	Method: AST	M D2974-87						
Percent Moisture	3.2	%	0.10	0.10	1		12/14/16 11:02		



ANALYTICAL RESULTS

Project: SR710 Ponds- 6511-12054A

Pace Project No.: 35281680

Date: 12/22/2016 04:12 PM

Sample: SB-15 Lab ID: 35281680015 Collected: 12/07/16 08:50 Received: 12/07/16 12:07 Matrix: Solid

Parameters	Results	Units	PQL	MDL	DF	Prepared	Analyzed	CAS No.	Qual
6010 MET ICP	Analytical	Method: EPA	6010 Prepara	ation Meth	od: EP/	A 3050			
Arsenic	0.32 U	mg/kg	0.63	0.32	1	12/14/16 06:50	12/17/16 02:59	7440-38-2	
Percent Moisture	Analytical	Method: AST	M D2974-87						
Percent Moisture	3.1	%	0.10	0.10	1		12/14/16 11:02		



ANALYTICAL RESULTS

Project: SR710 Ponds- 6511-12054A

Pace Project No.: 35281680

Date: 12/22/2016 04:12 PM

Sample: SB-16 Lab ID: 35281680016 Collected: 12/07/16 09:12 Received: 12/07/16 12:07 Matrix: Solid

Parameters	Results	Units	PQL	MDL	DF	Prepared	Analyzed	CAS No.	Qual
6010 MET ICP	Analytical	Method: EPA	6010 Prepara	ation Meth	od: EP/	A 3050			
Arsenic	0.27 U	mg/kg	0.54	0.27	1	12/14/16 06:50	12/17/16 03:12	7440-38-2	
Percent Moisture	Analytical	Method: AST	M D2974-87						
Percent Moisture	2.5	%	0.10	0.10	1		12/14/16 11:02		



ANALYTICAL RESULTS

Project: SR710 Ponds- 6511-12054A

Pace Project No.: 35281680

Date: 12/22/2016 04:12 PM

Sample: SB-17 Lab ID: 35281680017 Collected: 12/07/16 09:32 Received: 12/07/16 12:07 Matrix: Solid

Parameters	Results	Units	PQL	MDL	DF	Prepared	Analyzed	CAS No.	Qual
6010 MET ICP	Analytical	Method: EPA	6010 Prepara	ation Meth	od: EP	A 3050			
Arsenic	0.27 U	mg/kg	0.55	0.27	1	12/14/16 06:50	12/17/16 03:17	7440-38-2	
Percent Moisture	Analytical	Method: AST	M D2974-87						
Percent Moisture	7.9	%	0.10	0.10	1		12/14/16 11:02		



ANALYTICAL RESULTS

Project: SR710 Ponds- 6511-12054A

Pace Project No.: 35281680

Date: 12/22/2016 04:12 PM

Sample: SB-18 Lab ID: 35281680018 Collected: 12/07/16 09:47 Received: 12/07/16 12:07 Matrix: Solid

Parameters	Results	Units	PQL	MDL	DF	Prepared	Analyzed	CAS No.	Qual
6010 MET ICP	Analytical	Method: EPA	6010 Prepara	ation Meth	od: EP	A 3050			
Arsenic	0.29 U	mg/kg	0.58	0.29	1	12/14/16 06:50	12/17/16 03:21	7440-38-2	
Percent Moisture	Analytical	Method: AST	M D2974-87						
Percent Moisture	8.1	%	0.10	0.10	1		12/14/16 11:02		



ANALYTICAL RESULTS

Project: SR710 Ponds- 6511-12054A

Pace Project No.: 35281680

Date: 12/22/2016 04:12 PM

Sample: SB-19 Lab ID: 35281680019 Collected: 12/07/16 10:01 Received: 12/07/16 12:07 Matrix: Solid

Parameters	Results	Units	PQL	MDL	DF	Prepared	Analyzed	CAS No.	Qual
6010 MET ICP	Analytical	Method: EPA	6010 Prepara	ation Meth	od: EP/	A 3050			
Arsenic	0.31 U	mg/kg	0.61	0.31	1	12/14/16 06:50	12/17/16 03:26	7440-38-2	
Percent Moisture	Analytical	Method: AST	M D2974-87						
Percent Moisture	8.3	%	0.10	0.10	1		12/14/16 11:02		



ANALYTICAL RESULTS

Project: SR710 Ponds- 6511-12054A

Pace Project No.: 35281680

Date: 12/22/2016 04:12 PM

Sample: SB-20 Lab ID: 35281680020 Collected: 12/07/16 10:17 Received: 12/07/16 12:07 Matrix: Solid

Parameters	Results	Units	PQL	MDL	DF	Prepared	Analyzed	CAS No.	Qual
6010 MET ICP	Analytical	Method: EPA	6010 Prepar	ation Meth	od: EP	A 3050			
Arsenic	0.31 U	mg/kg	0.62	0.31	1	12/14/16 12:24	12/22/16 10:07	7440-38-2	
Percent Moisture	Analytical	Method: AST	M D2974-87						
Percent Moisture	9.5	%	0.10	0.10	1		12/14/16 11:02		

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QUALITY CONTROL DATA

Project: SR710 Ponds- 6511-12054A

Pace Project No.: 35281680

Date: 12/22/2016 04:12 PM

QC Batch: 338388 Analysis Method: EPA 6010
QC Batch Method: EPA 3050 Analysis Description: 6010 MET Solid

Associated Lab Samples: 35281680001, 35281680002, 35281680003, 35281680004, 35281680005, 35281680006, 35281680007,

35281680008, 35281680009, 35281680010, 35281680011, 35281680012, 35281680013, 35281680014,

35281680015, 35281680016, 35281680017, 35281680018, 35281680019

METHOD BLANK: 1813684 Matrix: Solid

Associated Lab Samples: 35281680001, 35281680002, 35281680003, 35281680004, 35281680005, 35281680006, 35281680007,

35281680008, 35281680009, 35281680010, 35281680011, 35281680012, 35281680013, 35281680014,

35281680015, 35281680016, 35281680017, 35281680018, 35281680019

Reporting Blank Parameter Result Limit MDL Qualifiers Units Analyzed Arsenic 0.31 U 0.62 0.31 12/17/16 01:24 mg/kg LABORATORY CONTROL SAMPLE: 1813685 LCS LCS % Rec Spike Parameter Units Conc. Result % Rec Limits Qualifiers Arsenic mg/kg 13.7 12.7 92 80-120

MATRIX SPIKE & MATRIX SPIKE DUPLICATE: 1813686 1813687 MS MSD MSD MS MSD 35281680001 Spike Spike MS % Rec Max Parameter Units Result Conc. Conc. Result Result % Rec % Rec Limits RPD RPD Qual mg/kg 0.35 U 16.9 17.8 13.3 78 75-125 20 Arsenic 13.8 77

Results presented on this page are in the units indicated by the "Units" column except where an alternate unit is presented to the right of the result.



QUALITY CONTROL DATA

Project: SR710 Ponds- 6511-12054A

Pace Project No.: 35281680

Date: 12/22/2016 04:12 PM

QC Batch: 338516 Analysis Method: EPA 6010
QC Batch Method: EPA 3050 Analysis Description: 6010 MET Solid

Associated Lab Samples: 35281680020

LABORATORY CONTROL SAMPLE: 1814148

Spike LCS LCS % Rec Parameter Units Conc. Result % Rec Limits Qualifiers Arsenic mg/kg 13.9 12.7 91 80-120

MATRIX SPIKE & MATRIX SPIKE DUPLICATE: 1814150 1814149 MSD MS MS MSD MS MSD 35281816006 Spike Spike % Rec Max Parameter Units Result Conc. Conc. Result Result % Rec % Rec Limits RPD RPD Qual 75-125 20 J(M1), 16.2 26.1 18.6 79 34 Arsenic mg/kg 9.3 21.4 58 J(R1)

MATRIX SPIKE & MATRIX SPIKE DUPLICATE: 1814256 1814257 MS MSD MS MS 35281816007 Spike Spike MSD MSD % Rec Max Parameter Units Result Conc. Result % Rec % Rec RPD RPD Qual Conc. Result Limits Arsenic mg/kg 5.0 22.9 27.5 26.9 31.6 96 97 75-125 16 20

Results presented on this page are in the units indicated by the "Units" column except where an alternate unit is presented to the right of the result.



QUALITY CONTROL DATA

Project: SR710 Ponds- 6511-12054A

Pace Project No.: 35281680

Parameter

Percent Moisture

Date: 12/22/2016 04:12 PM

QC Batch: 338449 Analysis Method: ASTM D2974-87

Units

%

QC Batch Method: ASTM D2974-87 Analysis Description: Dry Weight/Percent Moisture

Associated Lab Samples: 35281680001, 35281680002, 35281680003, 35281680004, 35281680005, 35281680006, 35281680007,

35281680012

Result

27.1

35281680008, 35281680009, 35281680010, 35281680011, 35281680012, 35281680013, 35281680014,

35281680015, 35281680016, 35281680017, 35281680018, 35281680019, 35281680020

SAMPLE DUPLICATE: 1813914 35279909001 Dup Max RPD **RPD** Units Result Qualifiers Parameter Result 95.7 94.7 10 Percent Moisture % SAMPLE DUPLICATE: 1813915 35281680003 Dup Max Parameter Units Result Result **RPD** RPD Qualifiers Percent Moisture 11.4 9.8 10 J(D6) % 15 SAMPLE DUPLICATE: 1813916

Dup

Result

25.2

RPD

7

Max

RPD

10

Qualifiers

Results presented on this page are in the units indicated by the "Units" column except where an alternate unit is presented to the right of the result.



QUALIFIERS

Project: SR710 Ponds- 6511-12054A

Pace Project No.: 35281680

DEFINITIONS

DF - Dilution Factor, if reported, represents the factor applied to the reported data due to dilution of the sample aliquot.

ND - Not Detected at or above adjusted reporting limit.

MDL - Adjusted Method Detection Limit.

PQL - Practical Quantitation Limit.

RL - Reporting Limit.

S - Surrogate

1,2-Diphenylhydrazine decomposes to and cannot be separated from Azobenzene using Method 8270. The result for each analyte is a combined concentration.

Consistent with EPA guidelines, unrounded data are displayed and have been used to calculate % recovery and RPD values.

LCS(D) - Laboratory Control Sample (Duplicate)

MS(D) - Matrix Spike (Duplicate)

DUP - Sample Duplicate

RPD - Relative Percent Difference

NC - Not Calculable.

SG - Silica Gel - Clean-Up

U - Indicates the compound was analyzed for, but not detected.

N-Nitrosodiphenylamine decomposes and cannot be separated from Diphenylamine using Method 8270. The result reported for each analyte is a combined concentration.

Pace Analytical is TNI accredited. Contact your Pace PM for the current list of accredited analytes.

TNI - The NELAC Institute.

LABORATORIES

PASI-O Pace Analytical Services - Ormond Beach

ANALYTE QUALIFIERS

Date: 12/22/2016 04:12 PM

I The reported value is between the laboratory method detection limit and the laboratory practical quantitation limit.

U Compound was analyzed for but not detected.

J(D6) Estimated Value. The relative percent difference (RPD) between the sample and sample duplicate exceeded laboratory control limits.

J(M1) Estimated Value. Matrix spike recovery exceeded QC limits. Batch accepted based on laboratory control sample (LCS) recovery.

J(R1) Estimated Value. RPD value was outside control limits.



QUALITY CONTROL DATA CROSS REFERENCE TABLE

Project: SR710 Ponds- 6511-12054A

Pace Project No.: 35281680

Date: 12/22/2016 04:12 PM

Lab ID	Sample ID	QC Batch Method	QC Batch	Analytical Method	Analytica Batch
35281680001	SB-1	EPA 3050	338388	EPA 6010	338508
35281680002	SB-2	EPA 3050	338388	EPA 6010	338508
35281680003	SB-3	EPA 3050	338388	EPA 6010	338508
35281680004	SB-4	EPA 3050	338388	EPA 6010	338508
35281680005	SB-5	EPA 3050	338388	EPA 6010	338508
35281680006	SB-6	EPA 3050	338388	EPA 6010	338508
35281680007	SB-7	EPA 3050	338388	EPA 6010	338508
35281680008	SB-8	EPA 3050	338388	EPA 6010	338508
35281680009	SB-9	EPA 3050	338388	EPA 6010	338508
35281680010	SB-10	EPA 3050	338388	EPA 6010	338508
5281680011	SB-11	EPA 3050	338388	EPA 6010	338508
35281680012	SB-12	EPA 3050	338388	EPA 6010	338508
35281680013	SB-13	EPA 3050	338388	EPA 6010	338508
35281680014	SB-14	EPA 3050	338388	EPA 6010	338508
35281680015	SB-15	EPA 3050	338388	EPA 6010	338508
35281680016	SB-16	EPA 3050	338388	EPA 6010	338508
5281680017	SB-17	EPA 3050	338388	EPA 6010	338508
5281680018	SB-18	EPA 3050	338388	EPA 6010	338508
5281680019	SB-19	EPA 3050	338388	EPA 6010	338508
5281680020	SB-20	EPA 3050	338516	EPA 6010	338661
35281680001	SB-1	ASTM D2974-87	338449		
35281680002	SB-2	ASTM D2974-87	338449		
5281680003	SB-3	ASTM D2974-87	338449		
5281680004	SB-4	ASTM D2974-87	338449		
5281680005	SB-5	ASTM D2974-87	338449		
5281680006	SB-6	ASTM D2974-87	338449		
35281680007	SB-7	ASTM D2974-87	338449		
35281680008	SB-8	ASTM D2974-87	338449		
35281680009	SB-9	ASTM D2974-87	338449		
35281680010	SB-10	ASTM D2974-87	338449		
5281680011	SB-11	ASTM D2974-87	338449		
5281680012	SB-12	ASTM D2974-87	338449		
5281680013	SB-13	ASTM D2974-87	338449		
5281680014	SB-14	ASTM D2974-87	338449		
5281680015	SB-15	ASTM D2974-87	338449		
35281680016	SB-16	ASTM D2974-87	338449		
5281680017	SB-17	ASTM D2974-87	338449		
35281680018	SB-18	ASTM D2974-87	338449		
5281680019	SB-19	ASTM D2974-87	338449		
35281680020	SB-20	ASTM D2974-87	338449		

WO#:35281680

S. Required Client Information:	Required Project Information:	Section C Invoice Information:		ă	Page:	4
	Report To: Awad, Sammy	Attention:		J N		
11 Temple Terrace Highway	Copy To:	Company Name:			Constitution Action	
	Purchase Order #:	Pace Quote:			regulatory Age	69
Phone:	Project Name: SR710 Ponds - 6511-12-054A	anager:	lori.palmer@pacelabs.com,		State / Location	
	Project #:	Pace Profile #: 7064-4	Requested Analys	Analysis Filtered (Y/N)	చ	
	(fiel of	Preservatives	N/A		ī	
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	act face	127/10/2000 FLX		12/1/16/2000		
		J WW I	-277 11	21-11425:40	7.77	5
	SAMPLER NAME AND SIGNATURE	ND SIGNATURE				
	PRINT Name of	Name of SAMPLER: SAMMAN HUSAC			oni GM Deviec	stody led bel
	SIGNATURE of SAMPLER:	Y	DATE Signed:	1111		Sea Goo (Y/)



CHAIN-OF-CUSTODY / Analytical Request Document The Chain-of-Custody is a LEGAL DOCUMENT. All relevant fields must be completed accurately.

	Man Sallilly	Allenion.			
7351 Temple Terrace Highway Cop	Copy To:	Company Name:			
	77-1-0	Address:			Regulatory Agency
Phone: Frankr @ Lierre 2011. Cow Pur	Purchase Order #: Project Name: SR710 Ponds - 6511-12-054A	Pace Project Manager:	ager: lori.palmer@pacelabs.com,		State / Location
	oject #:	Pace Profile #:	7064-4 Requested	Requested Analysis Filtered (Y/N)	Ft.
MATRIX	O H (fiel of se		Preservatives ×		
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(A-4, U-3 f) Sample Ids must be unique Tissue	TO THE DATE TIME DATE	TIME SAMPLE TE SAMPLE TE	HCI NaOH Neihanol Other Analy Arsonic		Residual C
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	with Pace	12/1/16/2000	FLX	12/1/12000	
	SAMPLER NAME AND	R NAME AND SIGNATURE			
	PRINT Name of SAMPLER:	SAMPLER: Sammy	Awad		ybola
	SIGNATURE of SAMPLER:		DATE Signed:	d: 17/2/16	Rec (Y/N Cus Seal



Project Manager Review:

Document Name Sample Condition Upon Receipt Form Document No.

Document Revised: August 10, 2016 Issuing Authority. Pace Florida Quality Office

ACONIEDA #:35281680

Project # PM: LAP

Date and Initials of person: Examining contents:

Project Manager: CLIENT: 37-TIETPA Label: Deliver: Date \2/7/6 Thermometer Used: Time 23 40 Initials: Samples shorted to lab (If Yes, complete) Shorted Date. Shorted Time. Qty: Cooler #1 Temp. C 26 (Visual) To 1 (Correction Factor) 1 (Actual) Samples on ice cooling process has begun Cooler #2 Temp. C___ ____(Visual) ______(Correction Factor) ______(Actual) Samples on ice, cooling process has begun Cooler #3 Temp. C (Visual) (Actual) Samples on ice, cooling process has begun Cooler #4 Temp. C __(Visual) _____(Correction Factor) ____ ___(Actual) Samples on ice, cooling process has begun Cooler #5 Temp. C___ ____(Visual) ______(Correction Factor) ______(Actual) Samples on ice, cooling process has begun Cooler #6 Temp. C_____(Visual) ______(Correction Factor)_____(Actual) Samples on ice, cooling process has begun Fed Ex UPS USPS Client Commercial Pace Other____ Shipping Method: ☐ First Overnight ☐ Priority Overnight ☐ Standard Overnight ☐ Ground ☐ Other____ Billing: Recipient D Sender D Third Party D Unknown Tracking # Custody Seal on Cooler/Box Present: Yes Seals intact: Yes No Ice: Wet Blue (None / MO Packing Material: Bubble Wrap Bubble Bags . None Other____ Comments: Chain of Custody Present ⊠Yes □ No □N/A Chain of Custody Filled Out ZYes [No DN/A Relinquished Signature & Sampler Name COC TYPES INO LINIA Samples Arrived within Hold Time ☑Yes ☐ No _N/A Rush TAT requested on COC DYes ZNo UN/A Sufficient Volume ☑Yes ☐ No ☐N/A Correct Containers Used ZiYes DNO DNIA Containers Intact ZiYes Ti No TINA Sample Labels match COC (sample IDs & date/time of LIYES I NO LINA All containers needing acid/base preservation have been Preservation Information. checked DYes T No TN/A Preservative_ All Containers needing preservation are found to be in Lot #/Trace # compliance with EPA recommendation: TYES I NO LINIA Date Exceptions: VOA, Coliform, TOC, O&G, Carbamates Headspace in VOA Vials? (>6mm). □Yes □ No ZN/A Trip Blank Present: DYes INO ZNIA Client Notification Resolution: Person Contacted: Date/Time Comments/ Resolution (use back for additional comments):

Date:

Appendix D

Soil Boring Logs

Kend	Sik	18												Page 1 of
	Well Num	iber:				Permit	Number				FDEP Fac	cility Iden	tificatio	n Number:
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	mental C	ontracto.	г:			Geolog	ist's Name:				Environm	ental Tec	hnician	i's Name:
TIERR	A, INC.					Clare I	Kramer				Sammy A	wad		
Drilling	Company	у;			Paveme	nt Thickr	ness (inches	3):	Borehole Dia	ameter (inches):	E	Borehole	Depth ((feef):
TIERR	A, INC.					1	AV			3.25			6	
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Disposi	tion of Dri	ill Cutting	gs (check n	nethod(s)]	: [_ Dru	n 🖵	Spread	[₹E	Backfill	Stockpile	T	Other	
(descrit	e if other	r or multi _l	ole items a	re checke	d):			- ,		·	•	·		
Boreho	e Comple	etion (ch	eck one);		Well Well	Γ	Grout	∏ В	entonite	Backfill	[○	ther (de:	scribe)	
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Sample Type	Sample Depth Interval (feet)	Sample Recovery (inches)	SPT Blows (per six inches)	Unfiltered OVA	Filtered OVA	Net OVA	Depth (feet)	(Inclu	ide grain siz	le Description e based on USC and other remark		USCS Symbol	Moisture Content	Lab Soil and Groundwater Samples (list sample number and depth or temporary screen
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								on; ST	Shelby Tub	e; DP = Direct i	Push; SC:	Sonic C	ore; D	C = Drill Cuffings
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<u>Rond</u>	Sik	18_			 .			******						Page 1 of
Boring/	Well Num	ber;				Permit	Number:				FDEP F	acility Iden	tification	n Number:
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TIERR	A, INC.					Clare I	Kramer				Sammy	/ Awad		
Drilling	Company	r.			Paveme	nt Thickr	ness (Inches)):	Borehole Dia	meter (inches):		Borehole	Depth (feet):
TIERR	A, INC.					l	NA.			3.25			6	1
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Boreho	le Comple	etjon (cha	eck one);		┌ Well	Γ	Grout	Г. в	entonite	[Backfill	Г.	Other (de	scribe)	•
Sample Type	Sample Depth Interval (feet)	Sample Recovery (inches)	SPT Blows (per six inches)	Unfiltered OVA	Filtered OVA	Net OVA	Depth (feet)	(în c lı	ude grain siza staining, a	le Description e based on USC and other reman		USCS Symbol	Moisture Content	Lab Soil and Groundwater Samples (list sample number and depth or temporary screen interval)
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	RA, INC.				····	Clare Kr		·		Sammy A			
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3oring/V	Well Numi	ber:				Permit Nu	umber:				FDEP Fa	adlify Ideni	iffication	n Number:
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Oritling '	Company	ŗ.			Рачетег	it Thickne	ss (inches)):	Borehole Dia	ameter (inches):	`	Borehole l	Depth (1	feet):
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TIERRA, INC.		Clare Kramer			Sammy A			
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Sample Type	Sample Depth Interval (feet)	Sample Recovery (Inches)	SPT Blows (per six inches)	Unflitered OVA	Filtered OVA	Net OVA	Depth (feet)	(inc	lude grain size	e Description e based on US nd other remat		USCS Symbol	Moisture Content	Lab Soil and Groundwater Samples (list sample number and depth or temporary screen interval)
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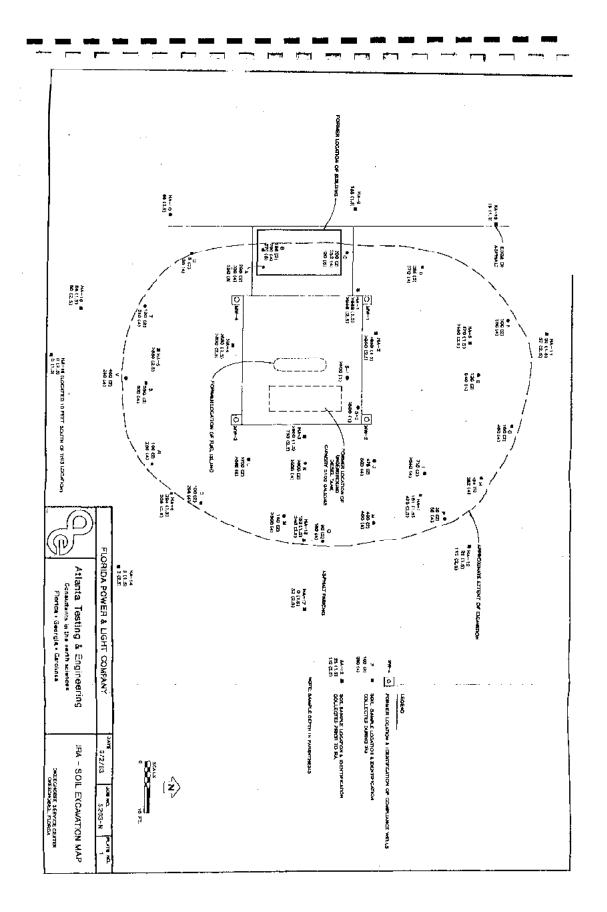
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Appendix 5 Cultural Resource Assessment Survey (CRAS) of Proposed Pond Sites (April 2015) & Cultural Resource Assessment Survey (CRAS) of Preferred Pond Sites (November 2016)

CULTURAL RESOURCE ASSESSMENT SURVEY OF PREFERRED POND SITES SR 710 FROM US 441 TO THE L-63N CANAL OKEECHOBEE COUNTY, FLORIDA

Financial Project No.: 419344-3-32-01 Federal Project No.: NA

Prepared for:

Federal Highway Administration 545 John Knox Road Suite 200 Tallahassee, Florida 32303

and the:

Florida Department of Transportation
District One
P.O. Box
Bartow, Florida 33830-1249

April 2015

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On Behalf of:

Wantman Group, Inc. 213 South Dillard Street, Suite 210 Winter Garden, Florida 34787

Prepared by:

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CULTURAL RESOURCE ASSESSMENT SURVEY OF PREFERRED POND SITES SR 710 FROM US 441 TO THE L-63N CANAL OKEECHOBEE COUNTY, FLORIDA

Financial Project ID.: 419344-3-32-01 Federal Aid Project ID: NA

1. Executive Summary

Archaeological Consultants, Inc. (ACI) conducted a cultural resource assessment survey (CRAS) of 17 pond sites along the new SR 710 proposed alignment, from the intersection with US 441 to south of the L-63N Canal (Interceptor Creek), Okeechobee County, Florida (**Figure 1**). The purpose was to locate and identify any cultural resources within the area of potential effects (APE), and to assess their significance in terms of eligibility for listing at the national level in the National Register of Historic Places (NRHP). The CRAS was conducted in February 2014.

Background research indicated that no historic or prehistoric archaeological sites or historic structures were recorded within the APE, which was defined as the area contained in each pond site. As a result of field investigations, no prehistoric archaeological sites or historic structures were identified within the APE.

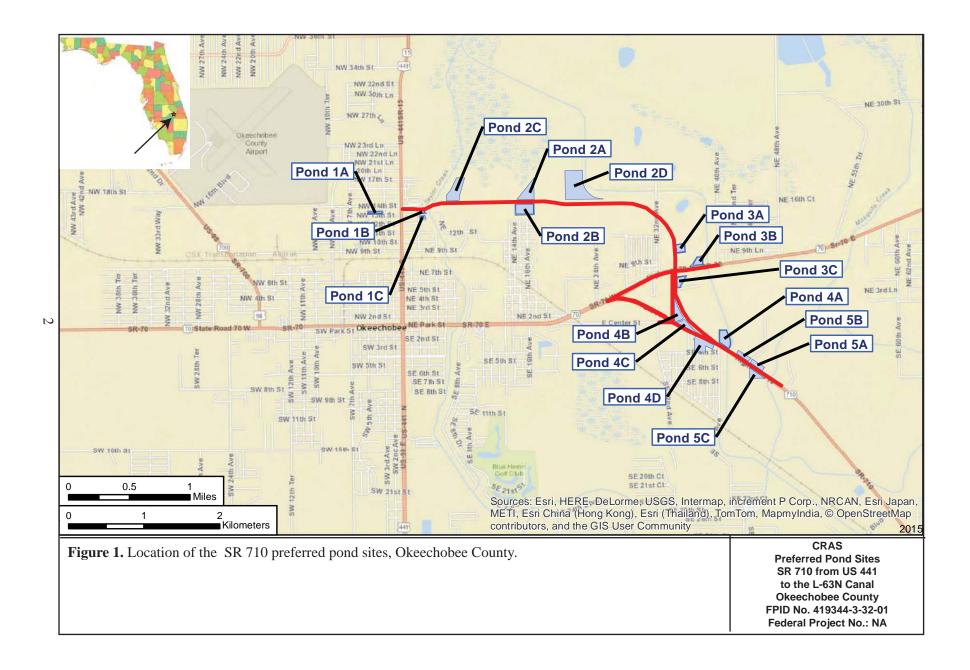
Based on the results of the CRAS, this undertaking will have no effect on resources listed, determined eligible, or potentially eligible for listing in the NRHP.

2. Introduction

The purpose of the survey was to locate and identify any archaeological sites and historic resources located within the APE and to assess their significance in terms of eligibility for listing in the NRHP. This work was conducted in compliance with the provision of the National Historic Preservation Act of 1966 (Public Law 89-665), as amended; The Archaeological and Historic Preservation Act (Public Law 93-291) as amended; Executive Order 11593; and Chapter 267, Florida Statutes (FS). All work was carried out in conformity with Part 2, Chapter 12 (Archaeological and Historical Resources) of the Florida Department of Transportation's (FDOT) Project Development and Environment (PD&E) Manual (FDOT 1999) and complies with the standards contained in the Florida Division of Historic Resources' (FDHR) Cultural Resource Management Standards and Operational Manual (FDHR 2003).

3. <u>Project Description</u>

The project is located on SR 710, in Okeechobee County, Florida. The proposed project is a new alignment that begins at the intersection with US 441 and extends south easterly to



south of the L-63N Canal (Interceptor Creek), where it ties into the existing SR 710, in Okeechobee, Florida.

The new alignment of SR 710 has a total project length of approximately 3.8 miles (mi), and it is designated as an Urban and Rural Principal Arterial and a Strategic Intermodal System (SIS) facility. The existing SR 710 is currently classified by FDOT as an Access Management Class four facility. The proposed access classification for the new roadway extension is class three from US 441 to Taylor Creek and class two from Taylor Creek to SR 70, the remainder of the corridor would be classified as class three from SR 70 to Mosquito Creek. The design speed for the entire facility is 50 miles-per-hour (mph).

A four-lane high speed suburban typical section is proposed. The roadway will consist of two 12-foot (ft) wide travel lanes in each direction, separated by a raised 30-ft wide grassed median. This roadway section will also include 4-ft shoulders to the inside of the travel lanes and 6.5-ft (8-ft useable) shoulders adjacent to the outside travel lanes. Type E curb and gutter will be provided along the median and outside edges of the roadway along with a closed stormwater conveyance system. A continuous 5-ft wide concrete sidewalk will be provided on the south side of the roadway and a 10-ft wide shared-use path will be provided on the north side of the roadway. Appropriate left and/or right turn lanes will be provided at major intersections. This high-speed urban typical section has a 29-ft border width and is to be constructed within 160 ft minimum of right-of-way (ROW). The surrounding land uses consist primarily of large areas of rangeland, pastureland, residential developments, and rural residences (Wantman Group 2014).

4. Environmental Overview

This proposed undertaking is located in portions of Sections 13-16, and 24, Township 37 South, Range 35 East (**Figure 2**). Elevation of the general area is 20-25 ft above mean sea level (amsl).

Examination of the Okeechobee and Taylor Creek SE, Florida USGS quadrangle maps (USGS 1952, 1953), the *Okeechobee County Soil Survey* (United States Department of Agriculture [USDA] 1971, 2003), and a visual reconnaissance of the area revealed that the natural landscape of the survey area has somewhat been altered by development as a result of agriculture, commercial, and residential development (**Photos 1 and 2**). Based on a review of soil data prior to development (USDA 1971), the most common local soil types in the survey area was poorly drained soil of the broad flatwoods and open prairies (USDA 1971:3-4). The soil in the project APE is part of the Myakka-Basinger general soil association.

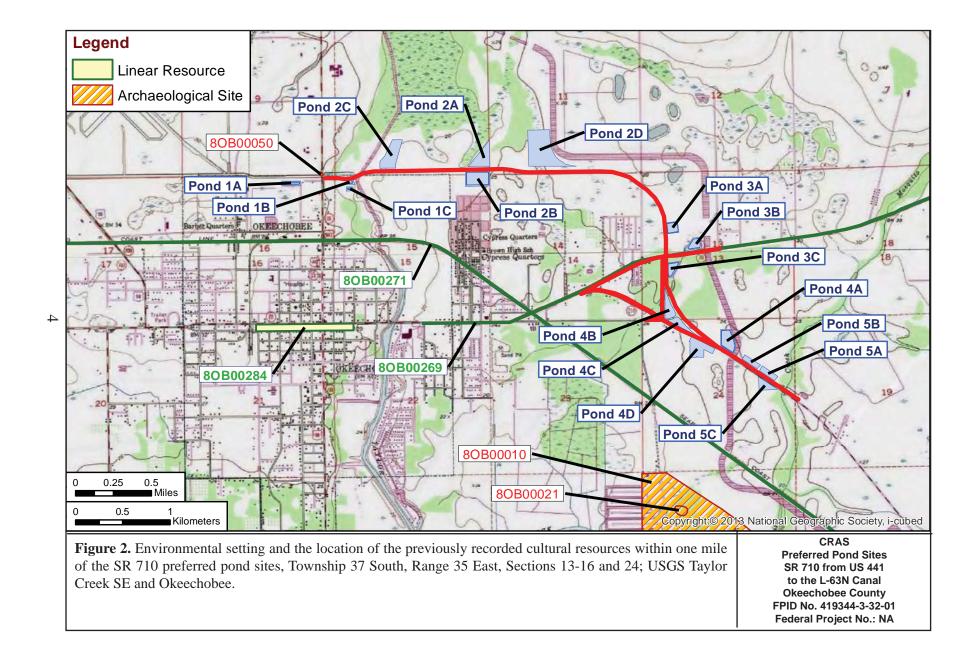




Photo 1. Looking north at Pond 2A.



Photo 2. Looking southeast towards Pond 4D.

5. Prehistoric Overview

An extensive prehistoric overview was included in the CRAS for the SR 710 PD&E Study from US 441 to CR 714 (SW Martin Avenue) in Okeechobee and Martin Counties (Janus Research 2010). Therefore, the prehistory is not repeated here.

6. Archaeological Background and Considerations

Archaeological: Prior to initiating the archaeological and historical survey for this project, ACI reviewed information at the Florida Master Site File (FMSF). This was followed by a review of previous archaeological surveys in the vicinity (ACI 2005, 2006, 2007a/b, 2010; Arbuthnot and Savage 2006; Beiter 2003; Coughlin 2010; Estabrook 1992; Janus Research 2000, 2001; PBS&J 2010) including the CRAS conducted for the project area (Janus Research 2010)

and the Preliminary Pond Memorandum (ACI 2013). Although several historic and prehistoric archaeological sites are recorded within one mile of the APE (**Figure 2; Table 1**), as a result of these surveys, no significant (NRHP eligible) prehistoric or historic archaeological sites were found within the project APE.

The research also revealed that archaeological sites in the Okeechobee Basin are quite different from those in other parts of peninsula Florida. Typically, the types of sites found within the Okeechobee Basin include earthworks, burial mounds, and habitation mounds or middens. Among the more spectacular sites are large earthworks found in the open savannah, often bordering creeks or major environmental zones. Earthwork types include circular ditches, linear embankments, and combined mound and midden embankments. However, this research identified no prehistoric archaeological resources within or near the proposed undertaking.

The data demonstrated that archaeological sites in Okeechobee County near and within the APE would most likely be located on better drained to somewhat poorly drained soils near a permanent or semi-permanent source of potable water such as seasonal depressions, sloughs, and ponds where foods such as fish, shellfish, and aquatic plants are readily accessible. The data also suggested that because of the urban setting and disturbances caused by the infrastructure, including buried cables, ditches, and other utilities, the potential for sites was very low.

Table 1. Previously recorded cultural resources within one mile.

Site No.	Site Name	Site Type	Cultural Period	NRHP Eligible	Recorder
8OB10	Okeechobee Battlefield	Military	American Historic 1821-45	NRHP Eligible	Carr 1975
8OB21	Hazelieff	Artifact Scatter; Historic Refuse	Belle Glade; American Late 19 th , Early 20 Century	Not Evaluated	AHC 1987
8OB50	City Limits	Single Artifact	Unknown	Ineligible	Janus Research 1995
8OB269	Okeechobee Road	Linear Resource	American 19 th Century	Ineligible	ACI 2007a, b, 2010; Janus Research 2010
8OB271	Seaboard Airline Railroad	Railroad	American 20 th Century	NRHP Eligible	Janus Research 2010
8OB284	Flagler Park	Historic Landscape	American 20 th Century	Ineligible	PBS&J 2010

Historic: Finally, although no historic archaeological sites were anticipated, portions of SR 70, adjacent to the APE, has been recorded in the FMSF (Okeechobee Road, 8OB269). As noted in **Figure 2**, Proposed Pond 3B is adjacent to 8OB269, and Proposed Pond 3C is south of the resource (**Figure 2**; **Table 1**; ACI 2006, 2007). The FMSF form for 8OB269 was updated in 2010 (Janus Research 2010), and the State Historic Preservation Office (SHPO) determined the resource was not eligible for listing in the NRHP. Therefore, no update was required during this survey.

7. Methods

Archaeological field survey methods: included both ground surface reconnaissance and judgmental subsurface shovel testing. To the extent possible, each shovel test pit measured .5 m

(20 inches [in]) in diameter and was dug to a depth of 1 m (3.3 ft) unless impeded by water. Soil from each test pit was screened through a 6.3 millimeter (mm) (.25 in) mesh hardware cloth to maximize the recovery of artifacts. The location of all shovel tests was plotted on the aerials, and, following the recording of relevant data such as stratigraphic profile, all test pits were refilled.

Interviews: One informant interview was conducted with the property owners of the area contained in Pond 5B, Jerry and Nancy Jolicoeur. They stated no archaeological material has ever been recovered from their land and they have not heard of anyone else finding artifacts on their property or in the general area (Jolicoeur 2014).

Laboratory Methods: No artifacts were found, therefore no laboratory or curation methods are included.

Curation of all project related materials (field notes, photos, maps, etc.) will take place at ACI in Sarasota, pending transfer to a FDOT designated repository. In addition, a copy of the CRAS report and Survey Log will be curated and on file at the FDHR in Tallahassee.

Unexpected Discoveries: If human burial sites such as Indian mounds, lost historic and prehistoric cemeteries, or other unmarked burials or associated artifacts were found, then the provisions and guidelines set forth in Chapter 872.05, *F.S.* (Florida's Unmarked Burial Law) would be followed. However, it was not anticipated that such sites would be found during survey.

8. Results and Summary

Archaeological Results: As a result of the archaeological field survey, 54 shovel test pits (TP) were placed judgmentally in 16 of the 17 pond sites (**Figures 3, 4; Table 2**). None of the TPs was positive and the soil stratigraphy was variable. Sample stratigraphy consisted of: 0-30 cm (0-12 in) of grey sand, 30-80 cm (12-31 in) of light grey/tan sand, and 80-100 cm (31-39 in) of dark brown hardpan; 0-50 cm (0-20 in) of black sandy-clay muck, 50-70 cm (20-28 in) of wet grey sand, and 70-100+ cm (28-39 in) of water; and 0-35 cm (0-14 in) of very dark grey/brown loam; 35-70 cm (13-28 in) of mottled grey/brown sandy loam, and 70-100 cm (28-39 in) of mottled light grey/brown sandy loam. The one pond (2D) not tested will be once the preferred ponds are chosen.

Historical Results: As a result of field survey and a visual reconnaissance, no historic structures were found to be located within the APE. This is in keeping with the background research.

Summary: As a result of background results and archaeological field survey, no prehistoric or historic sites were found within any of the 16 pond sites tested (APE). In addition, the proposed undertaking also will not impact that portion of SR 70 (8OB269) previously recorded adjacent to the project APE; this resource is not considered eligible for listing in the NRHP.

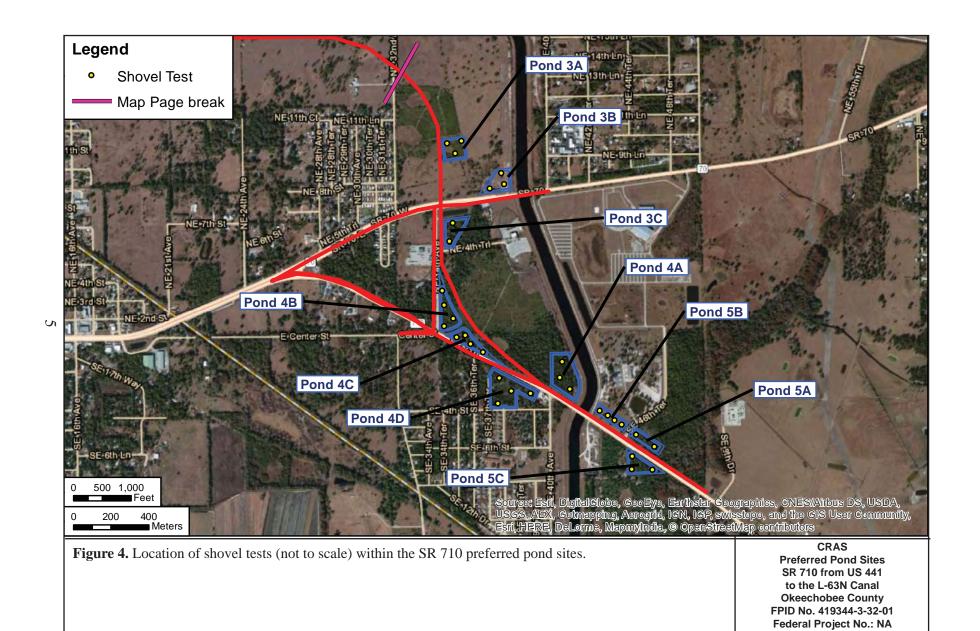
Table 2. Archaeological data.

Pond ID.	Acres	Soil Type, Elevation, Drainage, and Environmental Association	*ZAPs/Comments	Test Pits
1A	2.238	Immokalee fine sand: Nearly level, poorly drained in broad flatwoods	Low	2
1B	1.203	Manatee, Delray, and Okeelanta soils Nearly level, very poorly drained on marshy plains	Low	1
1C	.9290	Manatee, Delray, and Okeelanta soils Nearly level, very poorly drained on marshy plains	Low	1
2A	14.227	Immokalee fine sand Nearly level, poorly drained in broad flatwoods	Moderate	6
2B	15.372	Immokalee fine sand Nearly level, poorly drained in broad flatwoods	Moderate	8
2C	6.864	Pompano fine sand Nearly level, poorly drained in grassy sloughs and depressions	Low	4
2D	28	Immokalee fine sand Nearly level, poorly drained in broad flatwoods	Moderate	0
3A	4.181	Basinger and Pompano fine sands Nearly level, poorly drained, in sloughs and isolated depressions in the flatwoods Immokalee fine sand Nearly level, poorly drained in broad flatwoods	Low	3
3B	7.244	Immokalee fine sand Nearly level, poorly drained in broad flatwoods	Low	3
3C	5.778	Immokalee fine sand Nearly level, poorly drained in broad flatwoods	Low; a portion previously tested with negative results (Janus Research 2010)	2
4A	7.882	Myakka fine sand: Nearly level, poorly drained in broad flatwoods Placid fine sand: Nearly level, very poorly drained in low areas	Low	3
4B	8.168	Immokalee fine sand Nearly level, poorly drained in broad flatwoods	Moderate	4
4C	Combined with 4B	Immokalee fine sand Nearly level, poorly drained in broad flatwoods	Moderate; dilapidated sheds, ca. 1990 (not historic)	4
4D	8.616	Myakka fine sand: Nearly level, poorly drained in broad flatwoods Immokalee fine sand: Nearly level, poorly drained in broad flatwoods	Low	4
5A	2.624	Immokalee fine sand: Nearly level, poorly drained in broad flatwoods	Low	2
5B	2.534	Immokalee fine sand: Nearly level, poorly drained in broad flatwoods	Moderate	4
5C	3.528	Immokalee fine sand: Nearly level, poorly drained in broad flatwoods	Low	3

^{*} Zone of Archaeological Potential

Figure 3. Location of shovel tests (not to scale) within the SR 710 preferred pond sites. Pond 2D will be tested after preferred ponds are chosen.

CRAS
Preferred Pond Sites
SR 710 from US 441
to the L-63N Canal
Okeechobee County
FPID No. 419344-3-32-01
Federal Project No.: NA



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Wantman Group, Inc.

2014 Project Description for Pond Sites Provided to ACI, Sarasota.

Ent D (FMSF only)



Survey Log Sheet

Florida Master Site File

Survey # (FMSF only)

Consult Guide to the Survey Log Sheet for detailed instructions.

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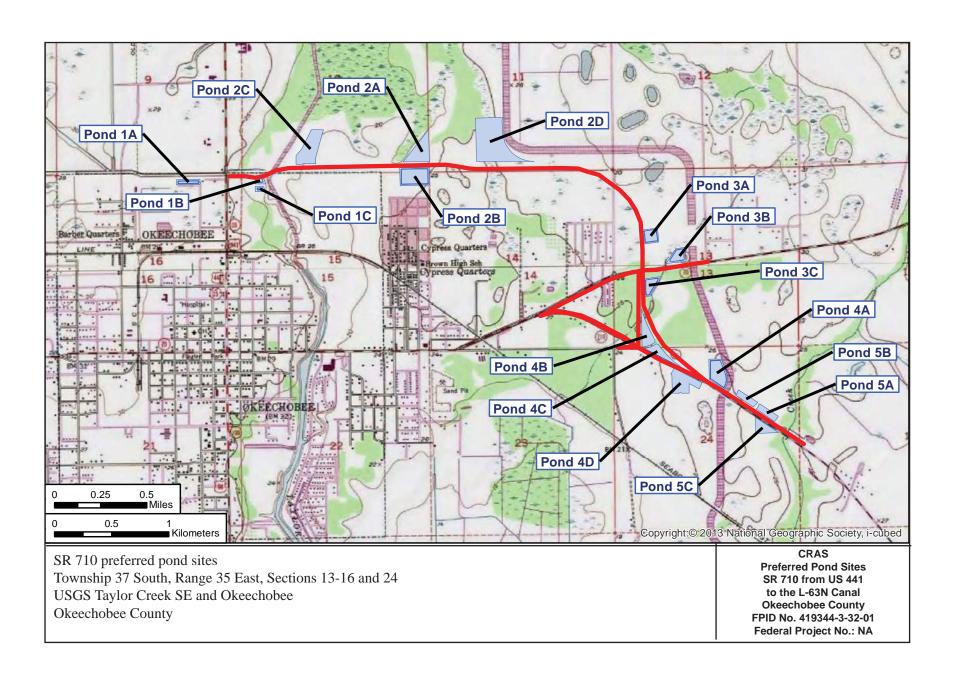
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CULTURAL RESOURCE ASSESSMENT SURVEY OF PREFERRED POND SITES SR 710 FROM US 441 TO THE L-63N CANAL OKEECHOBEE COUNTY, FLORIDA

Financial Project No.: 419344-3-32-01 Federal Project No.: NA

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Federal Highway Administration 545 John Knox Road Suite 200 Tallahassee, Florida 32303

and the:

Florida Department of Transportation District One P.O. Box Bartow, Florida 33830-1249

November 2016

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Financial Project ID.: 419344-3-32-01 Federal Aid Project ID: NA

1. <u>Executive Summary</u>

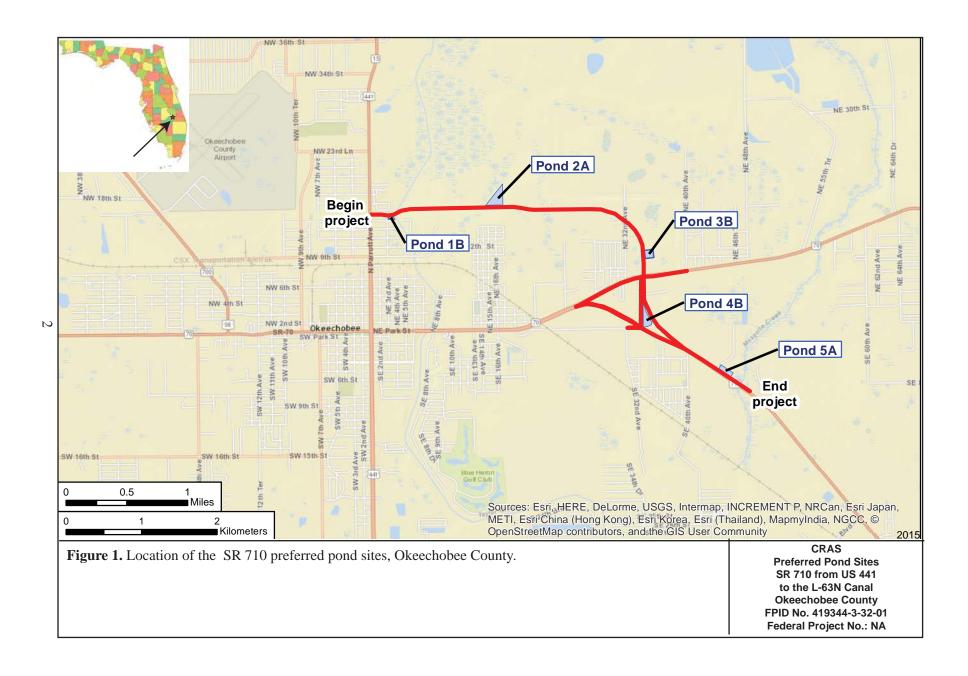
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Background research indicated that no historic or prehistoric archaeological sites or historic structures were recorded within the APE. The archaeological and historic APE is defined as the area contained within each pond site. As a result of field investigations, no prehistoric archaeological sites or historic buildings or structures were identified within the APE.

Based on the results of the CRAS, this undertaking will have no effect on resources listed, determined eligible, or potentially eligible for listing in the NRHP.

2. Introduction

The purpose of the survey was to locate and identify any archaeological sites and historic resources located within the APE and to assess their significance in terms of eligibility for listing in the NRHP. This work was conducted in compliance with the provision of the National Historic Preservation Act of 1966 (Public Law 89-665), as amended; The Archaeological and Historic Preservation Act (Public Law 93-291) as amended; Executive Order 11593; and Chapter 267, Florida Statutes (FS). All work was carried out in conformity with Part 2, Chapter 12 (Archaeological and Historical Resources) of the Florida Department of Transportation's (FDOT) Project Development and Environment (PD&E) Manual (FDOT 2016) and complies with the standards contained in the Florida Division of Historic Resources' (FDHR) Cultural Resource Management Standards and Operational Manual (FDHR 2003).



3. Project Description

The project is located on SR 710 in Okeechobee County, Florida. The proposed project is a new alignment that begins at the intersection with US 441 and extends south easterly to south of the L-63N Canal (Interceptor Creek), where it ties into the existing SR 710 in Okeechobee, Florida.

The new alignment of SR 710 is approximately 3.8 miles (mi) in length, and it is designated as an Urban and Rural Principal Arterial and a Strategic Intermodal System (SIS) facility. The existing SR 710 is currently classified by FDOT as an Access Management Class four facility. The proposed access classification for the new roadway extension is class three from US 441 to Taylor Creek and class two from Taylor Creek to SR 70, the remainder of the corridor would be classified as class three from SR 70 to Mosquito Creek. The design speed for the entire facility is 50 miles-per-hour (mph).

A four-lane high speed suburban typical section is proposed. The roadway will consist of two 12-foot (ft) wide travel lanes in each direction, separated by a raised 30-ft wide grassed median. This roadway section will also include 4-ft shoulders to the inside of the travel lanes and 6.5-ft (8-ft useable) shoulders adjacent to the outside travel lanes. Type E curb and gutter will be provided along the median and outside edges of the roadway along with a closed storm-water conveyance system. A continuous 5-ft wide concrete sidewalk will be provided on the south side of the roadway and a 10-ft wide shared-use path will be provided on the north side of the roadway. Appropriate left and/or right turn lanes will be provided at major intersections. This high-speed urban typical section has a 29-ft border width and is to be constructed within 160 ft minimum of right-of-way (ROW). The surrounding land uses consist primarily of large areas of rangeland, pastureland, residential developments, and rural residences (Wantman Group 2014).

4. Environmental Overview

The proposed undertaking is located in portions of Sections 13-16, and 24, Township 37 South, Range 35 East (**Figure 2**). Elevation of the general area is 20-25 ft above mean sea level (amsl).

Examination of the Okeechobee and Taylor Creek SE, Florida United States Geological Survey (USGS) quadrangle maps (USGS 1952, 1953), the *Okeechobee County Soil Survey* (United States Department of Agriculture [USDA] 1971, 2003), and a visual reconnaissance of the area revealed that the natural landscape of the survey area has somewhat been altered by development as a result of agriculture, commercial, and residential development (**Photos 1 and 2**). Based on a review of soil data prior to development (USDA 1971), the most common local soil types in the survey area was poorly drained soil of the broad flatwoods and open prairies (USDA 1971:3-4). The soil in the project APE is part of the Myakka-Basinger general soil association.

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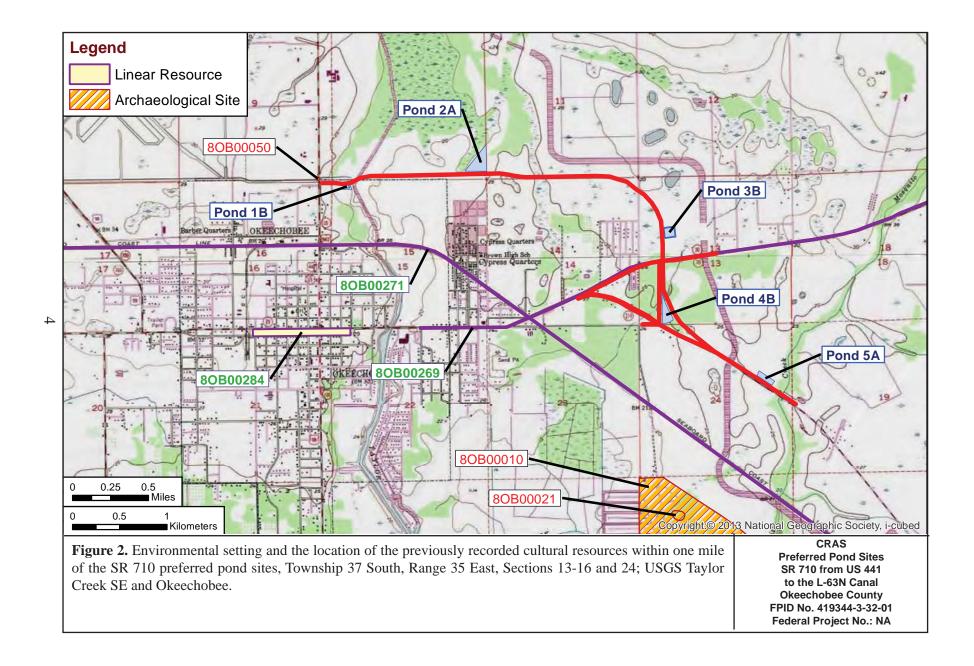




Photo 1. Looking north at Pond 2A.



Photo 2. Looking northwest at Pond 5A.

5. <u>Prehistoric Overview</u>

An extensive prehistoric overview was included in the CRAS for the SR 710 PD&E Study from US 441 to CR 714 (SW Martin Avenue) in Okeechobee and Martin Counties (Janus Research 2010). Therefore, the prehistory is not repeated here.

6. Archaeological Background and Considerations

Archaeological: Prior to initiating the archaeological and historical survey for this project, ACI reviewed information at the Florida Master Site File (FMSF). This was followed by a review of previous archaeological surveys in the vicinity (ACI 2005, 2006, 2007a/b, 2010; Arbuthnot and Savage 2006; Beiter 2003; Coughlin 2010; Estabrook 1992; Janus Research 2000, 2001; PBS&J 2010) including the CRAS conducted for the project area (Janus Research 2010) the Preliminary Pond Memorandum (ACI 2013), and a technical memorandum of 17 pond sites (ACI 2015). Although several historic and prehistoric archaeological sites are recorded within one mile of the APE (Figure 2; Table 1), as a result of these surveys, no significant (NRHP eligible) prehistoric or historic archaeological sites were found within the project APE.

The research also revealed that archaeological sites in the Okeechobee Basin are quite different from those in other parts of peninsula Florida. Typically, the types of sites found within the Okeechobee Basin include earthworks, burial mounds, and habitation mounds or middens. Among the more spectacular sites are large earthworks found in the open savannah, often bordering creeks or major environmental zones. Earthwork types include circular ditches, linear embankments, and combined mound and midden embankments. However, this research identified no prehistoric archaeological resources within or near the proposed undertaking.

Prehistoric settlement data demonstrates that archaeological sites in Okeechobee County near and within the APE would most likely be located on better drained to somewhat poorly drained soils near a permanent or semi-permanent source of potable water such as seasonal depressions, sloughs, and ponds where foods such as fish, shellfish, and aquatic plants are readily accessible. The data also suggest that because of the urban setting and disturbances caused by the infrastructure, including buried cables, ditches, and other utilities, the potential for sites was very low.

Table 1. Previously recorded cultural resources within one mile.

Site No.	Site Name	Site Type	Cultural Period	NRHP Eligible	Recorder
8OB00010	Okeechobee Battlefield	Military	American Historic 1821-45	NRHP Eligible	Carr 1975
8OB00021	Hazelieff	Artifact Scatter; Historic Refuse	Belle Glade; American Late 19 th , Early 20 Century	Not Evaluated	AHC 1987
8OB00050	City Limits	Single Artifact	Unknown	Ineligible	Janus Research 1995
8OB00269	Okeechobee Road	Linear Resource	American 19 th Century	Ineligible	ACI 2007a, b, 2010; Janus Research 2010
8OB00271	Seaboard Airline Railroad	Railroad	American 20 th Century	NRHP Eligible	Janus Research 2010
8OB00284	Flagler Park	Historic Landscape	American 20 th Century	Ineligible	PBS&J 2010

Historic: Although no historic archaeological sites were anticipated, portions of SR 70, adjacent to the APE, have been recorded in the FMSF (Okeechobee Road, 8OB00269). As noted in **Figure 2**, Pond 3C is south of this linear resource (**Figure 2**; **Table 1**; ACI 2006, 2007). The FMSF form for 8OB00269 was updated in 2010 (Janus Research 2010), and the State Historic Preservation Office (SHPO) determined the resource was not eligible for listing in the NRHP. Therefore, no update was required during this survey.

7. Methods

Archaeological field survey methods: included both ground surface reconnaissance and judgmental subsurface shovel testing. To the extent possible, each shovel test pit measured .5 meter (m) (20 inches [in]) in diameter and was dug to a depth of 1 m (3.3 ft) unless impeded by water. Soil from each test pit was screened through a 6.3 millimeter (mm) (.25 in) mesh hardware cloth to maximize the recovery of artifacts. The location of all shovel tests was plotted on the aerials, and, following the recording of relevant data such as stratigraphic profile, all test pits were refilled.

Interviews: No interviews were conducted in relation to any of the five preferred pond sites.

Laboratory Methods: No artifacts were found, therefore no laboratory or curation methods are included.

Curation of all project related materials (field notes, photos, maps, etc.) will take place at ACI (P12087) in Sarasota, pending transfer to a FDOT designated repository. In addition, a copy of the CRAS report and Survey Log will be curated and on file at the FDHR in Tallahassee.

Unexpected Discoveries: If human burial sites such as Indian mounds, lost historic and prehistoric cemeteries, or other unmarked burials or associated artifacts were found, then the provisions and guidelines set forth in Chapter 872.05, *FS* (Florida's Unmarked Burial Law) would be followed. However, it was not anticipated that such sites would be found during survey.

8. Results and Summary

Archaeological Results: As a result of the archaeological field survey, 16 shovel test pits (TP) were placed judgmentally in the pond sites (**Figures 3, 4; Table 2**). None of the TPs was positive and the soil stratigraphy was variable. Sample stratigraphy consisted of: 0-30 cm (0-12 in) of grey sand, 30-80 cm (12-31 in) of light grey/tan sand, and 80-100 cm (31-39 in) of dark brown hardpan; 0-50 cm (0-20 in) of black sandy-clay muck, 50-70 cm (20-28 in) of wet grey sand, and 70-100+ cm (28-39 in) of water; and 0-35 cm (0-14 in) of very dark grey/brown loam; 35-70 cm (13-28 in) of mottled grey/brown sandy loam, and 70-100 cm (28-39 in) of mottled light grey/brown sandy loam.

Historical Results: As a result of field survey, including a visual reconnaissance, no historic structures were found to be located within the APE. This is in keeping with the background research.

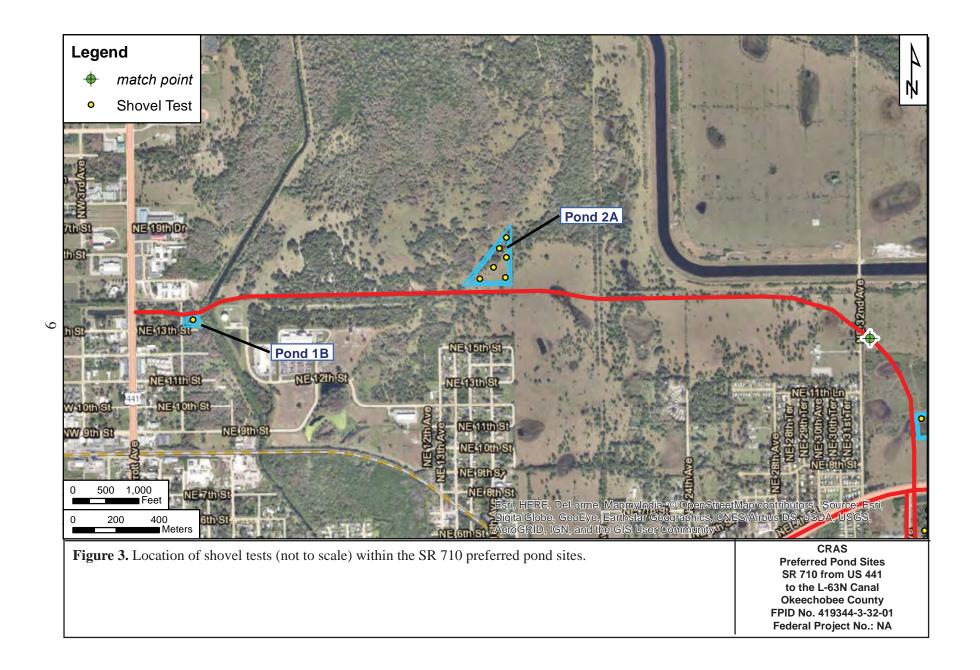
Summary: As a result of background results and archaeological field survey, no prehistoric or historic sites were found within any of the five pond sites tested (APE). In addition, the proposed undertaking also will not impact that portion of SR 70 (8OB00269) previously recorded adjacent to the project APE; this resource is not considered eligible for listing in the NRHP.

 Table 2. Archaeological data.

Pond ID.	Acres	Soil Type, Elevation, Drainage, and Environmental Association	*ZAPs/Comments	Test Pits
1B	1.203	Manatee, Delray, and Okeelanta soils Nearly level, very poorly drained on marshy plains	Low	1
2A	14.227	Immokalee fine sand Nearly level, poorly drained in broad flatwoods	Moderate	6
3В	4.181	Basinger and Pompano fine sands Nearly level, poorly drained, in sloughs and isolated depressions in the flatwoods Immokalee fine sand Nearly level, poorly drained in broad flatwoods	Low	3
4B	8.168	Immokalee fine sand Nearly level, poorly drained in broad flatwoods	Moderate	4
5A	2.624	Immokalee fine sand: Nearly level, poorly drained in broad flatwoods	Low	2

^{*} Zone of Archaeological Potential

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to the L-63N Canal Okeechobee County FPID No. 419344-3-32-01 Federal Project No.: NA

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Wantman Group, Inc.

2014 Project Description for Pond Sites Provided to ACI, Sarasota.

12

APPENDIX: Survey Log

Ent D (FMSF only)



Survey Log Sheet Florida Master Site File Version 4.1 1/07

Survey # (FMSF only)

Consult Guide to the Survey Log Sheet for detailed instructions.

1	dentification and	l Bibliographic Inf	formation		
Survey Project (name and project phase)	710 Ponds, Ph	ase I			
Report Title (exactly as on title page)	ral Resource <i>A</i>	Assessment Surv	rey of Preferred	Pond Sites,	SR 710 from
US 441 to the L-63N Canal, Okee					
Report Authors (as on title page, last names first) 1. ACI		3		
	2		4		
Publication Date (year) 2016 To Publication Information (Give series, number in P12087, ACI, Sarasota					
Supervisors of Fieldwork (even if same as auth			C.a.,		
Affiliation of Fieldworkers: Organization A Key Words/Phrases (Don't use county name, or				Sarasota	
•		• .	•		
1. 3. 2. 4.		6.	8		
Name Wantman Group Address/Phone/E-mail 213 South Dill Recorder of Log Sheet Lee Hutchinson	ard Street, Si	uite 210 Winter	Date Log Shee	et Completed _	
Is this survey or project a continuation of a	previous project?	⊠ivo ∐tes:	Previous survey #s (FN	/ISF ONIY)	
		Mapping			
${\bf C}$ ounties (List each one in which field survey was					
1. Okeechobee 2.	3		5		
2	4		6		
USGS 1:24,000 Map Names/Year of Latest	Revision (attach ad	Iditional sheet if neces:	sary)		
1. Name SEARS	Year 1958	4. Name			Year
2. Name	Year				Year
3. Name	Year	6. Name			Year
	Descripti	ion of Survey Are	a		
Dates for Fieldwork: Start 10-1-2016 Number of Distinct Tracts or Areas Surveye If Corridor (fill in one for each) Width:	ed5		rveyed (fill in one) gth:kilometer		31 acres

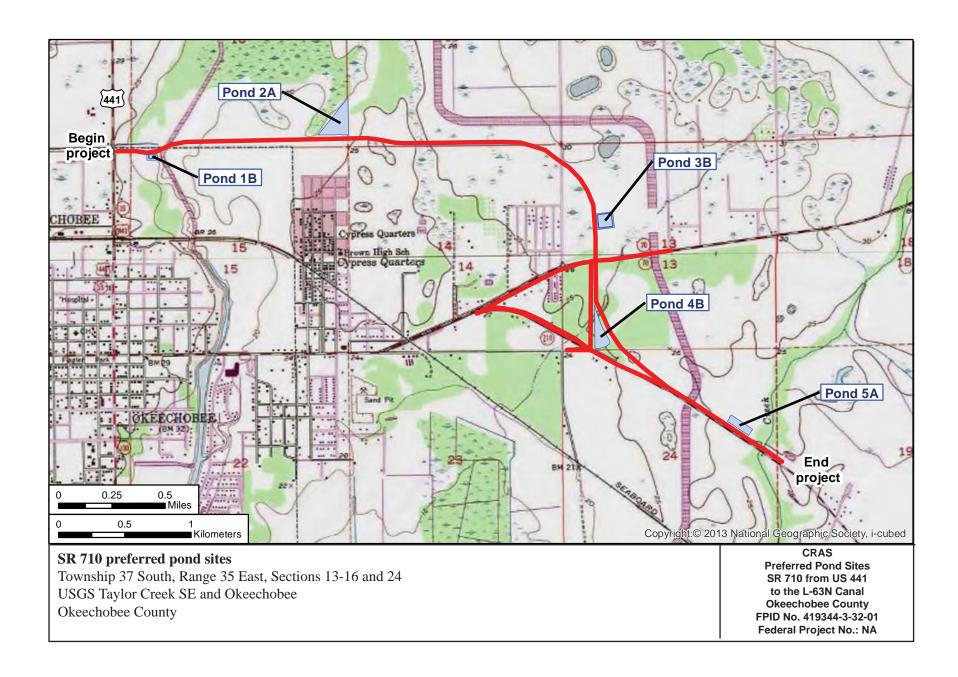
Document Destination:

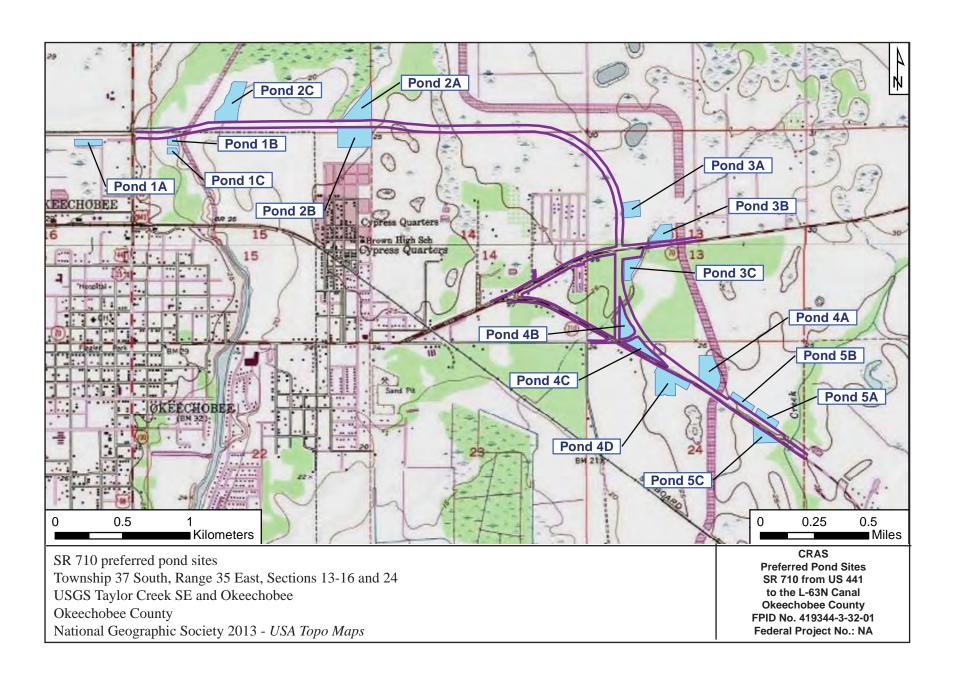
Survey Log Sheet

Survey	#		
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	Resea	arch and Field Me	thods		
Types of Survey (check all that apply):	⊠archaeological □damage assessment	⊠architectural □monitoring repo	⊠historical/ rt □other(desc		□underwater
Scope/Intensity/Proceduresback	ground research,	systematic an	d judgmental	subsurfa	ce testing, 1 m deep,
50 cm diameter, 6.4 mm mes	sh screen; all st	erile; photos	taken, tech	memo prep	ared
Preliminary Methods (check as many	as apply to the project as a	a whole)			
	□library research- <i>local publi</i>		local property or tax	_	other historic maps
	□library-special collection - <i>n</i> ▼Public Lands Survey (maps		newspaper files literature search		⊠soils maps or data ⊠windshield survey
	□local informant(s)		Sanborn Insurance m		⊠aerial photography
other (describe):					
Archaeological Methods (check as ma	any as apply to the project	as a whole)			
Check here if NO archaeological metho					
surface collection, controlled	_	t-other screen size	1	□block excavat	ion (at least 2x2 m)
surface collection, <u>un</u> controlled	water scre		-	soil resistivity	
■ shovel test-1/4"screen	posthole te			magnetomete	
□ shovel test-1/8" screen □ shovel test 1/16"screen	☐ auger tests ☐ coring	S		□ side scan son: ⊠pedestrian su	
shovel test-unscreened	_ •	ation (at least 1x2 m)		unknown	vey
other (describe):			'		
Historical/Architectural Methods (cl Check here if NO historical/architectur building permits commercial permits interior documentation other (describe):		i	neighbor interview loccupant interview loccupation permits		□subdivision maps □tax records □unknown
6 '. 0' 't'		ts (cultural resou	rces recorded)		
Site Significance Evaluated?					
Count of Previously Recorded Sites Previously Recorded Site #'s with S			Recorded Sites Mattach additional		ssary.) n/a
Newly Recorded Site #'s (Are all orig	inals and not updates? Lis	t site #'s without "8".	Attach additional p	pages if necess	ary.) _{n/a}
Site Forms Used: Site File Pa	per Form 🗵 Site Fi	ile Electronic Record	ing Form		
REQUIRED: ATTACH	PLOT OF SURVE	Y AREA ON PH	OTOCOPY O	F USGS 1:	24,000 MAP(S)
SHPO USE ONLY		SHPO USE ONL'	/		SHPO USE ONLY
Origin of Report: □872 □CARL □□Grant Project #]UW □1A32 #	Compliance Re	Academic	Contract	□Avocational
	vey □Historical/Architect cavation Report □Multi-Si □TG □Other: □	ural Survey Marine	Survey Cell Tov		Monitoring Report orary, Hist. or Archival Doc

Plotability:





Appendix 6 Preliminary Pond Right-of-Way & Construction Cost Estimates

S	Preliminary Pond Right-of-Way & Construction Cost & stimates &	s1sots51sss
SS	Basins1s	s7sofs51s
S	Basins2s	s14sofs51s
S	Basins3s	2 6sofs51s
S	Basins4s	3 3sofs51s
SSS	Basins5s	4 3sofs51s

PROJECT: SR 710 PREPARED: LCS
LOCATION: OKEECHOBEE COUNTY, FLORIDA CHECKED: GS

PondlCosts

Pond Site	Construction Cost*	Wetland Mitigation Cost	Protected Species Mitigation	Mainline R/W & Construction Cost Increase for Raising Road	R/W Cost	Total Cost
1A	\$214,012	\$0	\$0	N/A	\$141,000	\$355,012
1B	\$144,073	\$30,000	\$0	N/A	\$146,000	\$320,073
1C	\$166,864	\$52,800	\$0	N/A	\$105,000	\$324,664
2A - Option 1	\$1,072,314	\$0	\$0	\$0	\$265,000	\$1,337,314
2A - Option 2	\$1,114,607	\$0	\$0	\$317,812	\$212,000	\$1,644,419
2A - Option 3	\$1,148,255	\$0	\$0	\$635,625	\$193,000	\$1,976,879
2B - Option 1	\$925,064	\$0	\$0	\$0	\$405,000	\$1,330,064
2B - Option 2	\$1,005,232	\$0	\$0	\$317,812	\$278,000	\$1,601,045
2B - Option 3	\$1,053,637	\$0	\$0	\$635,625	\$209,000	\$1,898,262
2C - Option 1	\$1,042,526	\$0	\$0	\$0	\$297,000	\$1,339,526
2C - Option 2	\$1,067,257	\$0	\$0	\$317,812	\$280,000	\$1,665,070
3A	\$430,448	\$0	\$0	N/A	\$471,000	\$901,448
3B	\$300,565	\$18,000	\$0	N/A	\$383,000	\$701,565
3C	\$408,483	\$0	\$0	N/A	\$365,000	\$773,483
4A - Option 1	\$635,121	\$0	\$18,000	\$0	\$435,000	\$1,088,121
4A - Option 2	\$637,566	\$0	\$18,000	\$296,392	\$391,000	\$1,342,958
4B/4C - Option 1	\$559,843	\$6,000	\$0	\$0	\$658,000	\$1,223,843
4B - Option 2	\$501,222	\$0	\$0	\$0	\$403,000	\$904,222
4D - Option 1	\$565,066	\$0	\$15,000	\$0	\$491,000	\$1,071,066
4D - Option 2	\$594,761	\$0	\$15,000	\$296,392	\$373,000	\$1,279,153
5A	\$269,696	\$48,000	\$0	N/A	\$127,000	\$444,696
5B	\$265,083	\$30,000	\$0	N/A	\$171,000	\$466,083
5C	\$266,723	\$0	\$0	N/A	\$195,000	\$461,723
Total Costs for Selected Sites	\$2,284,897	\$48,000	\$0	\$0	\$1,392,000	\$3,724,897

^{*}sConstructionsCostsssIncludessthescostssavingsswhichsoccursswhensthespondsexcavationsmaterialscansbesusedsforsroadwaysfillstherebysthes contractorsdoessnotshavescopurchasesroadwaysfill.sAllspondsitesshavescuitablesfillsmaterials(sand)sexceptsforsPondsiCs(clayspresent).sPondsitesspavescuitablesfillsmaterials(sand)sexceptsforsPondsitesspavescuitablesfillsmaterials(

Note 1: Pond 2C was assessed a value of \$42,000 for wetland mitigation, however, this site has been modified to have a 25 foot buffer from wetlands. Pond 4B was initially assessed a wetland mitigation value of \$6,000, however, the field analysis showed no wetland impacts on this site.

Note 2: Pond 3A has utility costs associated with it that are as yet undetermined.

 $Note {\bf S}: {\bf C}ontamination {\bf x}osts {\bf s}or {\bf P}onds {\bf S}A {\bf x}and {\bf s}C {\bf s}ave {\bf s}een {\bf x}estimated {\bf x}t {\bf s}125, {\bf y}00 {\bf s}or {\bf x}orst {\bf x}ase {\bf x}leanup {\bf x}of {\bf s}ive {\bf s}tock {\bf s}olding {\bf x}ens. {\bf x}estimated {\bf x}ot {\bf s}ot {\bf x}estimated {\bf x}ot {\bf s}ot {\bf x}estimated {\bf x}ot {\bf x}ot {\bf x}estimated {\bf x}ot$

CONCEPTUAL ESTIMATE, ALTERNATES / SEGMENTS SUMMARY

The costs below are not based on an appraisal!

ITEM SEG: 4193443 - Okeechobee - SR 710 Pond Siting Report - January 2014

COUNTY: Okeechobee

DESCRIPTION: SR 710 from US 441 to L63 Canal

COST ESTIMATE NUMBER: 16012 SMF Alternatives

FOR: A. Rodriguez, P.E., Senior Project Engineer; Wantman Group Inc.

BY: J. Harper, Senior Cost Estimator; FDOT

DATE: May 4, 2016

Alternate / Segment: Five Stormwater Basins, Multiple profiles and storage regs.

Description:	Size Acres:	Phase: 4B	Phase: 41	Phase: 43	Phase: 45	Total:
Pond 1 A	2.238	\$23,000	\$12,000	\$106,000	\$0	\$141,000
Pond 1 B	1.079	\$50,000	\$30,000	\$66,000	\$0	\$146,000
Pond 1 C	1.153	\$23,000	\$12,000	\$70,000	\$0	\$105,000
Pond 2 A Option 1	9.428	\$29,000	\$12,000	\$224,000	\$0	\$265,000
Pond 2 A Option 2	7.204	\$29,000	\$12,000	\$171,000	\$0	\$212,000
Pond 2 A Option 3	6.419	\$29,000	\$12,000	\$171,000	\$0	\$193,000
Pond 2 B Option 1	15.372	\$29,000	\$12,000	\$364,000	\$0	\$405,000
Pond 2 B Option 2	10.002	\$29,000	\$12,000	\$237,000	\$0	\$278,000
Pond 2 B Option 3	7.084	\$29,000	\$12,000	\$168,000	\$0	\$209,000
Pond 2 C Option 1	6.864	\$29,000	\$12,000	\$256,000	\$0	\$297,000
Pond 2 C Option 2	6.139	\$29,000	\$12,000	\$239,000	\$0	\$280,000
·			* ,		* -	
Pond 3 A	3.471	\$29,000	\$12,000	\$430,000	\$0	\$471,000
Pond 3 B	2.444	\$29,000	\$12,000	\$342,000	\$0	\$383,000
Pond 3 C	1.814	\$36,000	\$12,000	\$317,000	\$0	\$365,000
Pond 4 A Option 1	3.984	\$36,000	\$12,000	\$387,000	\$0	\$435,000
Pond 4 A Option 2	3.343	\$36,000	\$12,000	\$343,000	\$0	\$391,000
Pond 4 B + 4 C	7.165	\$36,000	\$12,000	\$610,000	\$0	\$658,000
Pond 4 B Option 2	4.201	\$29,000	\$12,000	\$362,000	\$0	\$403,000
Pond 4 D Option 1	6.075	\$29,000	\$12,000	\$450,000	\$0	\$491,000
Pond 4 D Option 2	4.328	\$29,000	\$12,000	\$332,000	\$0	\$373,000
Pond 5 A	2.624	\$29,000	\$12,000	\$86,000	\$0	\$127,000
Pond 5 B	2.534	\$29,000	\$12,000	\$130,000	\$0	\$171,000
Pond 5 C	3.528	\$29,000	\$12,000	\$150,000	\$0	\$171,000
1 0110 3 0	3.320	Ψ29,000	Ψ12,000	Ψ104,000	φ0	ψ190,000

Notes

- > Pond 1B reflects corrections to the parcel count in Phases 4B and 41 revised size is reflected in Phase 43.
- > Pond 1C was given at 0.929 acre and its outfall at 0.224 acre / 9,757 square feet.
- > Pond 3C includes an exsiting FDOT pond for a net requirement of 1.785 acres, plus outfall of 0.029 = 1.814 acres.
- > Pond 4B is 4.201 Acres; 4C is 2.964 Acres.
- > Highlighted indicates the sites which have been updated

CONCEPTUAL ESTIMATE, ALTERNATES / SEGMENTS SUMMARY

The costs below are not based on an appraisal!

ITEM SEG: 4193443 - Okeechobee - SR 710 Road Profile Sensitivity - February 2014

COUNTY: Okeechobee

DESCRIPTION: SR 710 from US 441 to L63 Canal

COST ESTIMATE NUMBER: 14002 (special)

FOR: A. Rodriguez, P.E., Senior Project Engineer; Wantman Group Inc.

BY: J. Harper, Senior Cost Estimator; FDOT

DATE: February 18, 2014

Alternate / Segment: Variable Road Profile + Five Stormwater Basins (six ponds)

Description:	Size Acres:	Phase: 4B	Phase: 41	Phase: 42	Phase: 43	Phase: 45	Total:
Current Design	89.43	\$654,000	\$168,000	\$252,000	\$13,546,000	\$0	\$14,620,000
21 Parcels incl. 6 Ponds	67.35 Mainline; 22.08 Ponds				\$3.48/sf		\$3.75/sf
One-Foot Profile	105.10	\$654,000	\$168,000	\$252,000	\$14,584,000	\$0	\$15,658,000
21 Parcels incl. 6 Ponds	83.03 Mainline; 22.07 Ponds				\$3.19/sf		\$3.42/sf
Two-Foot Profile	108.25	\$654,000	\$168,000	\$252,000	\$15,015,000	\$0	\$16,089,000
21 Parcels incl. 6 Ponds	86.17 Mainline; 22.08 Ponds				\$3.18/sf		\$3.41/sf
Three-Foot Profile	112.96	\$654,000	\$168,000	\$252,000	\$15,660,000	\$0	\$16,734,000
21 Parcels incl. 6 Ponds	90.87 Mainline; 22.09 Ponds				\$3.18/sf		\$3.40/sf
Average	103.93	\$ 654,000	168,000	252,000	\$14,701,250	0	\$ 15,775,250

rev: 2/18/14

S:\ROW\EST\a-Estimates\Okeechobe_91\14002 4193443 SR 710 441 to Canal\[Summary 14002 - 4193443 - Profile Sensitivity Feb 2014 a.xlsx]SUMMARY

- > If the alternative pond site abuts proposed mainline, Phase 42 is not included because costs would be included in mainline.
- > Pond 1C was given at 0.929 acre and its outfall at 0.224 acre / 9,757 square feet.
- > Pond 3C was given at 5.778 acres and its outfall at 0.029 acre / 1,263 square feet.
- > Pond 3C includes an exsiting FDOT pond for a net requirement of 3.750 acres, plus outfall of 0.029 = 3.779 acres.
- > Pond 4B is 4.591 Acres; 4C is 3.577 Acres.
- > Pond Sizes vary between Profile alternatives due to rounding.

FPID: 1419344-3-32-01 from US 441 to south of L-63N Canal RIGHT-OF-WAYAND&ARTHWORKOPTIONS&FORPOND&ITING&REPORT TotalkRight-of-Wayb TotalkRight-of-WaykCostb RoadwaykEmbankmentb RoadwaylEmbankmentb TotalkCostk(withb Differencebnb Profile**b**Options Impactsbncludingbondsl includinglPondsl(\$) (cubichyards) Costl(\$6/CY) ponds) Costb (AC) Current Proposed Profile 89.43 \$\$14,620,000 396,975 \$2,381,850 \$17,001,850 \$£0 1' Above Current 105.10 \$\$15,658,000 511,975 \$\$3,071,850 \$18,729,850 \$1,728,000 Proposed Profile 2' Above Current \$16,089,000 \$19,880,850 108.25 631,975 \$\$3,791,850 \$\$1,151,000 Proposed Profile 3' Above Current 112.96 \$16,743,000 761,375 \$\$4,568,250 \$21,311,250 \$\$1,430,400 Proposed Profile

FDOT included Ponds 1C, 2C, 3C, 4B/4C, and 5A

Price Increase Used for Analysis = Avergaesof\$1,430,400s and\$1,151,000spersoots

151,000spersfoots \$\$1,290,700

raiseds=s

 $NOTE: \c Lorenti Proposed \c Profile bincludes \c Lorenti Proposed \c Profile bincludes \c Lorenti Proposed \c Lorenti Propo$

Basin	BasinliLengthl(feet)	CostlPerlBasinlllllllllllllllPerl FootlRaised	IslRaisinglOptionb Available?	Comments
1	1086	\$69,029	No	ControlledsbysUSs441sTie-inselevation
2	9900	\$629,269	Yes	Onlysneedstosraiseswestshalfsofsbasin
3	2817	\$179,056	No	ControlledsbysRs70sTie-inælevation
4	4663	\$296,392	Yes	Raisesentiresbasin
5	1840	\$116,955	No	ControlledsbysMosquitosCreeksBridgestie-inselevation
Totals=	20306	\$1,290,700.00		

			LengthsRaisedswithins	MainlinesR/WsandsConsts
Option	PondsArea	HeightsRaiseds(Feet)	Basins(feet)	Costdncrease
Ponds2sAsOptions1	14.227	0	0	\$0.00
Ponds2sAsOptions2	7.929	1	5000	\$317,812.47
Ponds2sAsOptions3	6.419	2	5000	\$635,624.94
Ponds2s8sOptions1	15.372	0	0	\$0.00
Ponds2s9Options2	10.002	1	5000	\$317,812.47
Ponds2s9Options3	7.084	2	5000	\$635,624.94
Ponds2sCsOptions1	6.864	0	0	\$0.00
Ponds2sCsOptions2	6.139	1	5000	\$317,812.47
Ponds4sA:Options1	3.984	0	0	\$0.00
Ponds4sAsOptions2	3.343	1	4663	\$296,391.91
Ponds4s8s+s4sCsOptions1	8.168	0	0	\$0.00
Ponds4s9Options2	4.591	0	0	\$0.00
Ponds4sDsOptions1	6.075	0	0	\$0.00
Ponds4sDsOptions2	4.328	1	4663	\$296,391.91

UnithCostsh(FrombFDOT)bbUsedbStatewidebPriceshexceptbashnotedbbelow.

				Unit	Price
Pay Item	Description	Unit Meas	No. of Contracts (Area 9)	Area 9 Avg., 12 mo.	Statewide Avg., 12 mo.
0120 1	REGULAR EXCAVATION	CY	1	\$3.25	\$4.68
120-6	EMBANKMENT	CY	1	\$2.00	\$6.48
430175118	PIPE CULV, OPT MATL, ROUND, 18"S/CD	LF	1	\$29.71	\$47.49
430175124	PIPE CULV, OPT MATL, ROUND, 24"S/CD	LF	1	\$34.31	\$52.81
430175130	PIPE CULV, OPT MATL, ROUND, 30"S/CD	LF	1	\$40.97	\$64.20
430175136	PIPE CULV, OPT MATL, ROUND, 36"S/CD	LF	1	\$59.10	\$88.90
430175142	PIPE CULV, OPT MATL, ROUND, 42"S/CD	LF	1	\$71.70	\$111.76
430175148	PIPE CULV, OPT MATL, ROUND, 48"S/CD	LF	1	\$99.36	\$116.13
430175154	PIPE CULV, OPT MATL, ROUND, 54"S/CD	LF			\$149.46
430175160	PIPE CULV, OPT MATL, ROUND, 60"S/CD	LF			\$180.88
0440 1 50	UNDERDRAIN, TYPE V	LF			\$40.00
0514 72	LINER IMPERMEABLE PVC	SY	1	\$14.00	\$12.04
530-3-4	RUBBLE RIPRAP, F&I, DITCH LINING	TN			\$74.42
550-10-220	FENCING, TYPE B, 5.1' to 6', STD.	LF		\$8.90	
570-1-2	PERFORMANCE TURF, SOD	SY		\$2.02	

Notes: \$Fencing \$ Sodding \$ unit \$ rices \$ ded \$ ded \$ in ing) \$ ded \$ ded \$ in ing) \$ ded \$ ded \$ in ing) \$ ded \$ ded \$ ded \$ in ing) \$ ded \$

 $Note \mathfrak{L}: \underline{\$Unit} \mathfrak{P}rices \underline{\$of} \$4.75/CY \underline{\$or} \pounds x cavation/Fill \underline{\$Placement} \$\$6/CY \underline{\$or} \Re oadway/Pond \underline{\$fill} \# rovided \underline{\$oy} \$Thes Wantman \underline{\$Group}$

Basin 1

PROJECT: SR 710 - Pond 1A PREPARED: LCS 5/19/2016

LOCATION: OKEECHOBEE COUNTY, FLORIDA CHECKED: GS 5/19/2016

Pondb1A

PipelCosts:

pc			
Pipel S izeb		Unit Priceb	
(inch)	PipelLengthl(ft)	(\$/ft)	Costl(\$)
18	369	\$47.49	\$17,525
24	300	\$52.81	\$15,821
30	99	\$64.20	\$6,356
36	1250	\$88.90	\$111,125
		Totals=	\$150,826

PipelCostlforlPondl1Ab= \$150,826

Earthwork:

Pondb		
Excavationb	Unitb Priceb	
(CY)	(\$/CY)	Costl(\$)
24,674	\$4.75	\$117,202

Importbillb 24,674 CY

SavingsbybmportingbillbobRoadway:

	Unit Priceb		
RoadlFilll(CY)	(\$/ft)	Cost l (\$)	
24,674	6.00	\$148,044	

Importbavingsb=	(\$30,843)

Item	Unit	Quantity	Unit b Priceb	Costl(\$)
Sodding	SY	5,538	\$2.02s	\$11,187b
Clearingl&kGrubbing	AC	2.24	\$\$\$7,723.80	\$17,286b
RubblekRiprapk(DitchkLining)	TN	857.90	\$74.42s	\$63,845b
SedimentlBarrierl(SiltlFence)	LF	1,645	\$1.04s	\$1,711b

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Note: bip ipels izes land bengths lass sumed brombin odification both preliminary betorm but ain but abulations before production by the lass of the l

SR-710 POND SITE REPORT Estimated Earthwork Calculations

Pond Site 1A:

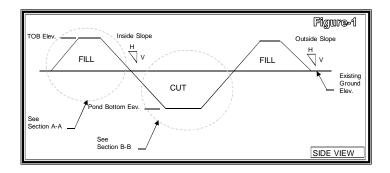
Earthwork Calculations:

1. Earthwork Fill Calculations:

A. Proposed Slopes and Elevations. Existing Ground Elev. (ft) = 26.5 Top of Berm Elev. (ft) = 24.5Pond Bottom Elev. (ft) = 9.5 Outside Slope (V:H) - 1: 4

Inside Slope (V:H) - 1: 2

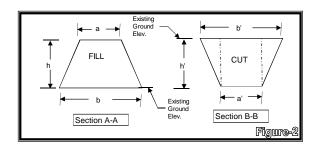
Control Elev. (ft) = 21.5



B. Berm Fill Calculations.

FILL AREA (S.F.) = 0.5 (a + b) h Perimetter @ CL of the Berm (ft) = 1,426 a (ft) = 20 b(ft) = 8h(ft) = -2FILL AREA (S.F.) = 0 Fill VOLUME (C.F.) = 0 Fill VOLUME (C.Y.) = 0

> Area Inside Berm (SF) = 9,566 Area Outside Berm (SF) = 11,759 AreaTop of Berm (SF) = 28,520 **Sodding (SY) =** 5,538



2. Earthwork Cut Calculations:

CUT VOLUME (C.F.) = 0.5 (Area at a' + Area at b')* h' = 0.5 (Area between a' & b') * h' <- Average Area Ratio Method <- Area of Cut along Side slope = (Area of specified elevation a') * h' <- Area of Cut to specified elevation

From Exist Ground To Berm:

Area Between a' & b' elevations (sf) = 12,113 (Exist Ground to TOP) h' (ft) = 2 CUT VOLUME (C.F.) = 12,113

To Berm Elevation:

Area at Outside TOB (sf) = 83,445 (Existing Ground to TOP) h'(ft) = 2CUT VOLUME (C.F.) = 166,891

Pond Side Slopes From TOB to Pond Bottom:

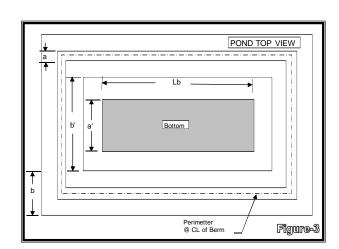
Area Between a' & b' elevation (sf) = 44,885 (TOP to Pond Bottom) h'(ft) = 15CUT VOLUME (C.F.) = 336,636

Pond Bottom:
Area of Pond Bottom (sf) = 10,037 (TOP to Pond Bottom) h'(ft) = 15CUT VOLUME (C.F.) = 150,560

TOTAL CUT VOLUME (C.F.) = 666,199

TOTAL CUT VOLUME (C.Y.) = 24,674

Used 1:2 slopes to pond bottom due to long thin pond



Fencing (ft) = 1,645

Note: Sodding quantity taken to control elevation & fencing measured at R/W line

PROJECT: SR 710 - Pond 1B PREPARED: LCS 5/5/2016
LOCATION: OKEECHOBEE COUNTY, FLORIDA CHECKED: GS 5/5/2016

Pondl1B

PipelCosts:

PipelSizeb		Unit b riceb	
(inch)	PipelLengthl(ft)	(\$/ft)	Costl(\$)
18	344	\$47.49	\$16,338
24	303	\$52.81	\$15,979
30	380	\$64.20	\$24,387
		Totalb≠	\$56,704

PipelCostlforlPondl1Bl= \$56,704

Embankment:

	Unit b Priceb	
PondlFilll(CY)	(\$/ft)	Costl(\$)
3205.0	6.00	\$19,230

Underdrain:

Lengthbofb		
Underdrainb	Unit b Priceb	
(ft)	(\$/CY)	Costl(\$)
1232.0	40.00	\$49,280

Estimatedsbysmeasurements-s14s@s88'slengths

Item	Unit	Quantity	Unitl Priceb	Costl(\$)
Sodding	SY	4,703	\$2.02s	\$9,500b
Clearingl&kGrubbing	AC	1.08	\$\$\$7,723.80	\$8,342b
SedimentlBarrierl(SiltlFence)	LF	978	\$1.04s	\$1,017b

Total b Costb=	\$144,073

Note: blipebsizes band blengths brombpreliminary bstorm bullation brombpond bl. B. b. Pipeblength bl. 140 bofb. 8" bpipe) brombpond brom

Estimated Earthwork Calculations

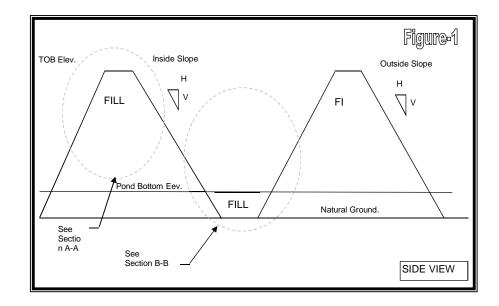
Pond Site 1B:

Earthwork Calculations:

1. Earthwork Fill Calculations:

A. Proposed Slopes and Elevations.

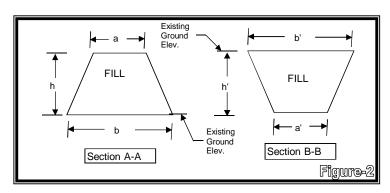
Existing Ground Elev. (ft) = 18
Top of Berm Elev. (ft) = 21.28
Pond Bottom Elev. (ft) = 18.28
Outside Slope (V:H) - 1: 4
Inside Slope (V:H) - 1: 4



B. Berm Fill Calculations.

 $\begin{array}{ll} \text{FILL AREA (S.F.)} = 0.5 \ (a+b) \ h \\ \text{Perimetter @ CL of the Berm (ft)} = 700 \\ a \ (ft) = 20 \\ b \ (ft) = 52 \\ h \ (ft) = 3.28 \\ \text{FILL AREA (S.F.)} = 118.08 \\ \text{Fill VOLUME (C.F.)} = 82,656 \\ \text{Fill VOLUME (C.Y.)} = 3,061 \\ \end{array}$

Sodding (SY) = 4,703



2. Embankment Fill Calculations:

FILL AREA (S.F.) = 0.5 (a' + b') h'

Pond bottom Length (ft) = 147

a' (ft) = 92.76

b' (ft) = 95

h' (ft) = 0.28

FILL AREA (S.F.) = 26.2864

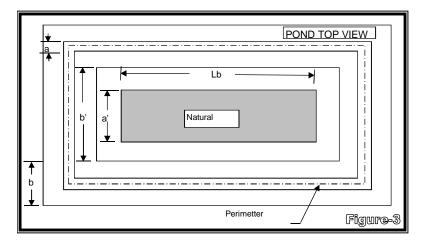
FILL VOLUME (C.F.) = 3,867

FILL VOLUME (C.Y.) = 143



Note: b' and Lb are the length and width of pond bottom. The a' is the width of natural ground elevation

Fencing (ft) = 978



Note: Sodding quantity taken as entire dry pond & fencing measured at R/W line

PROJECT: SR 710 - Pond 1C PREPARED: LCS 5/11/2015
LOCATION: OKEECHOBEE COUNTY, FLORIDA CHECKED: GS 5/11/2015

Pondb1C

PipelCosts:

PipelSizeb	PipelLengthb	Unit b Priceb	
(inch)	(ft)	(\$/ft)	Costl(\$)
18	419	\$47.49	\$19,899
24	303	\$52.81	\$15,979
30	794	\$64.20	\$50,966
•		Totalb₌	\$86,844

PipelCostlforlPondl1C= \$86,844

Embankment:

	Unit b Priceb	
PondlFilll(CY)	(\$/CY)	Costl(\$)
7159.0	6.00	\$42,954

Underdrain:

Lengthbofb		
Underdrainb	Unit Priceb	
(ft)	(\$/ft)	Costl(\$)
480.0	40.00	\$19,200

Estimatedsbysmeasurements-s12s@s40'slengths

Item	Unit	Quantity	Unit b Priceb	Costb(\$)
Sodding	SY	4,010	\$2.02s	\$8,100b
Clearingl&kGrubbing	AC	1.15	\$\$\$7,723.80	\$8,906b
SedimentlBarrierl(Siltb				
Fence)	LF	827	\$1.04s	\$860b

TotalkCostk=	\$166,864
--------------	-----------

Note: thPipelSizes band blengths bfrom to preliminary is torm but rain but abulation before Pond to B. bit Measured bank extrated 14' to ft 20 binch to pipe but ue but obtistance before blast is tructure by ond to C. biPipel bength (215' to ft 18" to pipe) bfrom be pond to bout fall balso bincluded bin bestimate.

Estimated Earthwork Calculations

Pond Site 1C:

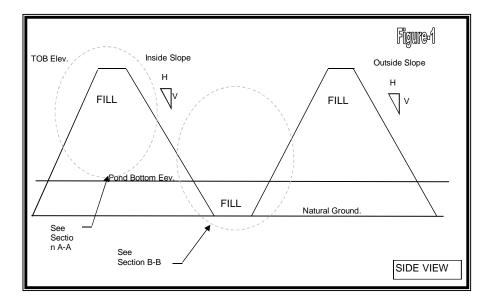
Earthwork Calculations:

1. Earthwork Fill Calculations:

A. Proposed Slopes and Elevations.

Existing Ground Elev. (ft) = 15
Top of Berm Elev. (ft) = 22
Pond Bottom Elev. (ft) = 16.5
Outside Slope (V:H) - 1: 4

Inside Slope (V:H) - 1: 4

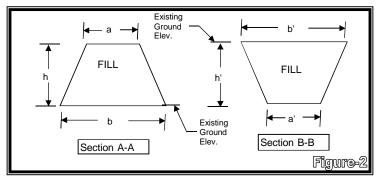


B. Berm Fill Calculations.

FILL AREA (S.F.) = 0.5 (a + b) h Perimetter @ CL of the Berm (ft) = 634a (ft) = 20b (ft) = 65h (ft) = 7FILL AREA (S.F.) = 297.5Fill VOLUME (C.F.) = 188,466

Sodding (SY) = 4010

Fill VOLUME (C.Y.) = 6,980



2. Embankment Fill Calculations:

FILL AREA (S.F.) = 0.5 (a' + b') h'

Pond bottom Length (ft) = 120

a' (ft) = 21

b' (ft) = 33

h' (ft) = 1.5

FILL AREA (S.F.) = 40.5

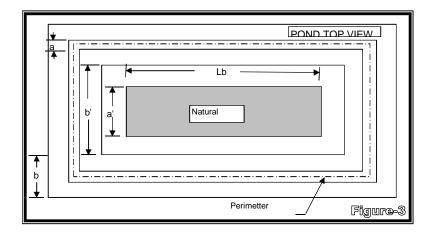
FILL VOLUME (C.F.) = 4,840

FILL VOLUME (C.Y.) = 179



Note: b' and Lb are the length and width of pond bottom. The a' is the width of natural ground elevation

Fencing (ft) = 827



Note: Sodding quantity taken as entire dry pond & fencing measured at R/W line

Basin 2

PROJECT: SR 710 - Pond 2A

PREPARED: LCS 5/5/2016 OKEECHOBEE COUNTY, FLORIDA LOCATION: CHECKED: GS 5/5/2016

Pondb2Ab

PipelCosts:

	PipelLengthb UnithPrice		
PipelSizel(inch)	(ft)	(\$/ft)	Costl(\$)
18	2231	\$47.49s	\$105,950
24	1170	\$52.81s	\$61,788
30	2045	\$64.20s	\$131,289
36	0	\$88.90s	\$0
42	4548	\$111.76s	\$508,284
48	1707	\$116.13	\$198,234
60	95	\$180.88	\$17,184
		Totalb=	\$1,022,729

PipelCostlforlPondl2Al= \$1,022,729

Note:s300'sofs24"spipesaddedsforspondsoutfall

Earthwork:-Optionb

PondlExcavationb	UnithPriceb	
(CY)	(\$/CY)	Costl(\$)
97,405	\$4.75	\$462,674

PondlFilll(CY)	UnitbPriceb (\$/ft)	Costl(\$)
11,191	0.00	\$0

ImportbFillb= 86,214 CY

SavingslbybmportinglFillltolRoadway:

	UnitlPriceb	
RoadlFilll(CY)	(\$/ft)	Costl(\$)
86,214	6.00	\$517,284

(\$54,610) EarthworkbCost/Savingsb=

Note:sRedstypes&sparenthesissindicatesscostssavings

Item	Unit	Quantity	Unitl Priceb	Costl(\$)
Sodding	SY	13,980	\$2.02s	\$28,240b
Clearingb&b				
Grubbing	AC	9.43	\$\$\$\$7,723.80	\$72,835b
SedimentlBarrierl	•			
(SiltlFence)	LF	3,000	\$1.04s	\$3,120b
-				

TotalbConstructionbCost:

\$1,072,314b Optionb#1b=

Earthwork:-Optionb2

Pondb	UnithPriceb	
Excavationb(CY)	(\$/CY)	Costl(\$)
58,638	\$4.75	\$278,531

	Unith Priceb	
PondlFilll(CY)	(\$/ft)	Costl(\$)
13,265	0.00	\$0

ImportlFillb= 45,373 CY

SavingsthythmnortingtfilltotRoadway.

Javingswyninportingumikonoauway.		
	UnithPriceb	
RoadlFilll(CY)	(\$/ft)	Costl(\$)
45,373	6.00	\$272,238

EarthworklCost/Savingsl= \$6,293

Optionb#2b= \$1,114,607b

Item	Unit	Quantity	UnithPriceb	Costl(\$)
Sodding	SY	13,434	\$2.02s	\$27,137b
Clearing t &b				
Grubbing	AC	7.20	\$\$\$7,723.80	\$55,611b
Sedimentb				
Barrierb(Siltb				
Fence)	LF	2,728	\$1.04s	\$2,837b

EarthworkOptions			
Pondb			
Excavationb	UnitlPriceb		
(CY)	(\$/CY)	Costb(\$)	
44,423	\$4.75	\$211,009	

PondlFilll(CY)	UnitbPriceb (\$/ft)	Costl(\$)
16,663	0.00	\$0

ImportlFillb= 27,760 CY

SavingslbylbmportinglFillbolRoadway:

UnitbPriceb	
(\$/ft)	Costl(\$)
6.00	\$166,560
	(\$/ft)

EarthworklCost/Savingsb= \$44,449

Item	Unit	Quantity	UnitbPriceb	Costl(\$)
Sodding	SY	14,267	\$2.02s	\$28,819
Clearingt&b				
Grubbing	AC	6.42	\$\$\$7,723.80	\$49,579
Sedimentb				
Barriert(Siltb				
Fence)	LF	2,575	\$1.04s	\$2,678

Option#3b= \$1,148,255b

Estimated Earthwork Calculations

Pond Site 2A - Option 1:

Earthwork Calculations:

1. Earthwork Fill Calculations:

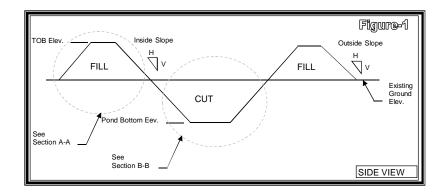
A. Proposed Slopes and Elevations. Existing Ground Elev. (ft) = 21

Top of Berm Elev. (ft) = 24.43Pond Bottom Elev. (ft) = 9.0

Outside Slope (V:H) - 1: 4

Inside Slope (V:H) - 1: 4

Control Elev. (ft) = 21.03



B. Berm Fill Calculations.

FILL AREA (S.F.) = 0.5 (a + b) h

Perimetter @ CL of the Berm (ft) = 2,613

a(ft) = 20b(ft) = 47.44

h(ft) = 3.43

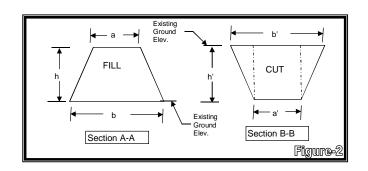
FILL AREA (S.F.) = 115.6596

Fill VOLUME (C.F.) = 302,168

Fill VOLUME (C.Y.) = 11,191

Area Inside Berm (SF) = 36624

Area Outside Berm (SF) = 36948 AreaTop of Berm (SF) = 52251 Sodding (SY) = 13980



2. Earthwork Cut Calculations:

CUT VOLUME (C.F.) = 0.5 (Area between a' & b') * h' <- Area of Cut along Side slope

= (Area of specified elevation a') * h' <- Area of Cut to specified elevation

Pond Side Slopes From Inside Pond Contour at Exist. Ground Elev. to Pond Bottom: Area Between a' & b' elevations (sf) = 107,067

(Exist. Ground Elev. to Pond Bottom)

h' (ft) = 12.0

CUT VOLUME (C.F.) = 640,796

Pond Bottom:

Area of Pond Bottom (sf) = 166,177

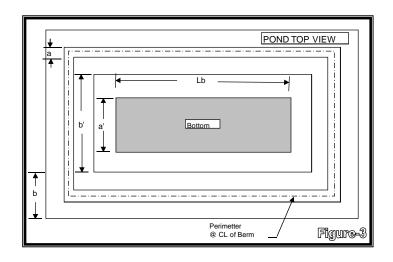
(Exist. Ground Elev. to Pond Bottom)

h'(ft) = 12.0

CUT VOLUME (C.F.) = 1,989,144

TOTAL CUT VOLUME (C.F.) = 2,629,940

TOTAL CUT VOLUME (C.Y.) = **97,405**



Estimated Earthwork Calculations

Pond Site 2A - Option 2:

Earthwork Calculations:

1. Earthwork Fill Calculations:

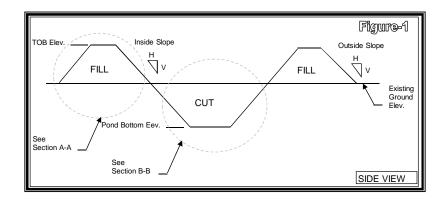
A. Proposed Slopes and Elevations.

Existing Ground Elev. (ft) = 21
Top of Berm Elev. (ft) = 25.43
Pond Bottom Elev. (ft) = 9.0

Outside Slope (V:H) - 1: 4

Inside Slope (V:H) - 1: 4

Control Elev. (ft) = 21.03



B. Berm Fill Calculations.

FILL AREA (S.F.) = 0.5 (a + b) h Perimetter @ CL of the Berm (ft) = $\frac{2,143}{2}$

a (ft) = 20

b(ft) = 55.44

h(ft) = 4.43

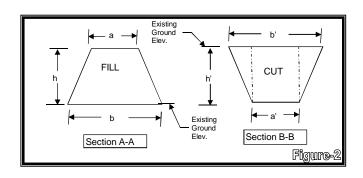
FILL AREA (S.F.) = 167.10 Fill VOLUME (C.F.) = 358,160

Fill VOLUME (C.Y.) = 13,265

Area Inside Berm (SF) = 38885 Area Outside Berm (SF) = 39150

AreaTop of Berm (SF) = 42868

Sodding (SY) = 13,434



2. Earthwork Cut Calculations:

CUT VOLUME (C.F.) = 0.5 (Area between a' & b') * h' <- Area of Cut along Side slope = (Area of specified elevation a') * h' <- Area of Cut to specified elevation

Pond Side Slopes From Inside Pond Contour at Exist. Ground Elev. to Pond Bottom:

Area Between a' & b' elevations (sf) = 82,477

(Exist. Ground Elev. to Pond Bottom)

h' (ft) = 12.0

CUT VOLUME (C.F.) = 493,626

Pond Bottom:

Area of Pond Bottom (sf) = 91,026

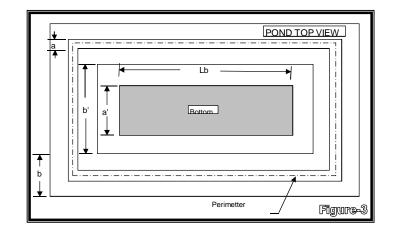
(Exist. Ground Elev. to Pond Bottom)

h' (ft) = 12.0

CUT VOLUME (C.F.) = 1,089,586

TOTAL CUT VOLUME (C.F.) = 1,583,213

TOTAL CUT VOLUME (C.Y.) = 58,638



Fencing (ft) = 2728

Note: Sodding quantity taken to control elevation & fencing measured at R/W line

Estimated Earthwork Calculations

Pond Site 2A - Option 3:

Earthwork Calculations:

1. Earthwork Fill Calculations:

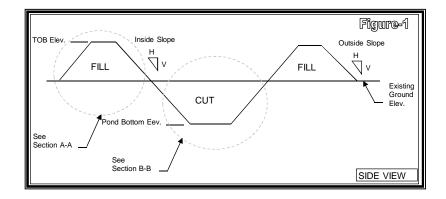
A. Proposed Slopes and Elevations.

Existing Ground Elev. (ft) = 21 Top of Berm Elev. (ft) = 26.43Pond Bottom Elev. (ft) = 9.0

Outside Slope (V:H) - 1: 4

Inside Slope (V:H) - 1: 4

Control Elev. (ft) = 21.03



B. Berm Fill Calculations.

FILL AREA (S.F.) = 0.5 (a + b) h Perimetter @ CL of the Berm (ft) = 1,986a (ft) = 20b(ft) = 63.44

h (ft) = 5.43

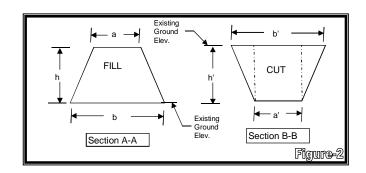
FILL AREA (S.F.) = 226.5396 Fill VOLUME (C.F.) = 449,908

Fill VOLUME (C.Y.) = 16,663

Area Inside Berm (SF) = 44218 Area Outside Berm (SF) = 44463

AreaTop of Berm (SF) = 39720

Sodding (SY) = 14267



2. Earthwork Cut Calculations:

CUT VOLUME (C.F.) = 0.5 (Area between a' & b') * h' <- Area of Cut along Side slope = (Area of specified elevation a') * h' <- Area of Cut to specified elevation

Pond Side Slopes From Inside Pond Contour at Exist. Ground Elev. to Pond Bottom:

Area Between a' & b' elevations (sf) = 71,283 (Exist. Ground Elev. to Pond Bottom)

h'(ft) = 12.0

CUT VOLUME (C.F.) = 426,631

Pond Bottom:

Area of Pond Bottom (sf) = 64,561

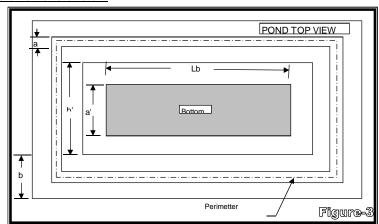
(Exist. Ground Elev. to Pond Bottom)

h'(ft) = 12.0

CUT VOLUME (C.F.) = 772,797

TOTAL CUT VOLUME (C.F.) = 1,199,429

TOTAL CUT VOLUME (C.Y.) = 44,423



Fencing (ft) = 2575

Note: Sodding quantity taken to control elevation & fencing measured at R/W line

PROJECT: SR 710 - Pond 2B

PREPARED: LCS 5/11/2015 OKEECHOBEE COUNTY, FLORIDA CHECKED: GS LOCATION: 5/11/2015

Pondb2Bb

PipelCosts:

i ipeneosts.			
	PipelLengthb	Unitl Priceb	
PipelSizel(inch)	(ft)	(\$/ft)	Costl(\$)
18	2433	\$47.49s	\$115,543
24	870	\$52.81s	\$45,945
30	2045	\$64.20s	\$131,289
36	0	\$88.90s	\$0
42	4548	\$111.76s	\$508,284
48	1707	\$116.13	\$198,234
60	95	\$180.88	\$17,184
		Totalb=	\$1,016,479

PipelCostlforlPondl2Bl= \$1,016,479

Note:s202'sofs18"spipesaddedsforspondsoutfall

Earthwork:-Optionb

PondlExcavation	UnitbPriceb	
(CY)	(\$/CY)	Costl(\$)
215,527	\$4.75	\$1,023,753

D. HEIMON	UnithPriceb	0 - 11(4)
PondlFilll(CY)	(\$/ft)	Costl(\$)
4,641	0.00	\$0

ImportbFillb= 210,886 CY

SavingslbybmportinglFillbtobRoadway:

	UnitbPriceb	
RoadlFilll(CY)	(\$/ft)	Costl(\$)
210,886	6.00	\$1,265,316

EarthworklCost/Savingsl= (\$241,563)

Item	Unit	Quantity	UnitbPriceb	Costl(\$)
Sodding	SY	13,674	\$2.02s	\$27,621b
Clearingt&b Grubbing	AC	15.37	\$\$\$\$7,723.80	\$118,730b
Grubbing	AC	15.57	\$3339,723.60	\$118,7300
SedimentlBarrierl (SiltlFence)	LF	3,650	\$1.04s	\$3,796b

Earthwork:-Optionb2

Pondb	UnithPriceb	
Excavationb(CY)	(\$/CY)	Costl(\$)
123,621	\$4.75	\$587,200

	UnitbPriceb	
PondlFilll(CY)	(\$/ft)	Costl(\$)
6,500	0.00	\$0

ImportbFillb= 117,121 CY

SavingslbybmportinglFillbtobRoadway:

	UnitbPriceb	
RoadbFillb(CY)	(\$/ft)	Costl(\$)
117,121	6.00	\$702,726

EarthworklCost/Savingsl= (\$115,526)

Note: sRed type & sparenthesis and icates costs avings

Note: areaxype axparenties is an aleates a cost and vings				
Item	Unit	Quantity	Unitb Priceb	Costl(\$)
Sodding	SY	11,979	\$2.02s	\$24,198b
Clearingh&b				
Grubbing	AC	10.00	\$\$7,723.80	\$77,253b
Sedimentb				
Barrierl(Siltb				
Fence)	LF	2,720	\$1.04s	\$2,829b

Earthwork:-Optionb

 Luitinvoiki Optiona				
Pondb				
Excavationb	UnitlPriceb			
(CY)	(\$/CY)	Costl(\$)		
74,296	\$4.75	\$352,906		

	Unit b Priceb	
PondbFillb(CY)	(\$/ft)	Costl(\$)
8,336	0.00	\$0

ImportbFillb= 65,960 CY

SavingsbybmportingbillbobRoadway:

satings by sinportings into stouctury.				
	UnitlPriceb			
RoadlFilll(CY)	(\$/ft)	Costl(\$)		
65,960	6.00	\$395,760		

EarthworklCost/Savingsl=

Item	Unit	Quantity	UnitbPriceb	Costl(\$)
Sodding	SY	11,376	\$2.02s	\$22,980b
Clearing t& b				
Grubbing	AC	7.08	\$\$\$7,723.80	\$54,715b
Sedimentb				
Barriert(Siltb				
Fence)	LF	2,228	\$1.04s	\$2,317b

TotalkConstructionkCost:

\$925,064b Optionb#2b= \$1,005,232b Optionb#3b= \$1,053,637b Optionb#1b=

Estimated Earthwork Calculations

Pond Site 2B - Option 1:

Earthwork Calculations:

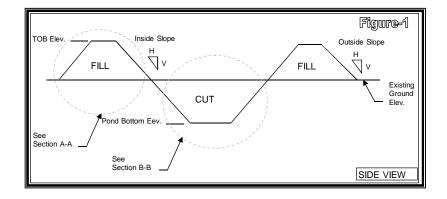
1. Earthwork Fill Calculations:

A. Proposed Slopes and Elevations.

Existing Ground Elev. (ft) = 23Top of Berm Elev. (ft) = 24.43Pond Bottom Elev. (ft) = 10.0Outside Slope (V:H) - 1: 4

Inside Slope (V:H) - 1: 4

Control Elev. (ft) = 21.95



B. Berm Fill Calculations.

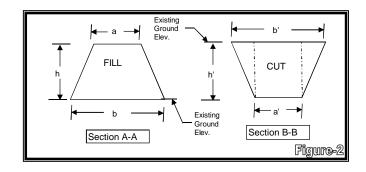
FILL AREA (S.F.) = 0.5 (a + b) h Perimetter @ CL of the Berm (ft) = 3,407 a (ft) = 20b(ft) = 31.44h(ft) = 1.43FILL AREA (S.F.) = 36.7796

Fill VOLUME (C.F.) = 125,308 Fill VOLUME (C.Y.) = 4,641

Area Inside Berm (SF) = 34838 Area Outside Berm (SF) = 20088

AreaTop of Berm (SF) = 68140

Sodding (SY) = 13674



2. Earthwork Cut Calculations:

CUT VOLUME (C.F.) = 0.5 (Area between a' & b') * h' <- Area of Cut along Side slope = (Area of specified elevation a') * h' <- Area of Cut to specified elevation

Pond Side Slopes From Inside Pond Contour at Exist. Ground Elev. to Pond Bottom:

Area Between a' & b' elevations (sf) = 162,791

(Exist. Ground Elev. to Pond Bottom)

h'(ft) = 13.1CUT VOLUME (C.F.) = 1,062,213

Pond Bottom:

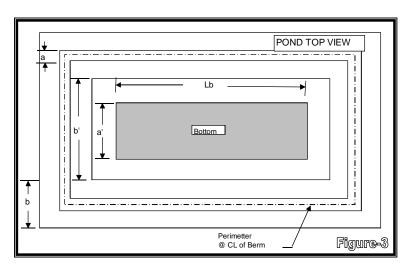
Area of Pond Bottom (sf) = 364,522

(Exist. Ground Elev. to Pond Bottom)

h'(ft) = 13.1

CUT VOLUME (C.F.) = 4,757,011

TOTAL CUT VOLUME (C.F.) = 5,819,224 TOTAL CUT VOLUME (C.Y.) = 215,527



Estimated Earthwork Calculations

Pond Site 2B - Option 2:

Earthwork Calculations:

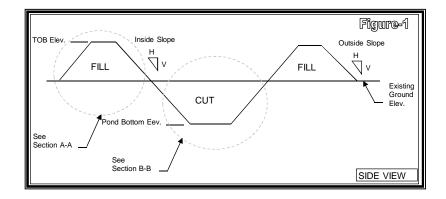
1. Earthwork Fill Calculations:

A. Proposed Slopes and Elevations.

Existing Ground Elev. (ft) = 23Top of Berm Elev. (ft) = 25.43Pond Bottom Elev. (ft) = 10.0Outside Slope (V:H) - 1: 4

Inside Slope (V:H) - 1: 4

Control Elev. (ft) = 21.95



B. Berm Fill Calculations.

FILL AREA (S.F.) = 0.5 (a + b) h Perimetter @ CL of the Berm (ft) = 2,430a (ft) = 20

b(ft) = 39.44h(ft) = 2.43

FILL AREA (S.F.) = 72.2196

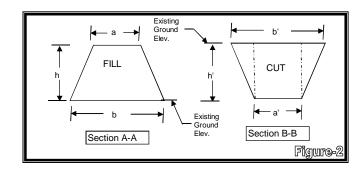
Fill VOLUME (C.F.) = 175,494

Fill VOLUME (C.Y.) = **6,500**

Area Inside Berm (SF) = 34867

Area Outside Berm (SF) = 24347 Area Top of Berm (SF) = 48600

Sodding (SY) = 11979



2. Earthwork Cut Calculations:

CUT VOLUME (C.F.) = 0.5 (Area between a' & b') * h' <- Area of Cut along Side slope = (Area of specified elevation a') * h' <- Area of Cut to specified elevation

Pond Side Slopes From Inside Pond Contour at Exist. Ground Elev. to Pond Bottom:

Area Between a' & b' elevations (sf) = 110,199

(Exist. Ground Elev. to Pond Bottom)

h'(ft) = 13.1

CUT VOLUME (C.F.) = 719,050

Pond Bottom:

Area of Pond Bottom (sf) = 200,667

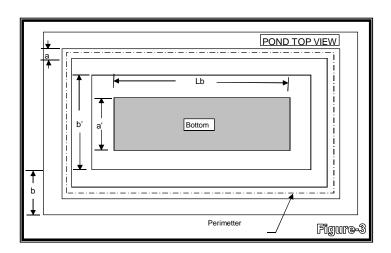
(Exist. Ground Elev. to Pond Bottom)

h'(ft) = 13.1

CUT VOLUME (C.F.) = 2,618,709

TOTAL CUT VOLUME (C.F.) = 3,337,759

TOTAL CUT VOLUME (C.Y.) = 123,621



Estimated Earthwork Calculations

Pond Site 2B - Option 3:

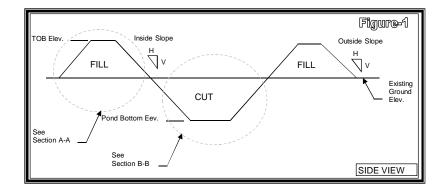
Earthwork Calculations:

1. Earthwork Fill Calculations:

A. Proposed Slopes and Elevations.

Existing Ground Elev. (ft) = 23
Top of Berm Elev. (ft) = 26.43
Pond Bottom Elev. (ft) = 10.0
Outside Slope (V:H) - 1: 4
Inside Slope (V:H) - 1: 4

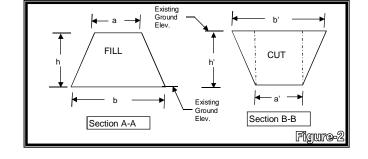
Control Elev. (ft) = 21.95



B. Berm Fill Calculations.

FILL AREA (S.F.) = 0.5 (a + b) h
Perimetter @ CL of the Berm (ft) = 1,946
a (ft) = 20
b (ft) = 47.44
h (ft) = 3.43
FILL AREA (S.F.) = 115.6596
Fill VOLUME (C.F.) = 225,074
Fill VOLUME (C.Y.) = 8,336

Area Inside Berm (SF) = 35946 Area Outside Berm (SF) = 27521 AreaTop of Berm (SF) = 38920 Sodding (SY) = 11376



2. Earthwork Cut Calculations:

CUT VOLUME (C.F.) = 0.5 (Area between a' & b') * h' <- Area of Cut along Side slope = (Area of specified elevation a') * h' <- Area of Cut to specified elevation

Pond Side Slopes From Inside Pond Contour at Exist. Ground Elev. to Pond Bottom:

Area Between a' & b' elevations (sf) = 81,323

(Exist. Ground Elev. to Pond Bottom)

h' (ft) = 13.1

CUT VOLUME (C.F.) = 530,631

Pond Bottom:

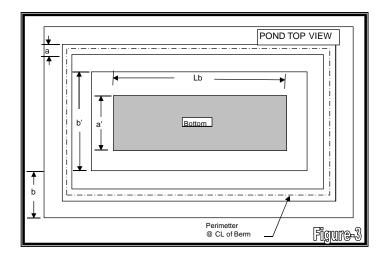
Area of Pond Bottom (sf) = 113,055

(Exist. Ground Elev. to Pond Bottom)

h' (ft) = 13.1

CUT VOLUME (C.F.) = 1,475,361

TOTAL CUT VOLUME (C.F.) = 2,005,993 TOTAL CUT VOLUME (C.Y.) = **74,296**



PROJECT: SR 710 - Pond 2C

PREPARED: LCS 5/19/2016 LOCATION: OKEECHOBEE COUNTY, FLORIDA CHECKED: GS 5/19/2016

Pondl2Cb

PipelCosts:

	PipelLengthb	UnithPriceb	
PipelSizel(inch)	(ft)	(\$/ft)	Costl(\$)
60	4236	\$180.88	\$766,208
18	1322	\$47.49	\$62,782
		Totals=	\$828,989

PipelCostlforlPondl2Cb= \$828,989

Note:s868'sofs18"spipesaddedsforspondsoutfall

Earthwork:-Optionb

Optionb#1b=

PondlExcavationb	UnithPriceb				
(CY)	(\$/CY)	Costl(\$)			
54,038	\$4.75	\$256,681			

PondlFilll(CY)	UnitbPriceb (\$/ft)	Costl(\$)
14,346	0.00	\$0

ImportbFillb= 39,692 CY

SavingslbybmportinglFillbtolRoadway:

savings by simportings in a concountry.				
Unith Priceb				
RoadlFilll(CY)	(\$/ft)	Costk(\$)		
39,692	6.00	\$238,152		

Ear

artnworksLost/Savingss	\$18,529		Earthwork b .
		Note:sRedstypes&sparenthesissindic	atess:ostssavings

				c.m.caxypexxpare
Item	Unit	Quantity	UnitbPriceb	Costk(\$)
Sodding	SY	16,333	\$2.02s	\$32,993b
Clearingt&b				
Grubbing	AC	6.86	\$\$\$\$7,723.80	\$53,016b
RubblebRiprapb				
(Ditchlining)	TN	1,427.70	\$74.42s	\$106,249b
SedimentBarrierb				
(SiltlFence)	LF	2,644	\$1.04s	\$2,750b

Barrier
Fenc

Item

Earthwork:-Optionb2

Pondb	UnitbPriceb	
Excavationb(CY)	(\$/CY)	Costl(\$)
35,992	\$4.75	\$170,962

	UnitbPriceb	
PondbFillb(CY)	(\$/ft)	Costl(\$)
17,460	0.00	\$0

ImportbFillb= 18,532 CY

SavingslbybmportinglFillbtobRoadway:

	UnitbPriceb			
RoadlFilll(CY)	(\$/ft)	Costl(\$)		
18,532	6.00	\$111,192		

EarthworkhCost/Savingsh= \$59,770

Unit

Sodding SY 16,570 \$2.02s \$33,471b Clearingb&b Grubbing AC 6.14 \$\$7,723.80 \$47,416b RubblebRiprapb \$95,053b (Ditchbining) TN 1,277.25 \$74.42s Sedimentb r**t**(Siltb ce) LF 2,459 \$1.04s \$2,557b

Quantity

UnitbPriceb

Costl(\$)

TotalbConstructionbCost:

\$1,042,526b Optionb#2b= \$1,067,257b

Note: biRipraphassumed bto bbeh&'s tripharound bponds idels lopes.

Estimated Earthwork Calculations

Pond Site 2C - Option 1:

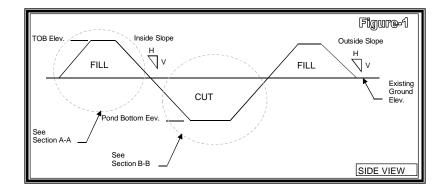
Earthwork Calculations:

1. Earthwork Fill Calculations:

A. Proposed Slopes and Elevations.

Existing Ground Elev. (ft) = 20
Top of Berm Elev. (ft) = 24.43
Pond Bottom Elev. (ft) = 6.3
Outside Slope (V:H) - 1: 4
Inside Slope (V:H) - 1: 4

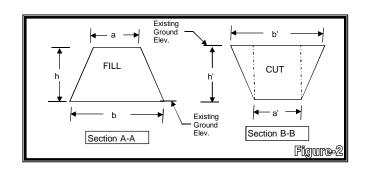
Control Elev. (ft) = 18.33



B. Berm Fill Calculations.

> Area Inside Berm (SF) = 58300 Area Outside Berm (SF) = 42339 AreaTop of Berm (SF) = 46360

Sodding (SY) = 16333



2. Earthwork Cut Calculations:

CUT VOLUME (C.F.) = 0.5 (Area between a' & b') * h' <- Area of Cut along Side slope = (Area of specified elevation a') * h' <- Area of Cut to specified elevation

Pond Side Slopes From Inside Pond Contour at Exist. Ground Elev. to Pond Bottom: Area Between a' & b' elevations (sf) = 105,716

Krea Between a & b elevations (St) = 105,716

(Exist. Ground Elev. to Pond Bottom)

h' (ft) = 13.7

CUT VOLUME (C.F.) = 722,567

Pond Bottom:

Area of Pond Bottom (sf) = 53,873

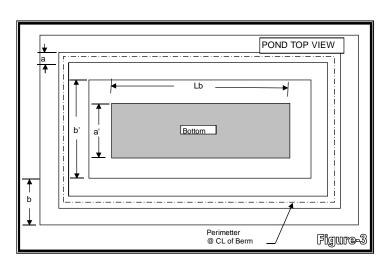
(Exist. Ground Elev. to Pond Bottom)

h'(ft) = 13.7

CUT VOLUME (C.F.) = 736,447

TOTAL CUT VOLUME (C.F.) = 1,459,014

TOTAL CUT VOLUME (C.Y.) = 54,038



Estimated Earthwork Calculations

Pond Site 2C - Option 2:

Earthwork Calculations:

1. Earthwork Fill Calculations:

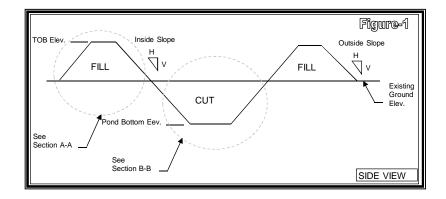
A. Proposed Slopes and Elevations.

Existing Ground Elev. (ft) = 20Top of Berm Elev. (ft) = 25.43Pond Bottom Elev. (ft) = 6.3

Outside Slope (V:H) - 1: 4

Inside Slope (V:H) - 1: 4

Control Elev. (ft) = 18.33



B. Berm Fill Calculations.

FILL AREA (S.F.) = 0.5 (a + b) h Perimetter @ CL of the Berm (ft) = 2,081

a (ft) = 20

b(ft) = 63.44

h(ft) = 5.43

FILL AREA (S.F.) = 226.5396

Fill VOLUME (C.F.) = 471,429

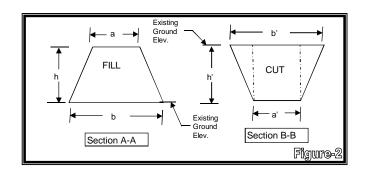
Fill VOLUME (C.Y.) = 17,460

Area Inside Berm (SF) = 60919

Area Outside Berm (SF) = 46590

Area Top of Berm (SF) = 41620

Sodding (SY) = 16570



2. Earthwork Cut Calculations:

CUT VOLUME (C.F.) = 0.5 (Area between a' & b') * h' = (Area of specified elevation a') * h' <- Area of Cut along Side slope <- Area of Cut to specified elevation

Pond Side Slopes From Inside Pond Contour at Exist. Ground Elev. to Pond Bottom:

Area Between a' & b' elevations (sf) = 88,826 (Exist. Ground Elev. to Pond Bottom)

h'(ft) = 13.7CUT VOLUME (C.F.) = 607,127

Pond Bottom:

Area of Pond Bottom (sf) = 26,675

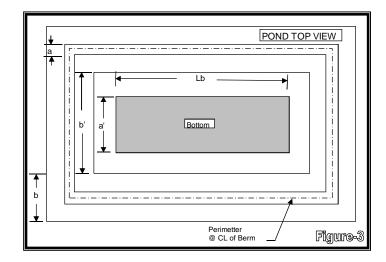
(Exist. Ground Elev. to Pond Bottom)

h'(ft) = 13.7

CUT VOLUME (C.F.) = 364,647

TOTAL CUT VOLUME (C.F.) = 971,774

TOTAL CUT VOLUME (C.Y.) = 35,992



Basin 3

 PROJECT:
 SR 710 - Pond 3A
 PREPARED: LCS
 5/5/2016

 LOCATION:
 OKEECHOBEE COUNTY, FLORIDA
 CHECKED: GS
 5/6/2016

Pondb3A

PipelCosts:

PipelSizeb	PipelLengthb	Unitl P riceb	
(inch)	(ft)	(\$/ft)	Costl(\$)
18	1161	\$47.49	\$55,116
24	410	\$52.81	\$21,668
30	0	\$64.20	\$0
36	1035	\$88.90	\$92,037
42	1511	\$111.76	\$168,883
		Totals=	\$337,704

PipelCostlforlPondl8Als \$337,704

Earthwork:

Pondb		
Excavationb	UnitbPriceb	
(CY)	(\$/CY)	Costl(\$)
39,249	\$4.75	\$186,433

ImportlFilll= 39,249 CY

SavingslbybmportinglFillbtolRoadway:

	UnitbPriceb	
RoadlFilll(CY)	(\$/ft)	Costl(\$)
39,249	6.00	\$235,494

EarthworkhCost/Savingsh=	(\$49,061)

 $Note: \underline{s} Red \underline{s} y pes \underline{\&} sparenthesis \underline{s} n dicates \underline{\&} ost \underline{\&} a vings$

Claybiner:

Arealath Pondl		
PeaklStageb	UnitbPriceb	
(SY)	(\$/SY)	Costl(\$)
9,885	\$10.00	\$98,851

^{*}Assumedsunitspricesofsclaysinersats\$10/SY

Item	Unit	Quantity	Unit b Priceb	Costl(\$)
Sodding	SY	7,052	\$2.02s	\$14,245b
Clearingl&lGrubbing	AC	3.47	\$\$7,723.80	\$26,802b
SedimentlBarrierl(Siltb				
Fence)	LF	1,834	\$1.04s	\$1,907b

TotalbConstructionbCost:

= \$430,448b

Note: biPipelsizes land bengths lass umed brombino diffication by fipreliminary is torm bulations b for brond baland bal

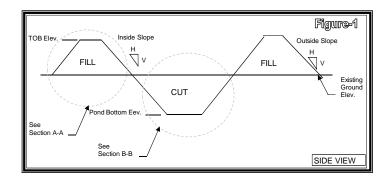
Pond Site 3A:

Earthwork Calculations:

1. Earthwork Fill Calculations:

A. Proposed Slopes and Elevations. Existing Ground Elev. (ft) = 30 Top of Berm Elev. (ft) = 29.73 Pond Bottom Elev. (ft) = 12.73 Outside Slope (V:H) - 1: 4
Inside Slope (V:H) - 1: 4

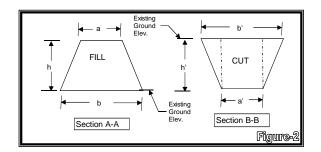
Control Elev. (ft) = 24.73 *Assume Pond Bottom 12' depth below NW



B. Berm Fill Calculations.

FILL AREA (S.F.) = 0.5 (a + b) h Perimetter @ CL of the Berm (ft) = 1,521 a (ft) = 20b(ft) = 17.84h(ft) = -0.27FILL AREA (S.F.) = 0Fill VOLUME (C.F.) = 0 Fill VOLUME (C.Y.) = 0

> Area Inside Berm (SF) = 31,356 Area Outside Berm (SF) = 1,693 Area Top of Berm (SF) = 30,420 **Sodding (SY) =** 7,052



2. Earthwork Cut Calculations:

CUT VOLUME (C.F.) = 0.5 (Area between a' & b') * h' <- Area of Cut along Side slope = (Area of specified elevation a') * h' <- Area of Cut to specified elevation

From Exist Ground To Berm:

Area Between a' & b' elevations (sf) = 1,714 (Exist Ground to TOP) h' (ft) = 0.27

CUT VOLUME (C.F.) = 231

To Berm Elevation:
Area at Outside TOB (sf) = 130,851 (Existing Ground to TOP) h' (ft) = 0.27

CUT VOLUMÉ (C.F.) = 35,330

Pond Side Slopes From Inside Pond Contour at Exist. Ground Elev. to Pond Bottom:

Area Between a' & b' elevations (sf) = 80,371 (Exist. Ground Elev. to Pond Bottom) h' (ft) = 17.0

CUT VOLUME (C.F.) = 683,151

Pond Bottom:

Area of Pond Bottom (sf) = 20,060 (Exist. Ground Elev. to Pond Bottom)

h'(ft) = 17.0CUT VOLUME (C.F.) = 341,023

TOTAL CUT VOLUME (C.F.) = 1,059,736 TOTAL CUT VOLUME (C.Y.) = 39,249

POND TOP VIEW Bottom b Perimetter @ CL of Berm Figure-3

Fencing (ft) = 1834



PROJECT: SR 710 - Pond 3B PREPARED: LCS 5/11/2015
LOCATION: OKEECHOBEE COUNTY, FLORIDA CHECKED: GS 5/11/2015

Pondb3B

PipelCosts:

Pipel S izeb	PipelLengthb	Unit b Priceb	
(inch)	(ft)	(\$/ft)	Costl(\$)
18	2232	\$47.49	\$105,978
24	970	\$52.81	\$51,227
30	0	\$64.20	\$0
36	1137	\$88.90	\$101,105
42	101	\$111.76	\$11,313
		Totalb=	\$269,624

PipelCostlforlPondl3Bl= \$269,624

Earthwork:

	Earthworkb	Unit Priceb	
	(CY)	(\$/CY)	Costl(\$)
Excavation	18,810	\$4.75	\$89,348
Fill	3,591	\$0.00	\$0

Importbill 15,219 CY

SavingslbybmportinglFillltolRoadway:

		•
	Unit b Priceb	
RoadlFilll(CY)	(\$/ft)	Costl(\$)
15,219	6.00	\$91,314

Item	Unit	Quantity	Unit b Priceb	Costl(\$)
Sodding	SY	6,267	\$2.02s	\$12,659b
Clearingl&lGrubbing	AC	2.44	\$\$7,723.80	\$18,877b
SedimentlBarrierl(Siltb	LF	1,319	\$1.04s	\$1,372b

TotalkConstructionkCost:

= \$300,565b

Estimated Earthwork Calculations

Pond Site 3B:

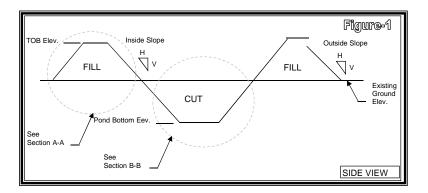
Earthwork Calculations:

1. Earthwork Fill Calculations:

A. Proposed Slopes and Elevations. Existing Ground Elev. (ft) = 27 Top of Berm Elev. (ft) = 29.73Pond Bottom Elev. (ft) = 13.4Outside Slope (V:H) - 1: 4 Inside Slope (V:H) - 1: 4

Control Elev. (ft) = 25.4

*Assume Pond Bottom 12' depth below NW

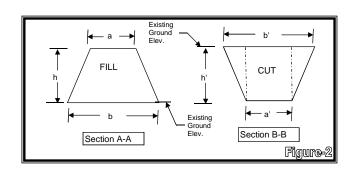


B. Berm Fill Calculations.

FILL AREA (S.F.) = 0.5 (a + b) hPerimetter @ CL of the Berm (ft) = 1,149 a (ft) = 20b (ft) = 41.84h(ft) = 2.73FILL AREA (S.F.) = 84.4116 Fill VOLUME (C.F.) = 96,955 Fill VOLUME (C.Y.) = 3,591

> Area Inside Berm (SF) = 20,506 Area Outside Berm (SF) = 12,929 Area Top of Berm (SF) = 22,972

Sodding (SY) = 6,267



2. Earthwork Cut Calculations:

CUT VOLUME (C.F.) = 0.5 (Area between a' & b') * h' = (Area of specified elevation a') * h'

<- Area of Cut along Side slope <- Area of Cut to specified elevation

Pond Side Slopes From Inside Pond Contour at Exist. Ground Elev. to Pond Bottom:

Area Between a' & b' elevations (sf) = 40,699 (Exist. Ground Elev. to Pond Bottom)

h'(ft) = 13.6

CUT VOLUME (C.F.) = 276,754

Pond Bottom:

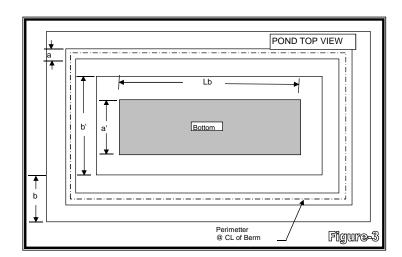
Area of Pond Bottom (sf) = 16,995 (Exist. Ground Elev. to Pond Bottom)

h'(ft) = 13.6

CUT VOLUME (C.F.) = 231,130

TOTAL CUT VOLUME (C.F.) = 507,883

TOTAL CUT VOLUME (C.Y.) = 18,810



Fencing (ft) = 1,319

PROJECT:	SR 710 - Pond 3C	PREPARED: LCS	5/11/2015
LOCATION:	OKEECHOBEE COUNTY, FLORIDA	CHECKED: GS	5/11/2015

Pondb3C

PipelCosts:

Pipel S izeb	PipelLengthb	Unitl P riceb	
(inch)	(ft)	(\$/ft)	Cost l(\$)
18	1106	\$47.49	\$52,504
24	410	\$52.81	\$21,668
30	0	\$64.20	\$0
36	1035	\$88.90	\$92,037
42	1803	\$111.76	\$201,517
48	95	\$116.13	\$11,032
		Totalb=	\$378,759

PipelCostlforlPondl3Cl= \$378,759

Earthwork:

	Earthworkb	Unit b Priceb	
	(CY)	(\$/CY)	Costl(\$)
Excavation	18,874	\$4.75	\$89,652
Fill	3,175	\$0.00	\$0

ImportlFilll= 15,699 CY

SavingsbybmportingbillbokRoadway:

	Unit b Priceb			
RoadlFilll(CY)	(\$/ft)	Costl(\$)		
15,699	6.00	\$94,194		

EarthworklCost/Savingsb=	(\$4,543)

Item	Unit	Quantity	Unit b Priceb	Costl(\$)
Sodding	SY	9,175	\$2.02s	\$18,534b
Clearingl&kGrubbing	AC	1.81	\$\$7,723.80	\$14,011b
SedimentlBarrierl(Siltb	LF	1,656	\$1.04s	\$1,722b

TotalkConstructionkCost:

= \$408,483b

Note: biPipebSizes band biengths birom bireliminary is torm birain birabulation biror brond is B. bbAssumed ban bextrab 292' bofb 72 binch bipeband bir 5' bofb 48 binch bipe bil ue bio bextrab bistance bio brond is C. biPipeb length bi 85' bofb 188' bpipe) birom birond bio bout fall balso bincluded bin bestimate.

Estimated Earthwork Calculations

Pond Site 3C:

Earthwork Calculations:

1. Earthwork Fill Calculations:

A. Proposed Slopes and Elevations. Existing Ground Elev. (ft) = 24.5

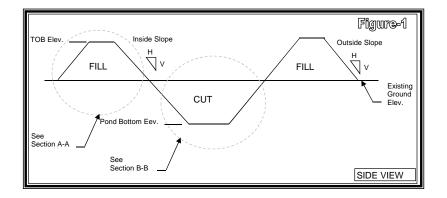
Top of Berm Elev. (ft) = 28

Pond Bottom Elev. (ft) = 10.45

Outside Slope (V:H) - 1: 4 Inside Slope (V:H) - 1: 4

Control Elev. (ft) = 22.45

*Assume Pond Bottom 12' depth below NW



B. Berm Fill Calculations.

FILL AREA (S.F.) = 0.5 (a + b) h

Perimetter @ CL of the Berm (ft) = 1,441

a (ft) = 20

b(ft) = 48

h(ft) = 3.5

FILL AREA (S.F.) = 119

Fill VOLUME (C.F.) = 171,455

Fill VOLUME (C.Y.) = 6,350 Fill VOLUME (C.Y.) = 3,175

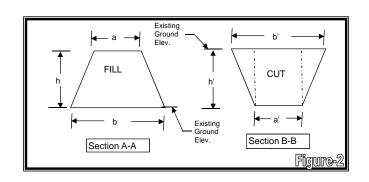
*Assumed half fill volume due to existing pond

Area Inside Berm (SF) = 32,970

Area Outside Berm (SF) = 20,792

Area Top of Berm (SF) = 28,816

Sodding (SY) = 9,175



2. Earthwork Cut Calculations:

<- Area of Cut along Side slope = (Area of specified elevation a') * h' <- Area of Cut to specified elevation

Pond Side Slopes From Inside Pond Contour at Exist. Ground Elev. to Pond Bottom:

Area Between a' & b' elevations (sf) = 60,785

(Exist. Ground Elev. to Pond Bottom)

h'(ft) = 14.1

CUT VOLUME (C.F.) = 427,012

Pond Bottom:

Area of Pond Bottom (sf) = 42,148

(Exist. Ground Elev. to Pond Bottom)

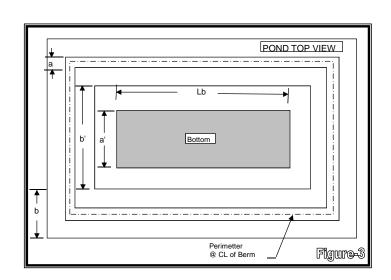
h'(ft) = 14.1CUT VOLUME (C.F.) = 592,173

TOTAL CUT VOLUME (C.F.) = 1,019,185

TOTAL CUT VOLUME (C.Y.) = 37,748

TOTAL CUT VOLUME (C.Y.) = 18,874

*Assumed half excavation volume due to existing pond



Fencing (ft) = 1656

Basin 4

 PROJECT:
 SR 710 - Pond 4A

 LOCATION:
 OKEECHOBEE COUNTY, FLORIDA

PREPARED: LCS 5/11/2015
CHECKED: GS 5/11/2015

Pondl 4Ab

PipelCosts:

i ipcacosts.			
Pipel S izeb	PipelLengthb	Unitl Priceb	
(inch)	(ft)	(\$/ft)	Costl(\$)
18	1207	\$47.49s	\$57,320
24	0	\$52.81s	\$0
30	0	\$64.20s	\$0
36	96	\$88.90	\$8,534
42	1490	\$111.76	\$166,522
48	2780	\$116.13	\$322,841
60	0	\$180.88	\$0
		Totals=	\$555,219

PipelCostlforlPondlsIAls \$555,219

Note:s200'sofs18"spipesaddedsforspondsoutfall

Earthwork:-Optionb

Pondb		
Excavationb	UnitbPriceb	
(CY)	(\$/CY)	Costl(\$)
31,090	\$4.75	\$147,678

	UnitbPriceb	
PondlFilll(CY)	(\$/CY)	Costl(\$)
10,978	0.00	\$0

ImportlFilll= 20,112 CY

SavingslbybmportinglFillltolRoadway:

	UnithPriceb	
RoadlFilll(CY)	(\$/CY)	Costl(\$)
20,112	6.00	\$120,672

EarthworkhCost/Savingsb= \$27,006

 $Note: \underline{\$Red\$ype\$\$parenthesis sindicates \$cost\$avings}$

Item	Unit	Quantity	Unitb Priceb	Costl(\$)
Sodding	SY	10,083	\$2.02s	\$20,368b
Clearingb&b				
Grubbing	AC	3.98	\$\$\$\$7,723.80	\$30,772b
Sedimentb				
Barrierl(Siltb				
Fence)	LF	1,690	\$1.04s	\$1,758b

Earthwork:-Optionb2			
Pondb			
Excavationb	UnitbPriceb		
(CY)	(\$/CY)	Costl(\$)	
20,481	\$4.75	\$97,285	

	UnitbPriceb	
PondlFilll(CY)	(\$/CY)	Costl(\$)
10,244	0.00	\$0

ImportbFillb= 10,237 CY

SavingslbybmportinglFillltolRoadway:

	UnitbPriceb	_
RoadlFilll(CY)	(\$/CY)	Costl(\$)
10,237	6.00	\$61,422

EarthworklCost/Savingsl= \$35,863

Item	Unit	Quantity	Unitb Priceb	Costl(\$)
Sodding	SY	9,409	\$2.02s	\$19,006b
Clearingt&b				
Grubbing	AC	3.34	\$\$\$\$7,723.80	\$25,821b
Sedimentb				
Barrier k (Siltb				
Fence)	LF	1,594	\$1.04s	\$1,658b

TotalkConstructionkCost:

Optionl#1b= \$635,121b Optionl#2b= \$637,566b

Estimated Earthwork Calculations

Pond Site 4A - Option 1:

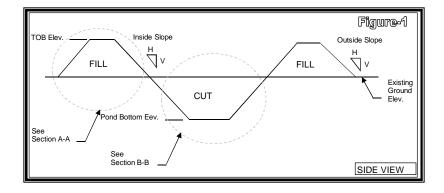
Earthwork Calculations:

1. Earthwork Fill Calculations:

A. Proposed Slopes and Elevations.

Existing Ground Elev. (ft) = 24
Top of Berm Elev. (ft) = 29
Pond Bottom Elev. (ft) = 12
Outside Slope (V:H) - 1: 4
Inside Slope (V:H) - 1: 4

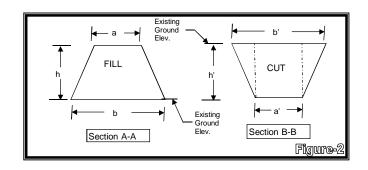
Control Elev. (ft) = 24



B. Berm Fill Calculations.

> Area Inside Berm (SF) = 30,552Area Outside Berm (SF) = 30,552Area Top of Berm (SF) = 29,640

Sodding (SY) = 10,083



2. Earthwork Cut Calculations:

CUT VOLUME (C.F.) = 0.5 (Area between a' & b') * h' <- Area of Cut along Side slope = (Area of specified elevation a') * h' <- Area of Cut to specified elevation

Pond Side Slopes From Inside Pond Contour at Exist. Ground Elev. to Pond Bottom:

Area Between a' & b' elevations (sf) = 53,889

(Exist. Ground Elev. to Pond Bottom)

h' (ft) = 12.0

CUT VOLUME (C.F.) = 323,335

Pond Bottom:

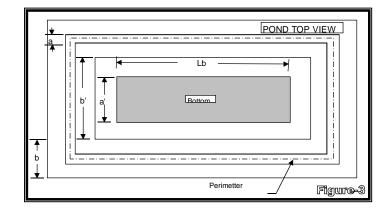
Area of Pond Bottom (sf) = 43,008

(Exist. Ground Elev. to Pond Bottom)

h' (ft) = 12.0

CUT VOLUME (C.F.) = 516,095

TOTAL CUT VOLUME (C.F.) = 839,429 TOTAL CUT VOLUME (C.Y.) = 31,090



Fencing (ft) = 1,690

Estimated Earthwork Calculations

Pond Site 4A - Option 2:

Earthwork Calculations:

1. Earthwork Fill Calculations:

A. Proposed Slopes and Elevations.

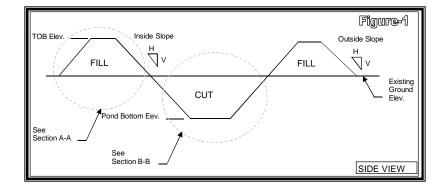
Existing Ground Elev. (ft) = 24

Top of Berm Elev. (ft) = 29

Pond Bottom Elev. (ft) = 12

Outside Slope (V:H) - 1: 4
Inside Slope (V:H) - 1: 4

Control Elev. (ft) = 24



B. Berm Fill Calculations.

FILL AREA (S.F.) = 0.5 (a + b) h

Perimetter @ CL of the Berm (ft) = 1,383

a (ft) = 20

b (ft) = 60

h (ft) = 5

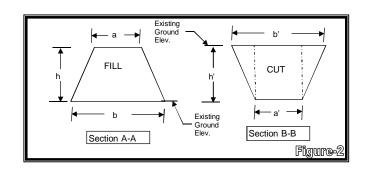
FILL AREA (S.F.) = 200

FILL OLLIMF (C.F.) = 276 600

Fill VOLUME (C.F.) = 276,600 Fill VOLUME (C.Y.) = **10,244**

Area Inside Berm (SF) = 28,511 Area Outside Berm (SF) = 28,511 Area Top of Berm (SF) = 27,660

Sodding (SY) = 9,409



2. Earthwork Cut Calculations:

CUT VOLUME (C.F.) = 0.5 (Area between a' & b') * h' <- Area of Cut along Side slope = (Area of specified elevation a') * h' <- Area of Cut to specified elevation

Pond Side Slopes From Inside Pond Contour at Exist. Ground Elev. to Pond Bottom:

Area Between a' & b' elevations (sf) = 46,628

(Exist. Ground Elev. to Pond Bottom)

h' (ft) = 12.0

CUT VOLUME (C.F.) = 279,767

Pond Bottom:

Area of Pond Bottom (sf) = 22,769

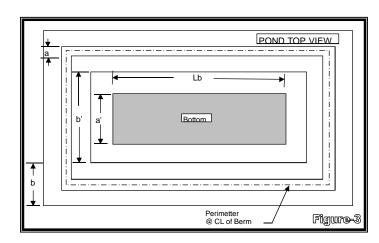
(Exist. Ground Elev. to Pond Bottom)

h' (ft) = 12.0

CUT VOLUME (C.F.) = 273,229

TOTAL CUT VOLUME (C.F.) = 552,996

TOTAL CUT VOLUME (C.Y.) = **20,481**



Fencing (ft) = 1,594

Note: Sodding quantity taken to control elevation & fencing measured at R/W line

SR 710 - Pond 4B/4C
OKEECHOBEE COUNTY, FLORIDA PROJECT: LOCATION:

PREPARED: LCS CHECKED: GS 5/5/2016 5/5/2016

Pondla4B/4Cb

PipelCosts:

i ipeacosts.			
PipelSizeb	PipelLengthb	Unit b Priceb	
(inch)	(ft)	(\$/ft)	Costl(\$)
18	1096	\$47.49	\$52,049
24	224	\$52.81	\$11,829
30	1849	\$64.20	\$118,706
36	707	\$88.90	\$62,852
42	0	\$111.76	\$0
48	1698	\$116.13	\$197,189
60	0	\$180.88	\$0
		Totals=	\$442,625

PipelCostlforlPondldB/4Cl= \$442,625

Note:s:100'sof:18"spipe:addedsforspond:soutfall

Earthwork:-Optionb

Pondb		
Excavationb	UnitbPriceb	
(CY)	(\$/CY)	Costl(\$)
50,379	\$4.75	\$239,300

	UnitbPriceb	
PondlFilll(CY)	(\$/CY)	Costl(\$)
13,344	0.00	\$0

ImportlFillb= 37,035 CY

SavingsbybmportingbillbobRoadway:

	UnitbPriceb	
RoadlFilll(CY)	(\$/CY)	Costl(\$)
37,035	6.00	\$222,210

EarthworkhCost/Savingsh= \$17,090

item	Unit	Quantity	Unitorriced	Cost n \$)
Sodding	SY	19,464	\$2.02s	\$39,317b
Clearingk&b				
Grubbing	AC	7.17	\$\$\$\$7,723.80	\$55,380b
Sedimentb				

Sodding	SY	19,464	\$2.02s	\$39,317b
Clearingk&b				
Grubbing	AC	7.17	\$\$\$\$7,723.80	\$55,380b
Sedimentb				
Barrier t (Siltb				
Fence)	LF	5,222	\$1.04s	\$5,431b

Farthwork:-Ontion®

Earthwork:-Optioniz				
Pondb				
Excavationb	UnitbPriceb			
(CY)	(\$/CY)	Costl(\$)		
33,471	\$4.75	\$158,987		

	UnitbPriceb	
PondlFilll(CY)	(\$/CY)	Costl(\$)
7,320	0.00	\$0

ImportlFillb= 26,151 CY

SavingsbybmportingbFillbobRoadway:

	UnithPriceb	-
RoadlFilll(CY)	(\$/CY)	Costl(\$)
26,151	6.00	\$156,906

EarthworkbCost/Savingsb= \$2,081

					7-/	_1	
	Note:sRedstypes&s	sparenthesissindi	catesscostssavings			_	
)	Costl(\$)		Item	Unit	Quantity	UnitbPriceb	Costl(\$)
	\$39,317b		Sodding	SY	10,621	\$2.02s	\$21,454b
			Clearingt&b				
)	\$55,380b		Grubbing	AC	4.20	\$\$\$\$7,723.80	\$32,448b
			Sedimentb				
			Barrier k (Siltb				
	\$5,431b		Fence)	LF	2,513	\$1.04s	\$2,614b

TotalbConstructionbCost:

Optionb#1b= \$559,843b Optionl#2b= \$501,222b

Estimated Earthwork Calculations

Pond Site 4B/4C - Option 1:

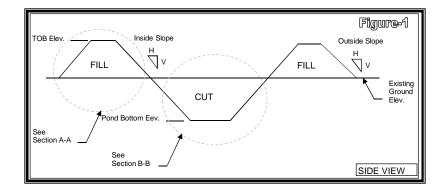
Earthwork Calculations:

1. Earthwork Fill Calculations:

A. Proposed Slopes and Elevations.

Existing Ground Elev. (ft) = 24
Top of Berm Elev. (ft) = 27.38
Pond Bottom Elev. (ft) = 10.25
Outside Slope (V:H) - 1: 4
Inside Slope (V:H) - 1: 4

Contol El. (ft) = 22.25



B. Berm Fill Calculations.

FILL AREA (S.F.) = 0.5 (a + b) h

Perimetter @ CL of the Berm (ft) = 3,180

a (ft) = 20

b (ft) = 47.04

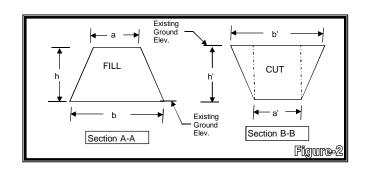
h (ft) = 3.38

FILL AREA (S.F.) = 113.2976

Fill VOLUME (C.F.) = 360,286

Fill VOLUME (C.Y.) = 13,344

Area Inside Berm (SF) = 67,262 Area Outside Berm (SF) = 44,317 Area Top of Berm (SF) = 63,600 Sodding (SY) = 19,464



2. Earthwork Cut Calculations:

CUT VOLUME (C.F.) = 0.5 (Area between a' & b') * h' <- Area of Cut along Side slope = (Area of specified elevation a') * h' <- Area of Cut to specified elevation

Pond Side Slopes From Inside Pond Contour at Exist. Ground Elev. to Pond Bottom:

Area Between a' & b' elevations (sf) = 121,368 (Exist. Ground Elev. to Pond Bottom)

h' (ft) = 13.8

CUT VOLUME (C.F.) = 834,406

Pond Bottom:

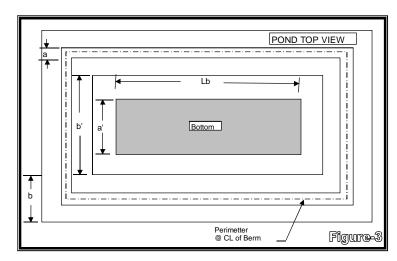
Area of Pond Bottom (sf) = 38,241 (Exist. Ground Elev. to Pond Bottom)

h' (ft) = 13.8

CUT VOLUME (C.F.) = 525,819

TOTAL CUT VOLUME (C.F.) = 1,360,225

TOTAL CUT VOLUME (C.Y.) = **50,379**



Fencing (ft) = 5,222

Note: Sodding quantity taken to control elevation & fencing measured at R/W line

Estimated Earthwork Calculations

Pond Site 4B - Option 2:

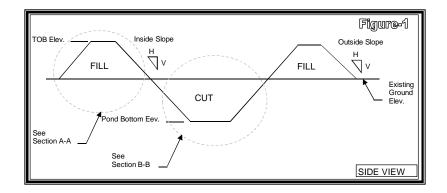
Earthwork Calculations:

1. Earthwork Fill Calculations:

A. Proposed Slopes and Elevations.

Existing Ground Elev. (ft) = 24
Top of Berm Elev. (ft) = 27.4
Pond Bottom Elev. (ft) = 10.25
Outside Slope (V:H) - 1: 4
Inside Slope (V:H) - 1: 4

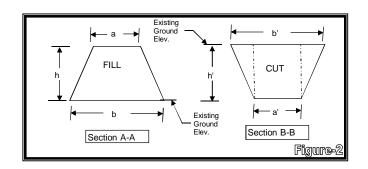
Contol El. (ft) = 22.25



B. Berm Fill Calculations.

> Area Inside Berm (SF) = 36,735Area Outside Berm (SF) = 24,252Area Top of Berm (SF) = 34,600

Sodding (SY) = 10,621



2. Earthwork Cut Calculations:

CUT VOLUME (C.F.) = 0.5 (Area between a' & b') * h' <- Area of Cut along Side slope = (Area of specified elevation a') * h' <- Area of Cut to specified elevation

Pond Side Slopes From Inside Pond Contour at Exist. Ground Elev. to Pond Bottom:

Area Between a' & b' elevations (sf) = 70,057

(Exist. Ground Elev. to Pond Bottom)

h' (ft) = 13.8

CUT VOLUME (C.F.) = 481,640

Pond Bottom:

Area of Pond Bottom (sf) = 30,696

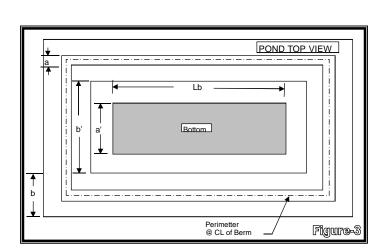
(Exist. Ground Elev. to Pond Bottom)

h' (ft) = 13.8

CUT VOLUME (C.F.) = 422,071

TOTAL CUT VOLUME (C.F.) = 903,712

TOTAL CUT VOLUME (C.Y.) = 33,471



Fencing (ft) = 2,513

Note: Sodding quantity taken to control elevation & fencing measured at R/W line

<u>Construction</u><u>Costs</u>

PROJECT: SR 710 - Pond 4D
LOCATION: OKEECHOBEE COUNTY, FLORIDA

PREPARED: LCS CHECKED: GS 5/11/2015 5/11/2015

Pondl#Db

PipelCosts:

Pipeucosts:			
PipelSizeb	PipelLengthb	Unit b Priceb	
(inch)	(ft)	(\$/ft)	Costl(\$)
18	2909	\$47.49	\$138,148
24	224	\$52.81	\$11,829
30	1849	\$64.20	\$118,706
36	803	\$88.90	\$71,387
42	1490	\$111.76	\$166,522
48	0	\$116.13	\$0
60	0	\$180.88	\$0
		Totals=	\$506,593

PipelCostlforlPondldDb= \$506,593

Note:s1800'sofs18"spipesaddedsforspondsoutfall

Earthwork:-Optionb

Pondb				
Excavationb	UnitbPriceb			
(CY)	(\$/CY)	Costl(\$)		
46,216	\$4.75	\$219,526		

	UnitbPriceb	
PondlFilll(CY)	(\$/CY)	Costl(\$)
7,065	0.00	\$0

ImportlFillb= 39,151 CY

SavingslbybmportinglFillltolRoadway:

	UnitbPriceb	
RoadlFilll(CY)	(\$/CY)	Costl(\$)
39,151	6.00	\$234,906

EarthworklCost/Savingsl=	(\$15,380)
--------------------------	------------

 $Note: \underline{sRedstypes\&sparenthesissindicates xcostssavings}$

Item	Unit	Quantity	UnitbPriceb	Costl(\$)
Sodding	SY	11,853	\$2.02s	\$23,943b
Clearingb&b				
Grubbing	AC	6.08	\$\$\$\$7,723.80	\$46,922b
Sedimentb				
Barrierl(Siltb				
Fence)	LF	2,873	\$1.04s	\$2,988b

TotalkConstructionkCost:

Optionl#1b= \$565,066b Optionl#2b= \$594,761b

Earthwork:-Optionb2

Pondb		
Excavationb	UnitbPriceb	
(CY)	(\$/CY)	Costl(\$)
28,710	\$4.75	\$136,373

	UnitbPriceb	
PondlFilll(CY)	(\$/CY)	Costl(\$)
9,401	0.00	\$0

ImportlFillb= 19,309 CY

SavingslbybmportinglFillbobRoadway:

	UnitbPriceb	
RoadlFilll(CY)	(\$/CY)	Costl(\$)
19,309	6.00	\$115,854

EarthworklCost/Savingsl=	\$20,519
--------------------------	----------

Item	Unit	Quantity	Unitl Priceb	Costl(\$)
Sodding	SY	15,772	\$2.02s	\$31,859b
Clearingt&b				
Grubbing	AC	4.33	\$\$\$\$7,723.80	\$33,429b
Sedimentb				
Barrierk(Siltb				
Fence)	LF	2,271	\$1.04s	\$2,362b

Estimated Earthwork Calculations

Pond Site 4D - Option 1:

Earthwork Calculations:

1. Earthwork Fill Calculations:

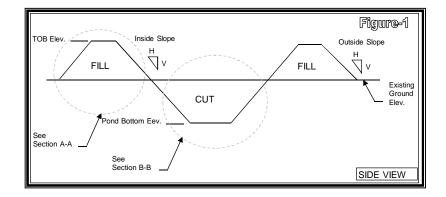
A. Proposed Slopes and Elevations.

Existing Ground Elev. (ft) = $\frac{26}{100}$ Top of Berm Elev. (ft) = 29Pond Bottom Elev. (ft) = 11.83

Outside Slope (V:H) - 1: 4

Inside Slope (V:H) - 1: 4

Contol El. (ft) = 23.83



B. Berm Fill Calculations.

FILL AREA (S.F.) = 0.5 (a + b) h Perimetter @ CL of the Berm (ft) = 1,987

a (ft) = 20b(ft) = 44

h(ft) = 3FILL AREA (S.F.) = 96

Fill VOLUME (C.F.) = 190,752

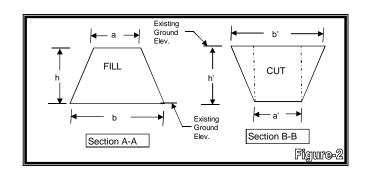
Fill VOLUME (C.Y.) = 7,065

Area Inside Berm (SF) = 42,356

Area Outside Berm (SF) = 24,578

Area Top of Berm (SF) = 39,740

Sodding (SY) = 11,853



2. Earthwork Cut Calculations:

CUT VOLUME (C.F.) = 0.5 (Area between a' & b') * h'

<- Area of Cut along Side slope = (Area of specified elevation a') * h' <- Area of Cut to specified elevation

Pond Side Slopes From Inside Pond Contour at Exist. Ground Elev. to Pond Bottom:

Area Between a' & b' elevations (sf) = 126,421

(Exist. Ground Elev. to Pond Bottom)

h'(ft) = 14.2

CUT VOLUME (C.F.) = 895,693

Pond Bottom:

Area of Pond Bottom (sf) = 24,851

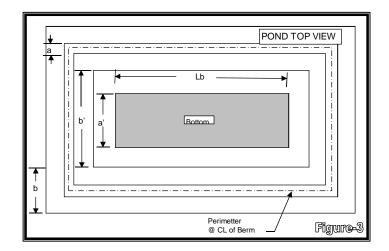
(Exist. Ground Elev. to Pond Bottom)

h'(ft) = 14.2

CUT VOLUME (C.F.) = 352,137

TOTAL CUT VOLUME (C.F.) = 1,247,830

TOTAL CUT VOLUME (C.Y.) = 46,216



Fencing (ft) = 2,873

Estimated Earthwork Calculations

Pond Site 4D - Option 2:

Earthwork Calculations:

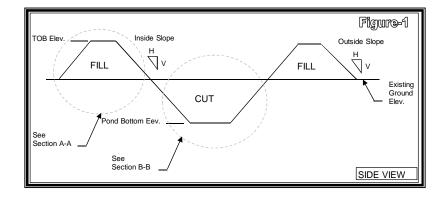
1. Earthwork Fill Calculations:

A. Proposed Slopes and Elevations.

Existing Ground Elev. (ft) = $\frac{26}{100}$ Top of Berm Elev. (ft) = 29Pond Bottom Elev. (ft) = 11.83 Outside Slope (V:H) - 1: 4

Inside Slope (V:H) - 1: 4

Contol El. (ft) = 23.83



B. Berm Fill Calculations.

FILL AREA (S.F.) = 0.5 (a + b) h Perimetter @ CL of the Berm (ft) = 2,644

a (ft) = 20b(ft) = 44

h(ft) = 3

FILL AREA (S.F.) = 96

Fill VOLUME (C.F.) = 253,824

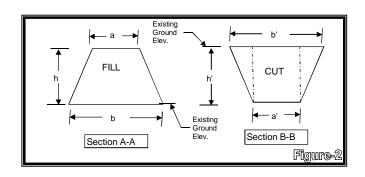
Fill VOLUME (C.Y.) = 9,401

Area Inside Berm (SF) = 56,361

Area Outside Berm (SF) = 32,704

Area Top of Berm (SF) = 52,880

Sodding (SY) = 15,772



2. Earthwork Cut Calculations:

CUT VOLUME (C.F.) = 0.5 (Area between a' & b') * h' = (Area of specified elevation a') * h' <- Area of Cut along Side slope <- Area of Cut to specified elevation

Pond Side Slopes From Inside Pond Contour at Exist. Ground Elev. to Pond Bottom:

Area Between a' & b' elevations (sf) = 92,573

(Exist. Ground Elev. to Pond Bottom)

h'(ft) = 14.2

CUT VOLUME (C.F.) = 655,878

Pond Bottom:

Area of Pond Bottom (sf) = 8,418

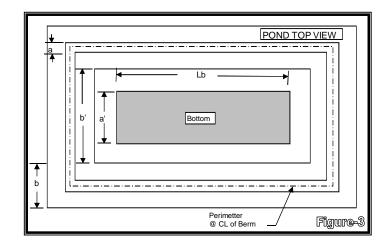
(Exist. Ground Elev. to Pond Bottom)

h'(ft) = 14.2

CUT VOLUME (C.F.) = 119,282

TOTAL CUT VOLUME (C.F.) = 775,161

TOTAL CUT VOLUME (C.Y.) = 28,710



Fencing (ft) = 2,271

Note: Sodding quantity taken to control elevation & fencing measured at R/W line

Basin 5

 PROJECT:
 SR 710 - Pond 5A
 PREPARED:
 LCS
 5/11/2015

 LOCATION:
 OKEECHOBEE COUNTY, FLORIDA
 CHECKED:
 GS
 5/11/2015

Pondl A

PipelCosts:lbOutfallbPipelOnly

	PipelLengthb	Unit Priceb	
PipelSizel(inch)	(ft)	(\$/ft)	Costl(\$)
18	595	\$47.49	\$28,257
		Totals=	\$28,257

PipelCostlforlPondl5Al= \$28,257

Embankment:

	Unitb Priceb	
PondlFilll(CY)	(\$/CY)	Costl(\$)
8,628	\$6.00	\$51,768

Underdrain:

Lengthlofb	Unit b Priceb	
Underdraink(ft)	(\$/ft)	Costl(\$)
3,570	\$40.00	\$142,800

Estimatedsbysmeasurements-s51s@s70'slengths

Item	Unit	Quantity	Unit b Priceb	Costk(\$)
Sodding	SY	12,330	\$2.02s	\$24,907b
Clearingl&kGrubbing	AC	2.62	\$s7,723.80	\$20,267b
SedimentlBarrierl(SiltlFence)	LF	1,632	\$1.04s	\$1,697b

TotalkConstructionkCost:

= \$269,696b

Note: bOutfall bPipe blength b (595' bofb 18" bpipe) bincluded bin bestimate.

Estimated Earthwork Calculations

Pond Site 5A:

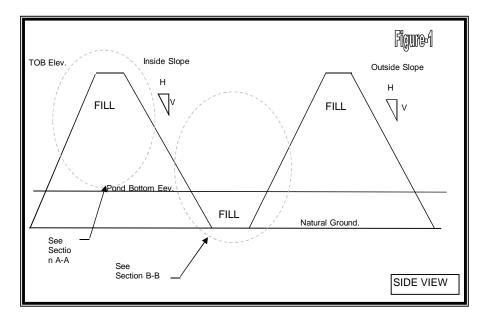
Earthwork Calculations:

1. Earthwork Fill Calculations:

A. Proposed Slopes and Elevations.

Existing Ground Elev. (ft) = 23
Top of Berm Elev. (ft) = 27
Pond Bottom Elev. (ft) = 24
Outside Slope (V:H) - 1: 4
Inside Slope (V:H) - 1: 4

Pond Bottom (ft) = 24



B. Berm Fill Calculations.

FILL AREA (S.F.) = 0.5 (a + b) h

Perimetter @ CL of the Berm (ft) = 1,408

a (ft) = 20

b (ft) = 47.5

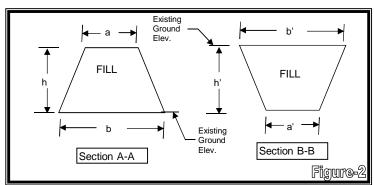
h (ft) = 4

FILL AREA (S.F.) = 135

Fill VOLUME (C.F.) = 190,134

Fill VOLUME (C.Y.) = 7,042

Sodding (SY) = 12,330



2. Embankment Fill Calculations:

FILL AREA (S.F.) = 0.5 (a' + b') h'

Pond bottom Length (ft) = 532

a' (ft) = 76.5

b' (ft) = 84.5

h' (ft) = 1

FILL AREA (S.F.) = 80.5

FILL VOLUME (C.F.) = 42,826

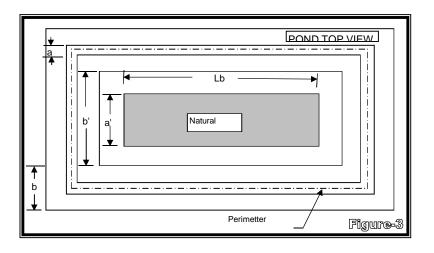
FILL VOLUME (C.Y.) = 1,586

Sodding (SY) = 545,097,574

Total Fill: 8,628 C.Y.

Note: b' and Lb are the length and width of pond bottom. The a' is the width of natural ground elevation

Fencing (ft) = 1,632



 PROJECT:
 SR 710 - Pond 5B
 PREPARED:
 LCS
 5/11/2015

 LOCATION:
 OKEECHOBEE COUNTY, FLORIDA
 CHECKED:
 GS
 5/11/2015

Pondl5B

PipelCosts:lbOutfallbPipelOnly

	Pipel <u>L</u> engthb	Unit b Priceb	
PipelSizel(inch)	(ft)	(\$/ft)	Costl(\$)
18	125.00	\$47.49	\$5,936
		Totalb=	\$5,936

PipelCostlforlPondl5Bl= \$5,936

Embankment:

	Unit b Priceb	
PondlFilll(CY)	(\$/CY)	Costl(\$)
10,020	\$6.00	\$60,120

Underdrain:

Lengthbofb	Unit b Priceb	
Underdraink(ft)	(\$/ft)	Costl(\$)
3,848	\$40.00	\$153,920

Estimatedsbysmeasurements-\$52\$@\$74'dengths

Item	Unit	Quantity	Unit b Priceb	Costl(\$)
Sodding	SY	11,800	\$2.02s	\$23,836b
Clearingl&kGrubbing	AC	2.53	\$s7,723.80	\$19,572b
SedimentlBarrierl(SiltlFence)	LF	1,633	\$1.04s	\$1,698b

TotalkConstructionkCost:

= \$265,083b

Note: bOutfall bPipe blength b(125' bofb18" bpipe) bincluded bin bestimate.

Estimated Earthwork Calculations

Pond Site 5B:

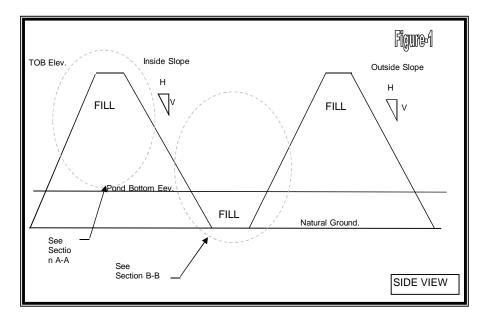
Earthwork Calculations:

1. Earthwork Fill Calculations:

A. Proposed Slopes and Elevations.

Existing Ground Elev. (ft) = 22.5 Top of Berm Elev. (ft) = 27 Pond Bottom Elev. (ft) = 24 Outside Slope (V:H) - 1: 4 Inside Slope (V:H) - 1: 4

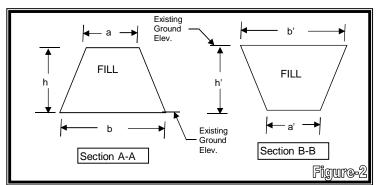
Pond Bottom (ft) = 24



B. Berm Fill Calculations.

FILL AREA (S.F.) = 0.5 (a + b) h Perimetter @ CL of the Berm (ft) = 1,376a (ft) = 20b (ft) = 50h (ft) = 4.5FILL AREA (S.F.) = 157.5Fill VOLUME (C.F.) = 216,720Fill VOLUME (C.Y.) = 8,027

Sodding (SY) = 11,800



2. Embankment Fill Calculations:

FILL AREA (S.F.) = 0.5 (a' + b') h'

Pond bottom Length (ft) = 523

a' (ft) = 62.6

b' (ft) = 74.6

h' (ft) = 1.5

FILL AREA (S.F.) = 102.9

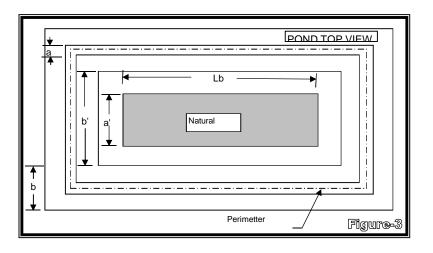
FILL VOLUME (C.F.) = 53,817

FILL VOLUME (C.Y.) = 1,993



Note: b' and Lb are the length and width of pond bottom. The a' is the width of natural ground elevation

Fencing (ft) = 1,633



 PROJECT:
 SR 710 - Pond 5C
 PREPARED:
 LCS
 5/11/2015

 LOCATION:
 OKEECHOBEE COUNTY, FLORIDA
 CHECKED:
 GS
 5/11/2015

Pondl5C

PipelCosts:lbOutfallbPipelOnly

PipelSizel(inch)	Pipebengthb (ft)	Unit b riceb (\$/ft)	Costl(\$)
18	400.00	\$47.49	\$18,996
		Total b ≠	\$18,996

PipelCostlforlPondl5Cl= \$18,996

Embankment:

	UnitlPriceb	
PondlFilll(CY)	(\$/CY)	Costl(\$)
5,878	\$6.00	\$35,268

Underdrain:

Lengthlofb Underdrainl(ft)	Unit b riceb (\$/ft)	Costl(\$)
3,750	\$40.00	\$150,000

Estimated by smeasurements-\$25\$@\$150's lengths

ltem	Unit	Quantity	Unitl Priceb	Costl(\$)
Sodding	SY	16,444	\$2.02s	\$33,217b
Clearingl&kGrubbing	AC	3.53	\$s7,723.80	\$27,250b
SedimentlBarrierl(SiltlFence)	LF	1,916	\$1.04s	\$1,993b

TotalkConstructionkCost:

= \$266,723b

Note: bOutfall bripe blength b 400 bofb 8" bpipe) bincluded bin bestimate.

Estimated Earthwork Calculations

Pond Site 5C:

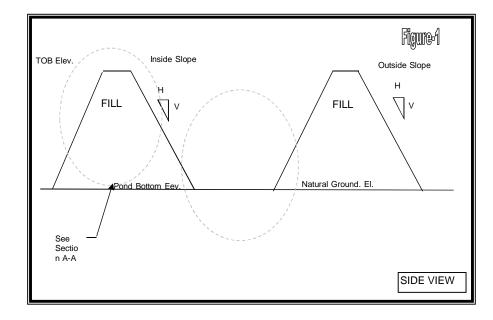
Earthwork Calculations:

1. Earthwork Fill Calculations:

A. Proposed Slopes and Elevations.

Existing Ground Elev. (ft) = 24
Top of Berm Elev. (ft) = 27
Pond Bottom Elev. (ft) = 24
Outside Slope (V:H) - 1: 4
Inside Slope (V:H) - 1: 4

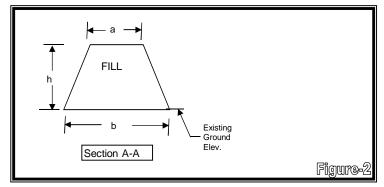
Pond Bottom (ft) = 24



B. Berm Fill Calculations.

FILL AREA (S.F.) = 0.5 (a + b) h
Perimetter @ CL of the Berm (ft) = 1,653
a (ft) = 20
b (ft) = 44
h (ft) = 3
FILL AREA (S.F.) = 96
Fill VOLUME (C.F.) = 158,707
Fill VOLUME (C.Y.) = 5,878

Sodding (SY) = 16,444



Fencing (ft) = 1,916

Note: Sodding quantity taken as entire dry pond & fencing measured at R/W line

Total Fill:	5.878 C.Y.

ENGINEERS OPINION OF PROBABLE COSTS - Regional Pond Option B

Estimated Cost for Construction Services

SR-710 (FPID 419344-3-52-01)									
Item	Description		Description		Unit	Quantity	Unit Price	Amount	
		General Conditions							
POND									
0104	10	3 Sediment Barrier (Silt Fence Staked)	LF	5,446	\$ 1.04	\$ 5,663.84			
0110	1	1 Clearing and Grubbing	AC	26.00	\$ 7,723.80	\$ 200,818.80			
0120	1	Excavation Regular	CY	385,180	\$ 4.75	\$ 1,829,605.00			
0120	6	Embankment	CY	30,430	\$ -	\$ -			
0530	3	4 Riprap, Rubble, F&I, Ditch Lining - (8' wide around pond)*	TN	80	\$ 94.33	\$ 7,549.04			
0570	1	1 Performance Turf (Seed and Mulch for dry bottom)	SY	0	\$ 0.49	\$ -			
0570	1	2 Performance Turf, Sod	SY	18,153	\$ 2.02	\$ 36,669.73			
Pump Station	<u> </u> ว								
0448	73	Pumping Station - Drainage	LS	1	\$500,000.00	\$ 500,000.00			
		Pond Accessories for Treatment	LS	1	\$200,000.00	\$ 200,000.00			
					Sub-Total:	\$ 2,780,306.41			
0101	1	Mobilization (L.S.) - 15%	L.S.	1	\$417,045.96 Grand Total:	\$ 417,045.96 \$ 3,197,352.38			

^{*} Estimated at 100 SY \$ 3,198,000.00

Note:

This opinion of costs is based on the best available information and on the opinion of the engineer. The items in the opinion of costs require proposals from other contractors and consultants. Some of the work stated in this opinion of costs requires investigative work that has not been completed. Although every effort has been made to provide a reasonable budget number it should be noted that the actual costs could be significantly more or less that stated in the opinion of costs. This opinion should be used to determine an order of magnitude for the costs. It is recommended that the owner obtain firm quotes from the various contractors in order to obtain a more accurate number. The costs stated in the opinion can also be influenced by market conditions, legal and regulatory conditions which are unforeseen.

Estimated Reduction in cost for use of excavation as embankment -				\$ (2,128,500
Pipe Cost - Storm Sewer (from total pipe cost of selected pond sites)				\$ 1,914,061
Total Pond Construction Cost				\$ 2,983,561
Estimated Right-of-Way Acquisition Cost from FDOT				\$ 586,000
Wetland Mitigation				\$ 211,200
Total Pond Cost				\$ 3,781,200
Pond Maint Cost (30 Years)	Ac	26	\$ 1,485.00	\$ 1,158,300
Pump Maint Cost	EA Year	30	\$ 15,000.00	\$ 450,000
Pump replacement Cost	EA	1	\$300,000.00	\$ 300,000
Pump Electical Cost	EA Year	30	\$ 7,200.00	\$ 216,000
Total Maintenance Cost				\$ 2,124,300
Total Pond Cost (30 Year Life Cycle)				\$ 5,905,500
Postage Stamp Pond Option				\$ 3,610,939
Pond Maint Cost (30 Years)	Ac	18.76	\$ 1,485.00	\$ 835,758
Total Postage Stamp Pond Cost (30 Year Life Cycle)				\$ 4,446,697
Cost Comparison				
Pond Initial Cost Comparison (Regional minus Postage Stamp)			\$ 170,261	
Pond 30 Year Life Cycle Cost Comparison (Regional minus Postag	ge Stamp)			\$ 1,458,803

Pond Site 2D - Regional Pond:

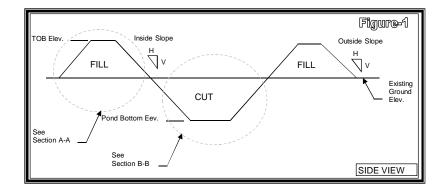
Earthwork Calculations:

1. Earthwork Fill Calculations:

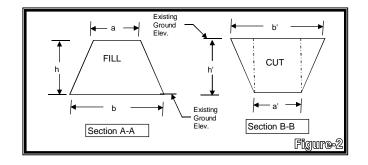
A. Proposed Slopes and Elevations.

Existing Ground Elev. (ft) = 23
Top of Berm Elev. (ft) = 28
Pond Bottom Elev. (ft) = 23.0
Outside Slope (V:H) - 1: 4
Inside Slope (V:H) - 1: 4

Control Elev. (ft) = 23



B. Berm Fill Calculations.



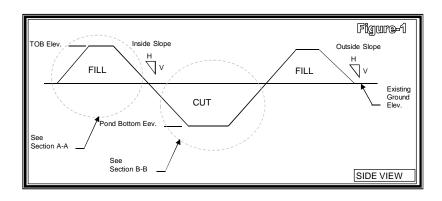
1. Earthwork Fill Calculations:

A. Proposed Slopes and Elevations.

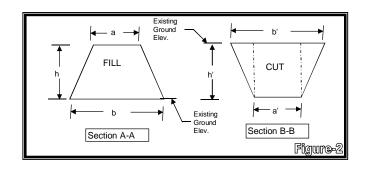
Existing Ground Elev. (ft) = 23 Top of Berm Elev. (ft) = 26 Pond Bottom Elev. (ft) = 23.0 Outside Slope (V:H) - 1: 4

Inside Slope (V:H) - 1: 4

Control Elev. (ft) = 23

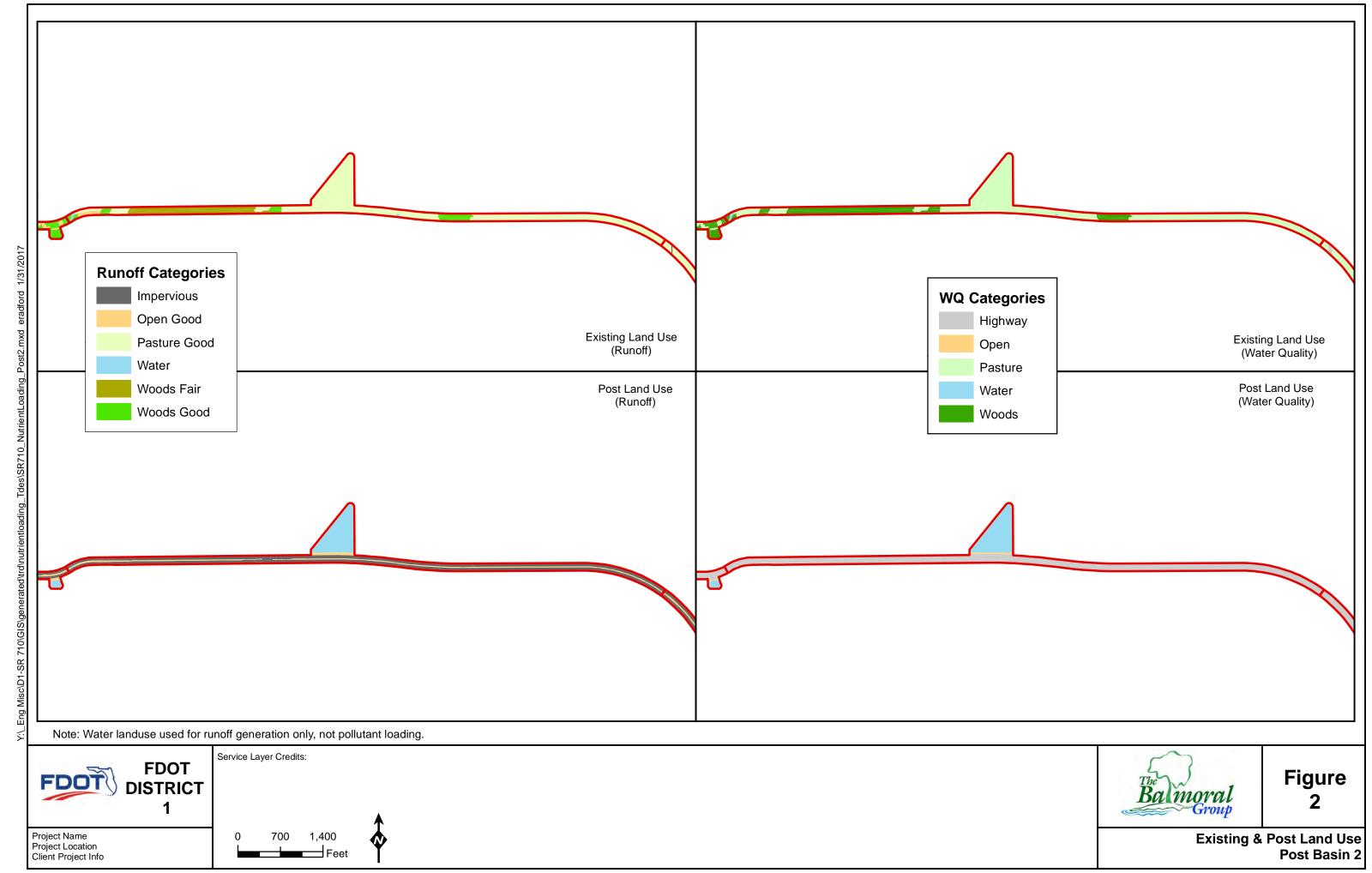


B. Berm Fill Calculations.



Appendix 7 Pollutant Loading Calculations





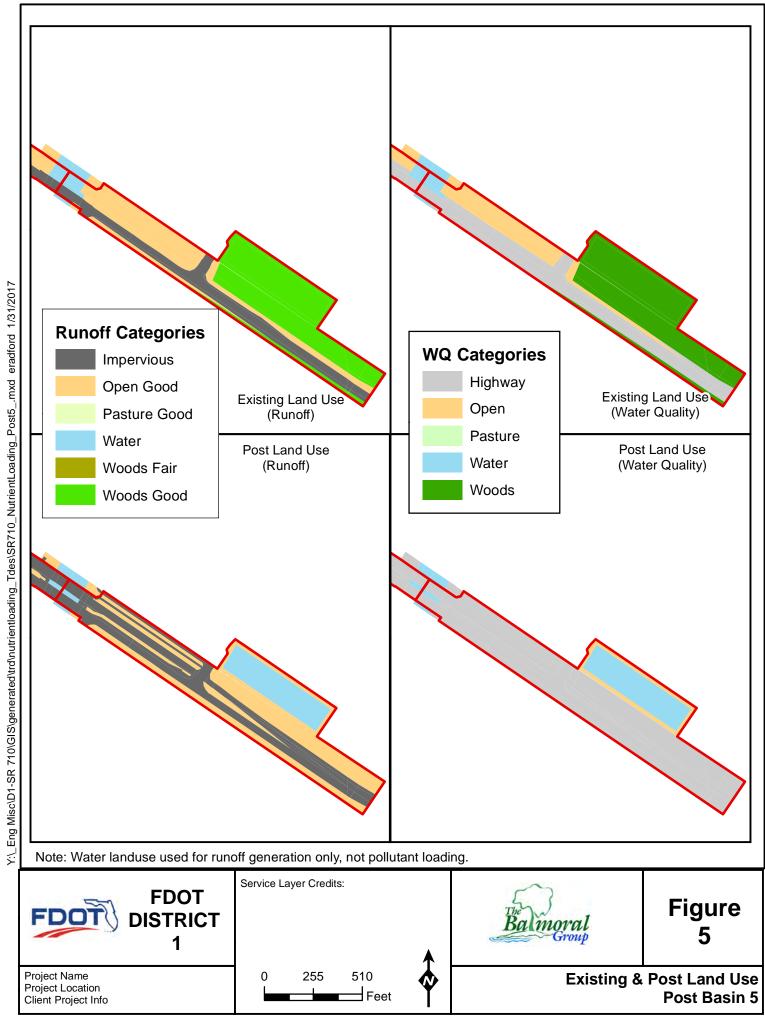


Table 1a. Curve Number Calculation Existing Condtions

	Exist Land Use for	Hydrologic Soil	1		
BasinID	CN Tables	Group	CN ¹	Area (ac)	Percent DCIA
	Impervious	B/D	*	0.00	100
	Open Good	B/D	61	1.54	5
	Water	B/D	*	0.00	100
Pre1	Woods Good	B/D	55	3.23	5
	Open Good	B/D	61	0.74	5
	Pasture Good	A/D	39	3.18	5
	Pasture Good	B/D	61	24.51	5
	Pasture Good	C/D	74	4.81	5
	Water	A/D	*	0.04	100
	Water	B/D	*	0.24	100
	Woods Fair	A/D	36	0.26	5
	Woods Fair	C/D	73	6.25	5
	Woods Good	A/D	30	0.19	5
	Woods Good	B/D	55	0.85	5
Pre2	Woods Good	C/D	70	3.68	5
	Impervious	A/D	*	0.04	100
	Impervious	B/D	*	0.26	100
	Open Good	B/D	61	0.03	5
	Pasture Good	A/D	39	1.80	5
	Pasture Good	B/D	61	10.38	5
Pre3	Water	A/D	*	0.00	100
1103	Impervious	A/D	*	0.08	100
	Impervious	B/D	*	1.91	100
	Impervious	W	*	0.05	100
	Open Good	A/D	39	0.84	5
	Open Good	B/D	61	5.02	5
	Pasture Good	B/D	61	3.16	5
	Water	B/D	*	0.14	100
	Water	W	*	0.16	100
	Woods Good	A/D	30	1.84	5
Pre4	Woods Good	B/D	55	9.54	5
1101	Impervious	B/D	*	2.23	100
	Impervious	C/D	*	0.11	100
	Impervious	W	*	0.16	100
	Open Good	B/D	61	3.13	5
	Open Good	C/D	74	0.11	5
	Open Good	W	*	0.10	5
	Water	W	*	0.10	100
	Woods Good	B/D	55	4.94	5
Pre5	Woods Good	C/D	70	0.53	5
1103	Impervious	A/D	*	0.33	100
	Impervious	B/D	*	3.15	100
	Open Good	A/D	39	0.98	5
	Open Good	B/D	61	3.45	<u>5</u>
	Water	A/D	*	0.42	100
EV 4			*	+ + + + + + + + + + + + + + + + + + + +	
EX 4	Water	B/D	4.	0.68	100

¹Non-DCIA Curve Number. Impervious areas and water were assumed to be DCIA and were removed from the CN calculations.

Table 1b. Curve Number Calculation Post Conditions

BasinID	Post Land Use for	Hydrologic Soil	CN^1	Area (ac)	Percent DCIA
DasiiiiD	CN Tables	Group	CIV	Area (ac)	refeelit DelA
	Impervious	B/D	*	2.55	100
Post1	Open Good	B/D	61	1.76	5
	Water	B/D	*	0.46	100
	Impervious	A/D	*	2.43	100
	Impervious	B/D	*	13.09	100
	Impervious	C/D	*	8.44	100
Post2	Open Good	A/D	39	1.24	5
F0312	Open Good	B/D	61	7.71	5
	Open Good	C/D	74	4.66	5
	Water	B/D	*	5.54	100
	Water	C/D	*	1.65	100
	Impervious	B/D	*	3.70	100
	Impervious	C/D	*	0.27	100
	Impervious	W	*	0.36	100
Post5	Open Good	B/D	61	4.69	5
	Open Good	C/D	74	0.48	5
	Open Good	W	*	0.06	5
	Water	B/D	*	2.12	100

¹Non-DCIA Curve Number. Impervious areas and water were assumed to be DCIA and were removed from the CN calculations.

Table 2a. Breakdown of Existing Conditions Land Use for Event Mean Concentration Lookup

	Existing Land Use for EMC		Event Mean Concentration			
BasinID	Tables	Area (ac)	(mg/L)			
	100.00		TP	TN		
	Highway	0.00	0.155	1.19		
	Pasture	1.54	0.7	2.48		
	Water	0.00	0	0		
Pre1	Woods	3.23	0.055	1.15		
	Pasture	33.25	0.7	2.48		
	Water	0.28	0	0		
Pre2	Woods	11.23	0.055	1.15		
	Highway	0.56	0.155	1.19		
	Pasture	11.96	0.7	2.48		
Pre3	Water	0.00	0	0		
	Highway	4.22	0.155	1.19		
	Open	3.69	0.055	1.15		
	Pasture	3.16	0.7	2.48		
	Water	0.30	0	0		
Pre4	Woods	11.38	0.055	1.15		
	Highway	3.78	0.155	1.19		
	Open	2.07	0.055	1.15		
	Water	0.37	0	0		
Pre5	Woods	5.47	0.055	1.15		
	Highway	6.57	0.155	1.19		
	Open	1.34	0.055	1.15		
EX 4	Water	1.04	0	0		

Table 2b. Breakdown of Proposed Conditions Land Use for Event Mean Concentration Lookup

			Event Mean Concentration		
BasinID	Post Land Use for EMC Tables	Area (ac)	(mg/L)		
			TP	TN	
	Highway	4.05	0.155	1.19	
	Open	0.26	0.055	1.15	
Post1	Water	0.46	0	0	
	Highway	36.29	0.155	1.19	
	Open	1.28	0.055	1.15	
Post2	Water	7.19	0	0	
	Highway	8.21	0.155	1.19	
	Open	0.95	0.055	1.15	
Post5	Water	2.44	0	0	

Table 3a. Summary of Values used for Existing Conditions Calculation

BasinID	Area (ac)	Non-DCIA CN	Percent DCIA	Runoff Coefficient	TP EMC (mg/L)	TN EMC (mg/L)
Pre1	4.77	56.94	5.00	0.06	0.26	1.58
Pre2	44.76	62.87	5.59	0.08	0.53	2.13
Pre3	12.52	57.76	7.34	0.08	0.68	2.42
Pre4	22.75	54.50	14.79	0.14	0.16	1.33
Pre5	11.68	58.31	28.37	0.24	0.09	1.13
EX 4	8.95	56.13	52.93	0.44	0.12	1.05

Total 105.43

Table 3b. Summary of Values used for Proposed Conditions Calculation

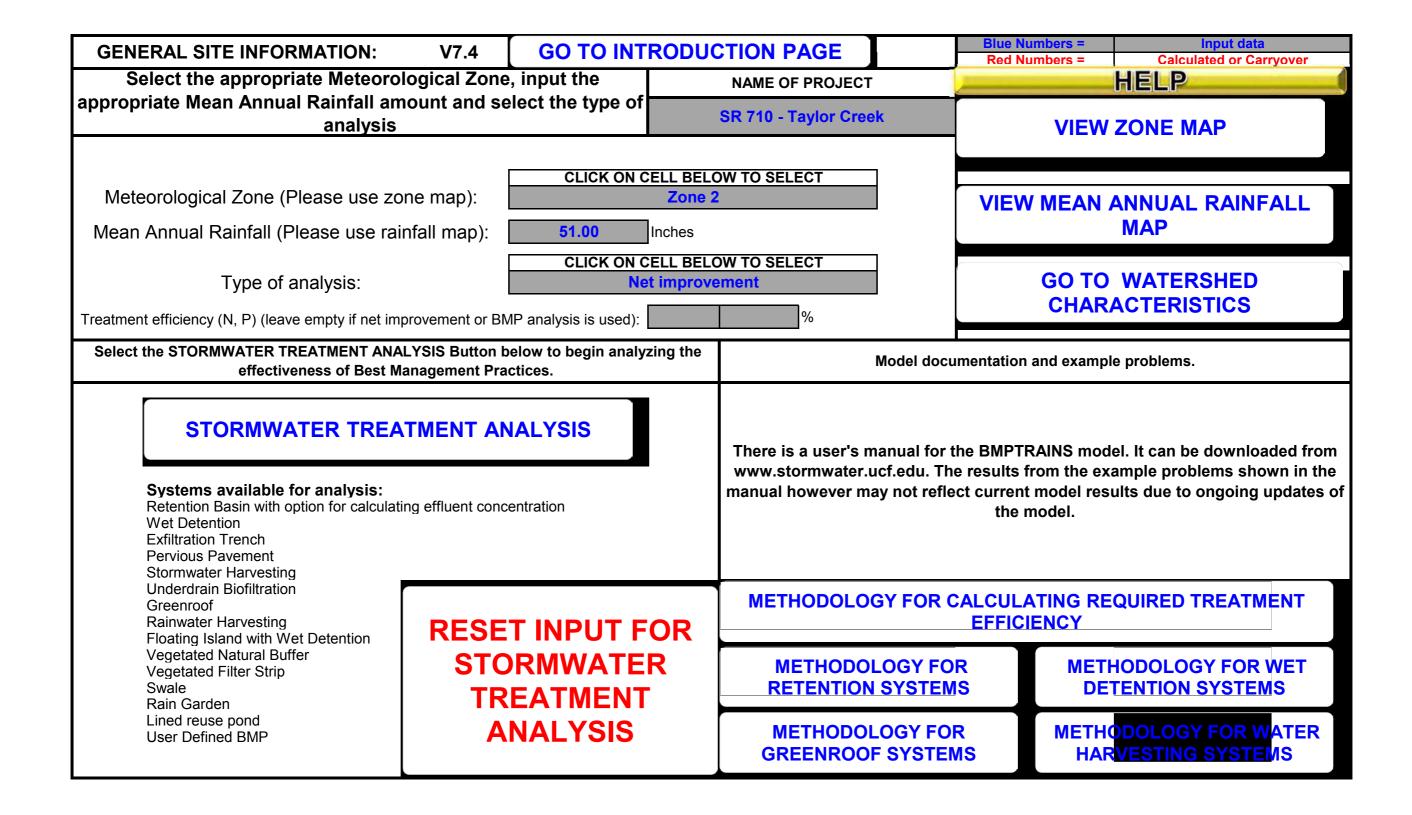
BasinID		Non-DCIA	Percent	Runoff	TP EMC	
	Area (ac)	CN	DCIA	Coefficient	(mg/L)	TN EMC (mg/L)
Post1	4.77	61.00	65.01	0.54	0.13	1.07
Post2	44.76	63.44	71.12	0.59	0.13	1.00
Post5	11.68	62.20	57.46	0.47	0.12	0.97

Total 61.21

Table 4. BMP Treatment Summary

Basin	Method	Annual Runoff (ac/ft/yr)	Retention Depth (in)*	Permanent Pool Volume (ac-ft)	Hydraulic Residence Time (days), Wet Detention Only
Post1	Dry Retention	10.9	1.08		
Post2	Wet Detention	111.6		37.47	122.52
Post5	Dry Retention	23.2	0.98		
EX 4	Wet Detention	16.7		4.85	105.79

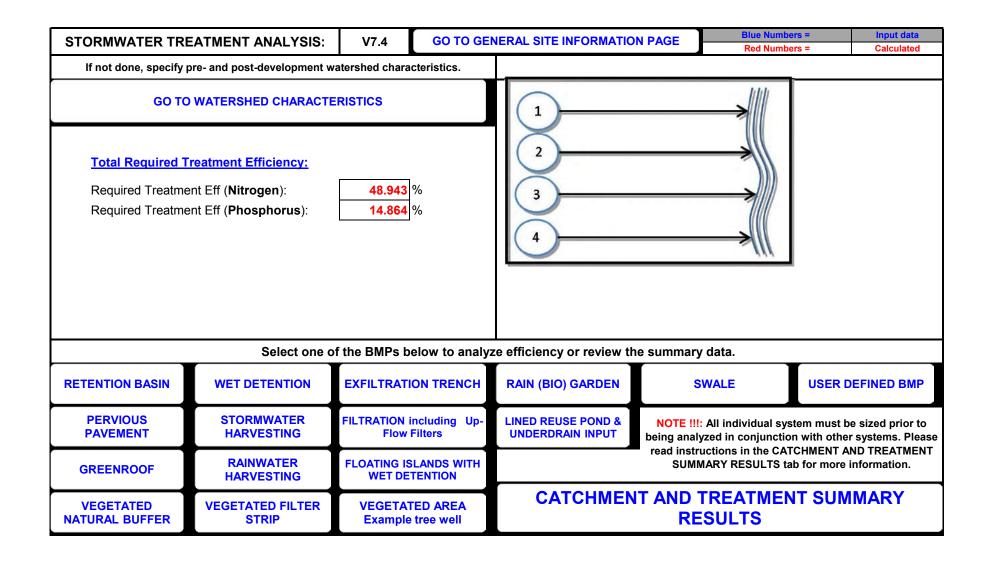
^{*}Treatment volume provided / basin acreage

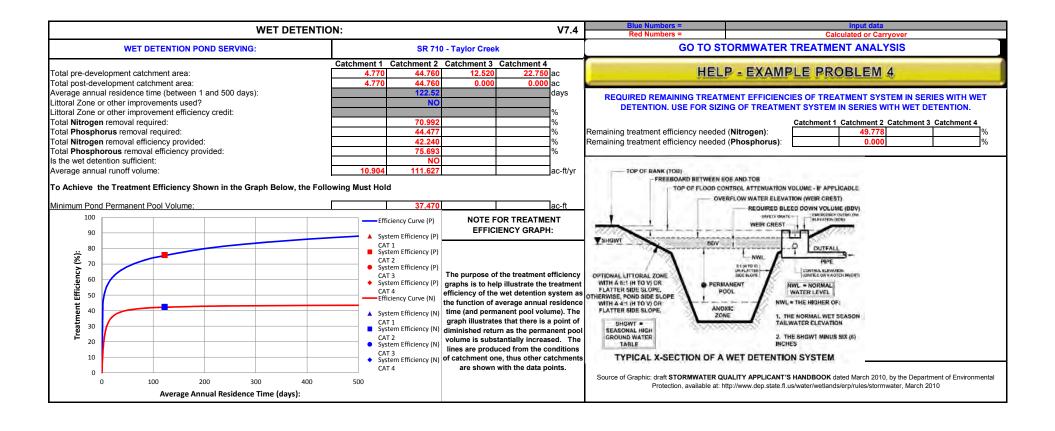


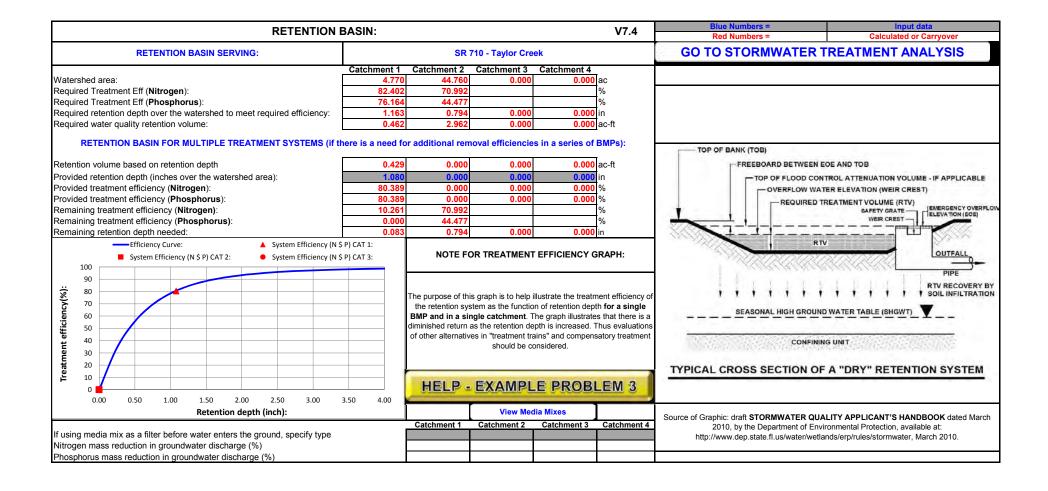
WATERSHED CHAP	RACTERISTICS V7.4	GO TO S	STORMWA	TER TREA	ATMENT AN	IALYSIS	Blue Numbers = Red Numbers =	Input data Calculated	HELP - LAND USES/EMG
SELECT CATCHME	ENT CONFIGURATION	CLICK ON C		W TO SELE		VIEW CATCHMENT CONFIGURATION			
CATCHMENT NO.1 CHARACT	TERISTICS:	\ If mix	ed land us	es (side c	alculation)		OVERWRITE	DEFAULT CONCE	NTRATIONS USING:
	CLICK ON CELL BELOW TO		Land use	Area Acres	non DCIA CN	%DCIA	PRE:	•	POST:
Pre-development land use:	User Defined (must over write conc						EMC(N): 1.580		1.070 mg/L
with default EMCs	CLICK ON CELL BELOW TO						EMC(P): 0.260	mg/L	0.130 mg/L
Post-development land use: with default EMCs	User Defined (must over write conce	entrations)	Total						
Total pre-development catchme	ent area	4 77	AC				OVERWR	ITE DEFAULT COI	NCENTRATIONS
Total post-development catching		4.77			Average an	nual pre run	off volume:		1.300 ac-ft/year
Pre-development Non DCIA CN: 56						nual post rur			10.904 ac-ft/year
Pre-development DCIA percentage:			%		Pre-develop	oment Annua	ll Mass Loading - Nitro	gen:	2.532 kg/year
Post-development Non DCIA CN:							ll Mass Loading - Phos		0.417 kg/year
Post-development DCIA percei							14.389 kg/year		
Estimated Area of BMP (used f	3-7	0.00				•	V	•	1.748 kg/year
CATCHMENT NO.2 CHARACT	TERISTICS:		\ If r	nixed land	uses (side	calculation	OVERWRI	TE DEFAULT CON	ICENTRATIONS:
	CLICK ON CELL BELOW TO		Land use	Area Acres	non DCIA CN	%DCIA	PRE:		POST:
Pre-development land use:	User Defined (must over write conc						EMC(N): 2.130		1.000 mg/L
with default EMCs	CLICK ON CELL BELOW TO						EMC(P): 0.530	mg/L	0.130 mg/L
Post-development land use: with default EMCs	User Defined (must over write conc	entrations)	Total						
Total pre-development catchme	ent area:	44.76					OVERWR	ITE DEFAULT COI	NCENTRATIONS
Total post-development catching		44.76			Average an	nual pre run	off volume:		15.202 ac-ft/year
Pre-development Non DCIA CN	,	62.87			_	nual post rur			111.627 ac-ft/year
Pre-development DCIA percen		5.59	%				ll Mass Loading - Nitro	gen:	39.934 kg/year
Post-development Non DCIA C		63.44					ıl Mass Loading - Phos		9.937 kg/year
Post-development DCIA percei		71.12					al Mass Loading - Nitr		137.665 kg/year
Estimated Area of BMP (used f	or raintall excess not loadings)	0.00	AC		Post-develo	opment Annu	al Mass Loading - Pho	sphorus:	17.896 kg/year

BMP Area set to zero because EMCs already weighted to include no pollutant loading from water bodies (applies to all catchments)

	CATCHMENT NO.3 CHARACT	TERISTICS:	\ If	mixed land	d uses (side	calculation	OVERWRITE DEFAULT C	ONCENTRATIONS:
		CLICK ON CELL BELOW TO SELECT	Land use	Area Acres	non DCIA CN	%DCIA	PRE:	POST:
	Pre-development land use:	User Defined (must over write concentrations)					EMC(N): 2.420 mg/L	1.040 mg/L
	with default EMCs	CLICK ON CELL BELOW TO SELECT					EMC(P): 0.680 mg/L	0.130 mg/L
	Post-development land use:	User Defined (must over write concentrations)						
	with default EMCs	<u></u>	Total				OVERWRITE DEFAULT C	ONCENTRATIONS
	Total pre-development catchm	ent area: 12.5	2 AC				OVERWRITE DEFAULT C	ONCENTRATIONS
က	Total post-development catchr	ment or BMP analysis area:	AC		Average an	nual pre rund	off volume:	4.463 ac-ft/year
Basin	Pre-development Non DCIA C		6			nual post rur		ac-ft/year
g	Pre-development DCIA percentage: 7.3				Pre-develop	oment Annua	ıl Mass Loading - Nitrogen:	13.320 kg/year
اشا	Post-development Non DCIA C					ll Mass Loading - Phosphorus:	3.743 kg/year	
	Post-development DCIA percentage:						al Mass Loading - Nitrogen:	kg/year
	Estimated Area of BMP (used	0 AC		Post-develo	pment Annu	al Mass Loading - Phosphorus:	kg/year	
	CATCHMENT NO.4 CHARAC	TERISTICS:	\ If	mixed land	d uses (side	calculation	OVERWRITE DEFAULT C	ONCENTRATIONS:
		CLICK ON CELL BELOW TO SELECT	Land use	Area Acres	non DCIA CN	%DCIA	PRE:	POST:
ll	Pre-development land use:	User Defined (must over write concentrations)					EMC(N): 1.330 mg/L	0.000 mg/L
ll	with default EMCs	CLICK ON CELL BELOW TO SELECT					EMC(P): 0.160 mg/L	0.000 mg/L
ll	Post-development land use:	User Defined (must over write concentrations)						
ll	with default EMCs		Total				OVERWRITE DEFAULT C	ONCENTRATIONS
ll	Total pre-development catchm		5 AC					
4	Total post-development catchr		AC			nual pre runo		13.320 ac-ft/year
⊇.	Pre-development Non DCIA Cl					nual post rur		ac-ft/year
	Pre-development DCIA percen Post-development Non DCIA (3 7/0				Il Mass Loading - Nitrogen: Il Mass Loading - Phosphorus:	21.848 kg/year
	Post-development DCIA perce		- %				al Mass Loading - Priosphorus:	2.628 kg/year kg/year
لـــــا			0 AC				al Mass Loading - Nitrogen. al Mass Loading - Phosphorus:	kg/year
	Louinated Aled of Divil (doed	ioi raimaii exeess net leadings;	, 10		i ost-develt	PHILEHI AHHU	ai mass Loading - r nospitorus.	ng/year







CATCHMENTS AND TREATMENT SUMMARY RESULTS

V7.4

CALCULATION METHODS:

Total Nitrogen Pre Load = 77.63+12.56 = 90.19 kg/yr

Total Phosphorus Pre Load = 16.72+0.63 = 17.35 kg/yr

been evaluated and in practice they are at this time not used,

3. If multiple BMPs are used in a single catchment and one of them is detention, then it is assumed to be last in series.

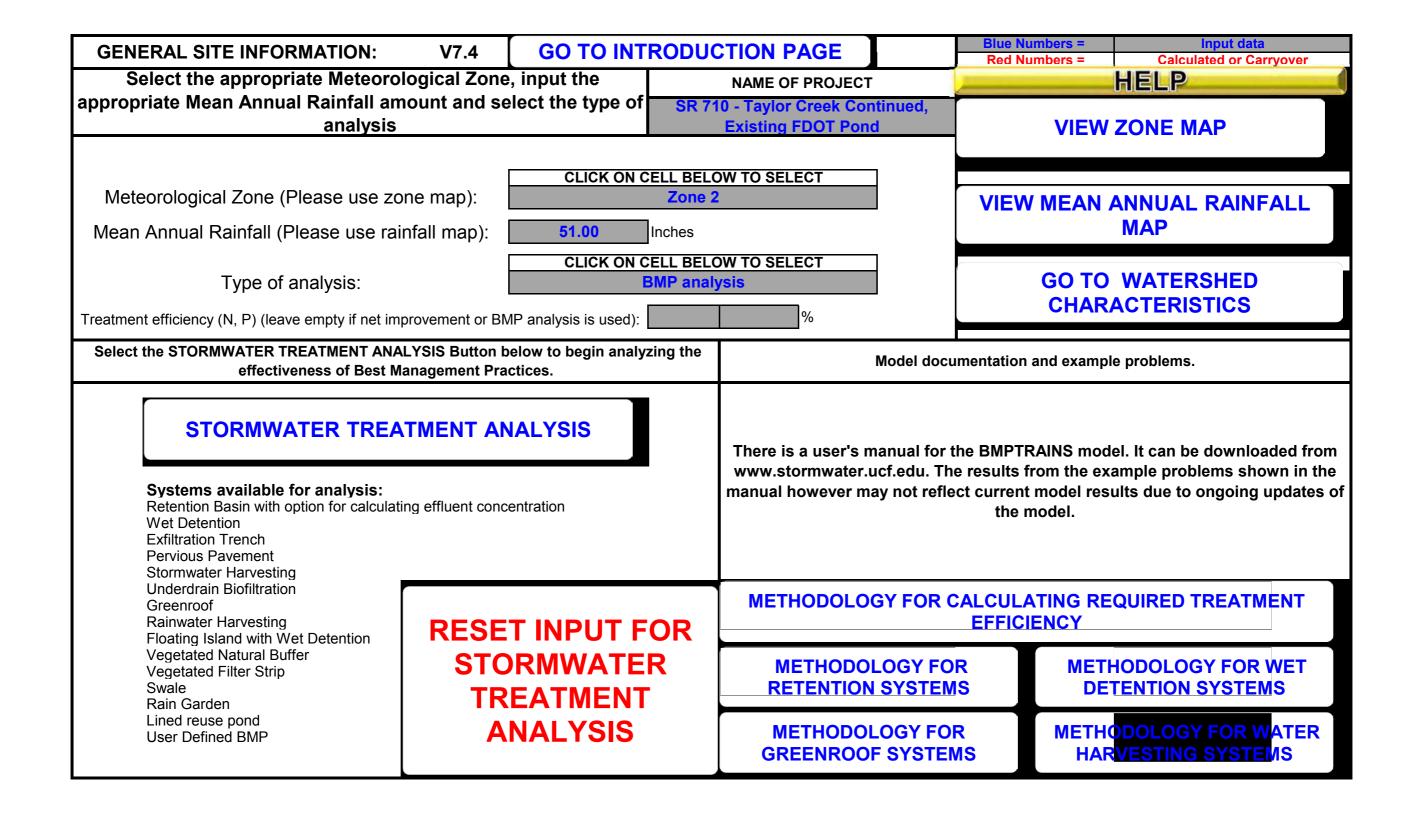
PROJECT TITLE	SR 710 ·	- Taylor Creek	Optional Identification			
		Catchment 1:	Catchment 2:	Catchment 3:	Catchment 4:	
BMP I	Name	Retention Basin	Wet Detention			
BMP I	Name			Note: T	aylor Creek is continu	ued on
BMP Name				/	t 4 pages to include t	

ERROR, ONE OR MORE CATCHMENT HAS BEEN SPECIFIED WITH existing FDOT pond. BMPTRAINS

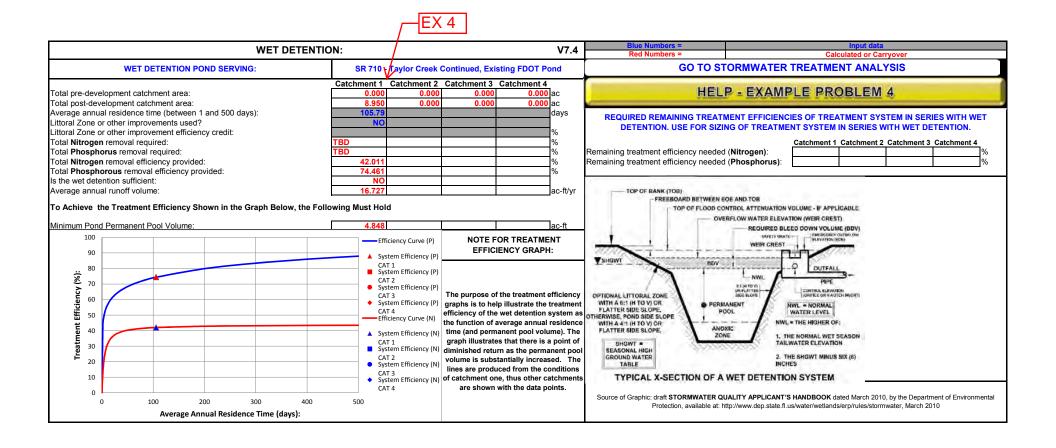
he only allows input of 4 catchments.

Summary Performance of Entire Watershed

Catchment Configuration	L - 4 Catch	ment-Parallel		1/31/2017
Nitrogen Pre	Load (kg/yr)	77.63		BMPTRAINS MODEL
Phosphorus Pr	re Load (kg/yr)	16.72	K	
Nitrogen Post	Load (kg/yr)	152.05	Treatment	- ldd
Phosphorus Po	st Load (kg/yr)	19.64		
Target Load Re	eduction (N) %	49	Objectives	
Target Load Re	eduction (P) %	15	Not Met	\sim
Target Discharge	Load, N (kg/yr)	77.63	- Not met	(2)
Target Discharge	e Load, P (kg/yr)	16.72		
Provided Overall	Efficiency, N (%):	46		
Provided Overall	Efficiency, P (%):	76		3
Discharged Load,	N (kg/yr & lb/yr):	82.34	181.36	
Discharged Load,	P (kg/yr & lb/yr):	4.69	10.34	(4)
Load Removed, I	N (kg/yr & lb/yr):	69.72	153.56	
Load Removed,	P (kg/yr & lb/yr):	14.95	32.93	



	WATERSHED CHAR	ACTERISTICS V7.4	GO TO S	STORMWA	TER TRE	ATMENT AN	IALYSIS	Red Numbers =	Calculated	HELP - LAND USES/EMC
	SELECT CATCUME	NT CONFIGURATION	CLICK ON C	ELL BELO	W TO SELE	CT CONFIGU	JRATION	VIEW C	ATCHMENT COM	MEIGURATION
	SELECT CATCHINE	NI CONFIGURATION		L - 4 C	atchment	-Parallel	_	VIEW	ATOTIMENT COL	HIGORATION
7	CATCHMENT NO.1 CHARACTI	ERISTICS:	\ If mixe	ixed land uses (side calculation)				OVERWRITE DEFAULT CONCENTRATIONS USING:		
		CLICK ON CELL BELOW TO	SELECT	Land use	Area Acres	non DCIA CN	%DCIA	PRE:	_	POST:
٠	Pre-development land use:	User Defined (must over write conce						EMC(N):	mg/L	1.050 mg/L
	with default EMCs	CLICK ON CELL BELOW TO						EMC(P):	mg/L	0.120 mg/L
Ц	Post-development land use:	User Defined (must over write conce	entrations)	T-4-1						
	with default EMCs Total pre-development catchme	nt area:		Total AC				OVERWR	ITE DEFAULT CO	NCENTRATIONS
	Total post-development catchme		8.95			Average an	nual pre run	off volume:		ac-ft/year
⋪	Pre-development Non DCIA CN		0.93	70			ınual post rui			16.727 ac-ft/year
	Pre-development DCIA percenta			%				al Mass Loading - Nitro	ogen:	kg/year
	Post-development Non DCIA CN		56.13					al Mass Loading - Pho		kg/year
	Post-development DCIA percent		52.93					ıal Mass Loading - Nit ı		21.661 kg/year
	Estimated Area of BMP (used fo	or rainfall excess not loadings)		AC				ıal Mass Loading - Pho		2.475 kg/year
	CATCHMENT NO.2 CHARACTI	ERISTICS:		\ If r	nixed land	l uses (side	calculation	OVERWR	ITE DEFAULT CON	ICENTRATIONS:
	Г	CLICK ON CELL BELOW TO	SELECT	Land use	Area Acres	non DCIA CN	%DCIA	PRE:		POST:
П	Pre-development land use:	User Defined (must over write conce	entrations)					EMC(N):	mg/L	mg/L
	with default EMCs	CLICK ON CELL BELOW TO	SELECT					EMC(P):	mg/L	mg/L
	Post-development land use:	User Defined (must over write conce	entrations)							
	with default EMCs			Total				OVERWR	ITE DEFAULT CO	NCENTRATIONS
	Total pre-development catchme			AC						
	Total post-development catchme			AC			inual pre run			ac-ft/year
	Pre-development Non DCIA CN Pre-development DCIA percenta			%			inual post rui			ac-ft/year
	Post-development Non DCIA CN			70				al Mass Loading - Nitro al Mass Loading - Pho s		kg/year kg/year
	Post dovelopment DCIA porcon			%				ial Mass Loading - Niti		kg/year
	Note: this is actually t			AC				ial Mass Loading - Pho		kg/year
	development conditio	· · · · · · · · · · · · · · · · · · ·		,		1 001 00101	5p11101167 41116	ia maco Loading The	эориогио:	[g.) oa.
	routed to L-63 in the p	post-aevelopment								
	condition. However, E	BMPTRAINS can								
	only include removals	associated with								
	post catchments.									



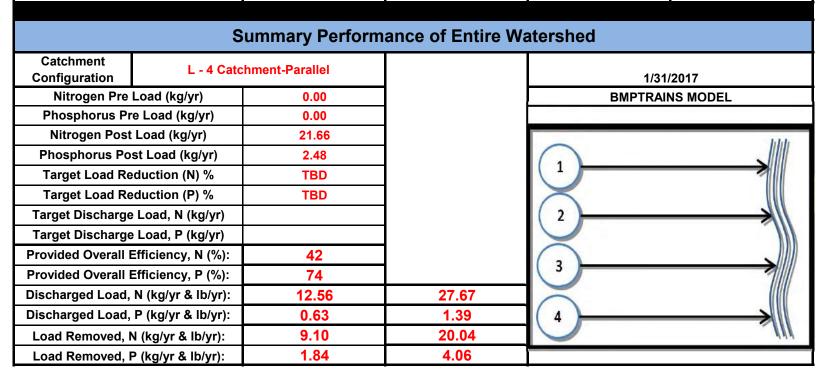
CATCHMENTS AND TREATMENT SUMMARY RESULTS

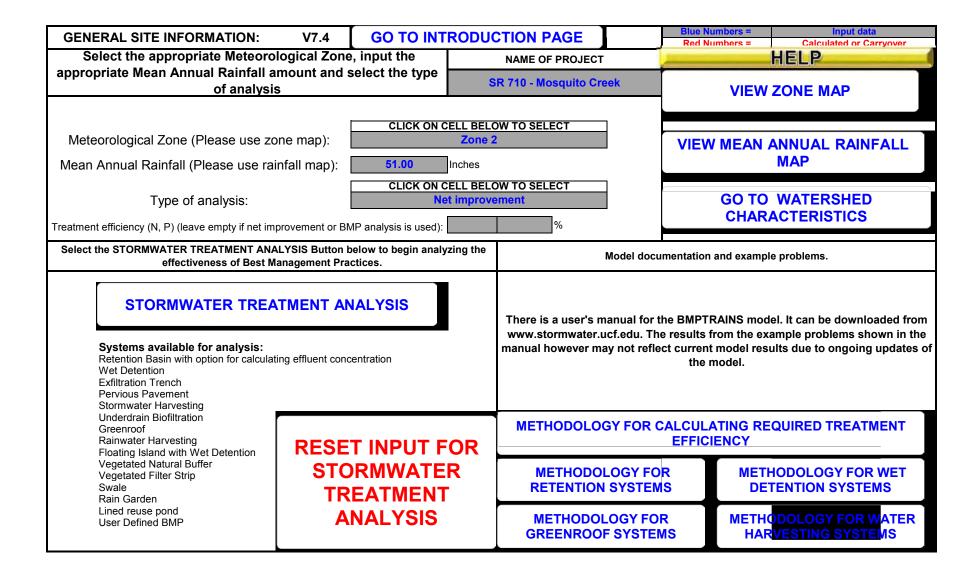
V7.4

CALCULATION METHODS:

- 1. The effectiveness of each BMP in a single catchment is converted to an equivalent capture volume.
- Certain BMP treatment train combinations have not been evaluated and in practice they are at this time not used, an example is a greenroof following a tree well.
- 3. If multiple BMPs are used in a single catchment and one of them is detention, then it is assumed to be last in series.

PROJECT TITLE 0	- Taylor Creek Co	ontinued, Existing FDOT	Optional Identification		
		Catchment 1:	Catchment 2:	Catchment 3:	Catchment 4:
BMP Na	ame	Wet Detention			
BMP Na	ame				
BMP Na	ame				



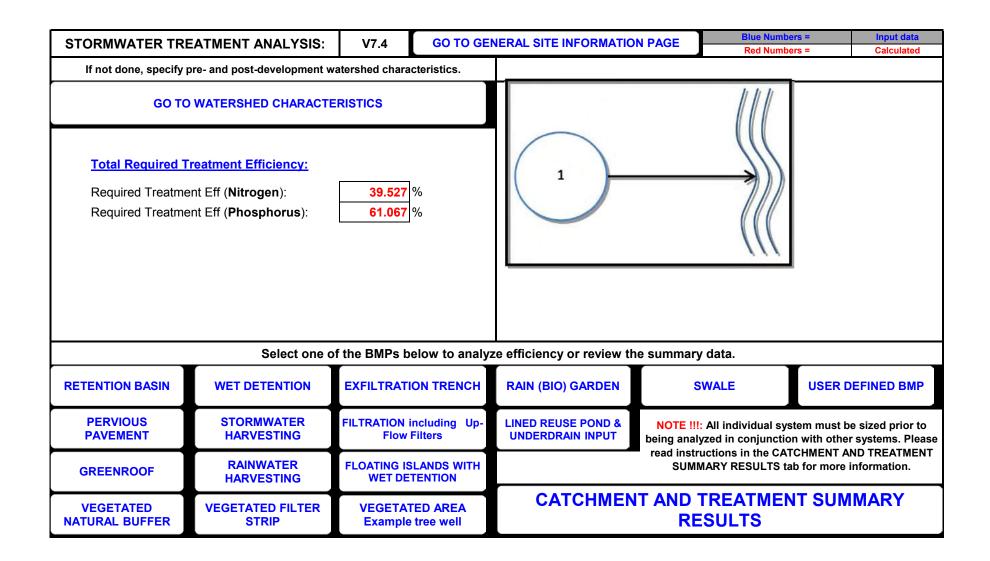


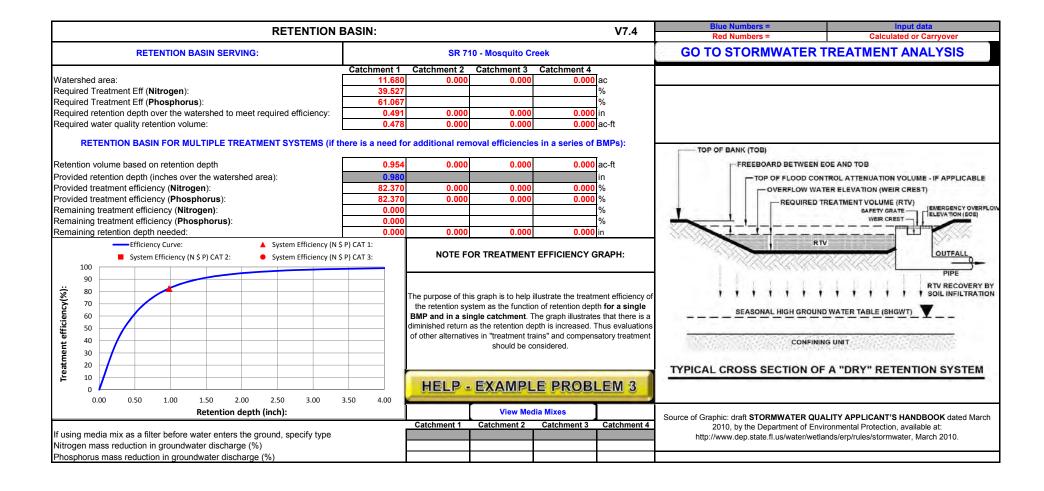
WATERSHED CHAI	RACTERISTICS V7.4	GO ТО S	TORM	NATER TREA	ATMENT AN	IALYSIS	Blue Numbers =	Input data	HELP - LAND USES/EMC
TOTAL CONTENTS OF THE		CLICK ON CELL BELOW TO SELECT CONFIGURATION					Red Numbers =	Calculated	photography (1) sport balance (1) purity translated balance (1)
SELECT CATCHME	ENT CONFIGURATION	CLICK ON C		- Single Cato		RATION	VIEW CATCHMENT CONFIGURATION		
CATCHMENT NO.1 CHARACT	TERISTICS:	\ If mix	ed land	uses (side c	alculation)		OVERWRITE	DEFAULT CONCE	NTRATIONS USING:
	CLICK ON CELL BELOW TO	SELECT	Land use	Area Acres	non DCIA CN	%DCIA	PRE:	_	POST:
Pre-development land use:	User Defined (must over write conce						EMC(N): 1.130		0.970 mg/L
with default EMCs	CLICK ON CELL BELOW TO						EMC(P): 0.090	mg/L	0.120 mg/L
Post-development land use:	User Defined (must over write conce	entrations)							
with default EMCs			To	tal			OVERWR	ITE DEFAULT CO	NCENTRATIONS
			AC						
Total post-development catchment or BMP analysis area: 11.6			AC			inual pre run			12.373 ac-ft/year
Pre-development Non DCIA CN: 58.3			.,			inual post rui			23.836 ac-ft/year
Pre-development DCIA percen	0	28.37 62.20	%				al Mass Loading - Nitro		17.243 kg/year
Post-development Non DCIA C		57.46	0/				al Mass Loading - Pho		1.373 kg/year
Post-development DCIA perce	for rainfall excess not loadings)	0.00					ıal Mass Loading - Nitr ıal Mass Loading - Pho		28.514 kg/year 3.527 kg/year
		0.00			-				
CATCHMENT NO.2 CHARACT	TERISTICS:		If mixed land uses (side calculatio			calculation	OVERWRITE DEFAULT CONCENTRATIONS:		
	CLICK ON CELL BELOW TO	SELECT	Land use	Area Acres	non DCIA CN	%DCIA	PRE:	_	POST:
Pre-development land use:							EMC(N):	mg/L	mg/L
with default EMCs	CLICK ON CELL BELOW TO	SELECT					EMC(P):	mg/L	mg/L
Post-development land use:									
with default EMCs	i			tal			USE	DEFAULT CONCE	NTRATIONS
Total pre-development catchm			AC						
Total post-development catchr			AC			nual pre run			ac-ft/year
Pre-development Non DCIA CI						ınual post rui			ac-ft/year
Pre-development DCIA percen			%				al Mass Loading - Nitro		kg/year
Post-development Non DCIA C			. ,				al Mass Loading - Pho		kg/year
Post-development DCIA perce			\% \^				ıal Mass Loading - Nitr		kg/year
Estimated Area of BMP (used	for rainfall excess not loadings)		AC		Post-develo	opment Annu	ıal Mass Loading - Pho	sphorus:	kg/year

BMP Area set to zero because

EMCs already weighted to include no pollutant loading

from water bodies





CATCHMENTS AND TREATMENT SUMMARY RESULTS

V7.4

CALCULATION METHODS:

- 1. The effectiveness of each BMP in a single catchment is converted to an equivalent capture volume.
- 2. Certain BMP treatment train combinations have not been evaluated and in practice they are at this time not used, an example is a greenroof following a tree well.
- 3. If multiple BMPs are used in a single catchment and one of them is detention, then it is assumed to be last in series.

PROJECT TITLE	SR 710 - I	Mosquito Creek	Optional Identification		
		Catchment 1:	Catchment 2:	Catchment 3:	Catchment 4:
ВМР	Name	Retention Basin			
ВМР	Name				
ВМР	Name				

	Summary Performance of Entire Watershed								
Catchment Configuration	A - Single Catchment			1/31/2017					
Nitrogen Pre Loa	ad (kg/yr)	17.24		BMPTRAINS MODEL					
Phosphorus Pre L	.oad (kg/yr)	1.37							
Nitrogen Post Lo	oad (kg/yr)	28.51	Treatment	1.1.1.					
Phosphorus Post I	Load (kg/yr)	3.53		// //					
Target Load Redu	ction (N) %	40	Objectives						
Target Load Reduction (P) %		61	Met						
Target Discharge Lo	oad, N (kg/yr)	17.24							
Target Discharge Lo	oad, P (kg/yr)	1.37		1					
Provided Overall Effi	ciency, N (%):	82							
Provided Overall Effi	ciency, P (%):	82							
Discharged Load, N ((kg/yr & lb/yr):	5.03	11.07						
Discharged Load, P ((kg/yr & lb/yr):	0.62	1.37	(//					
Load Removed, N (kg/yr & lb/yr):	23.49	51.73	1111					
Load Removed, P (k	(g/yr & lb/yr):	2.91	6.40						

Appendix 8 Engineering Calculations

h	
v	

b	bb Basins1s	29f246s
\$\$\$\$\$\$\$\$\$	‱Basin�s	\$7sofs246s
555555555	ssssBasins3s	123:sofs246s
555555555	ssssBasins4s	157sofs246s
SSSSSSSSSS	ssssBasins5s	201sofs246s
9999999	sssPreliminaryStorm Drains Tabulationss	935nf�469

Basin 1

RUNOFF CURVE NUMBER CALCULATIONS

PROJECT: SR 710 PREPARED: LCS DATE: 2/11/2014

LOCATION: OKEECHOBEE CO., FL CHECKED: GS DATE: 2/24/2014

Basin: BASIN 1 - PRE DEVELOPMENT - R/W Only

Drainage Area: From Station 500+34 to Station 511+20

Basin Length = 1086 feet (measured from roll plot)

R/W Width = 160 feet

1. Runoff curve number

Cover description	Soil name	Hydrologic group	CN	Area (Acre)	CN x Area
Open Space - Good Condition (Perv R/W)		D	80	3.99	319
Area to become Water Management Area		D	80	2.32	186
			Totals =	6.31	505

Note: Assumed Type D Soil as soil types were predominantly Types B/D & C/D

Time of Concentration

 PROJECT:
 SR 710
 BY:
 LCS
 DATE:
 10/24/2013

 LOCATION:
 Okeechobee County
 CHECKED:
 GSS
 DATE:
 10/24/2013

 EXISTING
 or
 DEVELOPED / UNDEVELOPED
 BASIN:
 1

 Tc
 or
 Tt (through subarea)

NOTES: Space for as many as two segments per flow type can be used for each worksheet. Include map, schematic, or description of flow segments.

Sheet flow (Applicable to Tc only)

Segment ID

- 1. Surface description (Table T-1, FDOT HB)
- 2. Mannings roughness coeff., n (Table T-1, FDOT HB) †
- 3. Flow length, L (total L \leq 100 ft.)
- 4. Design storm 72 hr. rainfall, P₇₂ (in.) ††
- 5. Land slope, s (ft./ft.)
- 6. Compute T_t in hr, $T_t = [0.007(nL)^{0.8}] / [P_{72hr}^{0.5} s^{0.4}] † †† Subtotal$

	AB					
	grass					
	0.15					
	100					
	9.0					
	0.057					
	0.06					
0.06	<u> </u>					

985 ft

Shallow concentrated flow

Segment ID

- 7. Surface description (Paved or Unpaved)
- 8. Flow length, L (ft)
- 9. Watercourse slope, s (ft/ft)
- 10. Average velocity, $V = k(S)^{0.5}$ (Equ. 5, FDOT HB)
- 11. Compute Tt in hr, $T_t = L / (3600*V)$

Subtotal

0.17

Shallow concentrated flow

Segment ID

- 7. Surface description (Paved or Unpaved)
- 8. Flow length, L (ft)
- 9. Watercourse slope, s (ft/ft)
- 10. Average velocity, $V = k(S)^{0.5}$ (Equ. 5, FDOT HB)
- 11. Compute Tt in hr, $T_t = L / (3600*V)$

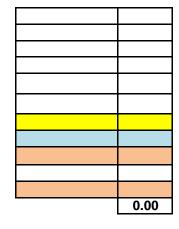
Subtotal

CD	
Unpaved	
102	
0.049	
3.57	
0.01	
	0.01

Channel Flow/Pipe Flow

Segment ID

- 12. Type of Flow
- 13. Diameter of Pipe (in.)
- 14. Cross sectional flow area, A (assumed d=0.5 ft)
- 15. Wetted perimeter, P_w
- 16. Hydraulic radius, r = A / P_w, Compute r
- 17. Channel slope, s (ft./ft.)
- 18. Manning's roughness coeff., n
- 19. V = $1.486 (r)^{0.667} (s)^{0.50} / n$, Compute V ††††
- 20. Flow length, L
- 21. Tt = L/(3600*V)
- 22. Subtotal



Time of Concentration, hr. (summation of subtotals)

Hours	0.23
Minutes	13.9
Total	13.9

Ref. FDOT Hydrology Handbook 2012.

† The use of Table T-1 is the "Overland Flow Manning's n Values" from FDOT Hydrology Handbook (2012).

†† The design storm of the basin is a 25-year storm frequency with a duration of 72-hours. Values found in SFWMD ERP Information Manual Volume IV, Surface Water Management Design Aids Figure C-8 (2012).

††† This equation is derived from the FDOT Hydrology HB overland flow equation which uses intensity instead of precipitation. The original equation mandates a trial and error process of a Type II rainfall distribution to find the correct intensity with the actual time of concentration. This derivative was created to bypass the trial and error process and is inclusive to both Type II and Type III rainfall distributions.

†††† Manning's Coefficient for Artifical Channels were found in FDOT Hydrology Handbook (2012) Table T-3. Manning's Coefficient for Natural Channels where calcuated with USGS Water-Supply Paper 2339.

Tcs-sABs-Firsts100sfeetsfromsweststoseast;sBC-987'stosTaylorsCreek

RUNOFF CURVE NUMBER CALCULATIONS

PROJECT: SR 710 PREPARED: LCS DATE: 5/14/2015

LOCATION: OKEECHOBEE CO., FL CHECKED: GS DATE: 5/14/2015

Basin: BASIN 1A - POST DEVELOPMENT - R/W Only

Drainage Area: From Station 500+34 to Station 511+20

Basin Length = 1086 feet R/W Width = 160 feet

1. Runoff curve number

Cover description	Soil name	Hydrologic group	CN	Area (Acre)	CN x Area
Pavement - Proposed SR 710			98	2.40	235
Open Space - Good Condition (Perv R/W)		D	80	1.60	128
Water Management Area (Perv.)		D	80	1.42	114
Water Management Area (Imperv.)			100	0.90	90
			Totals =	6.32	567

CN (weighted) = (total product) = 567 (total area) = 6.32

Note: Assumed Type D Soil as soil types were predominantly Types B/D & C/D

TREATMENT VOLUME CALCULATIONS FOR PROPOSED CONDITION

PROJECT: SR 71<u>0 - Pond 1A PREPARED: LCS 5/14/2015</u>

LOCATION: OKEECHOBEE COUNTY, FLORIDA CHECKED: GS 5/14/2015

Wet Detention Online Pond Treatment Calculations:

Proposed impervious area = 2.40 Ac

Total Drainage area = 6.32 Ac

1" runoff from total drainage area = 0.53 Ac-Ft

2.5" times percent imperviousness = 0.50 Ac-Ft

Treatment Volume = Greater of 1.0" over the total drainage area or 2.5" times the percent imperviousness

Required Treatment Volume (T.V.) = **0.53** Ac-Ft

= 22933 Cu-Ft

Pond Storage Calculations (Wet Detention - Pond 1A):

Elev. (NAVD)	h	Area	Area	Inc. Volume	Cum. Volume	Cum. Volume
(ft)	ft	sf	ac	Ac-ft	Ac-ft	Cu Ft.
24.50	1.0	54,922	1.261	1.199	3.136	136,604
23.50	1.0	49,519	1.137	1.075	1.937	84,376
22.50	0.9	44,106	1.013	0.862	0.862	37,549
21.60	0.0	39,318	0.903	0.000	0.000	0

Overflow Weir Elevation (Top of storage volume) (Pond1A)

Elev.	Storage	Area
21.60	0.000	39,318
22.50	0.862	44,106
	0.00-	1 1, 100

Elev. = 22.15 = 0.53 Ac-Ft 22946 Cu-Ft

Provided Treatment Volume (T.V.) =	0.527	Ac-ft

Treatment Depth = 0.55 ft

For Orifice Recovery Calculations (Pond1A)

Size the orifice to discharge no more than 0.5 inch of the required detention volume in 24 hours.

1/2" of the required detention volume = (0.5 in.* (Total DA - Water Area)/12in/ft)

1/2" of the required detention volume = 0.23 Ac-Ft = 9828 Cu-Ft

Elev.	Storage	Area
21.60	0.000	39,318
22.50	0.862	44,106

Elev. = 21.84 ft. provides 0.230 ac-ft of volume = 10013 cu ft of volume

From Geotechnical Information (10/13):

Boring PB-1A:

Est. Ground Elevation (at boring location) = 26 feet Subtract Est. SHGT Depth = -1.5-0.5 = 2 feet Estimated SHGT Elev. = 24 feet

Note: Used same control elevation as adjacent existing US 441, Pond 1 (orifice elev. At 22.7 feet NGVD or 21.53 feet NAVD

ORIFICE SIZING FOR PROPOSED CONDITION

PROJECT: SR 710 PREPARED: LCS DATE: 5/14/2015

LOCATION: Okeechobee County, FL CHECKED: GS DATE: 5/14/2015

Pond 1A Orifice Calculations

Size the orifice to discharge no more than 0.5 inch of the required detention volume in 24 hours.

Orifice Equation:

Average Discharge Rate: Drawdown 0.5 in of Required Detention Volume in 24 hrs.

Required Treatment Volume = 9828 ft³ Recovery Time (t) = 24.00 hr

Conversion Factor (CF) = 3600.00 sec/hr

$$Q = \frac{TV}{2 t CF}$$

Q = 0.057 cfs

Elevation of Required Treatment Volume = 21.84 ft

Flow line Elevation = 21.60 ft

Depth of water between top of treatment vol. and flow line (h1) = 0.24 ft

h = 0.24

Orifice Equation: $A = \frac{Q}{C\sqrt{2 g h}}$

 $A = 0.024 ft^2$

 $D = \sqrt{\frac{4 A}{\pi}}$

D = 0.18 ft = 2.10 in dia

Use 2 inch orifice with elbow
Use 3 inch minimum to prevent clogging

Nodes A Stage/Area V Stage/Volume T Time/Otage M Maninols Basins O Overland Plow U Scs Unit CN S SSUH CN S SSUH CN Y SCS Unit CA Z SSUH OA Links P Pipe W Weir C Channel D Drop Structure D Drop Structure B Rating Curve H Breach E Percolation F Filter X Exfil Trench T:City Ditch

```
Name: Basin 1
                                     Node: Pond 1A
                                     Type: SCS Unit Hydrograph CN
       Group: BASE
                                             Peaking Factor: 323.0
       Unit Hydrograph: Uh323
         Rainfall File:
                                          Storm Duration(hrs): 0.00
   Rainfall Amount(in): 0.000
Area(ac): 6.320
                                         Time of Conc(min): 15.00
Time Shift(hrs): 0.00
          Curve Number: 90.00
DCIA(%): 0.00
                                         Max Allowable Q(cfs): 999999.000
______
     Name: City Ditch
                                                            Init Stage(ft): 21.570
                            Base Flow(cfs): 0.000
    Group: BASE
                                                            Warn Stage(ft): 22.820
     Type: Time/Stage
From SJRWMD Permit Info. for US 441 Pond 1: Permit No. 47-000489-P (2004)
Converted from NGVD to NAVD
     Time(hrs)
                    Stage(ft)
               21.570
22.820
       336.00
     Name: Pond 1A Base Flow(cfs): 0.000
                                                           Init Stage(ft): 21.840
                                                            Warn Stage(ft): 23.460
    Group: BASE
     Type: Stage/Area
     Stage(ft)
                     Area(ac)
        21.600
        22.500
                       1.0130
        23.500
24.500
Name: Pond 1A Outfall From Node: Pond 1A
Group: BASE To Node: City Ditch
                                                             Length(ft): 270.00
       Group: BASE
                                                                  Count: 1
                                                     Friction Equation: Automatic
Solution Algorithm: Most Restrictive
              UPSTREAM
                            DOWNSTREAM
    Geometry: Circular
                            Circular
    Span(in): 18.00
Rise(in): 18.00
                            18.00
                                                     Flow: Both
Entrance Loss Coef: 0.500
                                                      Exit Loss Coef: 1.000
Outlet Ctrl Spec: Use dc or tw
Inlet Ctrl Spec: Use dc
   Invert(ft): 19.000
                            18.460
 Manning's N: 0.012000
                            0.012000
 Top Clip(in): 0.000
                            0.000
Bot Clip(in): 0.000
                                                           Solution Incs: 10
Upstream FHWA Inlet Edge Description:
Circular Concrete: Square edge w/ headwall
Downstream FHWA Inlet Edge Description:
Circular Concrete: Square edge w/ headwall
*** Weir 1 of 2 for Drop Structure Pond 1A Outfall ***
              Count: 1 Bottom Clip(in): 0.000
Type: Horizontal Top Clip(in): 0.000
Flow: Both Weir Disc Coef: 3.200
Geometry: Circular Orifice Disc Coef: 0.600
                                                                              TABLE
                                                Invert(ft): 21.000
              Span(in): 3.00
              Rise(in): 3.00
                                           Control Elev(ft): 21.600
*** Weir 2 of 2 for Drop Structure Pond 1A Outfall ***
                                                                             TABLE
                                            Bottom Clip(in): 0.000
Top Clip(in): 0.000
                 Count: 3
                  Type: Horizontal
                                          Top Clip(in): 0.000
Weir Disc Coef: 3.200
Orifice Disc Coef: 0.600
                  Flow: Both
              Geometry: Rectangular
                                             Invert(ft): 22.150
              Span(in): 79.00
              Rise(in): 36.00
                                           Control Elev(ft): 22.150
Filename: T:\00809.00\zTBG\drainage\ICPR\1A - 25-72.R32
     Override Defaults: Yes
   Storm Duration(hrs): 72.00
Rainfall File: Flmod
   Rainfall Amount(in): 9.00
```

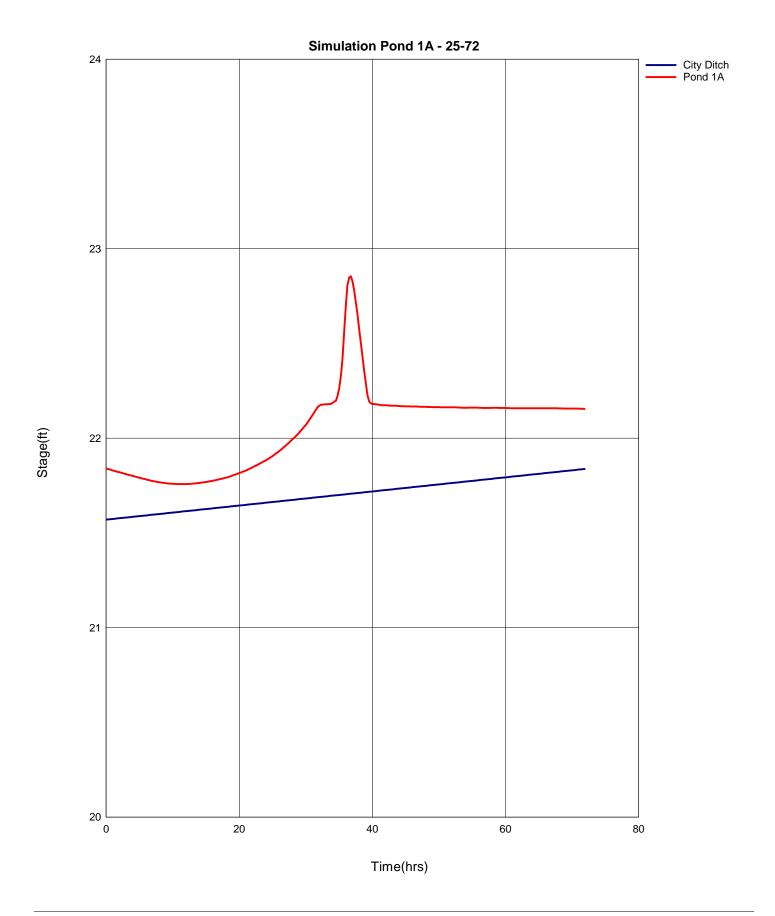
Group -----BASE

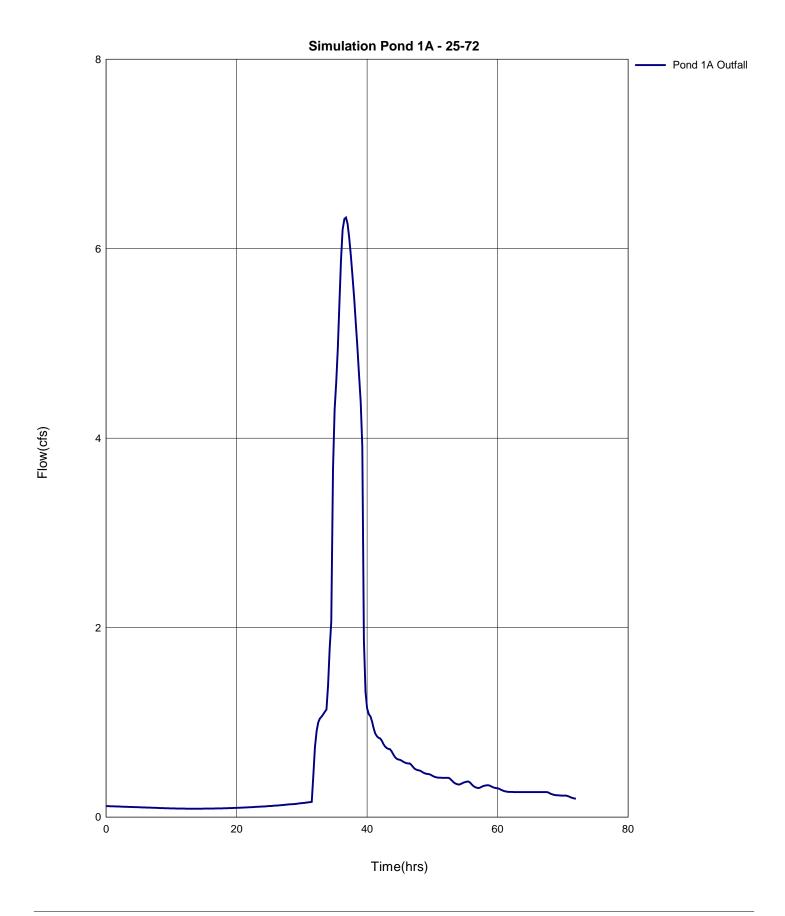
Yes

Print Inc(min) 72.000 15.00 Name: 1A-5-1 Filename: T:\00809.00\zTBG\drainage\ICPR\1A-5-1.R32 Override Defaults: Yes Storm Duration(hrs): 1.00
Rainfall File: Flmod Rainfall Amount(in): 2.98 Time(hrs) Print Inc(min) 15.00 1.000 ______ ---- Routing Simulations ------Restart: No Alternative: No Max Delta Z(ft): 1.00 Delta Z Factor: 0.00500 Time Step Optimizer: 10.000 Start Time(hrs): 0.000 Min Calc Time(sec): 0.5000 End Time(hrs): 72.00 Max Calc Time(sec): 60.0000 Boundary Flows: Boundary Stages: Print Inc(min) Time(hrs) 10.000 15.000 15.000 72.000 Group Run BASE Yes Name: Pond 1A - 5-1 Hydrology Sim: 1A-5-1 Filename: T:\00809.00\zTBG\drainage\ICPR\Pond 1A - 5-1.132 Execute: Yes Restart: No Patch: No Alternative: No Max Delta Z(ft): 1.00 Delta Z Factor: 0.00500 Time Step Optimizer: 10.000 Start Time(hrs): 0.000 End Time(hrs): 1.00 Min Calc Time(sec): 0.5000 Boundary Stages: Max Calc Time(sec): 60.0000 Boundary Flows: Time(hrs) Print Inc(min) 0 500 15 000 1.000

Basin Name: Basin 1 Group Name: BASE Simulation: 1A - 25-72 Node Name: Pond 1A Basin Type: SCS Unit Hydrograph Unit Hydrograph: Uh323 Peaking Fator: 323.0 Spec Time Inc (min): 2.00 Comp Time Inc (min): 2.00 Rainfall File: Flmod Rainfall Amount (in): 9.000 Storm Duration (hrs): 72.00 Status: Onsite Time of Conc (min): 15.00 Time Shift (hrs): 0.00 Area (ac): 6.320 Vol of Unit Hyd (in): 1.001 Curve Number: 90.000 DCIA (%): 0.000 Time Max (hrs): 36.00 Flow Max (cfs): 13.44
Runoff Volume (in): 7.795 Runoff Volume (ft3): 178826

Name	Group	Simulation	Max Time Stage hrs	Max Stage ft	Warning N Stage ft	Max Delta Stage ft	Max Surf Area ft2	Max Time Inflow hrs	Max Inflow cfs	Max Time Outflow hrs	Max Outflow cfs	
City Ditch		nd 1A - 25-72	72.00	21.84	22.82	0.0001	0	36.71	6.33	0.00	0.00	
Pond 1A	BASEPo	nd 1A - 25-72	36.72	22.85	23.46	-0.0050	46037	35.99	13.42	36.71	6.33	





RUNOFF CURVE NUMBER CALCULATIONS

PROJECT: SR 710 PREPARED: LCS DATE: 2/11/2014

LOCATION: OKEECHOBEE CO., FL CHECKED: GS DATE: 2/24/2014

Basin: BASIN 1B - POST DEVELOPMENT - R/W Only

Drainage Area: From Station 500+34 to Station 511+20

Basin Length = 1086 feet R/W Width = 160 feet

1. Runoff curve number

Cover description	Soil name	Hydrologic group	CN	Area (Acre)	CN x Area
Pavement - Proposed SR 710			98	2.40	235
Open Space - Good Condition (Perv R/W)		D	80	1.60	128
Water Management Area (Perv.)		D	80	1.20	96
Water Management Area (Imperv.)			100	0.00	0
			Totals =	5.20	459

CN (weighted) = (total product) = 459 (total area) 5.20

Note: Assumed Type D Soil as soil types were predominantly Types B/D & C/D

TREATMENT VOLUME CALCULATIONS FOR PROPOSED CONDITION

PROJECT: SR 710 - Pond 1B PREPARED: LCS 2/11/2014

LOCATION: OKEECHOBEE COUNTY, FLORIDA CHECKED: GS 2/24/2014

Dry Retention Online Pond Treatment Calculations:

Proposed impervious area = 2.40 Ac

Total Drainage area = 5.20 Ac

75% of 2.5" runoff from impervious area = 0.38 Ac-Ft

75% of 1" runoff from drainage area = 0.32 Ac-Ft

Treatment Volume = Greater of 75% of 2.50" times percent imperviousness or 75% of 1.0" over drainage area.

*Note: Dry Detention Volume Used If Nutrient Loading Can Be Eliminated

Required Treatment Volume (T.V.) = **0.38** Ac-ft

= 16335 ft^3

Pond Storage Calculations (Dry Retention - Pond 1B):

Elev. (NAVD)	h	Area	Area	Inc. Volume	Cum. Volume	Cum. Volume
(ft)	ft	sf	ac	Ac-ft	Ac-ft	Cu-ft
21.28	1.0	20,233	0.464	0.440	1.180	51401
20.28	1.0	18,133	0.416	0.393	0.740	32234
19.28	1.0	16,098	0.370	0.347	0.347	15115
18.28	0.0	14,164	0.325	0.000	0.000	0.000

SHGT El. = 16.75 feet

Overflow Weir Elevation (Top of storage volume) (Pond1B)

Elev.	Storage	Area
19.28	0.347	16,098
20.28	0.740	18,133

Elev. = 19.38 = 0.39 Ac-Ft 16827 Cu-Ft

Provided Treatment Volume (T.V.) =	0.386	Ac-ft

Treatment Depth = 1.10 ft

From Geotechnical Information (10/13):

Boring PB-1B:

Est. Ground Elevation (at boring location) = 18 feet
Subtract Est. SHGT Depth = -0.75-0.5 = 1.25 feet
Estimated SHGT Elev. = 16.75 feet

Nodes A Stage/Area V stage/Volume T Time/Stage M Manhole Basins O Overland Flow U SCS Unit CN S SBUH CN Y SCS Unit CA Z SBUH GA Links P Fipe Wift C Channel D Drop Structure B Bridge R Rating Curve H Breach E Percolation F Filter X Exfil Trench D:Pond 1B Outfall

T:Taylor Creek

```
______
______
        Name: Basin 1
                                    Node: Pond 1B
                                                               Status: Onsite
       Group: BASE
                                   Type: SCS Unit Hydrograph CN
   Unit Hydrograph: Uh323 Peaking Factor: 323.0
Rainfall File: Storm Duration(hrs): 0.00
Rainfall Amount(in): 0.000 Time of Conc(min): 14.15
Area(ac): 5.190 Time Shift(hrs): 0.00
Curve Number: 88.00 Max Allowable Q(cfs): 999999.000
DCIA(%): 0.00
              DCIA(%): 0.00
Name: Pond 1B
                            Base Flow(cfs): 0.000
                                                          Init Stage(ft): 18.280
    Group: BASE
                                                          Warn Stage(ft): 21.280
     Type: Stage/Area
     Stage(ft)
                     Area(ac)
       18.280 0.3250
19.280 0.3700
20.280 0.4160
21.280 0.4640
    Name: Taylor Creek Base Flow(cfs): 0.000 Init Stage(ft): 12.830 Group: BASE Warn Stage(ft): 14.830 Type: Time/Stage
Converted from NGVD to NAVD
FROM Raulerson Hospital Permit
   Time(hrs) Stage(ft)
             0 12.830
12.830
      0.00
       999.00
_____
______
        Name: Pond 1B Outfall From Node: Pond 1B
                                                         Length(ft): 140.00
                                 To Node: Taylor Creek
       Group: BASE
                                                                Count: 1
                                                  Friction Equation: Automatic
                          DOWNSTREAM
             UPSTREAM
    Geometry: Circular
Span(in): 18.00
                         Circular
18.00
                                                  Solution Algorithm: Most Restrictive
Flow: Both
                                                  Flow: Both
Entrance Loss Coef: 0.500
Exit Loss Coef: 1.000
Outlet Ctrl Spec: Use dc or tw
Inlet Ctrl Spec: Use dc
Spain(in): 10:00
Rise(in): 18:00
Invert(ft): 16:380
Manning's N: 0.012000
Top Clip(in): 0.000
Bot Clip(in): 0.000
                           18.00
                           14.000
0.012000
                           0.000
                                                         Solution Incs: 10
                           0.000
Upstream FHWA Inlet Edge Description:
Circular Concrete: Square edge w/ headwall
Downstream FHWA Inlet Edge Description:
Circular Concrete: Square edge w/ headwall
*** Weir 1 of 1 for Drop Structure Pond 1B Outfall ***
             Count: 1 Bottom Clip(in): 0.000
Type: Horizontal Top Clip(in): 0.000
Flow: Both Weir Disc Coef: 3.200
Geometry: Rectangular Orifice Disc Coef: 0.600
                                                                           TABLE
              Span(in): 37.00
                                                  Invert(ft): 19.380
              Rise(in): 24.00
                                          Control Elev(ft): 19.380
-----
Name: Post 1B - 25-72
    Filename: T:\00809.00\zTBG\drainage\ICPR\Post 1B - 25-72.R32
   Override Defaults: Yes
Storm Duration(hrs): 72.00
Rainfall File: Flmod
   Rainfall Amount(in): 9.00
Time(hrs)
              Print Inc(min)
```

Pond 1B 25 Yr, 72 Hr 5 Yr, 1 Hr

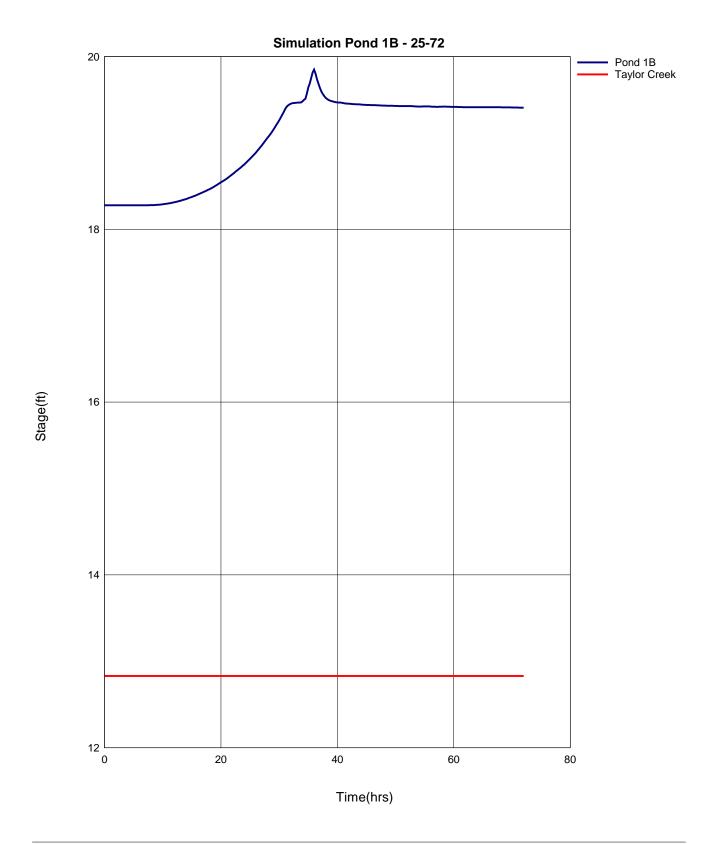
BASE

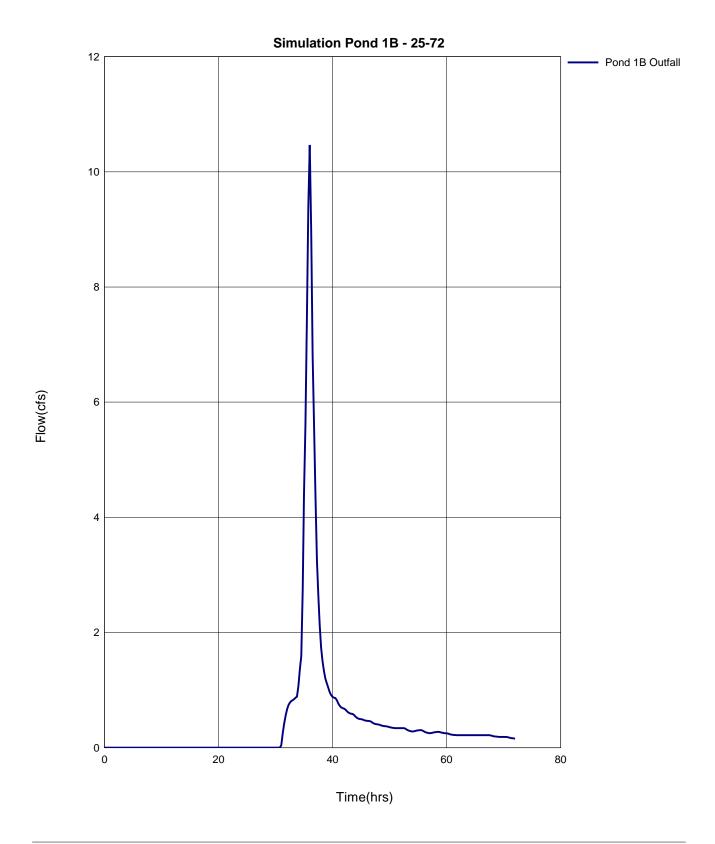
Yes

72.000 15.00 Name: Post 1B - 5-1 Filename: T:\00809.00\zTBG\drainage\ICPR\Post 1B - 5-1.R32 Override Defaults: Yes Storm Duration(hrs): 1.00 Rainfall File: Flmod Rainfall Amount(in): 2.98 Time(hrs) Print Inc(min) 1.000 15.00 ---- Routing Simulations -----Name: Pond 1B - 25-72 Hydrology Sim: Post 1B - 25-72 Filename: T:\00809.00\zTBG\drainage\ICPR\Pond 1B - 25-72.132 Execute: Yes Restart: No Patch: No Alternative: No Max Delta Z(ft): 1.00 Time Step Optimizer: 10.000 Start Time(hrs): 0.000 Min Calc Time(sec): 0.5000 Delta Z Factor: 0.00500 End Time(hrs): 72.00 Max Calc Time(sec): 60.0000 Boundary Stages: Boundary Flows:) Print Inc(min) Time(hrs) 10.000 72.000 15.000 15.000 Group Run Name: Pond 1B-5-1 Hydrology Sim: Post 1B - 5-1 Filename: T:\00809.00\zTBG\drainage\ICPR\Pond 1B-5-1.I32 Execute: Yes Restart: No Patch: No Alternative: No Max Delta Z(ft): 1.00 Delta Z Factor: 0.00500 Time Step Optimizer: 10.000 Start Time(hrs): 0.000 Min Calc Time(sec): 0.5000 End Time(hrs): 1.00
Max Calc Time(sec): 60.0000 Boundary Stages: Boundary Flows: Print Inc(min) Time(hrs) 0.500 15.000 15.000 Run Group

Basin Name: Basin 1 Group Name: BASE Simulation: Post 1B - 25-72 Node Name: Pond 1B Basin Type: SCS Unit Hydrograph Unit Hydrograph: Uh323 Peaking Fator: 323.0 Spec Time Inc (min): 1.89 Comp Time Inc (min): 1.89 Rainfall File: Flmod Rainfall Amount (in): 9.000 Storm Duration (hrs): 72.00 Status: Onsite Time of Conc (min): 14.15
Time Shift (hrs): 0.00 Area (ac): 5.190 Vol of Unit Hyd (in): 1.001 Curve Number: 88.000 DCIA (%): 0.000 Time Max (hrs): 36.00 Flow Max (cfs): 10.92 Runoff Volume (in): 7.550 Runoff Volume (ft3): 142248

Name	Group	Simulation	Max Time Stage hrs	Max Stage ft	Warning M Stage ft	ax Delta Stage ft	Max Surf Area ft2	Max Time Inflow hrs	Max Inflow cfs	Max Time Outflow hrs	Max Outflow cfs	
Pond 1B Taylor Creek		nd 1B - 25-72 nd 1B - 25-72	36.04 0.00	19.85 12.83	21.28 14.83	0.0049	17261 0	35.99 36.04	10.88 10.50	36.04 0.00	10.50	





RUNOFF CURVE NUMBER CALCULATIONS

PROJECT: SR 710 PREPARED: LCS DATE: 2/11/2014

LOCATION: OKEECHOBEE CO., FL CHECKED: GS DATE: 2/24/2014

Basin: BASIN 1C - POST DEVELOPMENT - R/W Only

Drainage Area: From Station 500+34 to Station 511+20

Basin Length = 1086 feet R/W Width = 160 feet

1. Runoff curve number

Cover description	Soil name	Hydrologic group	CN	Area (Acre)	CN x Area
Pavement - Proposed SR 710			98	2.39	235
Open Space - Good Condition (Perv R/W)		D	80	1.60	128
Water Management Area (Perv.)		D	80	0.88	71
Water Management Area (Imperv.)			100	0.00	0
			Totals =	4.87	433

CN (weighted) = (total product) = 433 (total area) 4.87 = 89

Note: Assumed Type D Soil as soil types were predominantly Types B/D & C/D

TREATMENT VOLUME CALCULATIONS FOR PROPOSED CONDITION

PROJECT: SR 710 - Pond 1C PREPARED: LCS 2/11/2014

LOCATION: OKEECHOBEE COUNTY, FLORIDA CHECKED: GS 2/24/2014

Dry Retention Online Pond Treatment Calculations:

Proposed impervious area = 2.39 Ac

Total Drainage area = 4.87 Ac

75% of 2.5" runoff from impervious area = 0.37 Ac-Ft

75% of 1" runoff from drainage area = 0.30 Ac-Ft

Treatment Volume = Greater of 75% of 2.50" times percent imperviousness or 75% of 1.0" over drainage area.

*Note: Dry Detention Volume Used If Nutrient Loading Can Be Eliminated

Required Treatment Volume (T.V.) = 0.37 Ac-ft

16290 ft³

Pond Storage Calculations (Dry Retention - Pond 1C):

Elev. (NAVD)	h	Area	Area	Inc. Volume	Cum. Volume	Cum. Volume
(ft)	ft	sf	ac	Ac-ft	Ac-ft	Ac-ft
22.00	1.0	10,281	0.236	0.217	0.739	32,191
21.00	1.0	8,600	0.197	0.180	0.522	22,738
20.00	1.0	7,067	0.162	0.146	0.342	14,898
19.00	1.0	5,621	0.129	0.113	0.196	8,538
18.00	1.0	4,239	0.097	0.083	0.083	3,615
17.00	0.0	2,984	0.069	0.000	0.000	0.000

SHGT El. = 14.5 feet

Overflow Weir Elevation (Top of storage volume) (Pond1C)

Elev.	Storage	Area
20.00	0.342	7,067
21.00	0.522	8,600

Elev. = 20.18 = 0.37 Ac-Ft 16309 Cu-Ft

Treatment Depth = 3.18 ft

Provided Treatment Volume (T.V.) = **0.374** Ac-ft

From Geotechnical Information (10/13):

Boring PB-1C:

Est. Ground Elevation (at boring location) = 15 feet
Subtract Est. SHGT Depth = -0.00-0.5 = 0.5 feet
Estimated SHGT Elev. = 14.5 feet

Nodes A Stage/Area V stage/Volume T Time/Stage M Manhole Basins O Overland Flow U SCS Unit CN S SBUH CN Y SCS Unit GA 2 SBUH GA Links P Pipe W Weir C Channel D Drop Structure B Bridge B Bridge B Bridge B Bredge :Taylor Creek

```
______
______
                                       Node: Pond 1C
        Name: Basin 1
                                                                    Status: Onsite
       Group: BASE
                                      Type: SCS Unit Hydrograph CN
   Unit Hydrograph: Uh323 Peaking Factor: 323.0 Rainfall File: Storm Duration(hrs): 0.00 Time of Conc(min): 10.00 Area(ac): 4.870 Time Shift(hrs): 0.00 OLTH(%): 0.00 Max Allowable Q(cfs): 999999.000
               DCIA(%): 0.00
Name: Pond 1C
                               Base Flow(cfs): 0.000
                                                               Init Stage(ft): 17.000
     Group: BASE
                                                              Warn Stage(ft): 22.000
      Type: Stage/Area
     Stage(ft)
                      Area(ac)
        17.000
        18.000
        19.000
                   0.1620
0.1620
0.1970
0.2360
         21.000
        22.000
                                                              Init Stage(ft): 12.830
Warn Stage(ft): 14.830
      Name: Taylor Creek Base Flow(cfs): 0.000
    Group: BASE
     Type: Time/Stage
Converted from NGVD to NAVD FROM RAULERSON HOSPITAL PERMIT
     Time(hrs)
                    Stage(ft)
      0.00
                 12.830
12.830
        999.00
To Node: Taylor Creek Count: 1
        Name: Pond 1C Outfall From Node: Pond 1C
       Group: BASE
                                          Friction Equation: Automatic
Solution Algorithm: Most Restrictive
                        DOWNSTREAM
Circular
18.00
18.00
16.750
0.012000
0.000
              UPSTREAM
 Geometry: Circular
Span(in): 18.00
Rise(in): 18.00
Invert(ft): 17.180
Manning's N: 0.012000
Top Clip(in): 0.000
                                                      Flow: Both
Entrance Loss Coef: 0.500
Exit Loss Coef: 1.000
Outlet Ctrl Spec: Use dc or tw
Inlet Ctrl Spec: Use dc
 Bot Clip(in): 0.000
                                                             Solution Incs: 10
Upstream FHWA Inlet Edge Description:
Circular Concrete: Square edge w/ headwall
Downstream FHWA Inlet Edge Description:
Circular Concrete: Square edge w/ headwall
*** Weir 1 of 1 for Drop Structure Pond 1C Outfall ***
                                                                                 TABLE
              Count: 1 Bottom Clip(in): 0.000
Type: Horizontal Top Clip(in): 0.000
Flow: Both Weir Disc Coef: 3.200
Geometry: Rectangular Orifice Disc Coef: 0.600
               Span(in): 37.00
                                                      Invert(ft): 20.180
               Rise(in): 24.00
                                              Control Elev(ft): 20.180
Name: Post 1C - 25-72 Filename: T:\00809.00\zTBG\drainage\ICPR\Post 1C - 25-72.R32
    Override Defaults: Yes
Storm Duration(hrs): 72.00
Rainfall File: Flmod
```

Rainfall Amount(in): 9.00

Time(hrs) Print Inc(min)

72.000 15.00

---- Routing Simulations -----

Name: Pond 1C - 25-72 Hydrology Sim: Post 1C - 25-72 Filename: T:\00809.00\zTBG\drainage\ICPR\Pond 1C - 25-72.I32

Execute: Yes Restart: No Patch: No Alternative: No

Max Delta Z(ft): 1.00
Time Step Optimizer: 10.000
Start Time(hrs): 0.000
Min Calc Time(sec): 0.5000

Delta Z Factor: 0.00500

End Time(hrs): 72.00

Max Calc Time(sec): 60.0000

Boundary Flows:

Time(hrs) Print Inc(min)

Yes

Boundary Stages:

10.000 15.000 72.000 15.000 Group Run

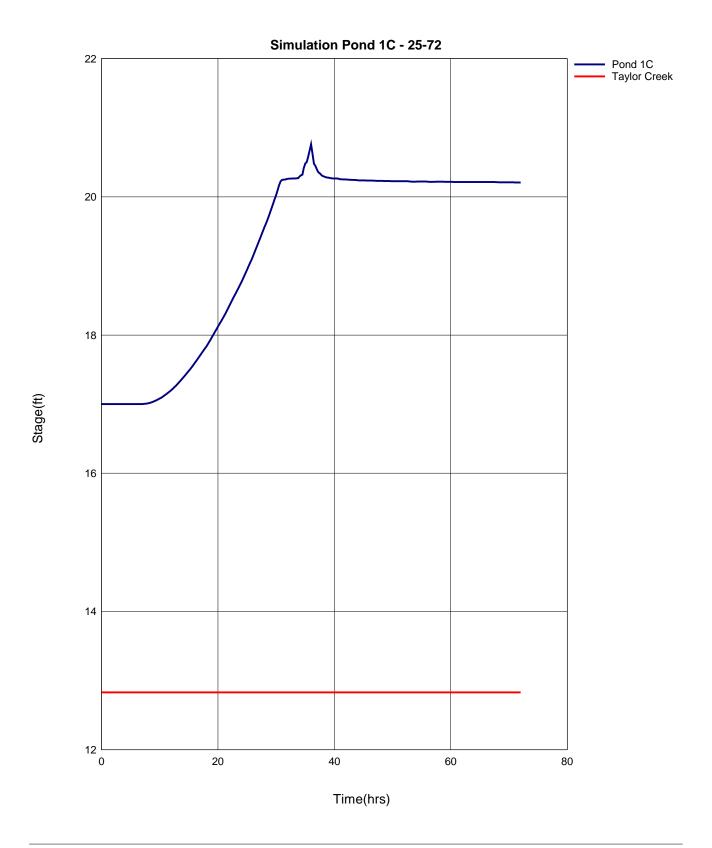
BASE

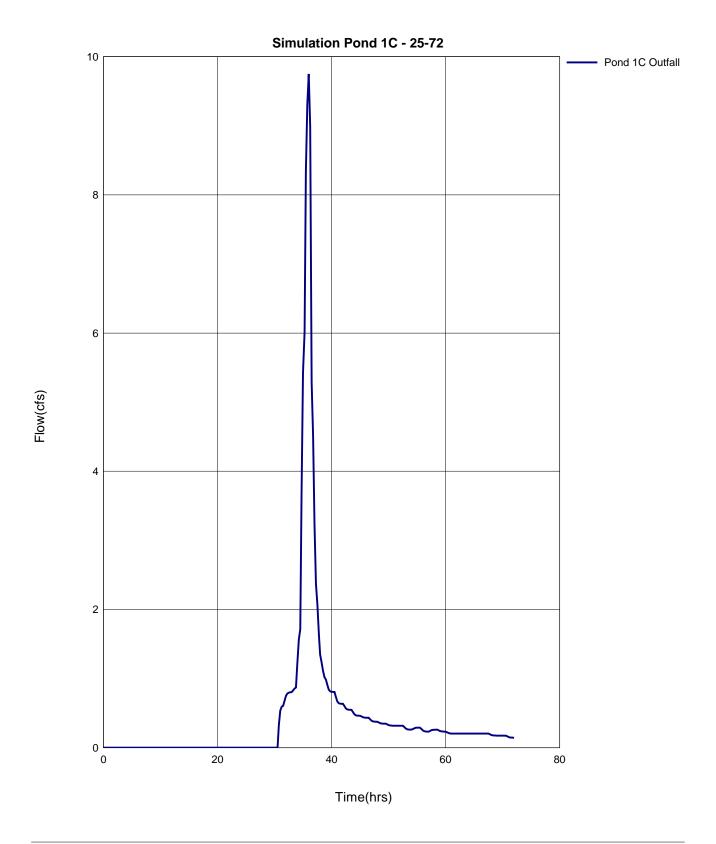
Basin Name: Basin 1
Group Name: BASE
Simulation: Post 1C - 25-72
Node Name: Post 1C - 25-72
Node Name: Pond 1C
Basin Type: SCS Unit Hydrograph
Unit Hydrograph: Uh323
Peaking Fator: 323.0
Spec Time Inc (min): 1.33
Comp Time Inc (min): 1.33
Rainfall File: Flmod
Rainfall Amount (in): 9.000
Storm Duration (hrs): 72.00
Status: Onsite
Time of Conc (min): 10.00
Time Shift (hrs): 0.00
Area (ac): 4.870
Vol of Unit Hyd (in): 1.001
Curve Number: 89.000
DCIA (%): 0.000

Time Max (hrs): 36.00
Flow Max (cfs): 10.55
Runoff Volume (ft3): 135645

Pond 1C Pond 1C 25 Yr, 72 Hr

Name	Group	Simulation	Max Time Stage hrs	Max Stage ft	Warning M Stage ft	ax Delta Stage ft	Max Surf Area ft2	Max Time Inflow hrs	Max Inflow cfs	Max Time Outflow hrs	Max Outflow cfs
Pond 1C	BASEPon	d 1C - 25-72	36.05	20.77	22.00	0.0050	8226	35.99	10.54	36.05	9.77
Taylor Creek	BASEPono	d 1C - 25-72	0.00	12.83	14.83	0.0000	0	36.05	9.77	0.00	0.00





Basin 2

RUNOFF CURVE NUMBER CALCULATIONS

PROJECT: SR 710 PREPARED: LCS DATE: 5/14/2015

LOCATION: OKEECHOBEE CO., FL CHECKED: GS DATE: 5/14/2015

Basin: BASIN 2A - Option 1 - POST DEVELOPMENT - R/W Only

Drainage Area: From Station 509+30 to Station 610+20

Basin Length = 10090 feet R/W Width = 160 feet

1. Runoff curve number

Cover description	Soil name	Hydrologic group	CN	Area (Acre)	CN x Area
Pavement - Proposed SR 710			98	22.35	2191
Open Space - Good Condition (Perv R/W)		D	80	14.71	1177
Water Management Area (Imperv.)			100	6.28	628
Water Management Area (Perv.)		D	80	3.15	252
			Totals =	46.49	4247

Note: Assumed Type D Soil as soil types were predominantly Types B/D & C/D

TREATMENT VOLUME CALCULATIONS FOR PROPOSED CONDITION

PROJECT: SR 710 - Pond 2A - Option 1 PREPARED: LCS 5/14/2015

LOCATION: OKEECHOBEE COUNTY, FLORIDA CHECKED: GS 5/14/2015

Wet Detention Online Pond Treatment Calculations:

Proposed impervious area = 22.35 Ac

Total Drainage area = 46.49 Ac

2.5" times percent imperviousness = 4.66 Ac-Ft

1" runoff from drainage area = 3.87 Ac-Ft

Treatment Volume = Greater of 2.50" times percent imperviousness or 1.0" over drainage area

Required Treatment Volume (T.V.) = 4.66 Ac-ft

= 202851 ft³

Pond Storage Calculations (Wet Detention - Pond 2A):

Elev. (NAVD)	h	Area	Area	Inc. Volume	Cum. Volume	Cum. Volume
(ft)	ft	sf	ac Ac-ft		Ac-ft	Cu-ft
24.43	1.0	308,767	7.088	6.967	22.714	989,422
23.43	1.0	298,215	6.846	6.727	15.747	685,939
22.43	1.0	287,820	6.607	6.490	9.020	392,911
21.43	0.4	277,584	6.372	2.530	2.530	110,207
21.03	0.0	273,534	6.279	0.000	0.000	0

Overflow Weir Elevation (Top of storage volume) (Pond2A)

Elev.	Storage	Area
21.43	2.530	277,584
22.43	9.020	287,820

Elev. = 21.76 = 4.672 203499.252 cu ft of volume

Surface Area @ TV Elev. = 280925 sf

Provided Treatment Volume (T.V.) = **4.672** Ac-ft

Treatment Depth = 0.73 ft

For Orifice Recovery Calculations (Pond2A)

Size the orifice to discharge no more than 0.5 inch of the required detention volume in 24 hours.

1/2" of the required detention volume = (0.5 in.* (Total DA - Water Area)/12in/ft)

1/2" runoff from drainage area = 1.68 Ac-Ft 72985 Cu-Ft

Elev.	Storage	Area
21.03	0.000	273,534
21.43	2.530	277,584

Elev. = 21.31 ft. provides 1.771 ac-ft of volume 77145 cu ft of volume

From Geotechnical Information (10/13):

Boring PB-2A:

Est. Ground Elevation (at boring location) = 22.2 feet

Estimated SHGT Depth = -0.67-0.5 = 1.17 feet

Estimated SHGT Elev. = 21.03 feet

ORIFICE SIZING FOR PROPOSED CONDITION

PROJECT: SR 710 - Pond 2A - Option 1 PREPARED: LCS 5/14/2015

LOCATION: OKEECHOBEE COUNTY, FLORIDA CHECKED: GS 5/14/2015

Pond 2A Orifice Calculations

Size the orifice to discharge no more than 0.5 inch of the required detention volume in 24 hours.

Orifice Equation:

Average Discharge Rate: Drawdown 0.5 in of Required Detention Volume in 24 hrs.

Required Treatment Volume = 72984.87 ft³

Recovery Time (t) = 24.00 hr

Conversion Factor (CF) = 3600.00 sec/hr

$$Q = \frac{TV}{2 t CF}$$

Q = 0.422 cfs

Elevation of Required Treatment Volume = 21.31 ft

Flow line Elevation = 21.03 ft

Depth of water between top of treatment vol. and flow line (h1) = 0.28 ft

h = 0.28

Orifice Equation: $A = \frac{Q}{C\sqrt{2}}$

 $A = 0.166 ft^2$

 $D = \sqrt{\frac{4 A}{\pi}}$

D = 0.46 ft = 5.51 in dia

Use 5 inch orifice

RUNOFF CURVE NUMBER CALCULATIONS

PROJECT: SR 710 PREPARED: LCS DATE: 5/14/2015

LOCATION: OKEECHOBEE CO., FL CHECKED: GS DATE: 5/14/2015

Basin: BASIN 2A - Option 2 - POST DEVELOPMENT - R/W Only

Drainage Area: From Station 509+30 to Station 610+20

Basin Length = 10090 feet R/W Width = 160 feet

1. Runoff curve number

Cover description	Soil name	Hydrologic group	CN	Area (Acre)	CN x Area
Pavement - Proposed SR 710			98	22.35	2191
Open Space - Good Condition (Perv R/W)		D	80	14.71	1177
Water Management Area (Imperv.)			100	3.99	399
Water Management Area (Perv.)		D	80	3.21	257
			Totals =	44.26	4023

CN (weighted) = (total product) = 4,023 (total area) 44.26

Note: Assumed Type D Soil as soil types were predominantly Types B/D & C/D

TREATMENT VOLUME CALCULATIONS FOR PROPOSED CONDITION

PROJECT: SR 710 - Pond 2A - Option 2 PREPARED: LCS 5/14/2015

LOCATION: OKEECHOBEE COUNTY, FLORIDA CHECKED: GS 5/14/2015

Wet Detention Online Pond Treatment Calculations:

Proposed impervious area = 22.35 Ac

Total Drainage area = 44.26 Ac

2.5" times percent imperviousness = 4.66 Ac-Ft

1" runoff from drainage area = 3.69 Ac-Ft

Treatment Volume = Greater of 2.50" times percent imperviousness or 1.0" over drainage area

Required Treatment Volume (T.V.) = 4.66 Ac-ft

= 202851 ft³

Pond Storage Calculations (Wet Detention - Pond 2A):

Elev. (NAVD)	h	Area	Area	Inc. Volume	Cum. Volume	Cum. Volume
(ft)	ft	sf	ac	Ac-ft	Ac-ft	Cu-ft
25.43	1.0	210,635	4.836	4.733	19.358	843,234
24.43	1.0	201,739	4.631	4.531	14.625	637,065
23.43	1.0	193,032	4.431	4.334	10.094	439,695
22.43	1.0	184,583	4.237	4.149	5.760	250,906
21.43	0.4	176,877	4.061	1.611	1.611	70,175
21.03	0.0	173,937	3.993	0.000	0.000	0

Overflow Weir Elevation (Top of storage volume) (Pond2A)

Elev.	Storage	Area
21.43	1.611	176,877
22.43	5.760	184,583

Elev. = 22.17 = 4.68 Ac-Ft 203916 Cu-Ft

Provided Treatment Volume (T.V.) = 4.681 Ac-ft

Treatment Depth = 1.14 ft

For Orifice Recovery Calculations (Pond2A)

Size the orifice to discharge no more than 0.5 inch of the required detention volume in 24 hours.

1/2" of the required detention volume = (0.5 in.* (Total DA - Water Area)/12in/ft)

1/2" runoff from drainage area = 1.68 Ac-Ft 73087 Cu-Ft

Elev.	Storage	Area
21.03	0.000	173,937
21.43	1.611	176,877

Elev. = 21.45 ft. provides 1.692 ac-ft of volume 73684 cu ft of volume

From Geotechnical Information (10/13):

Boring PB-2A:

Est. Ground Elevation (at boring location) = 22.2 feet
Estimated SHGT Depth = -0.67-0.5 = 1.17 feet
Estimated SHGT Elev. = 21.03 feet

ORIFICE SIZING FOR PROPOSED CONDITION

PROJECT: SR 710 - Pond 2A - Option 2 PREPARED: LCS 5/14/2015

LOCATION: OKEECHOBEE COUNTY, FLORIDA CHECKED: GS 5/14/2015

Pond 2A Orifice Calculations

Size the orifice to discharge no more than 0.5 inch of the required detention volume in 24 hours.

Orifice Equation:

Average Discharge Rate: Drawdown 0.5 in of Required Detention Volume in 24 hrs.

Required Treatment Volume = 73087.29 ft³

Recovery Time (t) = 24.00 hr

Conversion Factor (CF) = 3600.00 sec/hr

$$Q = \frac{TV}{2 t CF}$$

Q = 0.423 cfs

Elevation of Required Treatment Volume = 21.45 ft

Flow line Elevation = 21.03 ft

Depth of water between top of treatment vol. and flow line (h1) = 0.42 ft

h = 0.42

Orifice Equation:

$$1 = \frac{Q}{C\sqrt{2 g h}}$$

$$A = 0.136$$
 ft²

$$D = \sqrt{\frac{4 A}{\pi}}$$

$$D = 0.42 \text{ ft} = 4.99 \text{ in dia}$$

Use 5.00 inch orifice

RUNOFF CURVE NUMBER CALCULATIONS

PROJECT: SR 710 PREPARED: LCS DATE: 2/26/2014

LOCATION: OKEECHOBEE CO., FL CHECKED: GS DATE: 2/26/2014

Basin: BASIN 2A - Option 3 - POST DEVELOPMENT - R/W Only

Drainage Area: From Station 509+30 to Station 610+20

Basin Length = 10090 feet R/W Width = 160 feet

1. Runoff curve number

Cover description	Soil name	Hydrologic group	CN	Area (Acre)	CN x Area
Pavement - Proposed SR 710			98	22.35	2191
Open Space - Good Condition (Perv R/W)		D	80	14.71	1177
Water Management Area (Imperv.)			100	3.12	312
Water Management Area (Perv.)		D	80	3.30	264
			Totals =	43.48	3943

Note: Assumed Type D Soil as soil types were predominantly Types B/D & C/D

TREATMENT VOLUME CALCULATIONS FOR PROPOSED CONDITION

PROJECT: SR 710 - Pond 2A - Option 3 PREPARED: LCS 2/26/2014

LOCATION: OKEECHOBEE COUNTY, FLORIDA CHECKED: GS 2/26/2014

Wet Detention Online Pond Treatment Calculations:

Proposed impervious area = 22.35 Ac

Total Drainage area = 43.48 Ac

2.5" times percent imperviousness = 4.66 Ac-Ft

1" runoff from drainage area = 3.62 Ac-Ft

Treatment Volume = Greater of 2.50" times percent imperviousness or 1.0" over drainage area

Required Treatment Volume (T.V.) = 4.66 Ac-ft

= 202851 ft³

Pond Storage Calculations (Wet Detention - Pond 2A):

Elev. (NAVD)	h	Area	Area Inc. Volume		Cum. Volume	Cum. Volume		
(ft)	ft	sf	ac	Ac-ft	Ac-ft	Cu-ft		
26.43	1.0	177,837	4.083	3.989	19.401	845,108		
25.43	1.0	169,681	3.895	3.804	15.412	671,347		
24.43	1.0	161,713	3.712	3.623	11.608	505,644		
23.43	1.0	153,936	3.534	3.447	7.985	347,827		
22.43	1.0	146,348	3.360	3.275	4.538	197,675		
21.43	0.4	138,950	3.190	1.263	1.263	55,016		
21.03	0.0	136,044	3.123	0.000	0.000	0		

Overflow Weir Elevation (Top of storage volume) (Pond2A)

Elev.	Storage	Area
22.43	4.538	146,348
23.43	7.985	153,936

Elev. = 22.47 = 4.68 Ac-Ft 203681 Cu-Ft

Provided Treatment Volume (T.V.) =	4.676	Ac-ft

Treatment Depth =

For Orifice Recovery Calculations (Pond2A)

Size the orifice to discharge no more than 0.5 inch of the required detention volume in 24 hours.

1/2" of the required detention volume = (0.5 in.* (Total DA - Water Area)/12in/ft)

1/2" runoff from drainage area = 1.68 Ac-Ft 73249 Cu-Ft

Elev.	Storage	Area			
21.43	1.263	138,950			
22.43	4.538	146,348			

Elev. = 21.56 ft. provides 1.689 ac-ft of volume 73562 cu ft of volume

From Geotechnical Information (10/13):

Boring PB-2A:

Est. Ground Elevation (at boring location) = 22.2 feet Estimated SHGT Depth = -0.67- 0.5 = 1.17 feet

Estimated SHGT Elev. = 21.03 feet

ORIFICE SIZING FOR PROPOSED CONDITION

PROJECT: SR 710 - Pond 2A - Option 3 PREPARED: LCS 2/26/2014

LOCATION: OKEECHOBEE COUNTY, FLORIDA CHECKED: GS 02/26/14

Pond 2A Orifice Calculations

Size the orifice to discharge no more than 0.5 inch of the required detention volume in 24 hours.

Orifice Equation:

Average Discharge Rate: Drawdown 0.5 in of Required Detention Volume in 24 hrs.

Required Treatment Volume = 73248.90 ft³

Recovery Time (t) = 24.00 hr

Conversion Factor (CF) = 3600.00 sec/hr

$$Q = \frac{TV}{2 t CF}$$

Q = 0.424 cfs

Elevation of Required Treatment Volume = 21.56 ft

Flow line Elevation = 21.03 ft

Depth of water between top of treatment vol. and flow line (h1) = 0.53 ft

h = 0.53

Orifice Equation: $A = \frac{1}{2}$

A = 0.121 ft²

$$D = \sqrt{\frac{4 A}{\pi}}$$

D = 0.39 ft = 4.71 in dia

Use 4 inch orifice

Nodes
A Stage/Area
V Stage/Volume
T Time/Stage
M Manhole

Basins
O Overland Flow
U SCS Unit CN
S SBUH CN
Y SCS Unit GA
Z SBUH GA
U: Basin 2

Links
P Pipe
W Weir
C Channel
D Drop Structure
B Bridge
R Rating Curve
B Breach
E Percolation
F Filter
F Fitter
F Fitter
X Exfil Trench

T: Commerce Center

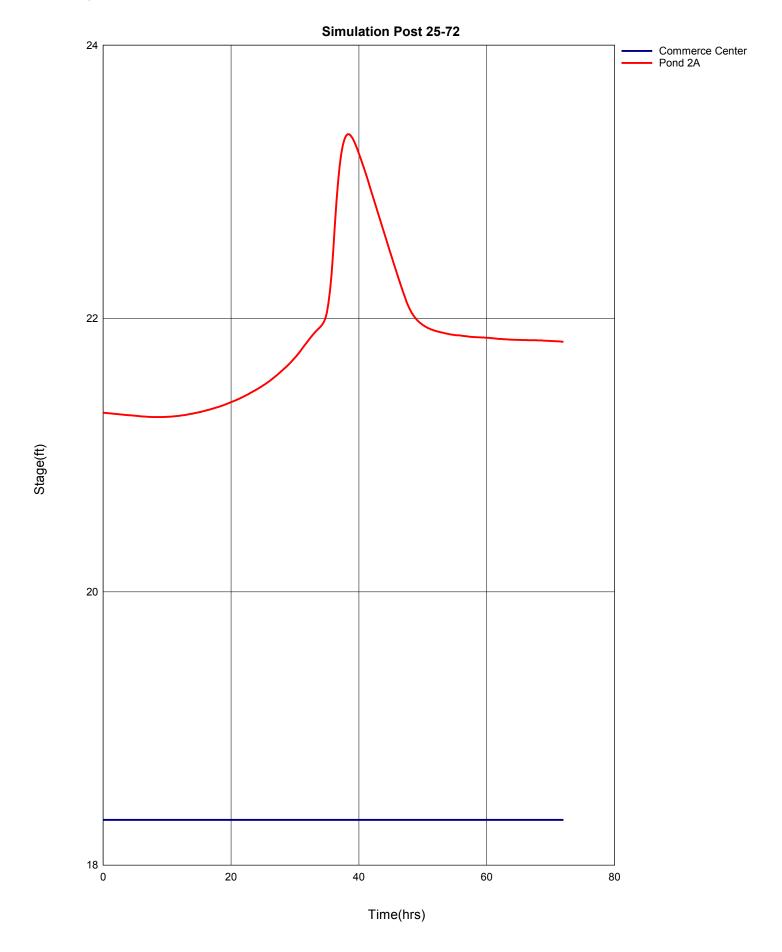
______ _____ Node: Pond 2A Name: Basin 2 Status: Onsite Group: BASE Type: SCS Unit Hydrograph CN Unit Hydrograph: Uh323 Peaking Factor: 323.0 Rainfall File: Storm Duration(hrs): 0.00 Time of Conc(min): 42.75 Rainfall Amount(in): 0.000 Time Shift(hrs): 0.00 Area(ac): 46.490 Curve Number: 91.00 Max Allowable Q(cfs): 999999.000 DCIA(%): 0.00 Base Flow(cfs): 0.000 Name: Commerce Center Init Stage(ft): 18.330 Warn Stage(ft): 999.000 Group: BASE Type: Time/Stage From ICPR: Pre-Analysis, Node Time Series for 25/72 Using Commerce Center Permit Information Converted from NGVD to NAVD Time(hrs) Stage(ft) 0.00 18.330 999.00 18.330 Name: Pond 2A Base Flow(cfs): 0.000 Init Stage(ft): 21.310 Group: BASE Warn Stage(ft): 23.430 Type: Stage/Area Stage(ft) Area(ac) 21.030 6.2790 21.430 22.430 6.3720 6.6070 23.430 24.430 7.0880 ______ ------Name: Pond 2A Outfall From Node: Pond 2A Length(ft): 300.00 To Node: Commerce Center Group: BASE Count: 1 UPSTREAM DOWNSTREAM Friction Equation: Automatic Geometry: Circular Circular Solution Algorithm: Most Restrictive Span(in): 24.00 24.00 Flow: Both Rise(in): 24.00 Invert(ft): 18.500 24.00 18.200 Entrance Loss Coef: 0.500 Exit Loss Coef: 1.000 Manning's N: 0.012000 Outlet Ctrl Spec: Use dc or tw 0.012000 Top Clip(in): 0.000 0.000 Inlet Ctrl Spec: Use dc Bot Clip(in): 0.000 0.000 Solution Incs: 10 Upstream FHWA Inlet Edge Description: Circular Concrete: Square edge w/ headwall Downstream FHWA Inlet Edge Description: Circular Concrete: Square edge w/ headwall *** Weir 1 of 2 for Drop Structure Pond 2A Outfall *** TABLE Count: 1 Bottom Clip(in): 0.000 Type: Horizontal Top Clip(in): 0.000 Weir Disc Coef: 3.200 Flow: Both Orifice Disc Coef: 0.600 Geometry: Circular Span(in): 5.00 Invert(ft): 20.530 Rise(in): 5.00 Control Elev(ft): 21.030 *** Weir 2 of 2 for Drop Structure Pond 2A Outfall *** TABLE Bottom Clip(in): 0.000 Type: Horizontal Flow: Both Top Clip(in): 0.000 Weir Disc Coef: 3.200

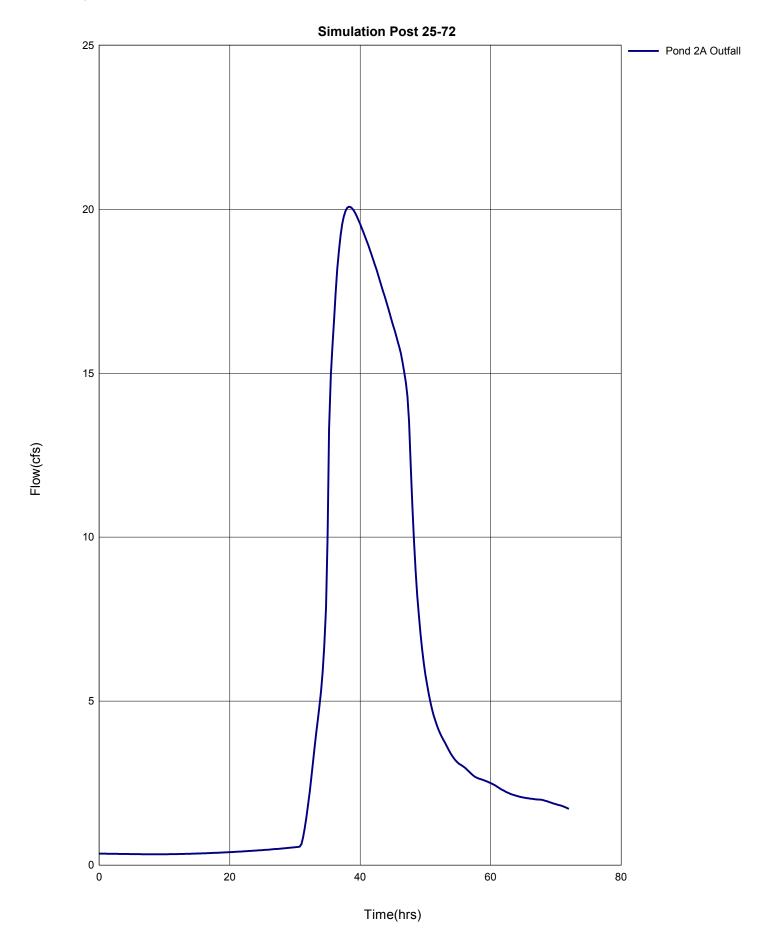
```
Geometry: Rectangular
                                    Orifice Disc Coef: 0.600
            Span(in): 79.00
                                           Invert(ft): 21.760
           Rise(in): 36.00
                                      Control Elev(ft): 21.760
______
Name: Post 25-72
   Filename: T:\00809.00\zTBG\drainage\ICPR\Post 2A - 25-72.R32
    Override Defaults: Yes
   Storm Duration(hrs): 72.00
       Rainfall File: Flmod
   Rainfall Amount(in): 9.00
           Print Inc(min)
72.000
           15.00
       Name: Post 5-1
   Filename: T:\00809.00\zTBG\drainage\ICPR\Post 2A - 5-1.R32
    Override Defaults: Yes
   Storm Duration(hrs): 1.00
       Rainfall File: Flmod
   Rainfall Amount(in): 2.98
        Print Inc(min)
Time(hrs)
           15.00
_____
______
       Name: Post 25-72
                           Hydrology Sim: Post 25-72
    Filename: T:\00809.00\zTBG\drainage\ICPR\Pond 2A - 25-72.I32
    Execute: Yes
                   Restart: No
                                       Patch: No
 Alternative: No
      Max Delta Z(ft): 1.00
                                       Delta Z Factor: 0.00500
   Time Step Optimizer: 10.000
   Start Time(hrs): 0.000
Min Calc Time(sec): 0.5000
                                    End Time(hrs): 72.00
Max Calc Time(sec): 60.0000
      Boundary Stages:
                                       Boundary Flows:
Time(hrs)
           Print Inc(min)
10.000
           15.000
72.000
            15.000
Group
BASE
            Yes
      Name: Post 5-1
                          Hydrology Sim: Post 5-1
   Filename: T:\00809.00\zTBG\drainage\ICPR\Pond 2A - 5-1.I32
    Execute: Yes
                   Restart: No
                                       Patch: No
 Alternative: No
                                      Delta Z Factor: 0.00500
      Max Delta Z(ft): 1.00
   Time Step Optimizer: 10.000
Start Time(hrs): 0.000
Min Calc Time(sec): 0.5000
                                        End Time(hrs): 1.00
                                    Max Calc Time(sec): 60.0000
      Boundary Stages:
                                       Boundary Flows:
Time(hrs)
           Print Inc(min)
0.500
            15.000
1.000
           15.000
Group
            Run
BASE
            Yes
```

Basin Name: Basin 2 Group Name: BASE Simulation: Post 25-72 Node Name: Pond 2A Basin Type: SCS Unit Hydrograph Unit Hydrograph: Uh323 Peaking Fator: 323.0 Spec Time Inc (min): 5.70 Comp Time Inc (min): 5.00 Rainfall File: Flmod Rainfall Amount (in): 9.000 Storm Duration (hrs): 72.00 Status: Onsite Time of Conc (min): 42.75 Time Shift (hrs): 0.00 Area (ac): 46.490 Vol of Unit Hyd (in): 1.001 Curve Number: 91.000 DCIA (%): 0.000 Time Max (hrs): 36.17 Flow Max (cfs): 78.69 Runoff Volume (in): 7.900 Runoff Volume (ft3): 1333208

Pond 2A - Option 1 25 Year, 72 Hour

		1	Max Time	Max	Warning M	ax Delta	Max Surf	Max Time	Max	Max Time	Max	
Name	Group	Simulation	Stage	Stage	Stage	Stage	Area	Inflow	Inflow	Outflow	Outflow	
			hrs	ft	ft	ft	ft2	hrs	cfs	hrs	cfs	
Commerce Center	BASE	Post 25-72	0.00	18.33	999.00	0.0000	0	38.35	20.07	0.00	0.00	
Pond 2A	BASE	Post 25-72	38.35	23.35	23.43	0.0050	297372	36.25	78.53	38.35	20.07	





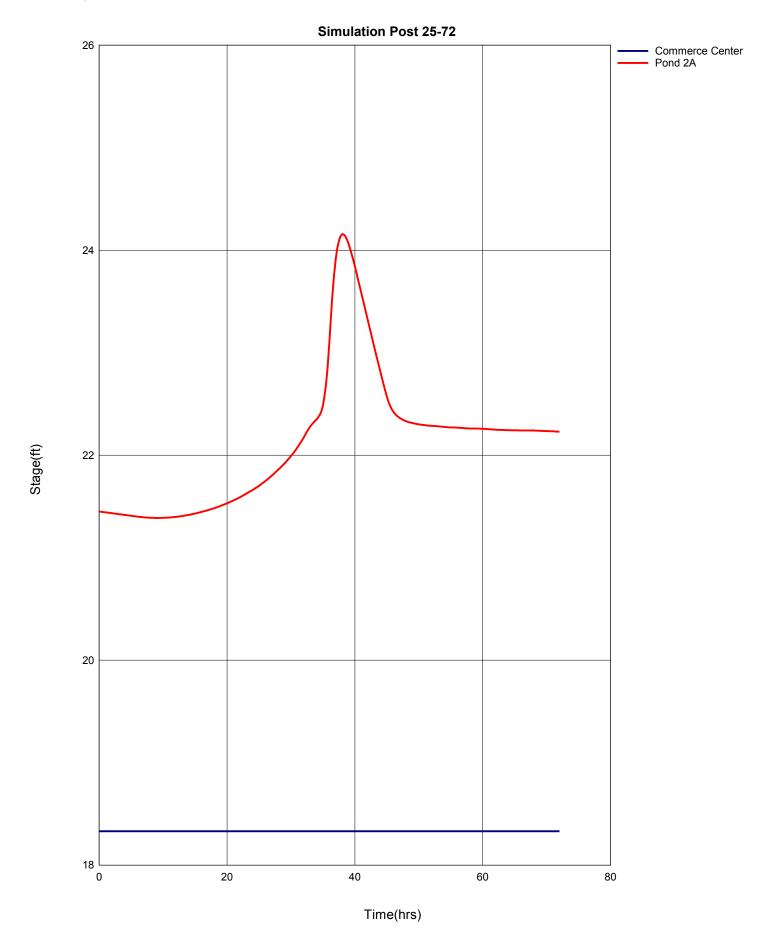
```
______
---- Basins ------
_____
                                 Node: Pond 2A
       Name: Basin 2
                                                         Status: Onsite
      Group: BASE
                                Type: SCS Unit Hydrograph CN
      Unit Hydrograph: Uh323
                                         Peaking Factor: 323.0
                                   Storm Duration(hrs): 0.00
       Rainfall File:
                                    Time of Conc(min): 42.75
   Rainfall Amount(in): 0.000
                                        Time Shift(hrs): 0.00
           Area(ac): 44.260
         Curve Number: 91.00
                                    Max Allowable Q(cfs): 999999.000
            DCIA(%): 0.00
                        Base Flow(cfs): 0.000
    Name: Commerce Center
                                                    Init Stage(ft): 18.330
                                                    Warn Stage(ft): 999.000
    Group: BASE
    Type: Time/Stage
From ICPR: Pre-Analysis, Node Time Series for 25/72
Using Commerce Center Permit Information
Converted from NGVD to NAVD
    Time(hrs)
                  Stage(ft)
         0.00
                    18.330
       999.00
                    18.330
    Name: Pond 2A
                     Base Flow(cfs): 0.000
                                                    Init Stage(ft): 21.450
    Group: BASE
                                                    Warn Stage(ft): 24.430
    Type: Stage/Area
    Stage(ft)
                  Area(ac)
       21.030
                 3.9930
       21.430 22.430
                    4.0610
       23.430
                    4.4310
       24.430
                    4.6310
       25.430
                    4.8360
______
       Name: Pond 2A Outfall From Node: Pond 2A
                                                     Length(ft): 300.00
                              To Node: Commerce Center
      Group: BASE
                                                          Count: 1
            UPSTREAM
                        DOWNSTREAM
                                                Friction Equation: Automatic
    Geometry: Circular
                        Circular
                                               Solution Algorithm: Most Restrictive
    Span(in): 24.00
Rise(in): 24.00
                        24.00
24.00
                                               Flow: Both Entrance Loss Coef: 0.500
  Invert(ft): 18.500
                         18.200
                                                  Exit Loss Coef: 1.000
 Manning's N: 0.012000
                         0.012000
                                                 Outlet Ctrl Spec: Use dc or tw
Top Clip(in): 0.000
                        0.000
                                                 Inlet Ctrl Spec: Use dc
Bot Clip(in): 0.000
                        0.000
                                                   Solution Incs: 10
Upstream FHWA Inlet Edge Description:
Circular Concrete: Square edge w/ headwall
Downstream FHWA Inlet Edge Description:
Circular Concrete: Square edge w/ headwall
*** Weir 1 of 2 for Drop Structure Pond 2A Outfall ***
                                                                    TABLE
                                        Bottom Clip(in): 0.000
              Count: 1
                                         Top Clip(in): 0.000
Weir Disc Coef: 3.200
               Type: Horizontal
               Flow: Both
            Geometry: Circular
                                     Orifice Disc Coef: 0.600
            Span(in): 5.00
                                            Invert(ft): 20.530
                                       Control Elev(ft): 21.030
            Rise(in): 5.00
*** Weir 2 of 2 for Drop Structure Pond 2A Outfall ***
                                                                    TABLE
                                        Bottom Clip(in): 0.000
              Count: 1
               Type: Horizontal
                                           Top Clip(in): 0.000
```

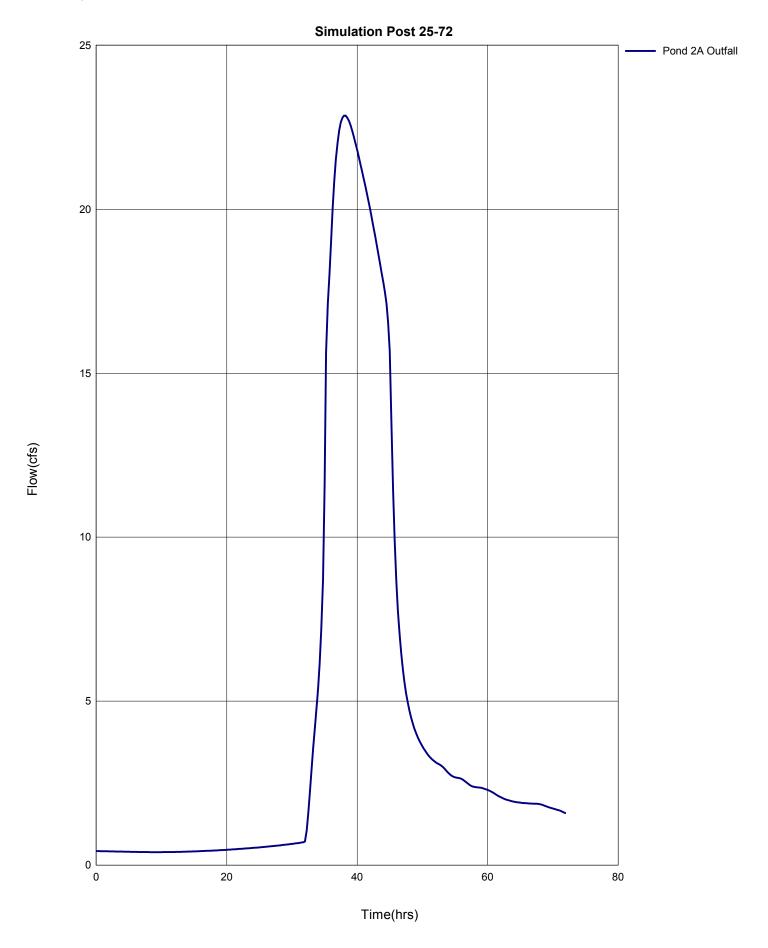
```
Flow: Both
                                        Weir Disc Coef: 3.200
            Geometry: Rectangular
                                     Orifice Disc Coef: 0.600
            Span(in): 79.00
                                           Invert(ft): 22.170
            Rise(in): 36.00
                                       Control Elev(ft): 22.170
Name: Post 25-72
    Filename: T:\00809.00\zTBG\drainage\ICPR\Post 2A - 25-72.R32
    Override Defaults: Yes
   Storm Duration(hrs): 72.00
Rainfall File: Flmod
   Rainfall Amount(in): 9.00
Time(hrs)
            Print Inc(min)
72.000
           15.00
   Filename: T:\00809.00\zTBG\drainage\ICPR\Post 2A - 5-1.R32
    Override Defaults: Yes
   Storm Duration(hrs): 1.00
       Rainfall File: Flmod
   Rainfall Amount(in): 2.98
Time(hrs)
            Print Inc(min)
1.000
      15.00
______
______
       Name: Post 25-72
                           Hydrology Sim: Post 25-72
    Filename: T:\00809.00\zTBG\drainage\ICPR\Pond 2A - 25-72.I32
    Execute: Yes
                                        Patch: No
                     Restart: No
 Alternative: No
      Max Delta Z(ft): 1.00
                                        Delta Z Factor: 0.00500
   Time Step Optimizer: 10.000
Start Time(hrs): 0.000
                                        End Time(hrs): 72.00
    Min Calc Time(sec): 0.5000
                                    Max Calc Time(sec): 60.0000
                                        Boundary Flows:
      Boundary Stages:
Time(hrs) Print Inc(min)
       15.000
72.000
Group
            Run
BASE
                     Hydrology Sim: Post 5-1
      Name: Post 5-1
   Filename: T:\00809.00\zTBG\drainage\ICPR\Pond 2A - 5-1.I32
    Execute: Yes
                     Restart: No
 Alternative: No
      Max Delta Z(ft): 1.00
                                        Delta 7 Factor: 0.00500
   Time Step Optimizer: 10.000
Start Time(hrs): 0.000
                                         End Time(hrs): 1.00
    Min Calc Time(sec): 0.5000
                                    Max Calc Time(sec): 60.0000
      Boundary Stages:
                                        Boundary Flows:
Time(hrs)
           Print Inc(min)
            15.000
0.500
1.000
            15.000
            Run
Group
BASE
            Yes
```

Basin Name: Basin 2 Group Name: BASE Simulation: Post 25-72 Node Name: Pond 2A Basin Type: SCS Unit Hydrograph Unit Hydrograph: Uh323 Peaking Fator: 323.0 Spec Time Inc (min): 5.70 Comp Time Inc (min): 5.00 Rainfall File: Flmod Rainfall Amount (in): 9.000 Storm Duration (hrs): 72.00 Status: Onsite Time of Conc (min): 42.75 Time Shift (hrs): 0.00 Area (ac): 44.260 Vol of Unit Hyd (in): 1.001 Curve Number: 91.000 DCIA (%): 0.000 Time Max (hrs): 36.17 Flow Max (cfs): 74.92 Runoff Volume (in): 7.900 Runoff Volume (ft3): 1269258

Pond 2A - Option 2 25 Year, 72 Hour Storm

Name	Group	Simulation	Max Time Stage hrs	Max Stage ft	Warning M Stage ft	ax Delta Stage ft	Max Surf Area ft2	Max Time Inflow hrs	Max Inflow cfs	Max Time Outflow hrs	Max Outflow cfs	
Commerce Center Pond 2A	BASE BASE	Post 25-72 Post 25-72	0.00 38.11	18.33 24.16	999.00	0.0000	0 199346	38.11 36.25	22.86 74.73	0.00 38.11	0.00	





Name: Basin 2 Node: Pond 2A Status: Onsite

Group: BASE Type: SCS Unit Hydrograph CN

Unit Hydrograph: Uh323 Peaking Factor: 323.0
Rainfall File: Storm Duration(hrs): 0.00
Rainfall Amount(in): 0.000 Time of Conc(min): 42.75
Area(ac): 43.480 Time Shift(hrs): 0.00
Curve Number: 91.00 Max Allowable Q(cfs): 999999.000

DCIA(%): 0.00

---- Nodes -----

Name: Commerce Center Base Flow(cfs): 0.000 Init Stage(ft): 18.330

Group: BASE Warn Stage(ft): 999.000

Type: Time/Stage

From ICPR: Pre-Analysis, Node Time Series for 25/72

Using Commerce Center Permit Information

Converted from NGVD to NAVD

0.00 18.330 999.00 18.330	Time(hrs)	Stage(ft)

Name: Pond 2A Base Flow(cfs): 0.000 Init Stage(ft): 21.560 Group: BASE Warn Stage(ft): 25.430

Type: Stage/Area

Stage(ft)	Area(ac)
21.030	3.1230
21.430	3.1900
22.430	3.3600
23.430	3.5340
24.430	3.7120
25.430	3.8950
26.430	4.0830

Name: Pond 2A Outfall From Node: Pond 2A Length(ft): 300.00

Group: BASE To Node: Commerce Center Count: 1

UPSTREAM DOWNSTREAM Friction Equation: Automatic
Geometry: Circular Circular Solution Algorithm: Most Restrictive
Span(in): 24.00 24.00 Flow: Both
Rise(in): 24.00 24.00 Entrance Loss Coef: 0.500
Invert(ft): 18.500 18.200 Exit Loss Coef: 1.000

Manning's N: 0.012000 0.012000 Outlet Ctrl Spec: Use dc or tw
Top Clip(in): 0.000 0.000 Inlet Ctrl Spec: Use dc
Bot Clip(in): 0.000 0.000 Solution Incs: 10

Upstream FHWA Inlet Edge Description: Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description: Circular Concrete: Square edge w/ headwall

*** Weir 1 of 3 for Drop Structure Pond 2A Outfall ***

```
TABLE
                                  Bottom Clip(in): 0.000
            Count: 1
             Type: Horizontal
                                    Top Clip(in): 0.000
                                   Weir Disc Coef: 3.200
             Flow: Both
          Geometry: Circular
                                Orifice Disc Coef: 0.600
                                      Invert(ft): 20.530
          Span(in): 4.00
          Rise(in): 4.00
                                 Control Elev(ft): 21.030
*** Weir 2 of 3 for Drop Structure Pond 2A Outfall ***
                                                          TABLE
            Count: 1
                                  Bottom Clip(in): 0.000
             Type: Horizontal
                                    Top Clip(in): 0.000
             Flow: Both
                                   Weir Disc Coef: 3.200
          Geometry: Rectangular
                              Orifice Disc Coef: 0.600
          Span(in): 79.00
                                      Invert(ft): 25.430
          Rise(in): 36.00
                                 Control Elev(ft): 25.430
*** Weir 3 of 3 for Drop Structure Pond 2A Outfall ***
                                                          TABLE
                                  Bottom Clip(in): 0.000
             Type: Vertical: Mavis
                                    Top Clip(in): 0.000
             Flow: Both
                                   Weir Disc Coef: 3.200
          Geometry: Rectangular
                                Orifice Disc Coef: 0.600
          Span(in): 24.00
                                      Invert(ft): 22.470
          Rise(in): 35.52
                                  Control Elev(ft): 22.470
______
______
      Name: Post 25-72
   Filename: T:\00809.00\zTBG\drainage\ICPR\Post 2A - 25-72.R32
    Override Defaults: Yes
   Storm Duration(hrs): 72.00
       Rainfall File: Flmod
   Rainfall Amount(in): 9.00
Time(hrs)
          Print Inc(min)
72.000
          15.00
______
      Name: Post 5-1
   Filename: T:\00809.00\zTBG\drainage\ICPR\Post 2A - 5-1.R32
    Override Defaults: Yes
   Storm Duration(hrs): 1.00
      Rainfall File: Flmod
   Rainfall Amount(in): 2.98
Time(hrs)
         Print Inc(min)
           15.00
______
______
      Name: Post 25-72
                        Hydrology Sim: Post 25-72
   Filename: T:\00809.00\zTBG\drainage\ICPR\Pond 2A - 25-72.132
    Execute: Yes
                 Restart: No
                                   Patch: No
 Alternative: No
     Max Delta Z(ft): 1.00
                                  Delta Z Factor: 0.00500
   Time Step Optimizer: 10.000
     Start Time(hrs): 0.000
                                   End Time(hrs): 72.00
   Min Calc Time(sec): 0.5000
                               Max Calc Time(sec): 60.0000
     Boundary Stages:
                                   Boundary Flows:
```

Time(hrs)	Print Inc(min)
10.000 72.000	15.000 15.000
Group	Run
BASE	Yes

Name: Post 5-1 Hydrology Sim: Post 5-1

Name: Post 5-1 Hydrology Sim: Post 5-1 Filename: T:\00809.00\zTBG\drainage\ICPR\Pond 2A - 5-1.I32

Execute: Yes Restart: No Patch: No

Alternative: No

 Max Delta Z(ft):
 1.00
 Delta Z Factor:
 0.00500

 Time Step Optimizer:
 10.000
 End Time(hrs):
 1.00

 Min Calc Time(sec):
 0.5000
 Max Calc Time(sec):
 60.0000

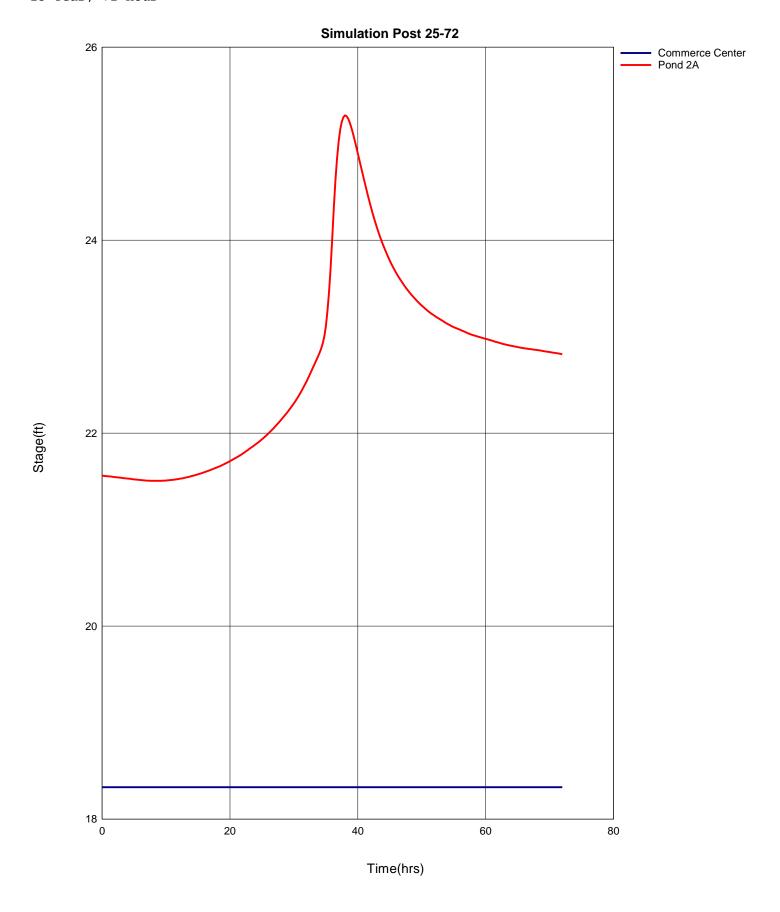
Boundary Stages: Boundary Flows:

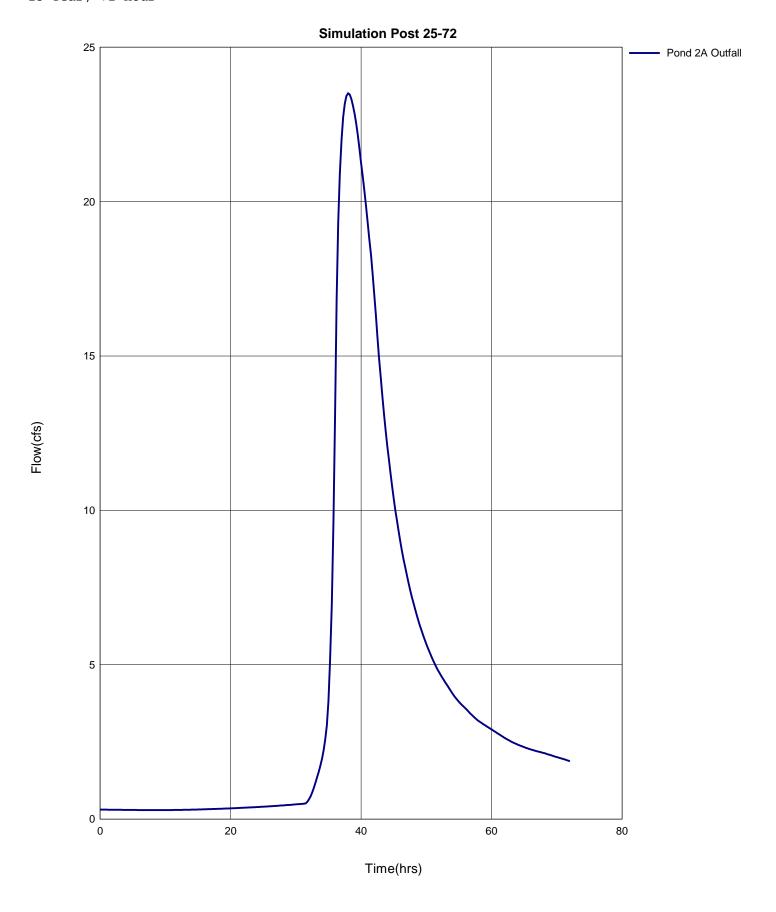
Time(hrs)	Print Inc(min)
0.500 1.000	15.000 15.000
Group	Run
BASE	Yes

Basin Name: Basin 2 Group Name: BASE Simulation: Post 25-72 Node Name: Pond 2A Basin Type: SCS Unit Hydrograph Unit Hydrograph: Uh323 Peaking Fator: 323.0 Spec Time Inc (min): 5.70 Comp Time Inc (min): 5.00 Rainfall File: Flmod Rainfall Amount (in): 9.000 Storm Duration (hrs): 72.00 Status: Onsite Time of Conc (min): 42.75 Time Shift (hrs): 0.00 Area (ac): 43.480 Vol of Unit Hyd (in): 1.001 Curve Number: 91.000 DCIA (%): 0.000 Time Max (hrs): 36.17 Flow Max (cfs): 73.60 Runoff Volume (in): 7.900 Runoff Volume (ft3): 1246889

Pond 2A-Option 3 25 Year, 72 hour

Name	Group	Simulation	Max Time Stage hrs	Max Stage ft	Warning M Stage ft	ax Delta Stage ft	Max Surf Area ft2	Max Time Inflow hrs	Max Inflow cfs	Max Time Outflow hrs	Max Outflow cfs	
Commerce Center Pond 2A	BASE BASE	Post 25-72 Post 25-72	0.00	18.33 25.29	999.00	0.0000	0 168578	38.04 36.25	23.51 73.43	0.00 38.04	0.00 23.51	





RUNOFF CURVE NUMBER CALCULATIONS

PROJECT: SR 710 PREPARED: LCS DATE: 2/26/2014

LOCATION: OKEECHOBEE CO., FL CHECKED: GS DATE: 2/26/2014

Basin: BASIN 2B - Option 1 - POST DEVELOPMENT - R/W Only

Drainage Area: From Station 509+30 to Station 610+20

Basin Length = 10090 feet R/W Width = 160 feet

1. Runoff curve number

Cover description	Soil name	Hydrologic group	CN	Area (Acre)	CN x Area
Pavement - Proposed SR 710			98	22.35	2191
Open Space - Good Condition (Perv R/W)		D	80	14.71	1177
Water Management Area (Imperv.)			100	11.78	1178
Water Management Area (Perv.)		D	80	3.59	287
			Totals =	52.43	4833

Note: Assumed Type D Soil as soil types were predominantly Types B/D & C/D

TREATMENT VOLUME CALCULATIONS FOR PROPOSED CONDITION

PROJECT: SR 710 - Pond 2B - Option 1 PREPARED: LCS 2/26/2014

LOCATION: OKEECHOBEE COUNTY, FLORIDA CHECKED: GS 2/26/2014

Wet Detention Online Pond Treatment Calculations:

Proposed impervious area = 22.35 Ac

Total Drainage area = 52.43 Ac

2.5" times percent imperviousness = 4.66 Ac-Ft

1" runoff from drainage area = 4.37 Ac-Ft

Treatment Volume = Greater of 2.50" times percent imperviousness or 1.0" over drainage area

Required Treatment Volume (T.V.) = 4.66 Ac-Ft

= 202851 ft

Pond Storage Calculations (Wet Detention - Pond 2B):

Elev. (NAVD)	h	Area	Area	Inc. Volume	Cum. Volume	Cum. Volume
(ft)	ft	sf	ac Ac-ft		Ac-ft	Cu-ft
24.43	1.0	546,326	12.542	12.387	30.154	1,313,508
23.43	1.0	532,823	12.232	12.078	17.767	773,931
22.43	0.5	519,447	11.925	5.689	5.689	247,813
21.95	0.0	513,071	11.778	0.000	0.000	0

Overflow Weir Elevation (Top of storage volume) (Pond2B)

Elev.	Storage	Area
21.95	0.000	513,071
22.43	5.689	519,447

Elev. = 22.35 ft = 4.74 Ac-Ft 206511 Cu-Ft

Provided Treatment Volume (T.V.) = 4.741 Ac-ft

Treatment Depth = 0.40 ft

For Orifice Recovery Calculations (Pond2B)

Size the orifice to discharge no more than 0.5 inch of the required detention volume in 24 hours.

1/2" of the required detention volume = (0.5 in.* (Total DA - Water Area)/12in/ft)

1/2" runoff from drainage area = 1.69 Ac-Ft 73788 Cu-Ft

Elev.	Storage	Area
21.95	0.000	513,071
22.43	5.689	519,447

Elev. = 22.10 ft. provides 1.778 ac-ft of volume 77442 cu ft of volume

From Geotechnical Information (10/13):

Boring PB-2B:

Est. Ground Elevation (at boring location) = 23.2 feet

Estimated SHGT Depth = -0.75-0.5 = 1.25 feet

Estimated SHGT Elev. = 21.95 feet

ORIFICE SIZING FOR PROPOSED CONDITION

PROJECT: SR 710 - Pond 2B - Option 1 PREPARED: LCS 2/26/2014

LOCATION: OKEECHOBEE COUNTY, FLORIDA CHECKED: GS 2/26/2014

Pond 2B Orifice Calculations

Size the orifice to discharge no more than 0.5 inch of the required detention volume in 24 hours.

Orifice Equation:

Average Discharge Rate: Drawdown 0.5 in of Required Detention Volume in 24 hrs.

Required Treatment Volume = 73787.99 ft³

Recovery Time (t) = 24.00 hr

Conversion Factor (CF) = 3600.00 sec/hr

$$Q = \frac{TV}{2 t CF}$$

Q = 0.427 cfs

Elevation of Required Treatment Volume = 22.10 ft

Flow line Elevation = 21.95 ft

Depth of water between top of treatment vol. and flow line (h1) = 0.15 ft

h = 0.15

Orifice Equation: $A = \frac{Q}{C\sqrt{2 g h}}$

 $A = 0.229 ft^2$

 $D = \sqrt{\frac{4 A}{\pi}}$

D = 0.54 ft = 6.48 in dia

Use 6 inch orifice

RUNOFF CURVE NUMBER CALCULATIONS

PROJECT: SR 710 PREPARED: LCS DATE: 2/26/2014

LOCATION: OKEECHOBEE CO., FL CHECKED: GS DATE: 2/26/2014

Basin: BASIN 2B - Option 2 - POST DEVELOPMENT - R/W Only

Drainage Area: From Station 509+30 to Station 610+20

Basin Length = 10090 feet R/W Width = 160 feet

1. Runoff curve number

Cover description	Soil name	Hydrologic group	CN	Area (Acre)	CN x Area
Pavement - Proposed SR 710			98	22.35	2191
Open Space - Good Condition (Perv R/W)		D	80	14.71	1177
Water Management Area (Imperv.)			100	6.91	691
Water Management Area (Perv.)		D	80	3.10	248
			Totals =	47.06	4306

CN (weighted) = (total product) = 4,306 (total area) = 47.06

Note: Assumed Type D Soil as soil types were predominantly Types B/D & C/D

TREATMENT VOLUME CALCULATIONS FOR PROPOSED CONDITION

PROJECT: SR 710 - Pond 2B - Option 2 PREPARED: LCS 2/26/2014

LOCATION: OKEECHOBEE COUNTY, FLORIDA CHECKED: GS 2/26/2014

Wet Detention Online Pond Treatment Calculations:

Proposed impervious area = 22.35 Ac

Total Drainage area = 47.06 Ac

2.5" times percent imperviousness = 4.66 Ac-Ft

1" runoff from drainage area = 3.92 Ac-Ft

Treatment Volume = Greater of 2.50" times percent imperviousness or 1.0" over drainage area

Required Treatment Volume (T.V.) = 4.66 Ac-ft

= 202851 ft³

Pond Storage Calculations (Wet Detention - Pond 2B):

Elev. (NAVD)	h	Area	Area	Inc. Volume	Cum. Volume	Cum. Volume
(ft)	ft	sf	ac	Ac-ft	Ac-ft	Cu-ft
25.43	1.0	333,561	7.658	7.548	25.331	1,103,418
24.43	1.0	323,996	7.438	7.330	17.783	774,627
23.43	1.0	314,558	7.221	7.114	10.453	455,333
22.43	0.5	305,247	7.008	3.339	3.339	145,447
21.95	0.0	300,823	6.906	0.000	0.000	0

Overflow Weir Elevation (Top of storage volume) (Pond2B)

Elev.	Storage	Area			
22.43	3.339	305,247			
23.43	10.453	314,558			

Elev. = 22.62 = 4.69 Ac-Ft 204325 Cu-Ft

Provided Treatment Volume (T.V.) = **4.691** Ac-ft

Treatment Depth = 0.67 ft

For Orifice Recovery Calculations (Pond2B)

Size the orifice to discharge no more than 0.5 inch of the required detention volume in 24 hours.

1/2" of the required detention volume = (0.5 in.* (Total DA - Water Area)/12in/ft)

1/2" runoff from drainage area = 1.67 Ac-Ft 72885 Cu-Ft

Elev.	Storage	Area
21.95	0.000	300,823
22.43	3.339	305,247

Elev. = 22.20 ft. provides 1.74 Ac-Ft 75754 Cu-Ft

From Geotechnical Information (10/13):

Boring PB-2B:

Est. Ground Elevation (at boring location) = 23.2 feet

Estimated SHGT Depth = -0.75-0.5 = 1.25 feet

Estimated SHGT Elev. = 21.95 feet

ORIFICE SIZING FOR PROPOSED CONDITION

PROJECT: SR 710 - Pond 2B - Option 2 PREPARED: LCS 2/26/2014

LOCATION: OKEECHOBEE COUNTY, FLORIDA CHECKED: GS 2/26/2014

Pond 2B Orifice Calculations

Size the orifice to discharge no more than 0.5 inch of the required detention volume in 24 hours.

Orifice Equation:

Average Discharge Rate: Drawdown 0.5 in of Required Detention Volume in 24 hrs.

Required Treatment Volume = 72885.31 ft³

Recovery Time (t) = 24.00 hr Conversion Factor (CF) = 3600.00 sec/hr

$$Q = \frac{TV}{2 t CF}$$

Q = 0.422 cfs

Elevation of Required Treatment Volume = 22.20 ft

Flow line Elevation = 21.95 ft

Depth of water between top of treatment vol. and flow line (h1) = 0.25 ft

Orifice Equation: $A = \frac{Q}{C\sqrt{2 g h}}$

$$A = 0.175$$
 ft²

$$D = \sqrt{\frac{4 A}{\pi}}$$

D = 0.47 ft = 5.67 in dia

Use 5 inch orifice

RUNOFF CURVE NUMBER CALCULATIONS

PROJECT: SR 710 PREPARED: LCS DATE: 2/26/2014

LOCATION: OKEECHOBEE CO., FL CHECKED: GS DATE: 2/26/2014

Basin: BASIN 2B -Option 3 - POST DEVELOPMENT - R/W Only

Drainage Area: From Station 509+30 to Station 610+20

Basin Length = 10090 feet R/W Width = 160 feet

1. Runoff curve number

Cover description	Soil name	Hydrologic group	CN	Area (Acre)	CN x Area
Pavement - Proposed SR 710			98	22.35	2191
Open Space - Good Condition (Perv R/W)		D	80	14.71	1177
Water Management Area (Imperv.)			100	4.30	430
Water Management Area (Perv.)		D	80	2.79	223
			Totals =	44.15	4020

CN (weighted) = (total product) = 4,020 (total area) 44.15

Note: Assumed Type D Soil as soil types were predominantly Types B/D & C/D

TREATMENT VOLUME CALCULATIONS FOR PROPOSED CONDITION

PROJECT: SR 710 - Pond 2B - Option 3 PREPARED: LCS 2/26/2014

LOCATION: OKEECHOBEE COUNTY, FLORIDA CHECKED: GS 2/26/2014

Wet Detention Online Pond Treatment Calculations:

Proposed impervious area = 22.35 Ac

Total Drainage area = 44.15 Ac

2.5" times percent imperviousness = 4.66 Ac-Ft

1" runoff from drainage area = 3.68 Ac-Ft

Treatment Volume = Greater of 2.50" times percent imperviousness or 1.0" over drainage area

Required Treatment Volume (T.V.) = 4.66 Ac-ft

= 202851 ft³

Pond Storage Calculations (Wet Detention - Pond 2B):

Elev. (NAVD)	h	Area	Area	Inc. Volume	Cum. Volume	Cum. Volume
(ft)	ft	sf	ac	Ac-ft	Ac-ft	Cu-ft
26.43	1.0	219,041	5.029	4.945	20.869	909,054
25.43	1.0	211,741	4.861	4.778	15.924	693,649
24.43	1.0	204,540	4.696	4.614	11.146	485,520
23.43	1.0	197,440	4.533	4.452	6.532	284,534
22.43	0.5	190,440	4.372	2.080	2.080	90,605
21.95	0.0	187,116	4.296	0.000	0.000	0

Overflow Weir Elevation (Top of storage volume) (Pond2B)

Elev.	Storage	Area
22.43	2.080	190,440
23.43	6.532	197,440

Elev. = 23.01 = 4.66 Ac-Ft 203084 Cu-Ft

Provided Treatment Volume (T.V.) = **4.662** Ac-ft

Treatment Depth = 1.06 ft

For Orifice Recovery Calculations (Pond2B)

Size the orifice to discharge no more than 0.5 inch of the required detention volume in 24 hours.

1/2" of the required detention volume = (0.5 in.* (Total DA - Water Area)/12in/ft)

1/2" runoff from drainage area = 1.66 Ac-Ft 72328 Cu-Ft

Elev.	Storage	Area
21.95	0.000	187,116
22.43	2.080	190,440

Elev. = 22.34 ft. provides 1.69 Ac-Ft 73616 Cu-Ft

From Geotechnical Information (10/13):

Boring PB-2B:

Est. Ground Elevation (at boring location) = 23.2 feet Subtract Estimated SHGT Depth = -0.75-0.5 = 0.25 feet

Estimated SHGT Elev. = 22.95 feet

ORIFICE SIZING FOR PROPOSED CONDITION

PROJECT: SR 710 - Pond 2B -Option 3 PREPARED: LCS 2/26/2014

LOCATION: OKEECHOBEE COUNTY, FLORIDA CHECKED: GS 2/26/2014

Pond 2B Orifice Calculations

Size the orifice to discharge no more than 0.5 inch of the required detention volume in 24 hours.

Orifice Equation:

Average Discharge Rate: Drawdown 0.5 in of Required Detention Volume in 24 hrs.

Required Treatment Volume = 72327.61 ft³

Recovery Time (t) = 24.00 hr Conversion Factor (CF) = 3600.00 sec/hr

$$Q = \frac{TV}{2 t CF}$$

Q = 0.419 cfs

Elevation of Required Treatment Volume = 22.34 ft

Flow line Elevation = 21.95 ft

Depth of water between top of treatment vol. and flow line (h1) = 0.39 ft

h = 0.39

Orifice Equation: $A = \frac{Q}{C\sqrt{2 g h}}$

A = 0.139 ft²

 $D = \sqrt{\frac{4 A}{\pi}}$

D = 0.42 ft = 5.05 in dia

Use 5 inch orifice

Nodes
A Stage/Area
V Stage/Volume
T Time/Stage
M Manhole

Basins
O Overland Flow
U SCS Unit CN
S SBUH CN
Y SCS Unit GA
Z SBUH GA

Links
P Pipe
W Weir
C Channel
D Drop Structure
B Bridge
R Rating Curve
B Breach
E Percolation
F Filter
F Fitter
X Exfil Trench

T: Commerce Center

```
Name: Basin 2
       Group: BASE
   Unit Hydrograph: Uh323
Rainfall File:
Rainfall Amount(in): 0.000
Area(ac): 52.430
Curve Number: 92.00
DCIA(%): 0.00
                                              Peaking Factor: 323.0
                                       Storm Duration(hrs): 0.00
Time of Conc(min): 42.75
Time Shift(hrs): 0.00
                                          Max Allowable Q(cfs): 999999.000
Tc from preliminary storm sewer tabulations
------
______
     Name: Commerce Center
                            Base Flow(cfs): 0.000
                                                             Init Stage(ft): 18.330
     Group: BASE
Type: Time/Stage
                                                             Warn Stage(ft): 999.000
From ICPR: Pre-Analysis, Node Time Series for 25/72
Using Commerce Center Permit Information
Converted from NGVD to NAVD
     Time(hrs)
      0.00

        Name:
        Pond 2B
        Base Flow(cfs):
        0.000
        Init Stage(ft):
        21.950

        Group:
        BASE
        Warn Stage(ft):
        23.430

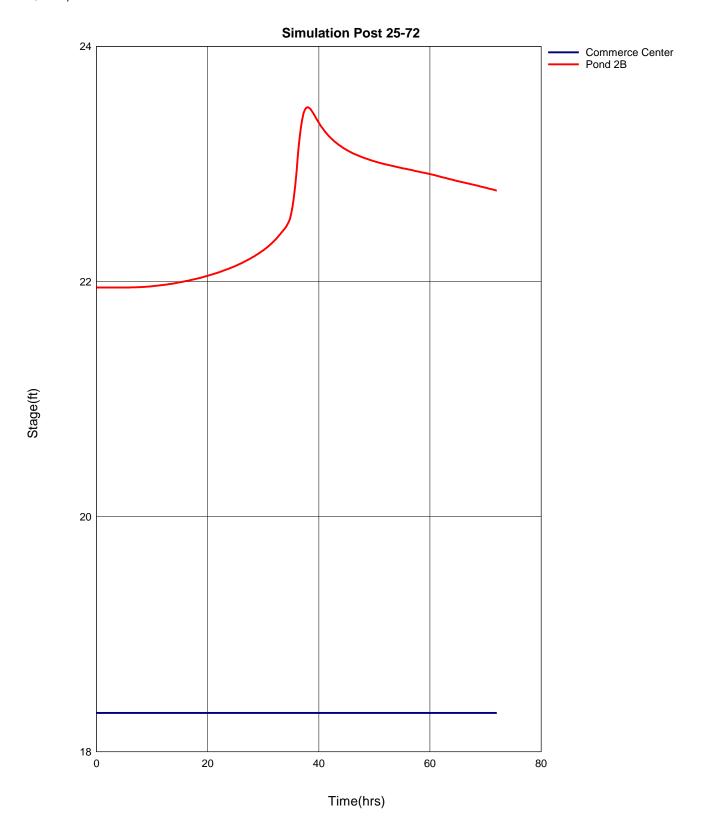
    Group: BASE
     Type: Stage/Area
     Stage(ft)
                     Area(ac)
                  11.7780
        21.950
        22.430
23.430
                       11.9250
12.2320
        24.430
                      12.5420
______
______
                                                              Length(ft): 0.00
                                 To Node:
       Group: BASE
                                                                    Count: 1
                                                        Friction Equation: Automatic
                        DOWNSTREAM
Circular
              UPSTREAM
                                                     Solution Algorithm: Most Restrictive
    Geometry: Circular
Span(in): 0.00
                            Circular
0.00
                                                     Flow: Both
Entrance Loss Coef: 0.00
                                                      Exit Loss Coef: 1.00
Bend Loss Coef: 0.00
Outlet Ctrl Spec: Use dc or tw
Inlet Ctrl Spec: Use dc
   Rise(in): 0.00
Invert(ft): 0.000
                            0.00
 Manning's N: 0.000000
Top Clip(in): 0.000
Bot Clip(in): 0.000
                             0.000000
                             0.000
                                                       Stabilizer Option: None
                             0.000
Upstream FHWA Inlet Edge Description:
Circular Concrete: Square edge w/ headwall
Downstream FHWA Inlet Edge Description:
Circular Concrete: Square edge w/ headwall
--- Drop Structures ------
        Name: Pond 2B Outfall From Node: Pond 2B
Group: BASE To Node: Commerce Center
                                                              Length(ft): 200.00
       Group: BASE
                                                                   Count: 1
              UPSTREAM
                            DOWNSTREAM
                                                        Friction Equation: Automatic
    Geometry: Circular
                                                       Solution Algorithm: Most Restrictive
                             Circular
    Span(in): 30.00
Rise(in): 30.00
                            30.00
                                                       Flow: Both
Entrance Loss Coef: 0.500
                                                         Exit Loss Coef: 1.000
Outlet Ctrl Spec: Use dc or tw
Inlet Ctrl Spec: Use dc
Solution Incs: 10
  Invert(ft): 17.950
Manning's N: 0.012000
                            17.030
0.012000
 Top Clip(in): 0.000
Bot Clip(in): 0.000
                             0.000
Upstream FHWA Inlet Edge Description:
Circular Concrete: Square edge w/ headwall
Downstream FHWA Inlet Edge Description:
Circular Concrete: Square edge w/ headwall
```

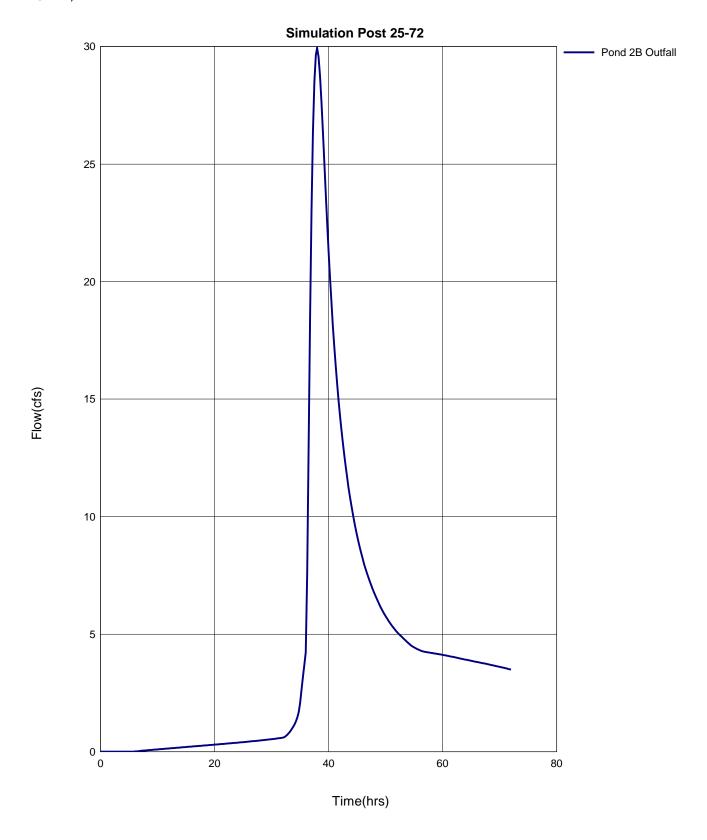
```
*** Weir 1 of 3 for Drop Structure Pond 2B Outfall ***
                                                                                     TABLE
               Count: 1 Bottom Clip(in): 0.000
Type: Horizontal Top Clip(in): 0.000
Flow: Both Weir Disc Coef: 3.200
Geometry: Circular Orifice Disc Coef: 0.600
                Span(in): 6.00
                                                        Invert(ft): 21.450
                                                Control Elev(ft): 21.950
                Rise(in): 6.00
*** Weir 2 of 3 for Drop Structure Pond 2B Outfall ***
                                                                                     TABLE
               Count: 1 Bottom Clip(in): 0.000
Type: Horizontal Top Clip(in): 0.000
Flow: Both Weir Disc Coef: 3.200
Geometry: Rectangular Orifice Disc Coef: 0.600
               Span(in): 79.00
Rise(in): 36.00
                                               Control Elev(ft): 22.950
*** Weir 3 of 3 for Drop Structure Pond 2B Outfall ***
                                                                                     TABLE
               Count: 1 Bottom Clip(in): 0.000
Type: Vertical: Mavis Top Clip(in): 0.000
Flow: Both Weir Disc Coef: 3.200
Geometry: Rectangular Orifice Disc Coef: 0.600
               Span(in): 48.00
Rise(in): 3.00
                                                 Invert(ft): 22.350
Control Elev(ft): 22.350
_______
Name: Post 2B 25-72
Filename: T:\00809.00\zTBG\drainage\ICPR\Post 2B - 25-72.R32
    Override Defaults: Yes
Storm Duration(hrs): 72.00
Rainfall File: Flmod
Rainfall Amount(in): 9.00
Time(hrs)
               Print Inc(min)
Restart: No
  Execute: Yes Alternative: No
                                                  Patch: No
                                                  Delta Z Factor: 0.00500
        Max Delta Z(ft): 1.00
    Time Step Optimizer: 10.000
Start Time(hrs): 0.000
Min Calc Time(sec): 0.5000
                                            End Time(hrs): 72.00
Max Calc Time(sec): 60.0000
        Boundary Stages:
                                                    Boundary Flows:
Time(hrs) Print Inc(min)
            15.000
15.000
72.000
                Run
Group
BASE
```

Basin Name: Basin 2
Group Name: BASE
Simulation: Post 2B 25-72
Node Name: Pond 2B
Basin Type: SCS Unit Hydrograph
Unit Hydrograph: Uh323
Peaking Fator: 323.0
Spec Time Inc (min): 5.70
Comp Time Inc (min): 5.00
Rainfall File: Flmod
Rainfall Amount (in): 9.000
Storm Duration (hrs): 72.00
Status: Onsite
Time of Conc (min): 42.75
Time Shift (hrs): 0.00
Area (ac): 52.430
Vol of Unit Hyd (in): 1.001
Curve Number: 92.000
DCIA (%): 0.000

Time Max (hrs): 36.17
Flow Max (cfs): 89.45
Runoff Volume (in): 8.021
Runoff Volume (ft3): 1526629

Name	Group	Simulation	Max Time Stage hrs	Max Stage ft	Warning M Stage ft	ax Delta Stage ft	Max Surf Area ft2	Max Time Inflow hrs	Max Inflow cfs	Max Time Outflow hrs	Max Outflow cfs
Commerce Center	BASE BASE	Post 25-72	0.00	18.33	999.00	0.0000	0 533556	37.97 36.24	29.94 89.15	0.00	0.00





```
..oue. rond 2B Status: Onsite
Type: SCS Unit Hydrograph CN
       Group: BASE
   Max Allowable Q(cfs): 999999.000
----- Nodes ------
______
                             Base Flow(cfs): 0.000
     Name: Commerce Center
                                                              Init Stage(ft): 18.330
    Group: BASE
Type: Time/Stage
                                                              Warn Stage(ft): 999.000
From ICPR: Pre-Analysis, Node Time Series for 25/72
Using Commerce Center Permit Information
Converted from NGVD to NAVD
     Time(hrs)
      0.00 18.330
999.00 18.330

        Name:
        Pond 2B
        Base Flow(cfs):
        0.000
        Init Stage(ft):
        21.950

        Group:
        BASE
        Warn Stage(ft):
        24.430

    Group: BASE
     Type: Stage/Area
     Stage(ft)
                     Area(ac)
        21.950
                 6.9060
        22.430
23.430
                        7.0080
7.2210
                      7.4380
7.6580
        24.430
Name:
                               From Node:
                                                              Length(ft): 0.00
       Group: BASE
                                                                     Count: 1
                            DOWNSTREAM
Circular
0.00
                                                         Friction Equation: Automatic
                                                    Friction Equation: Automatic
Solution Algorithm: Most Restrictive
Flow: Both
              UPSTREAM
    Geometry: Circular
                                                      Entrance Loss Coef: 0.00
Exit Loss Coef: 1.00
Bend Loss Coef: 0.00
Outlet Ctrl Spec: Use dc or tw
    Span(in): 0.00
                             0.00
     Rise(in): 0.00
   Invert(ft): 0.000
                             0.000
                             0.000
 Manning's N: 0.000000
Top Clip(in): 0.000
Bot Clip(in): 0.000
                             0.000
                             0.000
                                                        Stabilizer Option: None
Upstream FHWA Inlet Edge Description:
Circular Concrete: Square edge w/ headwall
Downstream FHWA Inlet Edge Description:
Circular Concrete: Square edge w/ headwall
______
______
                                    rom Node: Pond 2B Length(ft): 200.00
To Node: Commerce Center Count: 1
         Name: Pond 2B Outfall From Node: Pond 2B
       Group: BASE
                             DOWNSTREAM
                                                         Friction Equation: Automatic
              UPSTREAM
                                                       Friction Equation: Automatic
Solution Algorithm: Most Restrictive
Flow: Both
Entrance Loss Coef: 0.500
Exit Loss Coef: 1.000
Outlet Ctrl Spec: Use dc or tw
Inlet Ctrl Spec: Use dc
Solution Incs: 10
    Geometry: Circular
Span(in): 30.00
                              Circular
                             30.00
  Rise(in): 30.00
Invert(ft): 18.950
                             30.00
18.030
                             0.012000
0.000
0.000
 Manning's N: 0.012000
Top Clip(in): 0.000
Bot Clip(in): 0.000
Upstream FHWA Inlet Edge Description:
Circular Concrete: Square edge w/ headwall
Downstream FHWA Inlet Edge Description:
Circular Concrete: Square edge w/ headwall
```

```
*** Weir 1 of 3 for Drop Structure Pond 2B Outfall ***
                  Count: 1 Bottom Clip(in): 0.000
Type: Horizontal Top Clip(in): 0.000
Flow: Both Weir Disc Coef: 3.200
Geometry: Circular Orifice Disc Coef: 0.600
Span(in): 5.00
                                                                                                     TABLE
                                                      Invert(ft): 21.450
Control Elev(ft): 21.950
                  Span(in): 5.00
Rise(in): 5.00
*** Weir 2 of 3 for Drop Structure Pond 2B Outfall ***
                                                                                                     TABLE

        Count: 1
        Bottom Clip(in): 0.000

        Type: Horizontal
        Top Clip(in): 0.000

        Flow: Both
        Weir Disc Coef: 3.200

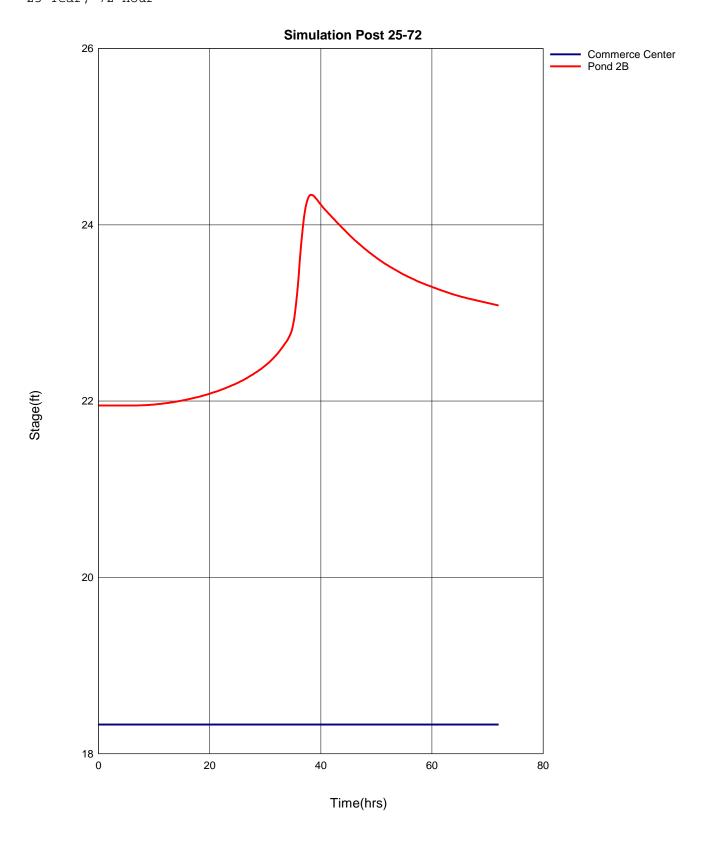
        Geometry: Rectangular
        Orifice Disc Coef: 0.600

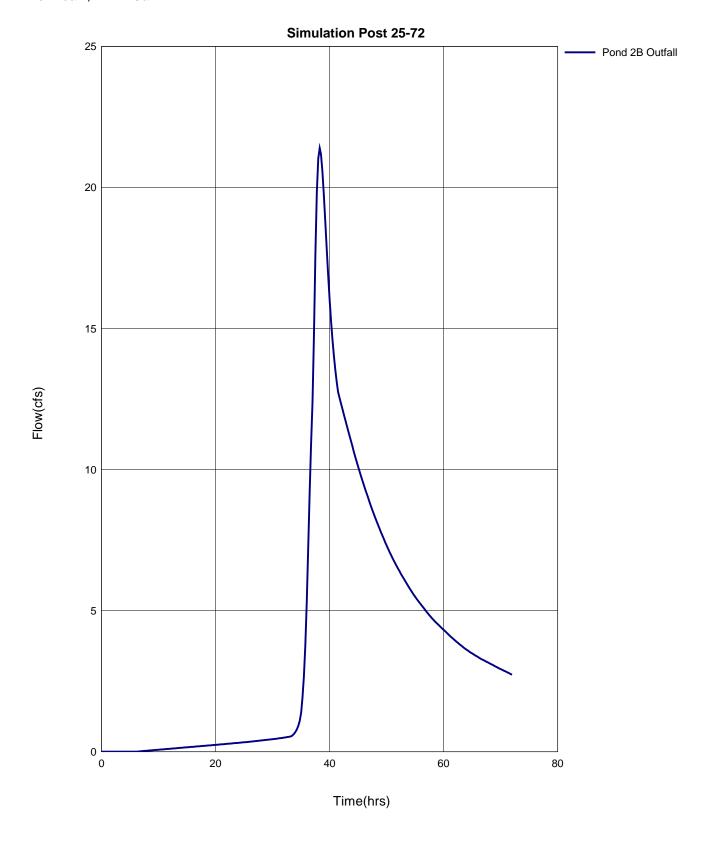
        Span(in): 79.00
        Invert(ft): 24.120

        Rise(in): 36.00
        Control Elev(ft): 24.120

*** Weir 3 of 3 for Drop Structure Pond 2B Outfall ***
                                                                                                     TARLE
                  Count: 1 Bottom Clip(in): 0.000
Type: Vertical: Mavis Top Clip(in): 0.000
Flow: Both Weir Disc Coef: 3.200
Geometry: Rectangular Orifice Disc Coef: 0.600
                                                       Invert(ft): 22.620
Control Elev(ft): 22.620
                  Span(in): 24.00
                  Rise(in): 18.00
______
           Name: Post 2B 25-72
      Filename: T:\00809.00\zTBG\drainage\ICPR\Post 2B - 25-72.R32
     Override Defaults: Yes
Storm Duration(hrs): 72.00
Rainfall File: Flmod
     Rainfall Amount(in): 9.00
Time(hrs)
                  Print Inc(min)
72.000
                 15.00
______
---- Routing Simulations ------
      Restart: No
  Alternative: No
         Max Delta Z(ft): 1.00
                                                           Delta Z Factor: 0.00500
    Time Step Optimizer: 10.000
Start Time(hrs): 0.000
Min Calc Time(sec): 0.5000
                                                    End Time(hrs): 72.00
Max Calc Time(sec): 60.0000
Boundary Flows:
          Boundary Stages:
Time(hrs)
                 Print Inc(min)
10.000
                   15.000
       Run
Group
BASE
```

			Max Time Max		Warning Max Delta		Max Surf	Max Time	Max	Max Time	Max
Name	Group	Simulation	Stage	Stage	Stage	Stage	Area	Inflow	Inflow	Outflow	Outflow
			hrs	ft	ft	ft	ft2	hrs	cfs	hrs	cfs
Commerce Center	BASE	Post 25-72	0.00	18.33	999.00	0.0000	0	38.26	21.40	0.00	0.00
Pond 2B	BASE	Post 25-72	38.26	24.34	24.43	0.0050	323161	36.25	79.45	38.26	21.40





```
Noue. Fond 2B Status: Onsite
Type: SCS Unit Hydrograph CN
        Name: Basin 2
       Group: BASE
   Unit Hydrograph: Uh323 Peaking Factor: 323.0
Rainfall File: Storm Duration(hrs): 0.00
Rainfall Amount(in): 0.000 Time of Conc(min): 42.75
Area(ac): 44.150 Time Shift(hrs): 0.00
Curve Number: 91.00 Max Allowable Q(cfs): 999999
                                          Max Allowable Q(cfs): 999999.000
_____
______
                            Base Flow(cfs): 0.000
     Name: Commerce Center
                                                              Init Stage(ft): 18.330
    Group: BASE
Type: Time/Stage
                                                             Warn Stage(ft): 999.000
From ICPR: Pre-Analysis, Node Time Series for 25/72
Using Commerce Center Permit Information
Converted from NGVD to NAVD
     Time(hrs)
                    Stage(ft)
      0.00 18.330
999.00 18.330

        Name:
        Pond 2B
        Base Flow(cfs):
        0.000
        Init Stage(ft):
        21.950

        Group:
        BASE
        Warn Stage(ft):
        25.430

    Group: BASE
     Type: Stage/Area
     Stage(ft)
                    Area(ac)
        21.950
                  4.2960
        22.430
23.430
                       4.5330
        24.430
25.430
                       4.6960
4.8610
        26.430
                       5.0290
_______
Length(ft): 0.00
       Group: BASE
                                    To Node:
                                                                    Count: 1
                                                     Friction Equation: Automatic
Solution Algorithm: Most Restrictive
              UPSTREAM DOWNSTREAM
    Geometry: Circular
Span(in): 0.00
Rise(in): 0.00
                             Circular
0.00
                                                      Flow: Both
Entrance Loss Coef: 0.00
                                                       Exit Loss Coef: 1.00
Bend Loss Coef: 0.00
Outlet Ctrl Spec: Use dc or tw
Inlet Ctrl Spec: Use dc
Stabilizer Option: None
                             0.00
 Invert(ft): 0.000
Manning's N: 0.000000
Top Clip(in): 0.000
Bot Clip(in): 0.000
                             0.000
0.000000
0.000
Upstream FHWA Inlet Edge Description:
Circular Concrete: Square edge w/ headwall
Downstream FHWA Inlet Edge Description:
Circular Concrete: Square edge w/ headwall
Length(ft): 200.00
To Node: Commerce Center Count: 1
        Name: Pond 2B Outfall From Node: Pond 2B
       Group: BASE
                                                      Friction Equation: Automatic
Solution Algorithm: Most Restrictive
              UPSTREAM
                             DOWNSTREAM
                             Circular
    Geometry: Circular
    Span(in): 30.00
Rise(in): 30.00
                             30.00
30.00
                                                       Flow: Both
Entrance Loss Coef: 0.500
Invert(ft): 18.950
Manning's N: 0.012000
Top Clip(in): 0.000
Bot Clip(in): 0.000
                                                       Exit Loss Coef: 1.000
Outlet Ctrl Spec: Use dc or tw
Inlet Ctrl Spec: Use dc
                             18.030
                            0.012000
0.000
                            0.000
                                                            Solution Incs: 10
Upstream FHWA Inlet Edge Description:
Circular Concrete: Square edge w/ headwall
Downstream FHWA Inlet Edge Description:
```

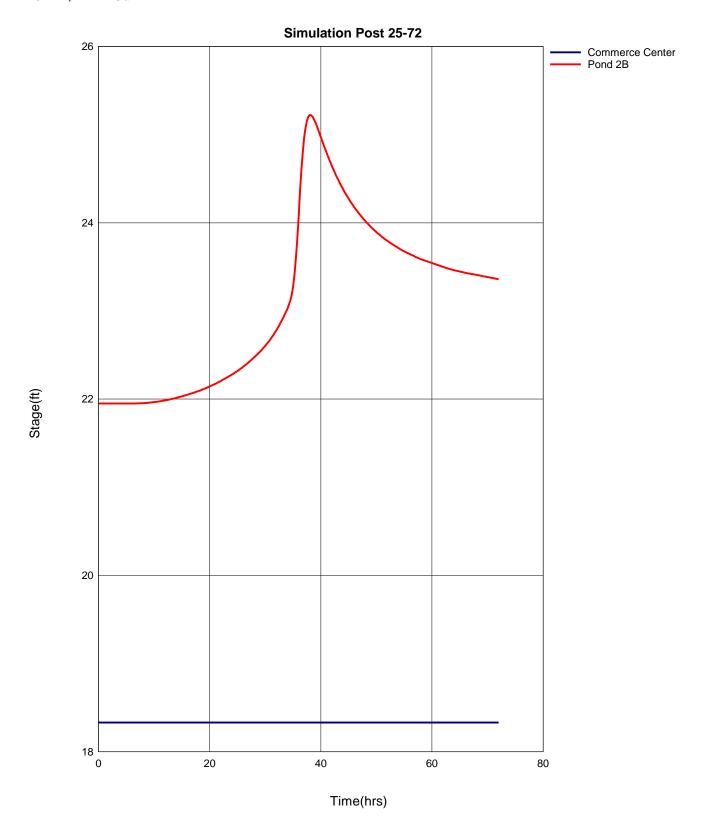
```
Circular Concrete: Square edge w/ headwall
*** Weir 1 of 3 for Drop Structure Pond 2B Outfall ***
                                                                                      TABLE
                                                Bottom Clip(in): 0.000
                   Count: 1
               Type: Horizontal
Flow: Both
Geometry: Circular
                                                Top Clip(in): 0.000
Weir Disc Coef: 3.200
Orifice Disc Coef: 0.600
               Span(in): 5.00
                                                        Invert(ft): 21.450
               Rise(in): 5.00
                                                Control Elev(ft): 21.950
*** Weir 2 of 3 for Drop Structure Pond 2B Outfall ***
                                                                                      TABLE
                                                 Bottom Clip(in): 0.000
                  Count: 1
               Type: Horizontal
Flow: Both
Geometry: Rectangular
                                                  Top Clip(in): 0.000
Weir Disc Coef: 3.200
                                              Orifice Disc Coef: 0.600
               Span(in): 79.00
Rise(in): 36.00
                                                        Invert(ft): 25.180
                                                Control Elev(ft): 25.180
*** Weir 3 of 3 for Drop Structure Pond 2B Outfall ***
                                                                                      TABLE
                  Count: 1
                                                Bottom Clip(in): 0.000
                                              Top Clip(in): 0.000
Weir Disc Coef: 3.200
Orifice Disc Coef: 0.600
                   Type: Vertical: Mavis
Flow: Both
               Flow: Both
Geometry: Rectangular
               Span(in): 24.00
Rise(in): 26.00
                                                Invert(ft): 23.010
Control Elev(ft): 23.010
______
Name: Post 2B 25-72
Filename: T:\00809.00\zTBG\drainage\ICPR\Post 2B - 25-72.R32
    Override Defaults: Yes
Storm Duration(hrs): 72.00
    Rainfall File: Flmod
Rainfall Amount(in): 9.00
            Print Inc(min)
72.000
              15.00
Name: Post 25-72
                                    Hydrology Sim: Post 2B 25-72
     Filename: T:\00809.00\zTBG\drainage\ICPR\Pond 2B - 25-72.I32
                         Restart: No
  Execute: Yes Alternative: No
    Max Delta Z(ft): 1.00
Time Step Optimizer: 10.000
Start Time(hrs): 0.000
Min Calc Time(sec): 0.5000
                                                  Delta Z Factor: 0.00500
                                               End Time(hrs): 72.00
Max Calc Time(sec): 60.0000
                                                    Boundary Flows:
        Boundary Stages:
      nrs) Print Inc(min)
        15.000
15.000
10.000
72.000
Group
                Run
BASE
                Yes
```

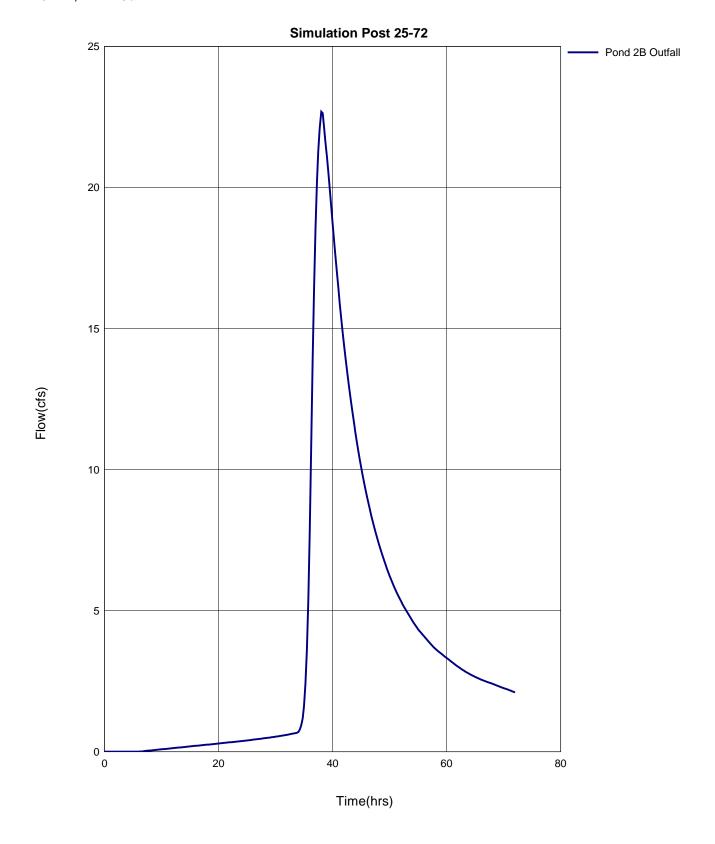
Basin Name: Basin 2
Group Name: BASE
Simulation: Post 2B 25-72
Node Name: Pond 2B
Basin Type: SCS Unit Hydrograph

Unit Hydrograph: Uh323
Peaking Fator: 323.0
Spec Time Inc (min): 5.70
Comp Time Inc (min): 5.70
Comp Time Inc (min): 5.00
Rainfall File: Flmod
Rainfall Amount (in): 9.000
Storm Duration (hrs): 72.00
Status: Onsite
Time of Conc (min): 42.75
Time Shift (hrs): 0.00
Area (ac): 44.150
Vol of Unit Hyd (in): 1.001
Curve Number: 91.000
DCIA (%): 0.000

Time Max (hrs): 36.17
Flow Max (cfs): 74.73
Runoff Volume (in): 7.900
Runoff Volume (ft3): 1266103

Name	Group	Simulation	Max Time Stage hrs	Max Stage ft	Warning M Stage ft	ax Delta Stage ft	Max Surf Area ft2	Max Time Inflow hrs	Max Inflow cfs	Max Time Outflow hrs	Max Outflow cfs
Commerce Center	BASE BASE	Post 25-72	0.00	18.33	999.00	0.0000	0 210263	38.11 36.25	22.73 74.56	0.00	0.00





RUNOFF CURVE NUMBER CALCULATIONS

PROJECT: SR 710 PREPARED: LCS DATE: 2/26/2014

LOCATION: OKEECHOBEE CO., FL CHECKED: GS DATE: 2/26/2014

Basin: BASIN 2C - Option 1 - POST DEVELOPMENT - R/W Only

Drainage Area: From Station 509+30 to Station 610+20

Basin Length = 10090 feet R/W Width = 160 feet

1. Runoff curve number

Cover description	Soil name	Hydrologic group	CN	Area (Acre)	CN x Area
Pavement - Proposed SR 710			98	22.35	2191
Open Space - Good Condition (Perv R/W)		D	80	14.71	1177
Water Management Area (Imperv.)			100	3.34	334
Water Management Area (Perv.)		D	80	3.53	282
			Totals =	43.93	3983

Note: Assumed Type D Soil as soil types were predominantly Types B/D & C/D

TREATMENT VOLUME CALCULATIONS FOR PROPOSED CONDITION

PROJECT: SR 710 - Pond 2C - Option 1 PREPARED: LCS 2/26/2014

LOCATION: OKEECHOBEE COUNTY, FLORIDA CHECKED: GS 2/26/2014

Wet Detention Online Pond Treatment Calculations:

Proposed impervious area = 22.35 Ac
Total Drainage area = 43.93 Ac

2.5" times percent imperviousness = 4.66 Ac-Ft

1" runoff from drainage area = 3.66 Ac-Ft

Treatment Volume = Greater of 2.50" times percent imperviousness or 1.0" over drainage area

Required Treatment Volume (T.V.) = 4.66 Ac-ft

202851 ft³

Pond Storage Calculations (Wet Detention - Pond 2C):

Elev. (NAVD)	h	Area	Area	Inc. Volume	Cum. Volume	Cum. Volume	
(ft)	ft	sf	ac	Ac-ft	Ac-ft	Cu-ft	
24.43	1.0	198,560	4.558	4.455	24.042	1,047,270	
23.43	0.6	189,590	4.352	2.575	19.587	853,210	
22.83	1.0	184,257	4.230	4.129	17.012	741,043	
21.83	1.0	175,449	4.028	3.928	12.883	561,183	
20.83	1.0	166,741	3.828	3.729	8.955	390,080	
19.83	1.0	158,133	3.630	3.533	5.226	227,645	
18.83	0.5	149,627	3.435	1.693	1.693	73,747	
18.33	0.0	145,411	3.338	0.000	0.000	0	

Overflow Weir Elevation (Top of storage volume) (Pond2C)

Elev. S	orage	Area
18.83	.693 1	49,627
19.83	.226 1	58,133
19.83	.226 1	58,

Elev. = 19.67 = 4.66 Ac-Ft 203021 Cu-Ft

Provided Treatment Volume (T.V.) = **4.661** Ac-ft

Treatment Depth = 1.34 ft

For Orifice Recovery Calculations (Pond2C)

Size the orifice to discharge no more than 0.5 inch of the required detention volume in 24 hours.

1/2" of the required detention volume = (0.5 in.* (Total DA - Water Area)/12in/ft)

1/2" runoff from drainage area = 1.69 Ac-Ft 73666 Cu-Ft

Elev.	Storage	Area
18.33	0.000	145,411
18.83	1.693	149,627

Elev. = 18.83 ft. provides 1.69 Ac-Ft 73747 Cu-Ft

From Geotechnical Information (10/13):

Boring PB-2C:

Est. Ground Elevation (at boring location) = 19.5 feet Subtract Estimated SHGT Depth = -0.67-0.5 = 1.17 feet

Estimated SHGT Elev. = 18.33 feet

ORIFICE SIZING FOR PROPOSED CONDITION

PROJECT: SR 710 - Pond 2C -Option 1 PREPARED: LCS 2/26/2014

LOCATION: OKEECHOBEE COUNTY, FLORIDA CHECKED: GS 2/26/2014

Pond 2C Orifice Calculations

Size the orifice to discharge no more than 0.5 inch of the required detention volume in 24 hours.

Orifice Equation:

Average Discharge Rate: Drawdown 0.5 in of Required Detention Volume in 24 hrs.

 ft^3 Required Treatment Volume = 73666.04

Recovery Time (t) = 24.00 hr Conversion Factor (CF) = sec/hr

3600.00

$$Q = \frac{TV}{2 t CF}$$

0.426 Q =cfs

Elevation of Required Treatment Volume = 18.83 ft

Flow line Elevation = 18.33 ft

Depth of water between top of treatment vol. and flow line (h1) = 0.50 ft

> h = 0.50

 $A = \frac{Q}{C\sqrt{2 g h}}$ Orifice Equation:

> A = 0.125

0.40 ft 4.79 in dia D =

4 inch orifice Use

RUNOFF CURVE NUMBER CALCULATIONS

PROJECT: SR 710 PREPARED: LCS DATE: 2/26/2014

LOCATION: OKEECHOBEE CO., FL CHECKED: GS DATE: 2/26/2014

Basin: BASIN 2C - Option 2 - POST DEVELOPMENT - R/W Only

Drainage Area: From Station 509+30 to Station 610+20

Basin Length = 10090 feet R/W Width = 160 feet

1. Runoff curve number

Cover description	Soil name	Hydrologic group	CN	Area (Acre)	CN x Area
Pavement - Proposed SR 710			98	22.35	2191
Open Space - Good Condition (Perv R/W)		D	80	14.71	1177
Water Management Area (Imperv.)			100	2.37	237
Water Management Area (Perv.)		D	80	3.77	302
			Totals =	43.20	3906

Note: Assumed Type D Soil as soil types were predominantly Types B/D & C/D

TREATMENT VOLUME CALCULATIONS FOR PROPOSED CONDITION

SR 710 - Pond 2C - Option 2 PROJECT: PREPARED: LCS 2/26/2014

LOCATION: CHECKED: GS 2/26/2014 OKEECHOBEE COUNTY, FLORIDA

Wet Detention Online Pond Treatment Calculations:

Proposed impervious area = 22.35 Ac 43.20 Ac Total Drainage area =

2.5" times percent imperviousness = 4.66 Ac-Ft

1" runoff from drainage area = 3.60 Ac-Ft

Treatment Volume = Greater of 2.50" times percent imperviousness or 1.0" over drainage area

Required Treatment Volume (T.V.) = 4.66 Ac-ft

ft³ 202851

Pond Storage Calculations (Wet Detention - Pond 2C):

Elev. (NAVD)	h	Area	Area Inc. Volume C		Cum. Volume	Cum. Volume
(ft)	ft	sf	ac	Ac-ft	Ac-ft	Cu-ft
25.43	1.0	157,870	3.624	3.532	21.199	923,428
24.43	1.0	149,845	3.440	3.349	17.667	769,575
23.43	1.0	141,920	3.258	3.168	14.318	623,692
22.43	1.0	134,095	3.078	2.990	11.150	485,694
21.43	1.0	126,371	2.901	2.814	8.160	355,450
20.43	1.0	118,748	2.726	2.640	5.346	232,872
19.43	1.1	111,227	2.553	2.706	2.706	117,873
18.33	0.0	103,092	2.367	0.000	0.000	0

Overflow Weir Elevation (Top of storage volume) (Pond2C)

Elev.	Storage	Area
19.43	2.706	111,227
20.43	5.346	118,748

Elev. = 20.17 4.66 Ac-Ft 202972 Cu-Ft

Provided Treatment Volume (T.V.) = 4.660 Ac-ft

> Treatment Depth = 1.84 ft

For Orifice Recovery Calculations (Pond2C)

Size the orifice to discharge no more than 0.5 inch of the required detention volume in 24 hours.

1/2" of the required detention volume = (0.5 in.* (Total DA - Water Area)/12in/ft)

1/2" runoff from drainage area = 1.70 Ac-Ft 74113 Cu-Ft

Elev.	Storage	Area
18.33	0.000	103,092
19.43	2.706	111,227

Elev. = 19.03 ft. provides 1.72 Ac-Ft 75010 Cu-Ft

From Geotechnical Information (10/13):

Boring PB-2C:

Est. Ground Elevation (at boring location) = 19.5 feet

Subtract Estimated SHGT Depth = -0.67- 0.5 = 0.67 feet

Estimated SHGT Elev. = 18.33 feet

ORIFICE SIZING FOR PROPOSED CONDITION

PROJECT: SR 710 - Pond 2C - Option 2 PREPARED: LCS 2/26/2014

LOCATION: OKEECHOBEE COUNTY, FLORIDA CHECKED: GS 2/26/2014

Pond 2C Orifice Calculations

Size the orifice to discharge no more than 0.5 inch of the required detention volume in 24 hours.

Orifice Equation:

Average Discharge Rate: Drawdown 0.5 in of Required Detention Volume in 24 hrs.

Required Treatment Volume = 74113.45 ft³

Recovery Time (t) = 24.00 hr

Conversion Factor (CF) = 3600.00 sec/hr

$$Q = \frac{TV}{2 t CF}$$

Q = 0.429 cfs

Elevation of Required Treatment Volume = 19.03 ft

Flow line Elevation = 18.33 ft

Depth of water between top of treatment vol. and flow line (h1) = 0.70 ft

h = 0.70

Orifice Equation: $A = \frac{Q}{C\sqrt{2 g h}}$

A = 0.106 ft²

 $D = \sqrt{\frac{4 A}{\pi}}$

D = 0.37 ft = 4.42 in dia

Use 4 inch orifice

Nodes
A Stage/Area
V Stage/Volume
T Time/Stage
M Manhole

Basins
O Overland Flow
U SCS Unit CN
S SBUH CN
Y SCS Unit GA
Z SBUH GA

Links
P Pipe
W Weir
C Channel
D Drop Structure
B Bridge
R Rating Curve
B Breach
E Percolation
F Filter
F Fitter
F Fitter
X Exfil Trench

T: Taylor Creek

```
______
_______
   Type: SCS Unit Hydrograph CN

Unit Hydrograph: Uh323
Rainfall File:
Rainfall Amount(in): 0.000
Area(ac): 43,930
Curve Number: 91.00
DCIA(%): 0.000

Star Type: SCS Unit Hydrograph CN

Storm Duration(hrs): 0.00
Time of Conc(min): 59.00
Time Shift(hrs): 0.00
Max Allowable Q(cfs): 999999
         Name: Basin 2
                                            Node: Pond 2C
                                                                             Status: Onsite
                                               Max Allowable Q(cfs): 999999.000
Base Flow(cfs): 0.000
                                                                      Init Stage(ft): 18.330
                                                                      Warn Stage(ft): 23.430
     Group: BASE
Type: Stage/Area
      Stage(ft)
                        Area(ac)
         18.330
                          3.3380
         18.830
          19.830
                           3.6300
         20.830
                           3.8280
          22.830
                          4.2300
          23 430
                          4 3520
         24.430
                          4.5580
                                                                      Init Stage(ft): 12.830
      Name: Taylor Creek Base Flow(cfs): 0.000
     Group: BASE
Type: Time/Stage
                                                                      Warn Stage(ft): 999.000
Converted from NGVD to NAVD
FROM DOUGLAS PARK PERMIT
REFLECTS THE SAME PEAK STAGE AS COMMERCE CENTER PERMIT
     Time(hrs)
                      Stage(ft)
       0.00 12.830
999.00 12.830
To Node: Taylor Creek Count: 1
         Name: Pond 2C Outfall From Node: Pond 2C
        Group: BASE
                                               Friction Equation: Automatic
Solution Algorithm: Most Restrictive
                          DOWNSTREAM
Circular
18.00
18.00
14.030
0.012000
0.000
                UPSTREAM
     Geometry: Circular
Span(in): 18.00
Rise(in): 18.00
                                                             Flow: Both
Entrance Loss Coef: 0.500
Exit Loss Coef: 1.000
Outlet Ctrl Spec: Use dc or tw
Inlet Ctrl Spec: Use dc
 Invert(ft): 14.830
Manning's N: 0.012000
Top Clip(in): 0.000
 Bot Clip(in): 0.000
                                                                    Solution Incs: 10
Upstream FHWA Inlet Edge Description:
Circular Concrete: Square edge w/ headwall
Downstream FHWA Inlet Edge Description:
Circular Concrete: Square edge w/ headwall
*** Weir 1 of 3 for Drop Structure Pond 2C Outfall ***
                                                                                           TABLE
                Count: 1 Bottom Clip(in): 0.000
Type: Horizontal Top Clip(in): 0.000
Flow: Both Weir Disc Coef: 3.200
Geometry: Circular Orifice Disc Coef: 0.600
                Span(in): 4.00
                                                            Invert(ft): 17.830
                Rise(in): 4.00
                                                   Control Elev(ft): 18.330
*** Weir 2 of 3 for Drop Structure Pond 2C Outfall ***
                                                                                           TABLE
                Count: 1 Bottom Clip(in): 0.000
Type: Vertical: Mavis Top Clip(in): 0.000
Flow: Both Weir Disc Coef: 3.200
Geometry: Rectangular Orifice Disc Coef: 0.600
                Span(in): 4.00
                                                            Invert(ft): 19.670
                                                   Control Elev(ft): 19.670
                Rise(in): 4.00
*** Weir 3 of 3 for Drop Structure Pond 2C Outfall ***
```

```
TABLE
                                             Bottom Clip(in): 0.000
Top Clip(in): 0.000
Weir Disc Coef: 3.200
Orifice Disc Coef: 0.600
               Count: 1
Type: Horizontal
Flow: Both
Geometry: Rectangular
                                                Invert(ft): 23.000
Control Elev(ft): 23.000
               Span(in): 37.00
               Rise(in): 24.00
______
         Name: Post 2C 10-24
    Filename: T:\00809.00\zTBG\drainage\ICPR\Post 2C - 10-24.R32
      Override Defaults: Yes
    Storm Duration(hrs): 24.00
Rainfall File: Flmod
    Rainfall Amount(in): 8.20
               Print Inc(min)
Time(hrs)
30.000
              15.00
Name: Post 2C 25-72
    Filename: T:\00809.00\zTBG\drainage\ICPR\Post 2C - 25-72.R32
    Override Defaults: Yes
Storm Duration(hrs): 72.00
    Rainfall File: Flmod Rainfall Amount(in): 9.00
Time(hrs)
               Print Inc(min)
              15.00
72.000
    Name: Post 2C 5-1 Filename: T:\00809.00\zTBG\drainage\ICPR\Post 2C - 5-1.R32
      Override Defaults: Yes
    Storm Duration(hrs): 1.00
    Rainfall File: Flmod
Rainfall Amount(in): 2.98
Time(hrs) Print Inc(min)
1.000
              15.00
------
         Name: Post 10-24
                                   Hydrology Sim: Post 2C 10-24
     Filename: T:\00809.00\zTBG\drainage\ICPR\Pond 2C - 10-24.I32
                       Restart: No
  Execute: No Alternative: No
                                           Delta Z Factor: 0.00500
    Max Delta Z(ft): 1.00
Time Step Optimizer: 10.000
Start Time(hrs): 0.000
Min Calc Time(sec): 0.5000
                                            End Time(hrs): 30.00
Max Calc Time(sec): 60.0000
                                                   Boundary Flows:
        Boundary Stages:
      nrs) Print Inc(min)
10.000
Group
               Run
BASE
    Name: Post 25-72 Hydrology Sim: Post 2C 25-72 Filename: T:\00809.00\zTBG\drainage\ICPR\Pond 2C - 25-72.I32
                        Restart: No
 Execute: Yes Alternative: No
       Max Delta Z(ft): 1.00
                                                 Delta Z Factor: 0.00500
    Time Step Optimizer: 10.000
Start Time(hrs): 0.000
Min Calc Time(sec): 0.5000
                                              End Time(hrs): 72.00
Max Calc Time(sec): 60.0000
        Boundary Stages:
                                                   Boundary Flows:
         Print Inc(min)
Time(hrs)
```

10.000 72.000 15.000 15.000 Run Group BASE Yes

Name: Post 5-1 Hydrology Sim: Post 2C 5-1 Filename: T:\00809.00\zTBG\drainage\ICPR\Pond 2C - 5-1.I32

Execute: Yes Alternative: No Restart: No Patch: No

 Max Delta Z(ft):
 1.00
 Delta Z Factor:
 0.00500

 Time Step Optimizer:
 10.000
 End Time(hrs):
 1.00

 Start Time(hrs):
 0.000
 Max Calc Time(sec):
 60.0000

 Min Calc Time(sec):
 60.0000
 Boundary Flows:

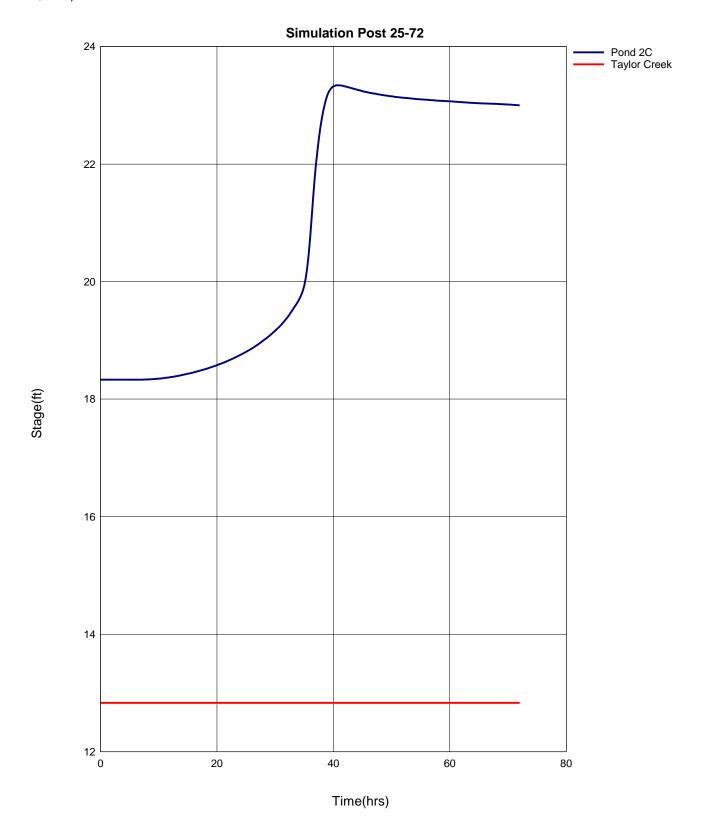
BASE Yes

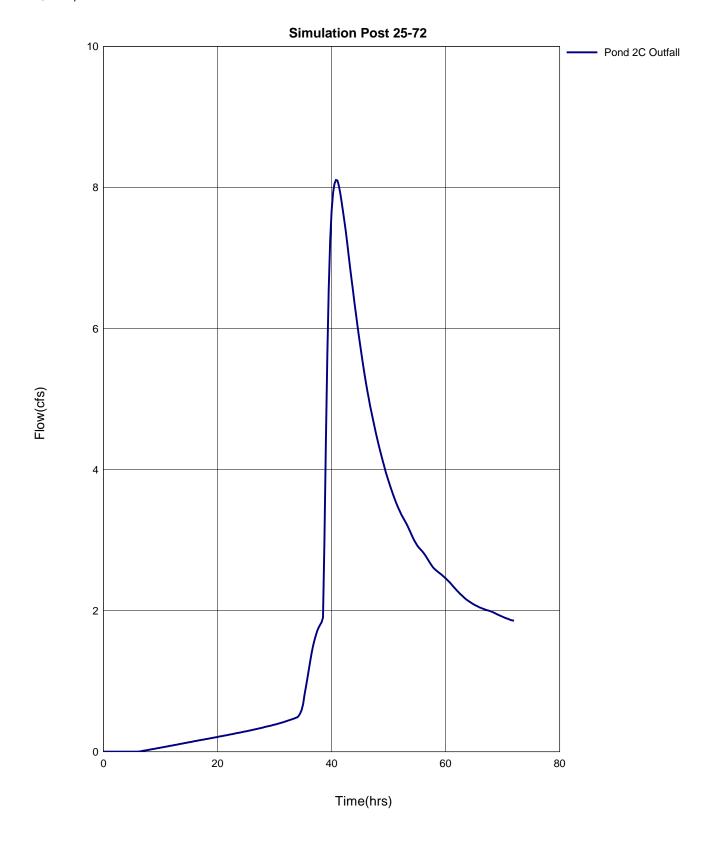
Basin Name: Basin 2
Group Name: BASE
Simulation: Post 2C 25-72
Node Name: Pond 2C
Basin Type: SCS Unit Hydrograph

Unit Hydrograph: Uh323
Peaking Fator: 323.0
Spec Time Inc (min): 7.87
Comp Time Inc (min): 5.00
Rainfall File: Flmod
Rainfall Amount (in): 9.000
Storm Duration (hrs): 72.00
Status: Onsite
Time of Conc (min): 59.00
Time Shift (hrs): 0.00
Area (ac): 43.930
Vol of Unit Hyd (in): 1.001
Curve Number: 91.000
DCIA (%): 0.000

Time Max (hrs): 36.33
Flow Max (cfs): 65.46
Runoff Volume (in): 7.904
Runoff Volume (ft3): 1260438

			Max Time	Max	Warning M	ax Delta	Max Surf	Max Time	Max	Max Time	Max
Name	Group	Simulation	Stage	Stage	Stage	Stage	Area	Inflow	Inflow	Outflow	Outflow
			hrs	ft	ft	ft	ft2	hrs	cfs	hrs	cfs
Pond 2C	BASE	Post 25-72	40.84	23.34	23.43	0.0050	188798	36.25	64.58	40.84	8.11
Taylor Creek	BASE	Post. 25-72	0.00	12.83	999.00	0.0000	0	40.84	8.11	0.00	0.00





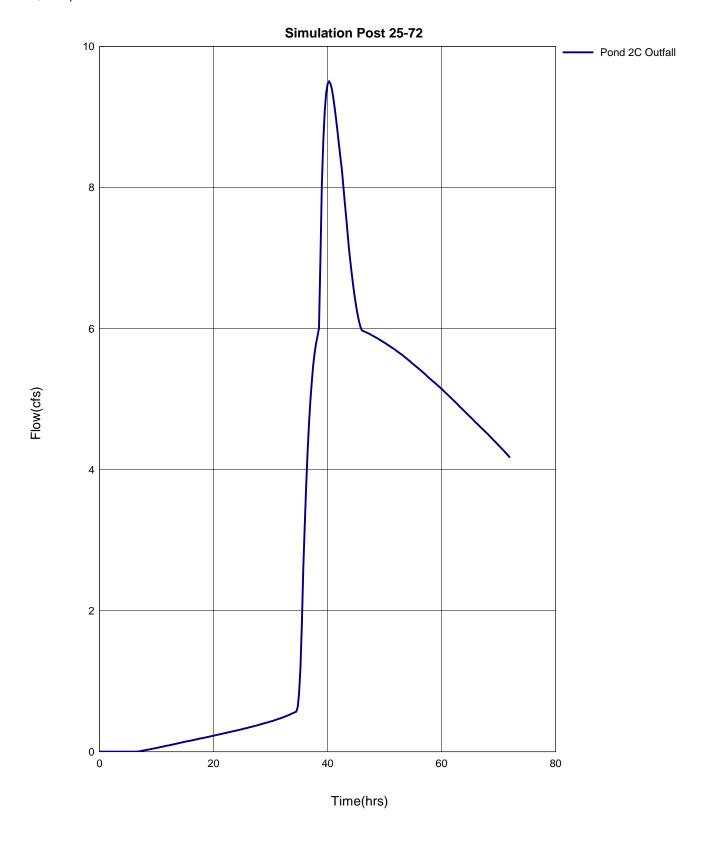
```
Type: SCS Unit Hydrograph CN
        Group: BASE
    Unit Hydrograph: Uh323
Rainfall File:
Rainfall Amount(in): 0.000
Area(ac): 43.200
Curve Number: 90.00
DCIA(%): 0.00
                                                    Peaking Factor: 323.0
                                            Storm Duration(hrs): 0.00
Time of Conc(min): 59.00
Time Shift(hrs): 0.00
                                                Max Allowable Q(cfs): 999999.000
______
______
      Name: Pond 2C
                                 Base Flow(cfs): 0.000
                                                                     Init Stage(ft): 18.330
     Group: BASE
Type: Stage/Area
                                                                     Warn Stage(ft): 24.430
      Stage(ft)
                       Area(ac)
         18.330
         19.430 20.430
                           2.5530
                           2.7260
          21.430 22.430
                           3.0780
          23.430
24.430
                          3.2580
                         3.6240
         25 430
      Name: Taylor Creek Base Flow(cfs): 0.000 Init Stage(ft): 12.830
     Group: BASE
Type: Time/Stage
                                                                    Warn Stage(ft): 999.000
Converted from NGVD to NAVD
FROM DOUGLAS PARK PERMIT
REFLECTS THE SAME PEAK STAGE AS COMMERCE CENTER PERMIT
                   Stage(ft)
_____
           0 00
                  12.830
12.830
         999.00
______
Name: Pond 2C Outfall From Node: Pond 2C Length(ft): 800.00 Group: BASE To Node: Taylor Creek Count: 1
                                                                            Count: 1
                                DOWNSTREAM
                UPSTREAM
                                                               Friction Equation: Automatic
UPSTREAM
Geometry: Circular
Span(in): 18.00
Rise(in): 18.00
Invert(ft): 14.830
Manning's N: 0.012000
Top Clip(in): 0.000
Bot Clip(in): 0.000
                                                             Solution Algorithm: Most Restrictive
Flow: Both
Entrance Loss Coef: 0.500
Exit Loss Coef: 1.000
Outlet Ctrl Spec: Use dc or tw
Inlet Ctrl Spec: Use dc
                               Circular
                                18.00
                                18.00
14.030
                                0.012000
                                                                    Solution Incs: 10
Upstream FHWA Inlet Edge Description:
Circular Concrete: Square edge w/ headwall
Downstream FHWA Inlet Edge Description:
Circular Concrete: Square edge w/ headwall
*** Weir 1 of 3 for Drop Structure Pond 2C Outfall ***
                Count: 1 Bottom Clip(in): 0.000
Type: Horizontal Top Clip(in): 0.000
Flow: Both Weir Disc Coef: 3.200
Geometry: Circular Orifice Disc Coef: 0.600
                                                                                         TABLE
                Span(in): 4.00
Rise(in): 4.00
                                                  Invert(ft): 17.830
Control Elev(ft): 18.330
*** Weir 2 of 3 for Drop Structure Pond 2C Outfall ***
                                                                                          TABLE
                Count: 1 Bottom Clip(in): 0.000
Type: Vertical: Mavis Top Clip(in): 0.000
Flow: Both Weir Disc Coef: 3.200
Geometry: Rectangular Orifice Disc Coef: 0.600
                Span(in): 10.00
Rise(in): 8.00
                                                   Invert(ft): 20.170
Control Elev(ft): 20.170
```

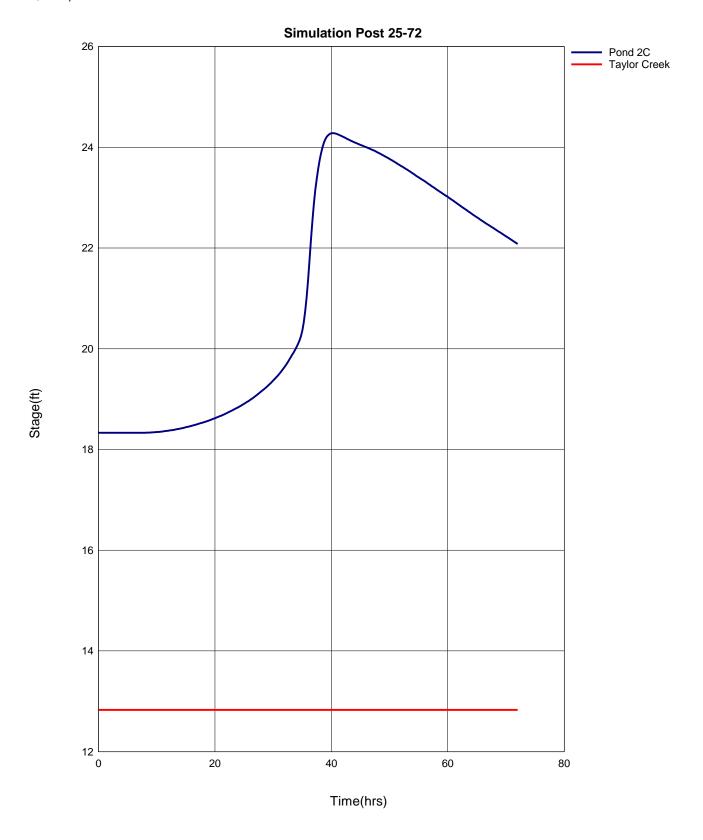
```
*** Weir 3 of 3 for Drop Structure Pond 2C Outfall ***
                                                                                            TABLE
                                                  Bottom Clip(in): 0.000
Top Clip(in): 0.000
Weir Disc Coef: 3.200
Orifice Disc Coef: 0.600
                    Count: 1
                     Type: Horizontal
Flow: Both
                 Geometry: Rectangular
                 Span(in): 37.00
Rise(in): 24.00
                                                   Invert(ft): 24.000
Control Elev(ft): 24.000
Name: Post 2C 25-72
Filename: T:\00809.00\zTBG\drainage\ICPR\Post 2C - 25-72.R32
    Override Defaults: Yes
Storm Duration(hrs): 72.00
Rainfall File: Flmod
    Rainfall Amount(in): 9.00
Time(hrs)
                Print Inc(min)
                 15.00
          Name: Post 2C 5-1
     Filename: T:\00809.00\zTBG\drainage\ICPR\Post 2C - 5-1.R32
    Override Defaults: Yes
Storm Duration(hrs): 1.00
Rainfall File: Flmod
    Rainfall Amount(in): 2.98
Time(hrs)
                Print Inc(min)
1.000
                15.00
______
---- Routing Simulations ------
     Name: Post 25-72 Hydrology Sim: Post 2C 25-72 Filename: T:\00809.00\zTBG\drainage\ICPR\Pond 2C - 25-72.I32
      Execute: Yes
  Alternative: No
        Max Delta Z(ft): 1.00
                                                       Delta Z Factor: 0.00500
    Time Step Optimizer: 10.000
Start Time(hrs): 0.000
Min Calc Time(sec): 0.5000
                                                End Time(hrs): 72.00
Max Calc Time(sec): 60.0000
         Boundary Stages:
                                                       Boundary Flows:
Time(hrs)
                 Print Inc(min)
10.000
                 15.000
Group
                 Run
BASE
                 Yes
     Name: Post 5-1 Hydrology Sim: Post 2C 5-1 Filename: T:\00809.00\zTBG\drainage\ICPR\Pond 2C - 5-1.132
       Execute: Yes
                           Restart: No
                                                      Patch: No
  Alternative: No
                                                     Delta Z Factor: 0.00500
        Max Delta Z(ft): 1.00
    Time Step Optimizer: 10.000
Start Time(hrs): 0.000
Min Calc Time(sec): 0.5000
                                              End Time(hrs): 1.00
Max Calc Time(sec): 60.0000
Boundary Flows:
         Boundary Stages:
         Print Inc(min)
Time(hrs)
0.500
10.000
Group
BASE
                 Yes
```

Basin Name: Basin 2
Group Name: BASE
Simulation: Post 2C 25-72
Node Name: Pond 2C
Basin Type: SCS Unit Hydrograph
Unit Hydrograph: Uh323
Peaking Fator: 323.0
Spec Time Inc (min): 7.87
Comp Time Inc (min): 5.00
Rainfall File: Flmod
Rainfall Amount (in): 9.000
Storm Duration (hrs): 72.00
Status: Onsite
Time of Conc (min): 59.00
Time Shift (hrs): 0.00
Area (ac): 43.200
Vol of Unit Hyd (in): 1.001
Curve Number: 90.000
DCIA (%): 0.000

Time Max (hrs): 36.33
Flow Max (cfs): 63.79
Runoff Volume (in): 7.783
Runoff Volume (ft3): 1220445

Name	Group	Simulation	Max Time Stage hrs	Max Stage ft	Warning M Stage ft	ax Delta Stage ft	Max Surf Area ft2	Max Time Inflow hrs	Max Inflow cfs	Max Time Outflow hrs	Max Outflow cfs
Pond 2C	BASE	Post 25-72	40.24	24.28	24.43	0.0050	148660	36.25	62.92	40.24	9.51
Tavlor Creek	BASE	Post 25-72	0.00	12.83	999.00	0.0000	0	40.24	9.51	0.00	0.00





Basin 3

RUNOFF CURVE NUMBER CALCULATIONS

PROJECT: SR 710 PREPARED: LCS DATE: 2/26/2014

LOCATION: OKEECHOBEE CO., FL CHECKED: GS DATE: 2/26/2014

Basin: BASIN 3A - POST DEVELOPMENT - R/W Only

Drainage Area: From Station 610+20 to Station 638+46.43

Basin Length = 2826.43 feet R/W Width = 160 feet

1. Runoff curve number

Cover description	Soil name	Hydrologic group	CN	Area (Acre)	CN x Area
Pavement - Proposed SR 710			98	6.26	614
Open Space - Good Condition (Perv R/W)		D	80	4.12	330
Water Management Area (Imperv.)			100	1.66	166
Water Management Area (Perv.)		D	80	2.52	201
			Totals =	14.56	1311

CN (weighted) = (total product) = 1,311 (total area) 14.56

Note: Assumed Type D Soil as soil types were predominantly Types B/D & C/D

Note: Profile at Sta. 638+30 controlled by Kimley Horn (Bridge at SR 70)

TREATMENT VOLUME CALCULATIONS FOR PROPOSED CONDITION

PROJECT: SR 710 - Pond 3A PREPARED: LCS 2/26/2014

LOCATION: OKEECHOBEE COUNTY, FLORIDA CHECKED: GS 2/26/2014

Wet Detention Online Pond Treatment Calculations:

Proposed impervious area = 6.26 Ac

Total Drainage area = 14.56 Ac

2.5" runoff from impervious area = 1.30 Ac-Ft

1" runoff from drainage area = 1.21 Ac-Ft

Treatment Volume = Greater of 2.50" times percent imperviousness or 1.0" over drainage area

Required Treatment Volume (T.V.) = 1.30 Ac-ft

= 56823 ft³

Pond Storage Calculations (Wet Detention - Pond 3A):

Elev. (NAVD)	h	Area	Area	Inc. Volume	Cum. Volume	Cum. Volume
(ft)	ft	sf	ac	Ac-ft	Ac-ft	Cu-ft
29.73	1.0	100,430	2.306	2.239	9.903	431,375
28.73	1.0	94,648	2.173	2.108	7.664	333,844
27.73	1.0	88,966	2.042	1.978	5.556	242,019
26.73	1.0	83,384	1.914	1.851	3.578	155,858
25.73	1.0	77,904	1.788	1.727	1.727	75,228
24.73	0.0	72,523	1.665	0.000	0.000	0

Overflow Weir Elevation (Top of storage volume) (Pond3A)

Elev.	Storage	Area
24.73	0.000	72,523
25.73	1.727	77,904

Elev. = 25.49 = 1.31 Ac-Ft 57173 Cu-Ft

Provided Treatment Volume (T.V.) = 1.313 Ac-ft

Treatment Depth = 0.76 ft

For Orifice Recovery Calculations (Pond3A)

Size the orifice to discharge no more than 0.5 inch of the required detention volume in 24 hours.

1/2" of the required detention volume = (0.5 in.* (Total DA - Water Area)/12in/ft)

1/2" runoff from drainage area = 0.54 Ac-Ft 23409 Cu-Ft

Elev.	Storage	Area
24.73	0.000	72,523
25.73	1.727	77,904

Elev. = 25.05 ft. provides 0.55 Ac-Ft = 24073 Cu-Ft

From Geotechnical Information (10/13):

Boring PB-3A:

Est. Ground Elevation (at boring location) = 31 feet

Subtract Est. SHGT Depth = -1.92-0.5 = 2.42 feet

Estimated SHGT Elev. = 28.58 feet

ORIFICE SIZING FOR PROPOSED CONDITION

PROJECT: SR 710 - Pond 3A PREPARED: LCS 2/26/2014

LOCATION: OKEECHOBEE COUNTY, FLORIDA CHECKED: GS 2/26/2014

Pond 3A Orifice Calculations

Size the orifice to discharge no more than 0.5 inch of the required detention volume in 24 hours.

Orifice Equation:

Average Discharge Rate: Drawdown 0.5 in of Required Detention Volume in 24 hrs.

Required Treatment Volume = 23409.03 ft³

Recovery Time (t) = 24.00 hr

Conversion Factor (CF) = 3600.00 sec/hr

$$Q = \frac{TV}{2 t CF}$$

Q = 0.135 cfs

Elevation of Required Treatment Volume = 25.05 ft

Flow line Elevation = 24.73 ft

Depth of water between top of treatment vol. and flow line (h1) = 0.32 ft

$$h = 0.32$$

Orifice Equation:

$$A = \frac{Q}{C\sqrt{2 g h}}$$

$$A = 0.050 ft^2$$

$$D = \sqrt{\frac{4 A}{\pi}}$$

$$D = 0.25 \text{ ft} = 3.02 \text{ in dia}$$

Use 3 inch orifice

Nodes
A Stage/Area
V Stage/Volume
T Time/Stage
M Manhole

Basins
O Overland Flow
U SCS Unit CN
S SBUH CN
Y SCS Unit GA
Z SBUH GA

Links
P Pipe
W Weir
C Channel
D Drop Structure
B Bridge
R Rating Curve
B Breach
E Percolation
F Filter
F Fitter
X Exfil Trench

T: L-63N Canal

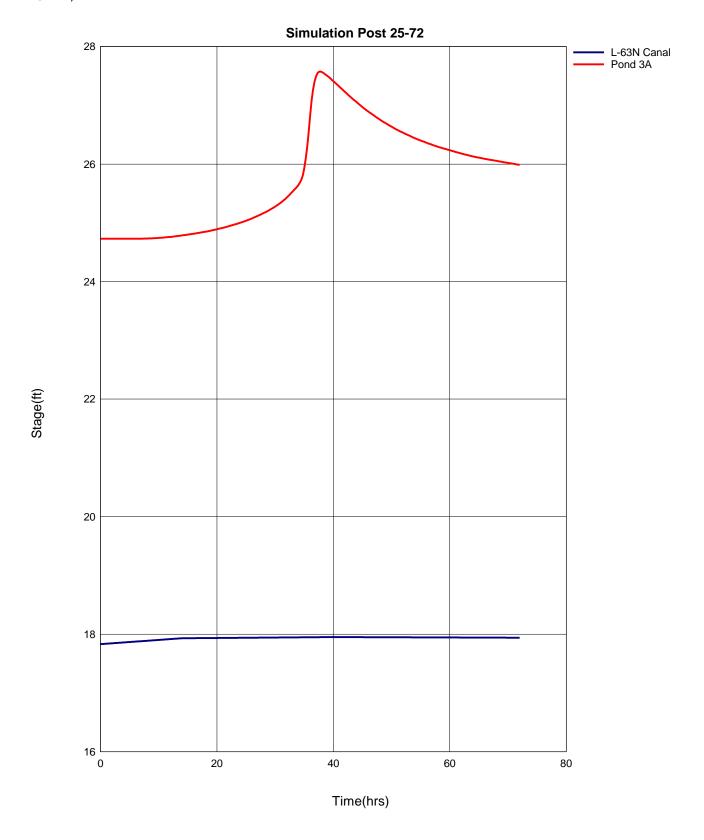
```
Group: BASE
    Unit Hydrograph: Uh323
Rainfall File:
Rainfall Amount(in): 0.000
Area(ac): 14.530
Curve Number: 90.00
DCIA(%): 0.00
                                                   Peaking Factor: 323.0
                                             Storm Duration(hrs): 0.00
Time of Conc(min): 21.82
Time Shift(hrs): 0.00
                                               Max Allowable Q(cfs): 999999.000
______
______
      Name: L-63N Canal
                                Base Flow(cfs): 0.000
                                                                   Init Stage(ft): 17.830
     Group: BASE
Type: Time/Stage
                                                                   Warn Stage(ft): 28.830
     Time(hrs)
                      Stage(ft)
                  17.830
17.930
          0.00
          14.00
                   17.950
17.930
           40.00
      Name: Pond 3A Base Flow(cfs): 0.000 Init Stage(ft): 24.730
Group: BASE Warn Stage(ft): 28.650
     Group: BASE
      Type: Stage/Area
      Stage(ft)
                       Area(ac)
         24.730
                         1.6650
         25.730
25.730
26.730
27.730
28.730
                          1.7880
                         2.0420
2.1730
         29.730
                          2.3060
______
---- Drop Structures ------
          Name: Pond 3A Outfall
                                    From Node: Pond 3A
To Node: L-63N Canal
                                                                     Length(ft): 140.00
        Group: BASE
                                                                           Count: 1
                UPSTREAM
                               DOWNSTREAM
                                                             Friction Equation: Automatic
                                                            Friction Equation: Automatic
Solution Algorithm: Most Restrictive
Flow: Both
Entrance Loss Coef: 0.500
Exit Loss Coef: 1.000
Outlet Ctrl Spec: Use dc or tw
Inlet Ctrl Spec: Use dc
Solution Incs: 10
     Geometry: Circular
Span(in): 18.00
                               Circular
18.00
     Rise(in): 18.00
                               18.00
 Invert(ft): 20.230
Manning's N: 0.012000
Top Clip(in): 0.000
Bot Clip(in): 0.000
                               19.950
0.012000
0.000
Upstream FHWA Inlet Edge Description:
Circular Concrete: Square edge w/ headwall
Downstream FHWA Inlet Edge Description:
Circular Concrete: Square edge w/ headwall
*** Weir 1 of 3 for Drop Structure Pond 3A Outfall ***
                                      Bottom Clip(in): 0.000
Top Clip(in): 0.000
Weir Disc Coef: 3.200
Orifice Disc Coef: 0.600
                                                                                       TABLE
                Type: Horizontal
Flow: Both
Geometry: Circular
                Span(in): 3.00
Rise(in): 3.00
                                                  Invert(ft): 24.730
Control Elev(ft): 24.730
*** Weir 2 of 3 for Drop Structure Pond 3A Outfall ***
                                       Bottom Clip(in): 0.000
avis Top Clip(in): 0.000
Weir Disc Coef: 3.200
Orifice Disc Coef: 0.600
                                                                                       TABLE
                Type: Vertical: Mavis
Flow: Both
Geometry: Rectangular
                                                 Invert(ft): 25.490
Control Elev(ft): 25.490
                Rise(in): 24.00
*** Weir 3 of 3 for Drop Structure Pond 3A Outfall ***
                                                                                        TARLE
```

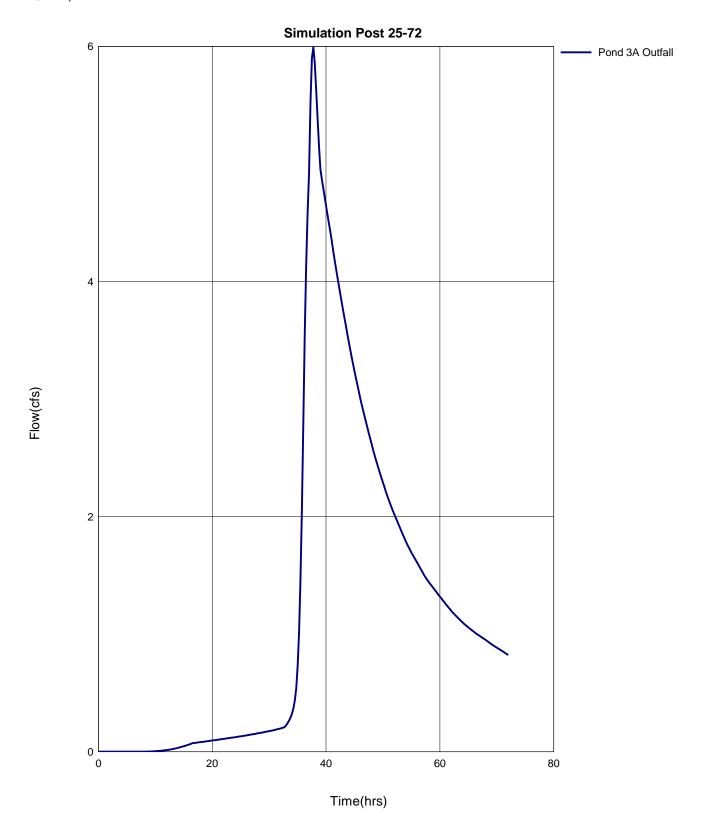
```
Bottom Clip(in): 0.000
Top Clip(in): 0.000
Weir Disc Coef: 3.200
Orifice Disc Coef: 0.600
              Count: 1
Type: Horizontal
Flow: Both
Geometry: Rectangular
                                              Invert(ft): 27.490
Control Elev(ft): 27.490
               Span(in): 37.00
              Rise(in): 24.00
______
         Name: Post 3A 25-72
    Filename: T:\00809.00\zTBG\drainage\ICPR\Post 3A - 25-72.R32
     Override Defaults: Yes
   Storm Duration(hrs): 72.00
Rainfall File: Flmod
    Rainfall Amount(in): 9.00
Time(hrs)
              Print Inc(min)
72.000
             15.00
        Name: Post 3A 5-1
    Filename: T:\00809.00\zTBG\drainage\ICPR\Post 3A - 5-1.R32
   Override Defaults: Yes
Storm Duration(hrs): 1.00
   Rainfall File: Flmod
Rainfall Amount(in): 2.98
Time(hrs)
               Print Inc(min)
10 000
              15.00
______
______
    Name: Post 25-72 Hydrology Sim: Post 3A 25-72 Filename: T:\00809.00\zTBG\drainage\ICPR\Pond 3A - 25-72.132
                    Restart: No
     Execute: Yes
                                                Patch: No
  Alternative: No
       Max Delta Z(ft): 1.00
                                               Delta Z Factor: 0.00500
   Time Step Optimizer: 10.000
Start Time(hrs): 0.000
Min Calc Time(sec): 0.5000
Boundary Stages:
                                          End Time(hrs): 72.00
Max Calc Time(sec): 60.0000
Boundary Flows:
Time(hrs)
             Print Inc(min)
               15.000
10.000
Group
BASE
               Yes
                                  Hydrology Sim: Post 3A 5-1
        Name: Post 5-1
    Filename: T:\00809.00\zTBG\drainage\ICPR\Pond 3A - 5-1.I32
     Execute: Yes
                         Restart: No
                                                Patch: No
   Max Delta Z(ft): 1.00
Time Step Optimizer: 10.000
Start Time(hrs): 0.000
Min_Calc Time(sec): 0.5000
                                                Delta Z Factor: 0.00500
                                          End Time(hrs): 1.00
Max Calc Time(sec): 60.0000
Boundary Flows:
       Boundary Stages:
              Print Inc(min)
Time(hrs)
                15.000
1.000
               15.000
Group
               Run
BASE
               Yes
```

Basin Name: Basin 3
Group Name: BASE
Simulation: Post 3A 25-72
Node Name: Pond 3A
Basin Type: SCS Unit Hydrograph
Unit Hydrograph: Uh323
Peaking Fator: 323.0
Spec Time Inc (min): 2.91
Comp Time Inc (min): 2.91
Rainfall File: Flmod
Rainfall Amount (in): 9.000
Storm Duration (hrs): 72.00
Status: Onsite
Time of Conc (min): 21.82
Time Shift (hrs): 0.00
Area (ac): 14.530
Vol of Unit Hyd (in): 1.001
Curve Number: 90.000
DCIA (%): 0.000

Time Max (hrs): 36.03
Flow Max (cfs): 29.37
Runoff Volume (in): 7.794
Runoff Volume (ft3): 411063

Name	Group	Simulation	Max Time Stage hrs	Max Stage ft	Warning M Stage ft	ax Delta Stage ft	Max Surf Area ft2	Max Time Inflow hrs	Max Inflow cfs	Max Time Outflow hrs	Max Outflow cfs
L-63N Canal	BASE	Post 25-72	40.00	17.95	28.83	0.0001	0	37.72	6.00	0.00	0.00
Pond 3A	BASE	Post. 25-72	37.72	27.58	28.65	0.0050	88091	36.00	29.22	37.72	6.00





RUNOFF CURVE NUMBER CALCULATIONS

PROJECT: SR 710 PREPARED: LCS DATE: 2/26/2014

LOCATION: OKEECHOBEE CO., FL CHECKED: GS DATE: 2/26/2014

Basin: BASIN 3B - POST DEVELOPMENT - R/W Only

Drainage Area: From Station 610+20 to Station 638+46.43

Basin Length = 2826.43 feet R/W Width = 160 feet

1. Runoff curve number

Cover description	Soil name	Hydrologic group	CN	Area (Acre)	CN x Area
Pavement - Proposed SR 710			98	6.26	614
Open Space - Good Condition (Perv R/W)		D	80	4.12	330
Water Management Area (Imperv.)			100	1.19	119
Water Management Area (Perv.)		D	80	1.26	101
			Totals =	12.83	1163

Note: Assumed Type D Soil as soil types were predominantly Types B/D & C/D

Note: Profile at Sta. 638+30 controlled by Kimley Horn (Bridge at SR 70)

TREATMENT VOLUME CALCULATIONS FOR PROPOSED CONDITION

PROJECT: SR 710 - Pond 3B PREPARED: LCS 2/26/2014

LOCATION: OKEECHOBEE COUNTY, FLORIDA CHECKED: GS 2/26/2014

Wet Detention Online Pond Treatment Calculations:

Proposed impervious area = 6.26 Ac

Total Drainage area = 12.83 Ac

2.5" times percent imperviousness = 1.30 Ac-Ft

1" runoff from drainage area = 1.07 Ac-Ft

Treatment Volume = Greater of 2.50" times percent imperviousness or 1.0" over drainage area

Required Treatment Volume (T.V.) = 1.30 Ac-Ft

= 56823 Cu-Ft

Pond Storage Calculations (Wet Detention - Pond 3B):

Elev. (NAVD)	h	Area	Area	Inc. Volume	Cum. Volume	Cum. Volume
(ft)	ft	sf	ac	Ac-ft	Ac-ft	Cu-ft
29.73	1.0	68,913	1.58	1.534	5.974	260,227
28.73	1.0	64,710	1.49	1.439	4.440	193,406
27.73	1.0	60,635	1.39	1.347	3.001	130,724
26.73	1.0	56,690	1.30	1.258	1.654	72,048
25.73	0.3	52,875	1.21	0.396	0.396	17,250
25.40	0.0	51,702	1.19	0.000	0.000	0

Overflow Weir Elevation (Top of storage volume) (Pond3B)

Elev.	Storage	Area
25.73	0.396	52,875
26.73	1.654	56,690

Elev. = 26.46 = 1.31 Ac-Ft 57253 Cu-Ft

Provided Treatment Volume (T.V.) =	1.314	Ac-ft	

Treatment Depth = 1.06 ft

For Orifice Recovery Calculations (Pond3B)

Size the orifice to discharge no more than 0.5 inch of the required detention volume in 24 hours.

1/2" of the required detention volume =

(0.5 in.* (Total DA - Water Area)/12in/ft)

1/2" runoff from drainage area =

0.48 Ac-Ft 2

21124 Cu-Ft

Elev.	Storage	Area
25.73	0.396	52,875
26.73	1.654	56,690

Elev. =

25.81 ft. provides

0.50 Ac-Ft

=

21634 Cu-Ft

From Geotechnical Information (10/13):

Boring PB-3B:

Est. Ground Elevation (at boring location) = 26.4 feet

Subtract Estimated SHGT Depth = -0.5-0.5 = 1 feet

Estimated SHGT Elev. = 25.4 feet

ORIFICE SIZING FOR PROPOSED CONDITION

PROJECT: SR 710 - Pond 3B PREPARED: LCS 2/26/2014

LOCATION: OKEECHOBEE COUNTY, FLORIDA CHECKED: GS 2/26/2014

Pond 3B Orifice Calculations

Size the orifice to discharge no more than 0.5 inch of the required detention volume in 24 hours.

Orifice Equation:

Average Discharge Rate: Drawdown 0.5 in of Required Detention Volume in 24 hrs.

Required Treatment Volume = 21124.48 ft³

Recovery Time (t) = 24.00 hr

Conversion Factor (CF) = 3600.00 sec/hr

$$Q = \frac{TV}{2 t CF}$$

Q = 0.122 cfs

Elevation of Required Treatment Volume = 25.81 ft

Flow line Elevation = 25.40 ft

Depth of water between top of treatment vol. and flow line (h1) = 0.41 ft

h = 0.41

Orifice Equation: $A = \frac{Q}{C\sqrt{2} a h}$

 $A = 0.040 ft^2$

 $D = \sqrt{\frac{4 A}{\pi}}$

D = 0.22 ft = 2.70 in dia

Use 3 inch orifice

Nodes
A Stage/Area
V Stage/Volume
T Time/Stage
M Manhole

Basins
O Overland Flow
U SCS Unit CN
S SBUH CN
Y SCS Unit GA
Z SBUH GA

Links
P Pipe
W Weir
C Channel
D Drop Structure
B Bridge
R Rating Curve
B Breach
E Percolation
F Filter
F Fitter
X Exfil Trench

T: Unnamed Ditch

```
..oue. rond 3B Status: Onsite
Type: SCS Unit Hydrograph CN
        Name: Basin 3
       Group: BASE
   Unit Hydrograph: Uh323
Rainfall File:
Rainfall Amount(in): 0.000
Area(ac): 12.830
Curve Number: 91.00
DCIA(%): 0.00
                                                Peaking Factor: 323.0
                                         Storm Duration(hrs): 0.00
Time of Conc(min): 24.39
Time Shift(hrs): 0.00
                                           Max Allowable Q(cfs): 999999.000
Tc from preliminary storm drain tabulations.
------
______
      Name: Pond 3B
                              Base Flow(cfs): 0.000
                                                               Init Stage(ft): 25.400
     Group: BASE
Type: Stage/Area
                                                              Warn Stage(ft): 28.650
     Stage(ft)
                    Area(ac)
                  1.1900
1.2100
        25.400
        25.730
26.730
27.730
28.730
                        1.3000
                       1.4900
1.5800
         29.730
    Name: Unnamed Ditch Base Flow(cfs): 0.000 Init Stage(ft): 21.810 Group: BASE Warn Stage(ft): 28.730
      Type: Time/Stage
From SR 70 Widening Calcs. - Converted to NAVD
                Stage(ft)
     Time(hrs)
       0.00
               21.810
          12.00
                        22.740
Length(ft): 850.00
        Name: Pond 3B Outfall From Node: Pond 3B
       Group: BASE
                                    To Node: Unnamed Ditch
              UPSTREAM
                             DOWNSTREAM
Circular
                                                        Friction Equation: Automatic
Solution Algorithm: Most Restrictive
    Geometry: Circular
     Span(in): 18.00
Rise(in): 18.00
                             18.00
                                                                      Flow: Both
                                                        Entrance Loss Coef: 0.500
                                                         Exit Loss Coef: 1.000
Outlet Ctrl Spec: Use dc or tw
Inlet Ctrl Spec: Use dc
   Invert(ft): 22.400
                             21.975
  Manning's N: 0.012000
                             0.012000
 Top Clip(in): 0.000
Bot Clip(in): 0.000
                             0.000
                                                             Solution Incs: 10
Upstream FHWA Inlet Edge Description:
Circular Concrete: Square edge w/ headwall
Downstream FHWA Inlet Edge Description:
Circular Concrete: Square edge w/ headwall
*** Weir 1 of 3 for Drop Structure Pond 3B Outfall ***
                                                                                 TABLE
                                              Bottom Clip(in): 0.000
Top Clip(in): 0.000
Weir Disc Coef: 3.200
                  Count: 1
                  Type: Horizontal
Flow: Both
              Flow: Both
Geometry: Circular
                                              Orifice Disc Coef: 0.600
               Span(in): 3 00
                                                     Invert(ft): 24 900
               Rise(in): 3.00
                                               Control Elev(ft): 25.400
*** Weir 2 of 3 for Drop Structure Pond 3B Outfall ***
                                                                                 TABLE
                                     Bottom Clip(in): 0.000
vis Top Clip(in): 0.000
Weir Disc Coef: 3.200
Orifice Disc Coef: 0.600
                  Count: 1
                   Type: Vertical: Mavis
Flow: Both
              Flow: Both
Geometry: Rectangular
               Span(in): 6.00
Rise(in): 18.00
                                               Invert(ft): 26.460
Control Elev(ft): 26.460
*** Weir 3 of 3 for Drop Structure Pond 3B Outfall ***
                                                                                 TABLE
                 Count: 1
                                                 Bottom Clip(in): 0.000
```

```
Type: Horizontal
Flow: Both
Geometry: Rectangular 0
                                             Top Clip(in): 0.000
Weir Disc Coef: 3.200
                                        Orifice Disc Coef: 0.600
              Span(in): 49.00
                                                Invert(ft): 27.960
                                           Control Elev(ft): 27.960
_______
Override Defaults: Yes
Storm Duration(hrs): 72.00
   Rainfall File: Flmod
Rainfall Amount(in): 9.00
            Print Inc(min)
72.000
            15.00
    Name: Post 3B 5-1 Filename: T:\00809.00\zTBG\drainage\ICPR\Post 3B - 5-1.R32
     Override Defaults: Yes
   Storm Duration(hrs): 1.00
Rainfall File: Flmod
   Rainfall Amount(in): 2.98
            Print Inc(min)
Time(hrs)
1.000
              15.00
______
_____
    Name: Post 25-72 Hydrology Sim: Post 3B 25-72 Filename: T:\00809.00\zTBG\drainage\ICPR\Pond 3B - 25-72.132
  Execute: Yes Alternative: No
       Max Delta Z(ft): 1.00
                                           Delta Z Factor: 0.00500
   Time Step Optimizer: 10.000
Start Time(hrs): 0.000
Min Calc Time(sec): 0.5000
                                      End Time(hrs): 72.00
Max Calc Time(sec): 60.0000
       Boundary Stages:
                                             Boundary Flows:
        ) Print Inc(min)
Time(hrs)
       15.000
15.000
72.000
Group
             Run
BASE
             Yes
    Name: Post 5-1 Hydrology Sim: Post 3B 5-1 Filename: T:\00809.00\zTBG\drainage\ICPR\Pond 3B - 5-1.I32
     Execute: Yes
                       Restart: No
                                            Patch: No
  Alternative: No
       Max Delta Z(ft): 1.00
                                          Delta Z Factor: 0.00500
   Time Step Optimizer: 10.000
Start Time(hrs): 0.000
Min Calc Time(sec): 0.5000
                                      End Time(hrs): 1.00
Max Calc Time(sec): 60.0000
Boundary Flows:
       Boundary Stages:
Time(hrs) Print Inc(min)
            15.000
15.000
0.500
1.000
Group
             Run
BASE
             Yes
```

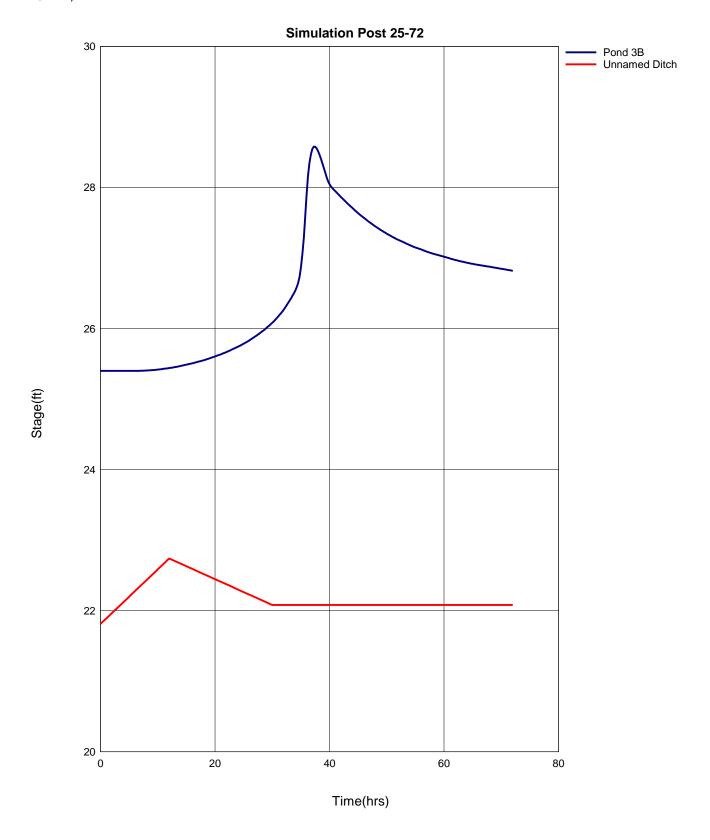
Basin Name: Basin 3
Group Name: BASE
Simulation: Post 3B 25-72
Node Name: Pond 3B
Basin Type: SCS Unit Hydrograph

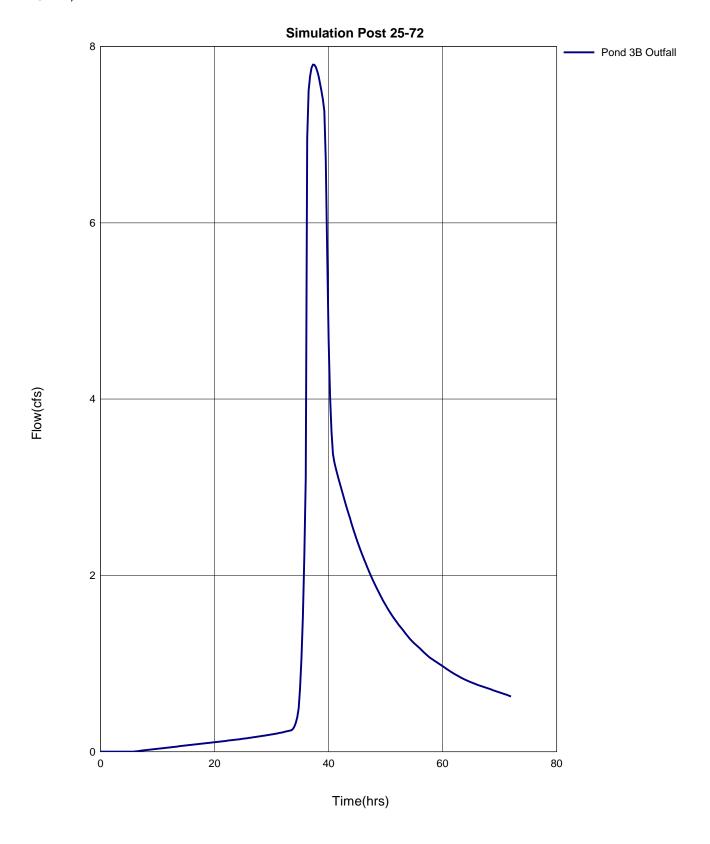
Unit Hydrograph: Uh323
Peaking Fator: 323.0
Spec Time Inc (min): 3.25
Comp Time Inc (min): 3.25
Rainfall File: Flmod
Rainfall Amount (in): 9.000
Storm Duration (hrs): 72.00
Status: Onsite
Time of Conc (min): 24.39
Time Shift (hrs): 0.00
Area (ac): 12.830
Vol of Unit Hyd (in): 1.001
Curve Number: 91.000
DCIA (%): 0.000

Time Max (hrs): 36.04
Flow Max (cfs): 25.58
Runoff Volume (in): 7.916
Runoff Volume (ft3): 368661

Pond 3B 25 Yr, 72 Hr

	Name	Group	Simulation	Max Time Stage hrs	Max Stage ft	Warning M Stage ft	ax Delta Stage ft	Max Surf Area ft2	Max Time Inflow hrs	Max Inflow cfs	Max Time Outflow hrs	Max Outflow cfs
	Pond 3B	BASE	Post 25-72	37.38	28.58	28.65	0.0050	64263	36.00	25.37	37.38	7.80
Unna	amed Ditch	BASE	Post 25-72	12.00	22.74	28.73	0.0013	0	37.38	7.80	0.00	0.00





RUNOFF CURVE NUMBER CALCULATIONS

PROJECT: SR 710 PREPARED: LCS DATE: 2/26/2014

LOCATION: OKEECHOBEE CO., FL CHECKED: GS DATE: 2/26/2014

Basin: BASIN 3C - POST DEVELOPMENT - R/W Only

Drainage Area: From Station 610+20 to Station 638+46.43

Basin Length = 2826.43 feet R/W Width = 160 feet

1. Runoff curve number

Cover description	Soil name	Hydrologic group	CN	Area (Acre)	CN x Area
Pavement - Proposed SR 710 & SR 70 to Exist Pond			98	10.44	1023
Open Space - Good Condition (Perv R/W)		D	80	7.47	598
Water Management Area (Imperv.)			100	2.13	213
Water Management Area (Perv.)		D	80	1.69	135
			Totals =	21.72	1968

CN (weighted) =	(total product)	=	1,968
	(total area)	_	21.72
		ı	
		=	l 91

Note: Assumed Type D Soil as soil types were predominantly Types B/D & C/D Note: Profile at Sta. 638+30 controlled by Kimley Horn (Bridge at SR 70) Merged with Proposed Pond 1 (SR 70 Widening Plans - Application #121210-2) Additional Drainage Area from Drainage Notebook Calcs for Pond 1

TREATMENT VOLUME CALCULATIONS FOR PROPOSED CONDITION

PROJECT: SR 710 - Pond 3C PREPARED: LCS 2/26/2014

LOCATION: OKEECHOBEE COUNTY, FLORIDA CHECKED: 2/26/2014

Wet Detention Online Pond Treatment Calculations:

Proposed impervious area = 10.44 Ac

Total Drainage area = 21.72 Ac

2.5" times percent imperviousness = 2.18 Ac-Ft

1" runoff from drainage area = 1.81 Ac-Ft

Treatment Volume = Greater of 2.50" times percent imperviousness or 1.0" over drainage area

Required Treatment Volume (T.V.) = 2.18 Ac-ft

= 94757 ft³

Pond Storage Calculations (Wet Detention - Pond 3C):

Elev. (NAVD)	h	Area	Area	Inc. Volume	Cum. Volume	Cum. Volume
(ft)	ft	sf	ac	Ac-ft	Ac-ft	Cu-ft
28.00	1.0	121,608	2.792	2.729	13.612	592,939
27.00	1.0	116,147	2.666	2.605	10.883	474,063
26.00	1.0	110,785	2.543	2.483	8.278	360,590
25.00	1.0	105,524	2.422	2.363	5.795	252,430
24.00	1.0	100,364	2.304	2.246	3.432	149,498
23.00	0.6	95,305	2.188	1.186	1.186	51,662
22.45	0.0	92,565	2.125	0.000	0.000	0

Overflow Weir Elevation (Top of storage volume) (Pond3C)

Elev.	Storage	Area
23.00	1.186	95,305
24.00	3.432	100,364

Elev. = 23.45 = 2.20 Ac-Ft 95688 Cu-Ft

Provided Treatment Volume (T.V.) = 2.197 Ac-ft

Treatment Depth = 1.00 ft

For Orifice Recovery Calculations (Pond3C)

Size the orifice to discharge no more than 0.5 inch of the required detention volume in 24 hours.

1/2" of the required detention volume = (0.5 in.* (Total DA - Water Area)/12in/ft)

1/2" runoff from drainage area = 0.82 Ac-Ft 35574 Cu-Ft

Elev.	Storage	Area
22.45	0.000	92,565
23.00	1.186	95,305

Elev. = 22.83 ft. provides 0.82 Ac-Ft 35694 Cu-Ft

From Geotechnical Information (10/13):

Boring PB-3C:

Est. Ground Elevation (at boring location) = 24.2 feet
Subtract Estimated SHGT Depth = -1.25- 0.5 = 1.75 feet
Estimated SHGT Elev. = 22.45 feet

ORIFICE SIZING FOR PROPOSED CONDITION

PROJECT: SR 710 - Pond 3C PREPARED: LCS 2/26/2014

LOCATION: OKEECHOBEE COUNTY, FLORIDA CHECKED: GS 2/26/2014

Pond 3C Orifice Calculations

Size the orifice to discharge no more than 0.5 inch of the required detention volume in 24 hours.

Orifice Equation:

Average Discharge Rate: Drawdown 0.5 in of Required Detention Volume in 24 hrs.

Required Treatment Volume = 35573.54 ft³

Recovery Time (t) = 24.00 hr Conversion Factor (CF) = 3600.00 sec/hr

$$Q = \frac{TV}{2 t CF}$$

Q = 0.206 cfs

Elevation of Required Treatment Volume = 22.83 ft

Flow line Elevation = 22.45 ft

Depth of water between top of treatment vol. and flow line (h1) = 0.38 ft

h = 0.38

Orifice Equation: $A = \frac{Q}{C\sqrt{2ah}}$

 $A = 0.069 ft^2$

 $D = \sqrt{\frac{4 A}{\pi}}$

D = 0.30 ft = 3.57 in dia

Use 3 inch orifice

Nodes
A Stage/Area
V Stage/Volume
T Time/Stage
M Manhole

Basins
O Overland Flow
U SCS Unit CN
S SBUH CN
Y SCS Unit GA
Z SBUH GA

Links
P Pipe
W Weir
C Channel
D Drop Structure
B Bridge
R Rating Curve
B Breach
E Percolation
F Filter
F Fitter
T Exfil Trench

T: UnnamedCanal

```
...... Fond 3C Status: Onsite Type: SCS Unit Hydrograph CN
        Group: BASE
    Unit Hydrograph: Uh323
Rainfall File:
Rainfall Amount(in): 0.000
Area(ac): 21.720
Curve Number: 91.00
DCIA(%): 0.00
                                                  Peaking Factor: 323.0
                                           Storm Duration(hrs): 0.00
Time of Conc(min): 24.39
Time Shift(hrs): 0.00
                                              Max Allowable Q(cfs): 999999.000
Tc from preliminary storm drain tabulation
______
______
      Name: Pond 3C
                                Base Flow(cfs): 0.000
                                                                  Init Stage(ft): 22.450
     Group: BASE
Type: Stage/Area
                                                                  Warn Stage(ft): 28.000
      Stage(ft)
                       Area(ac)
         22.450
                          2.1250
         23.000
         24.000
                          2.3040
         25.000
                         2.5430
         26.000
         27 000
         28.000
                         2.7920
                                                                  Init Stage(ft): 21.810
      Name: UnnamedCanal Base Flow(cfs): 0.000
     Group: BASE
                                                                  Warn Stage(ft): 28.730
      Type: Time/Stage
From SR 70 Widening Calcs.- Converted to NAVD
      Time(hrs)
                      Stage(ft)
           0.00 21.810
          30.00
                          22.080
______
---- Drop Structures ------
         Name: Pond 3C Outfall
                                   From Node: Pond 3C
To Node: UnnamedCanal
                                                                   Length(ft): 85.00
        Group: BASE
                                                                         Count: 1
               UPSTREAM
                               DOWNSTREAM
                                                            Friction Equation: Automatic
                                                           Solution Algorithm: Most Restrictive
Flow: Both
Entrance Loss Coef: 0.500
     Geometry: Circular
Span(in): 18.00
                               Circular
18.00
     Rise(in): 18.00
                               18.00
 Invert(ft): 21.500
Manning's N: 0.012000
Top Clip(in): 0.000
Bot Clip(in): 0.000
                               21.330
0.012000
0.000
                                                             Exit Loss Coef: 0.500

Outlet Ctrl Spec: Use dc or tw
Inlet Ctrl Spec: Use dc
Solution Incs: 10
Upstream FHWA Inlet Edge Description:
Circular Concrete: Square edge w/ headwall
Downstream FHWA Inlet Edge Description:
Circular Concrete: Square edge w/ headwall
*** Weir 1 of 3 for Drop Structure Pond 3C Outfall ***
                                                                                     TABLE
                                               Bottom Clip(in): 0.000
Top Clip(in): 0.000
Weir Disc Coef: 3.200
Orifice Disc Coef: 0.600
               Type: Horizontal
Flow: Both
Geometry: Circular
               Span(in): 3.00
Rise(in): 3.00
                                                 Invert(ft): 21.950
Control Elev(ft): 22.450
*** Weir 2 of 3 for Drop Structure Pond 3C Outfall ***
                                      Bottom Clip(in): 0.000
avis Top Clip(in): 0.000
Weir Disc Coef: 3.200
Orifice Disc Coef: 0.600
                                                                                     TABLE
               Type: Vertical: Mavis
Flow: Both
Geometry: Rectangular
                                                Invert(ft): 23.450
Control Elev(ft): 23.450
               Rise(in): 30.60
*** Weir 3 of 3 for Drop Structure Pond 3C Outfall ***
                                                                                      TARLE
```

Pond 3C 25 Year, 72 Hour

Invert(ft): 26.000 Control Elev(ft): 26.000 Span(in): 49.00 Rise(in): 37.00

Filename: T:\00809.00\zTBG\drainage\ICPR\Post 3C - 25-72.R32

Override Defaults: Yes Storm Duration(hrs): 72.00 Rainfall File: Flmod Rainfall Amount(in): 9.00

Time(hrs) Print Inc(min) 72.000 15.00

Alternative: No

Max Delta Z(ft): 1.00 Time Step Optimizer: 10.000
Start Time(hrs): 0.000
Min_Calc Time(sec): 0.5000

Boundary Stages:

Delta Z Factor: 0.00500 End Time(hrs): 72.00
Max Calc Time(sec): 60.0000
Boundary Flows:

Time(hrs) Print Inc(min) 10.000 15.000 15.000 72.000 Run Group

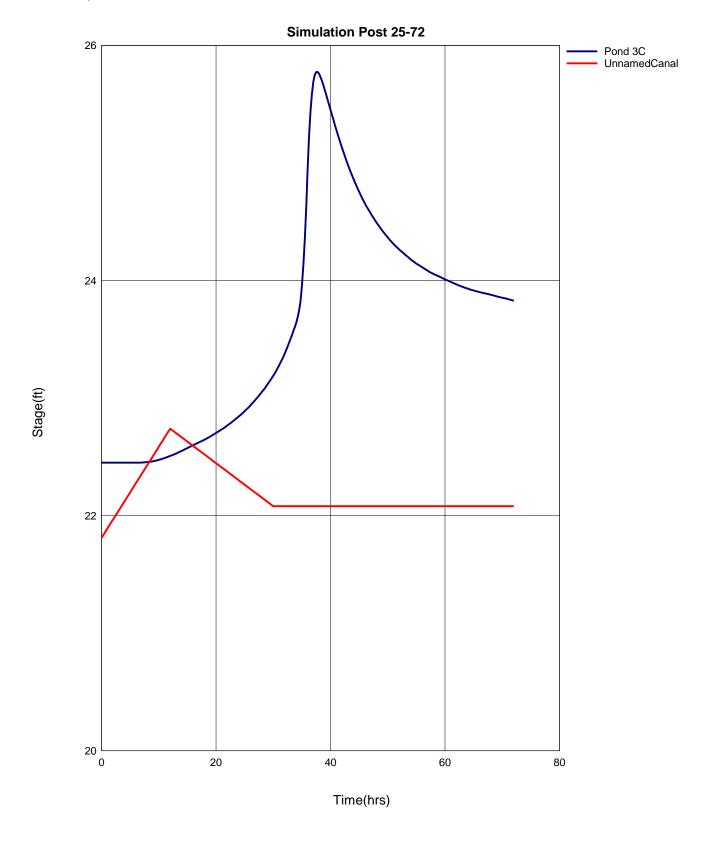
Yes

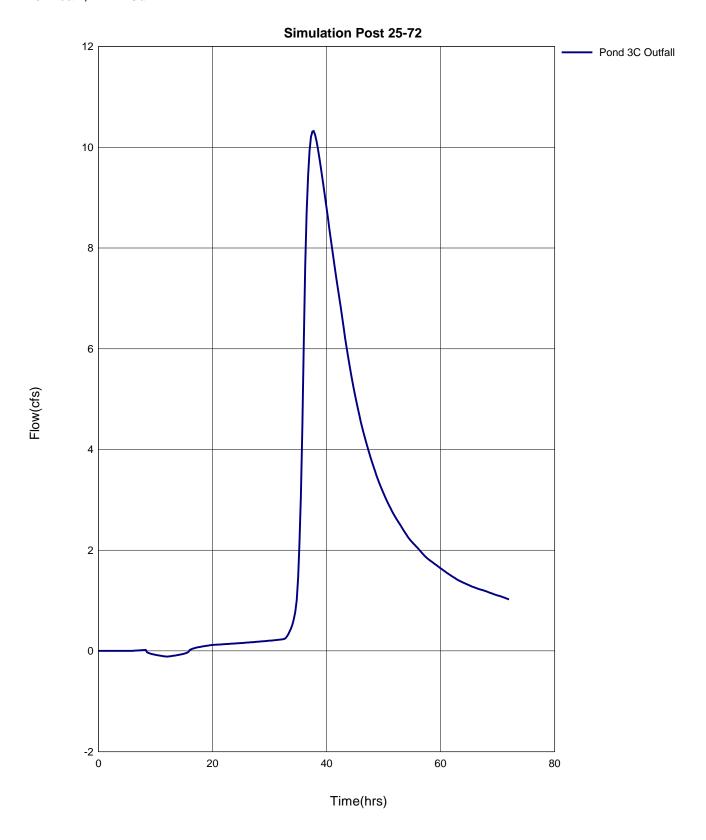
BASE

Basin Name: Basin 3
Group Name: BASE
Simulation: Post 3C 25-72
Node Name: Pond 3C
Basin Type: SCS Unit Hydrograph
Unit Hydrograph: Uh323
Peaking Fator: 323.0
Spec Time Inc (min): 3.25
Comp Time Inc (min): 3.25
Rainfall File: Flmod
Rainfall Amount (in): 9.000
Storm Duration (hrs): 72.00
Status: Onsite
Time of Conc (min): 24.39
Time Shift (hrs): 0.00
Area (ac): 21.720
Vol of Unit Hyd (in): 1.001
Curve Number: 91.000
DCIA (%): 0.000

Time Max (hrs): 36.04
Flow Max (cfs): 43.30
Runoff Volume (in): 7.916
Runoff Volume (ff3): 624109

Name	Group	Simulation	Max Time Stage hrs	Max Stage ft	Warning M Stage ft	ax Delta Stage ft	Max Surf Area ft2	Max Time Inflow hrs	Max Inflow cfs	Max Time Outflow hrs	Max Outflow cfs
Pond 3C	BASE	Post 25-72	37.65	25.78	28.00	0.0050	109600	36.00	42.96	37.65	10.33
UnnamedCanal	BASE	Post 25-72	12.00	22.74	28.73	0.0013	0	37.65	10.33	0.00	0.00





Basin 4

RUNOFF CURVE NUMBER CALCULATIONS

PROJECT: SR 710 PREPARED: LCS DATE: 2/26/2014

LOCATION: OKEECHOBEE CO., FL CHECKED: GS DATE: 2/26/2014

Basin: BASIN 4A- Option 1 - POST DEVELOPMENT - R/W Only

Drainage Area: From Station 638+36.94 to Station 685+00

Basin Length = 4663.06 feet R/W Width = 160 feet

1. Runoff curve number

Cover description	Soil name	Hydrolo gic group	CN	Area (Acre)	CN x Area
Pavement - Proposed SR 710 & Other Roads			98	15.37	1507
Open Space - Good Condition (Perv R/W)		D	80	11.69	935
Water Management Area (Imperv.)			100	2.22	222
Water Management Area (Perv.)		D	80	1.76	141
			Totals =	31.05	2805

Note: Assumed Type D Soil as soil types were predominantly Types B/D & C/D

TREATMENT VOLUME CALCULATIONS FOR PROPOSED CONDITION

PROJECT: SR 710 - Pond 4A - Option 1 PREPARED: LCS 2/26/2014

LOCATION: OKEECHOBEE COUNTY, FLORIDA CHECKED: GS 2/26/2014

Wet Detention Online Pond Treatment Calculations:

Proposed impervious area = 10.06 Ac

Total Drainage area = 31.05 Ac

2.5" runoff from impervious area = 2.10 Ac-Ft

1" runoff from drainage area = 2.59 Ac-Ft

*Proposed Impervious Area takes credit for existing pavement (5.309 ac.)

Treatment Volume = Greater of 2.50" times percent imperviousness or 1.0" over drainage area

Required Treatment Volume (T.V.) = 2.59 Ac-ft

 $= 112706 \text{ ft}^3$

Pond Storage Calculations (Wet Detention - Pond 4A):

Elev. (NAVD)	h	Area	Area	Inc. Volume	Cum. Volume	Cum. Volume
(ft)	ft	sf	ac	Ac-ft	Ac-ft	Cu-ft
29.00	1.0	124,030	2.847	2.783	12.657	551,339
28.00	1.0	118,401	2.718	2.655	9.874	430,111
27.00	1.0	112,874	2.591	2.529	7.219	314,460
26.00	1.0	107,448	2.467	2.406	4.690	204,296
25.00	1.0	102,122	2.344	2.284	2.284	99,491
24.00	0.0	96,897	2.224	0.000	0.000	0

Overflow Weir Elevation (Top of storage volume) (Pond4A)

Elev.	Storage	Area		
25.00	2.284	102,122		
26.00	4.690	107,448		

Elev. = 25.13 = 2.60 Ac-Ft 113116 Cu-Ft

Provided Treatment Volume (T.V.) = **2.597** Ac-ft

Treatment Depth = 1.13 ft

For Orifice Recovery Calculations (Pond4A)

Size the orifice to discharge no more than 0.5 inch of the required detention volume in 24 hours.

1/2" of the required detention volume = (0.5 in.* (Total DA - Water Area)/12in/ft)

1/2" runoff from drainage area = 1.20 Ac-Ft 52316 Cu-Ft

Elev.	Storage	Area
24.00	0.000	96,897
25.00	2.284	102,122

Elev. = 24.22 ft. provides 0.502 ac-ft of volume 21888 cu ft of volume

From Geotechnical Information (10/13):

Boring PB-4A: Station 680+40

Est. Ground Elevation (at boring location) = 25 feet

Estimated SHGT Depth = -1.08-0.5 = 1.58 feet
Estimated SHGT Elev. = 23.42 feet

Boring PB-4A: Station 683+15

Est. Ground Elevation (at boring location) = 26 feet

Estimated SHGT Depth = -1.08-0.5 = 1.58 feet

Estimated SHGT Elev. = 24.42 feet

RUNOFF CURVE NUMBER CALCULATIONS

PROJECT: SR 710 PREPARED: LCS DATE: 2/26/2014

LOCATION: OKEECHOBEE CO., FL CHECKED: GS DATE: 2/26/2014

Basin: BASIN 4A - Option 2 - POST DEVELOPMENT - R/W Only

Drainage Area: From Station 638+36.94 to Station 685+00

Basin Length = 4663.06 feet R/W Width = 160 feet

1. Runoff curve number

Cover description	Soil name	Hydrolo gic group	CN	Area (Acre)	CN x Area
Pavement - Proposed SR 710 & Other Roads			98	15.37	1507
Open Space - Good Condition (Perv R/W)		D	80	11.69	935
Water Management Area (Imperv.)			100	1.59	159
Water Management Area (Perv.)		D	80	1.75	140
			Totals =	30.41	2741

Note: Assumed Type D Soil as soil types were predominantly Types B/D & C/D

TREATMENT VOLUME CALCULATIONS FOR PROPOSED CONDITION

PROJECT: SR 710 - Pond 4A - Option 2 PREPARED: LCS 2/26/2014

LOCATION: OKEECHOBEE COUNTY, FLORIDA CHECKED: GS 2/26/2014

Wet Detention Online Pond Treatment Calculations:

Proposed impervious area = 10.06 Ac

Total Drainage area = 30.41 Ac

2.5" runoff from impervious area = 2.10 Ac-Ft

1" runoff from drainage area = 2.53 Ac-Ft

*Proposed Impervious Area takes credit for existing pavement (5.309 ac.)

Treatment Volume = Greater of 2.50" times percent imperviousness or 1.0" over drainage area

Required Treatment Volume (T.V.) = 2.53 Ac-ft

 $= 110376 \text{ ft}^3$

Pond Storage Calculations (Wet Detention - Pond 4A):

Elev. (NAVD)	h	Area	Area	Inc. Volume	Cum. Volume	Cum. Volume
(ft)	ft	sf	ac	Ac-ft	Ac-ft	Cu-ft
29.00	1.0	94,045	2.159	2.100	9.356	407,547
28.00	1.0	88,914	2.041	1.983	7.256	316,071
27.00	1.0	83,884	1.926	1.869	5.273	229,692
26.00	1.0	78,954	1.813	1.757	3.404	148,278
25.00	1.0	74,125	1.702	1.647	1.647	71,743
24.00	0.0	69,396	1.593	0.000	0.000	0

Overflow Weir Elevation (Top of storage volume) (Pond4A)

Elev.	Storage	Area
25.00	1.647	74,125
26.00	3.404	78,954

Elev. = 25.51 = 2.54 Ac-Ft 110776 Cu-Ft

Provided Treatment Volume (T.V.) = 2.543 Ac-ft

Treatment Depth = 1.51 ft

For Orifice Recovery Calculations (Pond4A)

Size the orifice to discharge no more than 0.5 inch of the required detention volume in 24 hours.

1/2" of the required detention volume = (0.5 in.* (Total DA - Water Area)/12in/ft)

1/2" runoff from drainage area = 1.20 Ac-Ft 52296 Cu-Ft

Elev.	Storage	Area
24.00	0.000	69,396
25.00	1.647	74,125

Elev. = 24.73 ft. provides 1.202 ac-ft of volume 52373 cu ft of volume

From Geotechnical Information (10/13):

Boring PB-4A: Station 680+40

Est. Ground Elevation (at boring location) = 25 feet

Estimated SHGT Depth = -1.08-0.5 = 1.58 feet
Estimated SHGT Elev. = 22.92 feet

Boring PB-4A: Station 683+15

Est. Ground Elevation (at boring location) = 26 feet

Estimated SHGT Depth = -1.08-0.5 = 1.58 feet

Estimated SHGT Elev. = 24.42 feet

Nodes
A Stage/Area
V Stage/Volume
T Time/Stage
M Manhole

Basins
O Overland Flow
U SCS Unit CN
S SBUH CN
Y SCS Unit GA
Z SBUH GA

Links
P Pipe
W Weir
C Channel
D Drop Structure
B Bridge
R Rating Curve
B Breach
E Percolation
F Filter
X Exfil Trench

T: L-63N

```
Noue. Fond 4A Status: Onsite
Type: SCS Unit Hydrograph CN
        Name: Basin 4
       Group: BASE
   Status: Onsite
                                           Max Allowable Q(cfs): 999999.000
               DCIA(%): 0.00
--- Nodes -----
                                                               Init Stage(ft): 17.830
Warn Stage(ft): 28.830
     Name: L-63N
                               Base Flow(cfs): 0.000
    Group: BASE
Type: Time/Stage
From SR 70 Widening Plans - Converted to NAVD
     Time(hrs)
                     Stage(ft)
                17.830
17.930
17.950
17.930
         14.00
          40.00
        100.00
                                                        Init Stage(ft): 17.830
Warn Stage(ft): 28.830
     Name: L-63N-2 Base Flow(cfs): 0.000
    Group: BASE
Type: Time/Stage
From SR 70 Widening Plans - Converted to NAVD
                 Stage(ft)
     Time(hrs)
         0.00 17.830
14.00 17.930
40.00 17.950
100.00 17.930
    Name: Pond 4A Base Flow(cfs): 0.000 Init Stage(ft): 24.000 Group: BASE Warn Stage(ft): 28.060 Type: Stage/Area
     Stage(ft)
                    Area(ac)

        Stage(ft)
        Area(ac)

        24.000
        2.2240

        25.000
        2.3440

        26.000
        2.4670

        27.000
        2.5910

        28.000
        2.7180

        29.000
        2.8470

     Name: Pond 4A-2 Base Flow(cfs): 0.000 Init Stage(ft): 24.000
Group: BASE Warn Stage(ft): 29.060
    Group: BASE
     Type: Stage/Area
     Stage(ft)
                       Area(ac)
               - -----
                1.5930
1.7020
1.8130
1.9260
2.0410
2.1590
        25.000
26.000
27.000
         28.000
```

```
Name: Pond 4A Outfall From Node: Pond 4A
                                                                                  Length(ft): 150.00
          Group: BASE
                                               To Node: L-63N
                                                                                          Count: 1
                   UPSTREAM
                                      DOWNSTREAM
                                                                           Friction Equation: Automatic
      Geometry: Circular
Span(in): 18.00
                                       Circular
                                                                          Solution Algorithm: Most Restrictive
                                                                         Flow: Both
Entrance Loss Coef: 0.500
Exit Loss Coef: 1.000
Outlet Ctrl Spec: Use dc or tw
                                      18.00
    Rise(in): 18.00
Invert(ft): 20.500
                                      18.00
 Manning's N: 0.012000
Top Clip(in): 0.000
Bot Clip(in): 0.000
                                      0.012000
                                      0.000
                                                                                Solution Incs: 10
Upstream FHWA Inlet Edge Description:
Circular Concrete: Square edge w/ headwall
Downstream FHWA Inlet Edge Description:
Circular Concrete: Square edge w/ headwall
*** Weir 1 of 3 for Drop Structure Pond 4A Outfall ***
                                                                                                          TABLE
                                                            Bottom Clip(in): 0.000
Top Clip(in): 0.000
Weir Disc Coef: 3.200
Orifice Disc Coef: 0.600
                       Count: 1
                        Type: Horizontal
Flow: Both
                   Geometry: Circular
                   Span(in): 5.00
                                                                    Invert(ft): 23.500
                   Rise(in): 5.00
                                                            Control Elev(ft): 24.000
*** Weir 2 of 3 for Drop Structure Pond 4A Outfall ***
                                                                                                          TABLE
                   Count: 2 Bottom Clip(in): 0.000
Type: Vertical: Mavis Top Clip(in): 0.000
Flow: Both Weir Disc Coef: 3.200
Geometry: Rectangular Orifice Disc Coef: 0.600
                   Span(in): 15.00
                                                                      Invert(ft): 25.130
                   Rise(in): 10.00
                                                            Control Elev(ft): 25.130
*** Weir 3 of 3 for Drop Structure Pond 4A Outfall ***
                                                                                                          TABLE
                   Count: 1
Type: Horizontal
Flow: Both
Geometry: Rectangular

Top Clip.
Weir Disc Coef: 3.200
Orifice Disc Coef: 0.600

Invert(ft): 27.90
                                                           Bottom Clip(in): 0.000
Top Clip(in): 0.000
Weir Disc Coef: 3.200
                                                            Invert(ft): 27.900
Control Elev(ft): 27.900
           Name: Pond 4A-2 Outfa From Node: Pond 4A-2 Length(ft): 150.00
                                              To Node: L-63N-2
          Group: BASE
                                                                                          Count: 1
                                                                         Friction Equation: Automatic
Solution Algorithm: Most Restrictive
                   UPSTREAM
                                      DOWNSTREAM
Circular
      Geometry: Circular
      Span(in): 18.00
Rise(in): 18.00
                                                                         Flow: Both
Entrance Loss Coef: 0.500
                                      18.00
                                                                          Exit Loss Coef: 1.000
Outlet Ctrl Spec: Use dc or tw
Inlet Ctrl Spec: Use dc
    Invert(ft): 20.500
                                      20.200
  Manning's N: 0.012000
                                      0.012000
 Top Clip(in): 0.000
 Bot Clip(in): 0.000
                                      0.000
                                                                                Solution Incs: 10
Upstream FHWA Inlet Edge Description:
Circular Concrete: Square edge w/ headwall
Downstream FHWA Inlet Edge Description:
Circular Concrete: Square edge w/ headwall
*** Weir 1 of 3 for Drop Structure Pond 4A-2 Outfa ***
                                                                                                          TABLE
                                                            Bottom Clip(in): 0.000
Top Clip(in): 0.000
Weir Disc Coef: 3.200
                       Count: 1
                        Type: Horizontal
Flow: Both
                   Geometry: Circular
                                                            Orifice Disc Coef: 0.600
                   Span(in): 5 00
                                                                      Invert(ft): 23 500
                   Rise(in): 5.00
                                                              Control Elev(ft): 24.000
*** Weir 2 of 3 for Drop Structure Pond 4A-2 Outfa ***
                                                                                                          TABLE
                                                           Bottom Clip(in): 0.000
Top Clip(in): 0.000
Weir Disc Coef: 3.200
Orifice Disc Coef: 0.600
                       Count: 2
                        Type: Vertical: Mavis
Flow: Both
                   Geometry: Rectangular
                   Span(in): 15.00
Rise(in): 8.00
                                                                      Invert(ft): 25.510
                                                              Control Elev(ft): 25.510
*** Weir 3 of 3 for Drop Structure Pond 4A-2 Outfa ***
                                                                                                          TABLE
                       Count: 1
                                                               Bottom Clip(in): 0.000
```

Pond 4A - Options 1 and 2 25 Yr, 72 Hr

Type: Horizontal Flow: Both Geometry: Rectangular Ori Top Clip(in): 0.000 Weir Disc Coef: 3.200 Orifice Disc Coef: 0.600

Span(in): 49.00 Invert(ft): 29.000 Control Elev(ft): 29.000

Name: Post 4A 25-72 Filename: T:\00809.00\zTBG\drainage\ICPR\Post 4A - 25-72.R32

Override Defaults: Yes Storm Duration(hrs): 72.00 Rainfall File: Flmod Rainfall Amount(in): 9.00

Time(hrs) Print Inc(min) 72.000 15.00

---- Routing Simulations -------

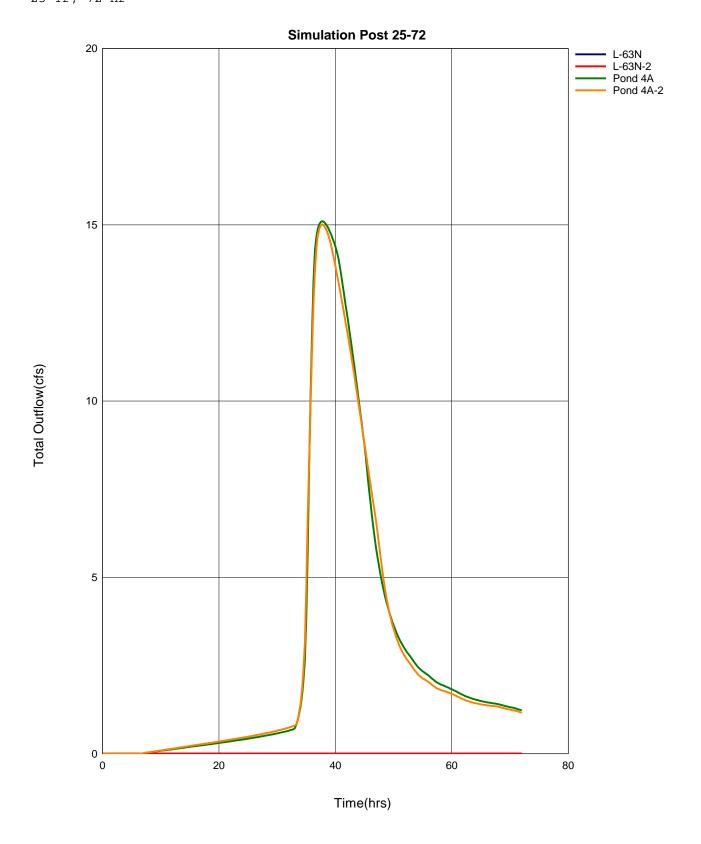
Hydrology Sim: Post 4A 25-72 Name: Post 25-72 Filename: T:\00809.00\zTBG\drainage\ICPR\Pond 4A - 25-72.I32

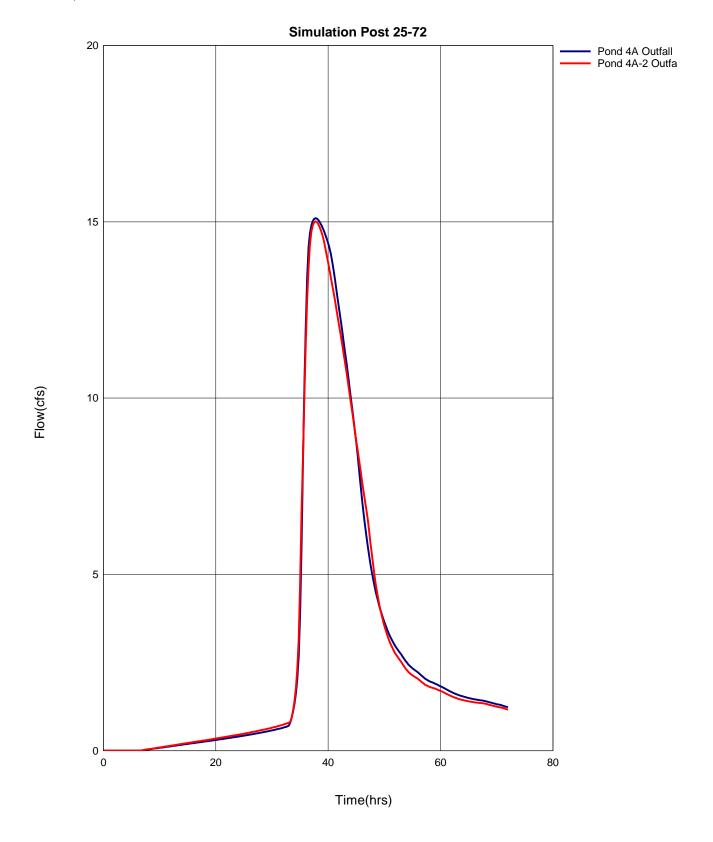
Execute: Yes Alternative: No Restart: No Patch: No

Max Delta Z(ft): 1.00 Time Step Optimizer: 10.000 Start Time(hrs): 0.000 Min Calc Time(sec): 0.5000 Delta Z Factor: 0.00500 End Time(hrs): 72.00 Max Calc Time(sec): 72.0000 Boundary Flows: Boundary Stages:

nrs) Print Inc(min) 15.000 15.000 10.000 72.000 BASE Yes

Name	Group	Simulation	Max Time Stage hrs	Max Stage ft	Warning M Stage ft	Max Delta Stage ft	Max Surf Area ft2	Max Time Inflow hrs	Max Inflow cfs	Max Time Outflow hrs	Max Outflow cfs
L-63N	BASE	Post 25-72	40.00	17.95	28.83	0.0001	0	37.77	15.11	0.00	0.00
L-63N-2	BASE	Post 25-72	40.00	17.95	28.83	0.0001	0	37.76	15.01	0.00	0.00
Pond 4A	BASE	Post 25-72	37.77	27.89	28.06	0.0040	117764	36.00	58.07	37.77	15.11
Pond 4A-2	BASE	Post 25-72	37.76	28.92	29.06	0.0050	93650	36.00	56.88	37.76	15.01





PROJECT: SR 710 PREPARED: LCS DATE: 2/26/2014

LOCATION: OKEECHOBEE CO., FL CHECKED: GS DATE: 2/26/2014

Basin: BASIN 4B/4C - Option 1 - POST DEVELOPMENT - R/W Only

Drainage Area: From Station 638+36.94 to Station 685+00

Basin Length = 4663.06 feet (measured from roll plot)

R/W Width = 160 feet

1. Runoff curve number

Cover description	Soil name	Hydrologic group	CN	Area (Acre)	CN x Area
Pavement - Proposed SR 710 & Other Roads			98	15.37	1507
Open Space - Good Condition (Perv R/W)		D	80	11.69	935
Water Management Area (Imperv.)			100	3.21	321
Water Management Area (Perv.)		D	80	4.96	397
			Totals =	35.23	3159

PROJECT: SR 710 - Pond 4B/4C - Option 1 PREPARED: LCS 2/26/2014

LOCATION: OKEECHOBEE COUNTY, FLORIDA CHECKED: GS 2/26/2014

Wet Detention Online Pond Treatment Calculations:

Proposed impervious area = 10.06 Ac

Total Drainage area = 35.23 Ac

2.5" runoff from impervious area = 2.10 Ac-Ft

1" runoff from drainage area = 2.94 Ac-Ft

*Proposed Impervious Area takes credit for existing pavement (5.309 ac.)

Treatment Volume = Greater of 2.50" times percent imperviousness or 1.0" over drainage area

Required Treatment Volume (T.V.) = 2.94 Ac-ft

= 127891 ft^3

Pond Storage Calculations (Wet Detention - Pond 4B-4C):

Elev. (NAVD)	h	Area	Area	Inc. Volume	Cum. Volume	Cum. Volume
(ft)	ft	sf	ac	Ac-ft	Ac-ft	Ac-ft
27.38	0.6	199,404	4.578	2.831	19.938	868,499
26.75	1.0	192,111	4.410	4.273	17.107	745,181
25.75	1.0	180,117	4.135	4.000	12.834	559,049
24.75	1.0	168,323	3.864	3.731	8.834	384,809
23.75	1.0	156,730	3.598	3.467	5.103	222,287
22.75	0.5	145,340	3.337	1.636	1.636	71,264
22.25	0.0	139,719	3.208	0.000	0.000	0

Overflow Weir Elevation (Top of storage volume) (Pond4B-4C)

Elev.	Storage	Area
22.75	1.636	145,340
23.75	5.103	156,730

Elev. = 23.13 = 2.95 Ac-Ft 128653 Cu-Ft

Provided Treatment Volume (T.V.) =	2.953	Ac-ft

Treatment Depth = 0.88 ft

For Orifice Recovery Calculations (Pond4B-4C)

Size the orifice to discharge no more than 0.5 inch of the required detention volume in 24 hours.

1/2" of the required detention volume = (0.5 in.* (Total DA - Water Area)/12in/ft)

1/2" runoff from drainage area = 1.33 Ac-Ft 58124 Cu-Ft

Elev.	Storage	Area
22.25	0.000	139,719
22.75	1.636	145,340

Elev. = 22.66 ft. provides 1.342 ac-ft of volume 58437 cu ft of volume

From Geotechnical Information (10/13):

Boring PB-4BC:

Est. Ground Elevation (at boring location) = 24 feet

Estimated SHGT Depth = -1.25-0.5 = 1.75 feet

Estimated SHGT Elev. = 22.25 feet

PROJECT: SR 710 PREPARED: LCS DATE: 2/26/2014

LOCATION: OKEECHOBEE CO., FL CHECKED: GS DATE: 2/26/2014

Basin: BASIN 4B - Option 2 - POST DEVELOPMENT - R/W Only

Drainage Area: From Station 638+36.94 to Station 685+00

Basin Length = 4663.06 feet R/W Width = 160 feet

1. Runoff curve number

Cover description	Soil name	Hydrologic group	CN	Area (Acre)	CN x Area
Pavement - Proposed SR 710 & Other Roads			98	15.37	1507
Open Space - Good Condition (Perv R/W)		D	80	11.69	935
Water Management Area (Imperv.)			100	2.06	206
Water Management Area (Perv.)		D	80	2.53	202
			Totals =	31.65	2850

CN (weighted) = (total product) = 2,850 (total area) 31.65

PROJECT: SR 710 - Pond 4B - Option 2 PREPARED: LCS 2/26/2014

LOCATION: OKEECHOBEE COUNTY, FLORIDA CHECKED: GS 2/26/2014

Wet Detention Online Pond Treatment Calculations:

Proposed impervious area = 10.06 Ac

Total Drainage area = 31.65 Ac

2.5" times percent imperviousness = 2.10 Ac-Ft

1" runoff from drainage area = 2.64 Ac-Ft

*Proposed Impervious Area takes credit for existing pavement (5.309 ac.)

Treatment Volume = Greater of 2.50" times percent imperviousness or 1.0" over drainage area

Required Treatment Volume (T.V.) = 2.64 Ac-ft

 $= 114906 \text{ ft}^3$

Pond Storage Calculations (Wet Detention - Pond 4B):

Elev. (NAVD)	h	Area	Area	Inc. Volume	Cum. Volume	Cum. Volume
(ft)	ft	sf	ac	Ac-ft	Ac-ft	Cu-ft
27.38	0.6	122,537	2.813	1.743	12.490	544,064
26.75	1.0	118,552	2.722	2.646	10.747	468,139
25.75	1.0	111,992	2.571	2.497	8.101	352,880
24.75	1.0	105,532	2.423	2.350	5.604	244,110
23.75	1.0	99,172	2.277	2.205	3.254	141,744
22.75	0.5	92,914	2.133	1.049	1.049	45,694
22.25	0.0	89,822	2.062	0.000	0.000	0

Overflow Weir Elevation (Top of storage volume) (Pond4B)

Elev.	Storage	Area
22.75	1.049	92,914
23.75	3.254	99,172

Elev. = 23.50 = 2.70 Ac-Ft 117732 Cu-Ft

Provided Treatment Volume (T.V.) = **2.703** Ac-ft

To a face of Death

Treatment Depth = 1.25 ft

(prefer 1' treatment depth)

For Orifice Recovery Calculations (Pond4B)

Size the orifice to discharge no more than 0.5 inch of the required detention volume in 24 hours.

1/2" of the required detention volume = (0.5 in.* (Total DA - Water Area)/12in/ft)

1/2" runoff from drainage area = 1.23 Ac-Ft 53711 Cu-Ft

Elev.	Storage	Area
22.75	1.049	92,914
23.75	3.254	99,172

Elev. = 22.84 ft. provides 1.247 ac-ft of volume 54339 cu ft of volume

From Geotechnical Information (10/13):

Boring PB-4BC:

Est. Ground Elevation (at boring location) = 24 feet Subtract Estimated SHGT Depth = -1.25-0.5 = 1.75 feet

Estimated SHGT Elev. = 22.25 feet

Nodes
A Stage/Area
V Stage/Volume
T Time/Stage
M Manhole

Basins
O Overland Flow
U SCS Unit CN
S SBUH CN
Y SCS Unit GA
Z SBUH GA

Links
P Pipe
W Weir
C Channel
D Drop Structure
B Bridge
R Rating Curve
B Breach
E Percolation
F Filter
F Fitter
X Exfil Trench

T: Unnamed Canal

```
______
______
       Name: Basin 4
                               Node: Pond 4B-4C
                                                       Status: Onsite
      Group: BASE
                              Type: SCS Unit Hydrograph CN
   Unit Hydrograph: Uh323 Peaking Factor 323.0 Rainfall File: Storm Duration(hrs): 0.00 Time of Conc(min): 15.00 Area(ac): 35.230 Time Shift(hrs): 0.00 Curve Number: 90.00 Max Allowable Q(cfs): 999999.000
   DCIA(%): 0.00
______
_______
                                                   Init Stage(ft): 22.250
     Name: Pond 4B
                        Base Flow(cfs): 0.000
    Group: BASE
Type: Stage/Area
                                                  Warn Stage(ft): 28.060
    Stage(ft)
                Area(ac)
       22.250
              2.0620
               2.0620
2.1330
2.2770
2.4230
2.5710
2.7220
2.8130
       22.750
23.750
       24.750
25.750
26.750
       27.380
   Name: Pond 4B-4C Base Flow(cfs): 0.000 Init Stage(ft): 22.250 Group: BASE Warn Stage(ft): 28.060 Type: Stage/Area
    Stage(ft)
                  Area(ac)
      22.250
                    3.2080
       22.750
22.750
23.750
24.750
                    3.5980
       25.750
26.750
                    4.4100
                   4.5780
    Name: Unnamed - 2 Base Flow(cfs): 0.000 Init Stage(ft): 21.810
Group: BASE Warn Stage(ft): 30.000
   Group: BASE
Type: Time/Stage
Outfall Ditch converted to NAVD
    Time(hrs)
                 Stage(ft)
       0.00 21.810
12.00 22.740
30.00 22.080
    Name: Unnamed Canal Base Flow(cfs): 0.000 Init Stage(ft): 21.810
Group: BASE Warn Stage(ft): 30.000
    Group: BASE
Type: Time/Stage
Outfall Ditch converted to NAVD
    Time(hrs) Stage(ft)
     0.00 21.810
12.00 22.740
                   22.080
       30.00
______
```

```
Name: Pond 4B Outf
                                             From Node: Pond 4B
                                                                                        Length(ft): 135.00
                                                To Node: Unnamed - 2
          Group: BASE
                                                                                                  Count: 1
                                   DOWNSTREAM
Circular
18.00
                    UPSTREAM
                                                                                 Friction Equation: Automatic
      Geometry: Circular
Span(in): 18.00
                                                                             Solution Algorithm: Most Restrictive
Flow: Both
                                                                             Entrance Loss Coef: 0.500
      Rise(in): 18.00
                                         18.00
                                         18.480
0.012000
                                                                                Exit Loss Coef: 0.500
Outlet Ctrl Spec: Use dc or tw
Inlet Ctrl Spec: Use dc
Solution Incs: 10
  Invert(ft): 18.750
Manning's N: 0.012000
 Top Clip(in): 0.000
Bot Clip(in): 0.000
Upstream FHWA Inlet Edge Description:
Circular Concrete: Square edge w/ headwall
Downstream FHWA Inlet Edge Description:
Circular Concrete: Square edge w/ headwall
*** Weir 1 of 3 for Drop Structure Pond 4B Outf ***
                                                                                                                   TARLE
                                                                Bottom Clip(in): 0.000
Top Clip(in): 0.000
Weir Disc Coef: 3.200
Orifice Disc Coef: 0.600
                         Count: 1
                    Count: 1
Type: Horizontal
Flow: Both
Geometry: Circular
                                                                       Invert(ft): 21.750
                     Span(in): 4.00
                                                              Control Elev(ft): 22.250
                     Rise(in): 4.00
*** Weir 2 of 3 for Drop Structure Pond 4B Outf ***
                                                                                                                   TABLE
                    Count: 1 Bottom Clip(in): 0.000
Type: Vertical: Mavis Top Clip(in): 0.000
Flow: Both Weir Disc Coef: 3.200
Geometry: Rectangular Orifice Disc Coef: 0.600
                     Span(in): 15.00
                                                                            Invert(ft): 23.500
                                                              Control Elev(ft): 23.500
                     Rise(in): 10.00
*** Weir 3 of 3 for Drop Structure Pond 4B Outf ***
                    Count: 1 Bottom Clip(in): 0.000
Type: Horizontal Top Clip(in): 0.000
Flow: Both Weir Disc Coef: 3.200
Geometry: Rectangular Orifice Disc Coef: 0.600

Span(in): 37.00 Invert(ft): 29.000
Rise(in): 24.00 Control Flow/f/
                                                                                                                   TABLE
                                                To Node: Unnamed Canal
            Name: Pond 4B-4C Outf From Node: Pond 4B-4C
          Group: BASE
                                  DOWNSTREAM
Circular
18.00
18.00
18.480
0.012000
0.000
                                                                              Friction Equation: Automatic
Solution Algorithm: Most Restrictive
                    UPSTREAM
       Geometry: Circular
 Span(in): 18.00
Rise(in): 18.00
Invert(ft): 18.750
Manning's N: 0.012000
Top Clip(in): 0.000
Rot Clip(in): 0.000
                                                                               Flow: Both
Entrance Loss Coef: 0.500
Exit Loss Coef: 1.000
Outlet Ctrl Spec: Use dc or tw
Inlet Ctrl Spec: Use dc
 Bot Clip(in): 0.000
                                                                                      Solution Incs: 10
Upstream FHWA Inlet Edge Description:
Circular Concrete: Square edge w/ headwall
Downstream FHWA Inlet Edge Description:
Circular Concrete: Square edge w/ headwall
*** Weir 1 of 3 for Drop Structure Pond 4B-4C Outf ***
                                                                                                                   TABLE
                    Count: 1 Bottom Clip(in): 0.000
Type: Horizontal Top Clip(in): 0.000
Flow: Both Weir Disc Coef: 3.200
Geometry: Circular Orifice Disc Coef: 0.600
                     Span(in): 4.00
                                                                            Invert(ft): 21.750
                     Rise(in): 4.00
                                                                 Control Elev(ft): 22.250
*** Weir 2 of 3 for Drop Structure Pond 4B-4C Outf ***
                                                                                                                   TABLE
                                                             Bottom Clip(in): 0.000
Top Clip(in): 0.000
Weir Disc Coef: 3.200
                         Count: 1
                          Type: Vertical: Mavis
Flow: Both
                    Flow: Both Weir Disc Coef: 3.200
Geometry: Rectangular Orifice Disc Coef: 0.600
                     Span(in): 4.00
                                                                            Invert(ft): 23.130
                     Rise(in): 6.00
                                                                  Control Elev(ft): 23.130
*** Weir 3 of 3 for Drop Structure Pond 4B-4C Outf ***
```

TABLE

Count: 1
Type: Horizontal
Flow: Both Bottom Clip(in): 0.000 Top Clip(in): 0.000 Weir Disc Coef: 3.200 Orifice Disc Coef: 0.600 Flow: Both Geometry: Rectangular

Span(in): 37.00 Rise(in): 24.00 Invert(ft): 23.630
Control Elev(ft): 23.630

---- Hydrology Simulations

Name: Post 4B4C 25-72 Filename: T:\00809.00\zTBG\drainage\ICPR\Post 4B4C - 25-72.R32

Override Defaults: Yes Storm Duration(hrs): 72.00 Rainfall File: Flmod Rainfall Amount(in): 9.00

Time(hrs) Print Inc(min) 15.00

______ --- Routing Simulations -----

Restart: No Patch: No

Execute: Yes Alternative: No

Max Delta Z(ft): 1.00 Time Step Optimizer: 10.000 Start Time(hrs): 0.000 Min Calc Time(sec): 0.5000 Delta Z Factor: 0.00500 End Time(hrs): 72.00 Max Calc Time(sec): 60.0000 Boundary Flows: Boundary Stages:

Print Inc(min) Time(hrs) 15.000 15.000 72.000 Group Run

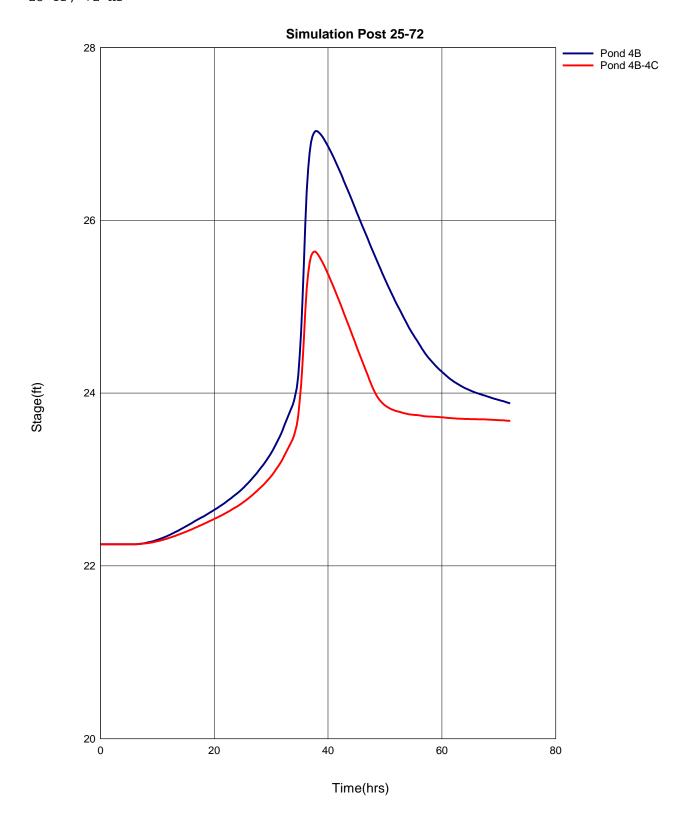
Yes

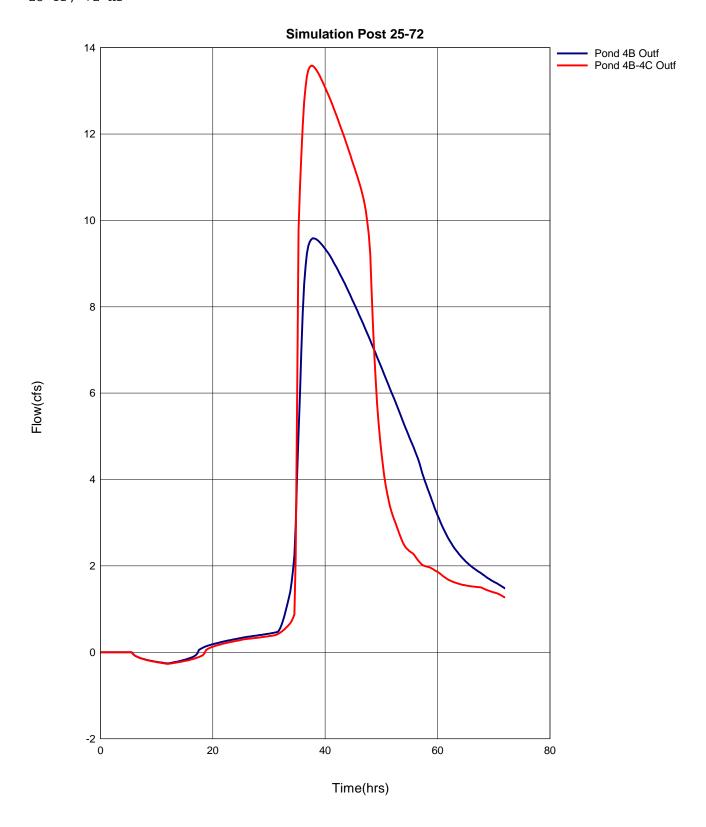
BASE

```
| Ratin Name: Basin 4 | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South Pales | South
```

Pond 4B/4C - Option 1 Pond 4B - Option 2 25 Yr, 72 Hr

Name	Group	Simulation	Max Time Stage hrs	Max Stage ft	Warning M Stage ft	Max Delta Stage ft	Max Surf Area ft2	Max Time Inflow hrs	Max Inflow cfs	Max Time Outflow hrs	Max Outflow cfs
Pond 4B	BASE	Post 25-72	37.89	27.04	28.06	0.0050	120367	36.00	67.26	37.89	9.59
Pond 4B-4C	BASE	Post 25-72	37.64	25.64	28.06	0.0041	178822	36.00	74.87	37.64	13.59
Unnamed - 2	BASE	Post 25-72	12.00	22.74	30.00	0.0013	0	37.89	9.59	0.00	0.00
Unnamed Canal	BASE	Post 25-72	12 00	22.74	30 00	0 0013	0	37 64	13 59	0 00	0.00





PROJECT: SR 710 PREPARED: LCS DATE: 2/26/2014

LOCATION: OKEECHOBEE CO., FL CHECKED: GS DATE: 2/26/2014

Basin: BASIN 4D - Option 1 - POST DEVELOPMENT - R/W Only

Drainage Area: From Station 638+36.94 to Station 685+00

Basin Length = 4663.06 feet (measured from roll plot)

R/W Width = 160 feet

1. Runoff curve number

Cover description	Soil name	Hydrologic group	CN	Area (Acre)	CN x Area
Pavement - Proposed SR 710 & Other Roads			98	15.37	1507
Open Space - Good Condition (Perv R/W)		D	80	11.69	935
Water Management Area (Imperv.)			100	3.02	302
Water Management Area (Perv.)		D	80	3.05	244
			Totals =	33.14	2988

SR 710 - Pond 4D - Option 1 PROJECT: PREPARED: LCS 2/26/2014

LOCATION: CHECKED: GS 2/26/2014 OKEECHOBEE COUNTY, FLORIDA

Wet Detention Online Pond Treatment Calculations:

Proposed impervious area = 10.06 Ac

Total Drainage area = 33.14 Ac

2.5" runoff from impervious area = 2.10 Ac-Ft

1" runoff from drainage area = 2.76 Ac-Ft

Proposed Impervious Area takes credit for existing pavement (5.309 ac.)

Treatment Volume = Greater of 2.50" over Impervious Area or 1.0" over drainage area

Required Treatment Volume (T.V.) = 2.76 Ac-ft

ft³ 120295

Pond Storage Calculations (Wet Detention - Pond 4D):

Elev. (NAVD)	h	Area	Area	Inc. Volume	Cum. Volume	Cum. Volume
(ft)	ft	sf	ac	Ac-ft	Ac-ft	Cu-ft
29.00	1.0	181,309	4.162	4.046	18.476	804,815
28.00	1.0	171,196	3.930	3.815	14.430	628,571
27.00	1.0	161,183	3.700	3.586	10.615	462,389
26.00	1.0	151,270	3.473	3.360	7.029	306,183
25.00	1.17	141,460	3.247	3.669	3.669	159,822
23.83	0.0	131,749	3.025	0.000	0.000	0.000

Overflow Weir Elevation (Top of storage volume) (Pond4D)

Elev.	Storage	Area
23.83	0.000	131,749
25.00	3.669	141,460

Elev. = 24.70 2.73 Ac-Ft 118842 Cu-Ft

Provided Treatment Volume (T.V.) =	2.728	Ac-ft	

Treatment Depth =

0.87 ft

For Orifice Recovery Calculations (Pond4D)

Size the orifice to discharge no more than 0.5 inch of the required detention volume in 24 hours.

1/2" of the required detention volume = (0.5 in.* (Total DA - Water Area)/12in/ft)

1/2" runoff from drainage area = 1.25 Ac-Ft 54658 Cu-Ft

Elev.	Storage	Area		
23.83	0.000	131,749		
26.00	7.029	151,270		

Elev. = 24.22 ft. provides 1.26 Ac-Ft 55028 Cu-Ft

From Geotechnical Information (10/13):

Boring PB-4D:

Est. Ground Elevation (at boring location) = 25.5 feet Subtract Estimated SHGT Depth = -1.17- 0.5 = 1.67 feet Estimated SHGT Elev. = 23.83 feet

PROJECT: SR 710 PREPARED: LCS DATE: 2/26/2014

LOCATION: OKEECHOBEE CO., FL CHECKED: GS DATE: 2/26/2014

Basin: BASIN 4D - Option 2 - POST DEVELOPMENT - R/W Only

Drainage Area: From Station 638+36.94 to Station 685+00

Basin Length = 4663.06 feet R/W Width = 160 feet

1. Runoff curve number

Cover description	Soil name	Hydrologic group	CN	Area (Acre)	CN x Area
Pavement - Proposed SR 710 & Other Roads			98	15.37	1507
Open Space - Good Condition (Perv R/W)		D	80	11.69	935
Water Management Area (Imperv.)			100	1.95	195
Water Management Area (Perv.)		D	80	2.37	190
			Totals =	31.39	2827

PROJECT: SR 710 - Pond 4D - Option 2 PREPARED: LCS 2/26/2014

LOCATION: OKEECHOBEE COUNTY, FLORIDA CHECKED: GS 2/26/2014

Wet Detention Online Pond Treatment Calculations:

Proposed impervious area = 10.06 Ac

Total Drainage area = 31.39 Ac

2.5" runoff from impervious area = 2.10 Ac-Ft

1" runoff from drainage area = 2.62 Ac-Ft

*Proposed Impervious Area takes credit for existing pavement (5.309 ac.)

Treatment Volume = Greater of 2.50" over Impervious Area or 1.0" over drainage area

Required Treatment Volume (T.V.) = 2.62 Ac-ft

= 113953 ft^3

Pond Storage Calculations (Wet Detention - Pond 4D):

Elev. (NAVD)	h	Area	Area	Inc. Volume	Cum. Volume	Cum. Volume
(ft)	ft	sf	ac	Ac-ft	Ac-ft	Cu-ft
29.00	1.0	123,687	2.839	2.751	12.367	538,706.520
28.00	1.0	116,021	2.663	2.577	9.616	418,872.960
27.00	1.0	108,455	2.490	2.404	7.039	306,618.840
26.00	1.0	100,990	2.318	2.234	4.635	201,900.600
25.00	1.17	93,626	2.149	2.401	2.401	104,587.560
23.83	0.0	85,137	1.954	0.000	0.000	0.000

Overflow Weir Elevation (Top of storage volume) (Pond4D)

Elev.	Storage	Area
23.83	0.000	85,137
25.00	2.401	93,626

Elev. = 25.20 = 2.81 Ac-Ft 122466 Cu-Ft

Provided Treatment Volume (T.V.) =	2.811	Ac-ft

Treatment Depth = 1.37 ft

For Orifice Recovery Calculations (Pond4D)

Size the orifice to discharge no more than 0.5 inch of the required detention volume in

1/2" of the required detention volume = (0.5 in.* (Total DA - Water Area)/12in/ft)

1/2" runoff from drainage area = 1.07 Ac-Ft 46637 Cu-Ft

Elev.	Storage	Area		
23.83	0.000	85,137		
26.00	4.635	100,990		

Elev. = 24.34 ft. provides 1.089 ac ft of volume 47451.29309 cu ft of volume

From Geotechnical Information (10/13):

Boring PB-4D:

Est. Ground Elevation (at boring location) = 25.5 feet Subtract Estimated SHGT Depth = -1.17-0.5 = 1.67 feet

Estimated SHGT Elev. = 23.83 feet

Nodes
A Stage/Area
V Stage/Volume
T Time/Stage
M Manhole

Basins
O Overland Flow
U SCS Unit CN
S SBUH CN
Y SCS Unit GA
Z SBUH GA

Links
P Pipe
W Weir
C Channel
D Drop Structure
B Bridge
R Rating Curve
B Breach
E Percolation
F Filter
F Fitter
X Exfil Trench

T: L-63N

```
Node: Pond 4D-Opt 1 Status: Onsite
Type: SCS Unit Hydrograph CN
            Name: Basin 4-Opt 1
          Group: BASE
    Name: Basin 4-Opt 2 Node: Pond 4D-Opt 2 Sta Group: BASE Type: SCS Unit Hydrograph CN

Unit Hydrograph: Uh323 Peaking Factor: 323.0 Rainfall File: Storm Duration(hrs): 0.00 Time of Conc(min): 27.40 Area(ac): 31.390 Time Shift(hrs): 0.00 Curve Number: 91.00 Max Allowable Q(cfs): 999999 DCIA(%): 0.00
                                                                                                  Status: Onsite
                                                              Max Allowable Q(cfs): 999999.000
--- Nodes -----
                                                                                         Init Stage(ft): 17.830
Warn Stage(ft): 28.830
        Name: L-63N-2
                                            Base Flow(cfs): 0.000
      Group: BASE
Type: Time/Stage
       Time(hrs)
                              Stage(ft)
            0.00 17.830
14.00 17.930
40.00 17.950
100.00 17.930
           100.00

        Name:
        L-63N-3
        Base Flow(cfs):
        0.000
        Init Stage(ft):
        17.830

        Group:
        BASE
        Warn Stage(ft):
        28.830

      Group: BASE
Type: Time/Stage
       Time(hrs)
                              Stage(ft)
             0.00 17.830
14.00 17.930
40.00 17.950
100.00 17.930
      Name: Pond 4D-Opt 1 Base Flow(cfs): 0.000 Init Stage(ft): 23.830 Group: BASE Warn Stage(ft): 28.060 Type: Stage/Area
       Stage(ft)
                            Area(ac)

        Stage(ft)
        Area(ac)

        23.830
        3.0250

        25.000
        3.2470

        26.000
        3.4730

        27.000
        3.7000

        28.000
        3.9300

        29.000
        4.1620

       Name: Pond 4D-Opt 2 Base Flow(cfs): 0.000 Init Stage(ft): 23.830
Group: BASE Warn Stage(ft): 28.060
      Group: BASE
        Type: Stage/Area
       Stage(ft)
                                Area(ac)
                     - -----
           23.830 1.9540
25.000 2.1490
26.000 2.3180
27.000 2.4900
28.000 2.6630
29.000 2.8390
```

```
Length(ft): 860.00
           Name: Pond 4D-Opt 2 O From Node: Pond 4D-Opt 2
                                               To Node: L-63N-2
          Group: BASE
                                                                                           Count: 1
                   UPSTREAM
                                       DOWNSTREAM
                                                                            Friction Equation: Automatic
      Geometry: Circular
Span(in): 24.00
                                        Circular
                                                                          Solution Algorithm: Most Restrictive
                                       24.00
                                                                                           Flow: Both
                                                                          Entrance Loss Coef: 0.500
Exit Loss Coef: 1.000
Outlet Ctrl Spec: Use dc or tw
Inlet Ctrl Spec: Use dc
    Rise(in): 24.00
Invert(ft): 20.330
                                      24.00
19.040
 Manning's N: 0.012000
Top Clip(in): 0.000
Bot Clip(in): 0.000
                                       0.012000
                                      0.000
                                                                                 Solution Incs: 10
Upstream FHWA Inlet Edge Description:
Circular Concrete: Square edge w/ headwall
Downstream FHWA Inlet Edge Description:
Circular Concrete: Square edge w/ headwall
*** Weir 1 of 3 for Drop Structure Pond 4D-Opt 2 O ***
                                                                                                           TABLE
                                                            Bottom Clip(in): 0.000
Top Clip(in): 0.000
Weir Disc Coef: 3.200
Orifice Disc Coef: 0.600
                       Count: 1
                         Type: Horizontal
Flow: Both
                   Geometry: Circular
                   Span(in): 4.00
                                                                     Invert(ft): 23.330
                   Rise(in): 4.00
                                                             Control Elev(ft): 23.830
*** Weir 2 of 3 for Drop Structure Pond 4D-Opt 2 O ***
                                                                                                           TABLE
                   Count: 2 Bottom Clip(in): 0.000
Type: Vertical: Mavis Top Clip(in): 0.000
Flow: Both Weir Disc Coef: 3.200
Geometry: Rectangular Orifice Disc Coef: 0.600
                   Span(in): 24.00
                                                                      Invert(ft): 25.200
                   Rise(in): 6.00
                                                            Control Elev(ft): 25.200
*** Weir 3 of 3 for Drop Structure Pond 4D-Opt 2 O ***
                                                                                                           TABLE
                   Count: 1
Type: Horizontal
Flow: Both
Geometry: Rectangular

Top Circ.
Weir Disc Coef: 3.200
Orifice Disc Coef: 0.600
Invert(ft): 29.00
Control Elev(ft): 29.00
                                                 Bottom Clip(in): 0.000
Top Clip(in): 0.000
Weir Disc Coef: 3.200
                                                            Invert(ft): 29.000
Control Elev(ft): 29.000
           Name: Pond 4D-Opt1 Ou From Node: Pond 4D-Opt 1 Length(ft): 860.00
                                               To Node: L-63N-3
          Group: BASE
                                                                                          Count: 1
                                                                          Friction Equation: Automatic
Solution Algorithm: Most Restrictive
                   UPSTREAM
                                      DOWNSTREAM
Circular
      Geometry: Circular
      Span(in): 24.00
Rise(in): 24.00
                                                                          Flow: Both
Entrance Loss Coef: 0.500
                                      24.00
                                                                           Exit Loss Coef: 1.000
Outlet Ctrl Spec: Use dc or tw
Inlet Ctrl Spec: Use dc
    Invert(ft): 20.330
                                       19.040
  Manning's N: 0.012000
                                       0.012000
 Top Clip(in): 0.000
 Bot Clip(in): 0.000
                                      0.000
                                                                                 Solution Incs: 10
Upstream FHWA Inlet Edge Description:
Circular Concrete: Square edge w/ headwall
Downstream FHWA Inlet Edge Description:
Circular Concrete: Square edge w/ headwall
*** Weir 1 of 3 for Drop Structure Pond 4D-Opt1 Ou ***
                                                                                                           TABLE
                                                            Bottom Clip(in): 0.000
Top Clip(in): 0.000
Weir Disc Coef: 3.200
                       Count: 1
                        Type: Horizontal
Flow: Both
                   Geometry: Circular
                                                             Orifice Disc Coef: 0.600
                   Span(in): 4 00
                                                                      Invert(ft): 23 330
                   Rise(in): 4.00
                                                              Control Elev(ft): 23.830
*** Weir 2 of 3 for Drop Structure Pond 4D-Opt1 Ou ***
                                                                                                           TABLE
                                                        Bottom Clip(in): 0.000
Top Clip(in): 0.000
Weir Disc Coef: 3.200
Orifice Disc Coef: 0.600
                       Count: 2
                         Type: Vertical: Mavis
Flow: Both
                   Geometry: Rectangular
                   Span(in): 24.00
Rise(in): 6.00
                                                                      Invert(ft): 24.700
                                                              Control Elev(ft): 24.700
*** Weir 3 of 3 for Drop Structure Pond 4D-Opt1 Ou ***
                                                                                                           TABLE
                       Count: 1
                                                                Bottom Clip(in): 0.000
```

```
Type: Horizontal
Flow: Both
Geometry: Rectangular Or
                                         Top Clip(in): 0.000
Weir Disc Coef: 3.200
                                      Orifice Disc Coef: 0.600
            Span(in): 79.00
                                            Invert(ft): 28.000
            Rise(in): 36.00
                                      Control Elev(ft): 28.000
_______
______
                            From Node:
To Node:
                                                    Flow: Both
Run WSPRO: No
      Group: BASE
                                            STAT(ft) SKEW(deg)
0.00 0.000
0.00 0.000
0.00 0.000
0.00 0.000
    XSEC TYPE
                                       STAT(ft)
0.00
0.00
0.00
0.00
                                INV(ft)
                                                                     0.500
0.500
0.500
                                                                         EXPAN
                                                                                     CONTRAC
                     NAME
                                  0.000
         Exit
                                                                                       0.000
   Full Valley
                                  0.000
                                                                                       0.000
                                  0.000
     Approach
      Roadway
                                  0.000
   Road Surface Material: Paved
Road Embankment Top Width(ft): 0.00
Road Unsubmerged Weir Q Coef: 0.000
RATING CURVE CONTROL
       TW(ft)
                QMin(cfs) QMax
                              QMax(cfs)
                                           OInc(cfs)
                                 0.000
_______
Name: Post 4D 25-72
Filename: T:\00809.00\zTBG\drainage\ICPR\Post 4D - 25-72.R32
   Override Defaults: Yes
Storm Duration(hrs): 72.00
        Rainfall File: Flmod
   Rainfall Amount(in): 9.00
Time(hrs)
            Print Inc(min)
       Name: Post 4D 5-1
   Filename: T:\00809.00\zTBG\drainage\ICPR\Post 4D - 5-1.R32
    Override Defaults: Yes
   Storm Duration(hrs): 1.00
Rainfall File: Flmod
   Rainfall Amount(in): 2.98
           Print Inc(min)
Time(hrs)
1.000
           15.00
______
---- Routing Simulations -------
   Name: Post 25-72 Hydrology Sim: Post 4D 25-72 Filename: T:\00809.00\zTBG\drainage\ICPR\Pond 4D - 25-72.132
     Execute: Yes
                     Restart: No
                                        Patch: No
 Alternative: No
      Max Delta Z(ft): 1.00
                                      Delta Z Factor: 0.00500
   Time Step Optimizer: 10.000
Start Time(hrs): 0.000
Min Calc Time(sec): 0.5000
                                         End Time(hrs): 72.00
                                   Max Calc Time(sec): 60.0000
Boundary Flows:
      Boundary Stages:
Time(hrs) Print Inc(min)
10.000
         15.000
15.000
Group
            Run
BASE
            Yes
                            Hydrology Sim: Post 4D 5-1
   Filename: T:\00809.00\zTBG\drainage\ICPR\Pond 4D - 5-1.132
    Execute: No
                    Restart: No
                                        Patch: No
 Alternative: No
```

Max Delta Z(ft): 1.00 Time Step Optimizer: 10.000 Start Time(hrs): 0.000 Min Calc Time(sec): 0.5000 Boundary Stages:

Delta Z Factor: 0.00500

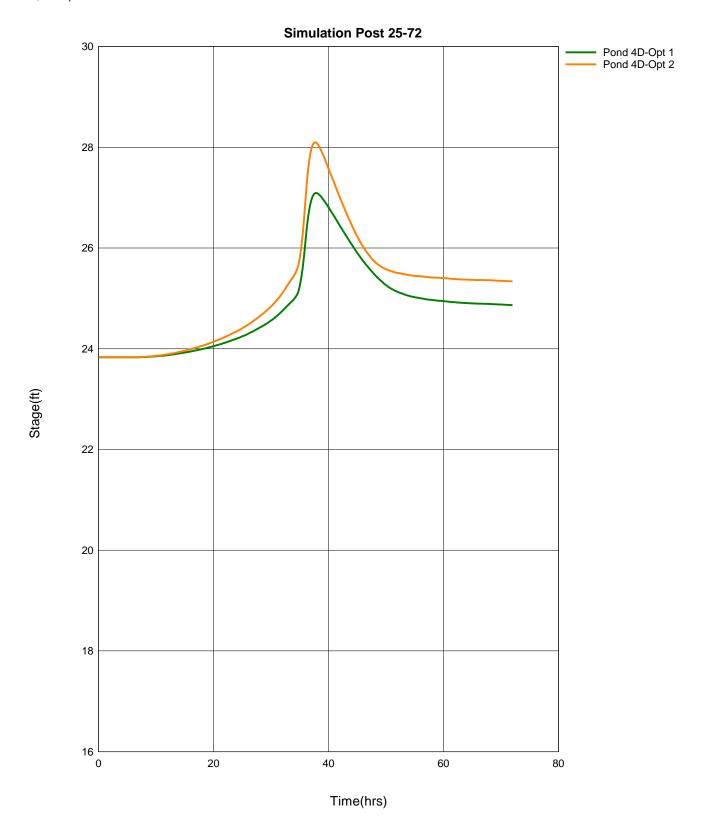
End Time(hrs): 3.00

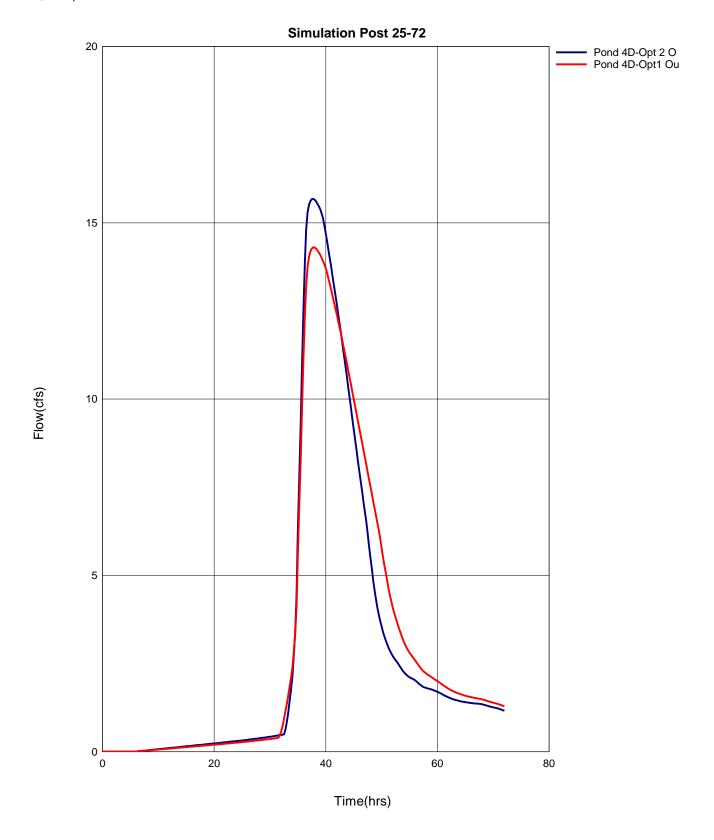
Max Calc Time(sec): 60.0000

Boundary Flows:

Time(hrs)	Print Inc(min)
0.500	5.000
3.000	5.000
Group	Run
BASE	Yes

	Name	Group	Simulation	Max Time Stage hrs	Max Stage ft	Warning M Stage ft	Max Delta Stage ft	Max Surf Area ft2	Max Time Inflow hrs	Max Inflow cfs	Max Time Outflow hrs	Max Outflow cfs
	L-63N-2	BASE	Post 25-72	40.01	17.95	28.83	0.0001	0	37.69	15.68	0.00	0.00
	L-63N-3	BASE	Post 25-72	40.01	17.95	28.83	0.0001	0	37.84	14.30	0.00	0.00
Pond 4	4D-Opt 1	BASE	Post 25-72	37.84	27.09	28.06	0.0039	162103	36.00	63.59	37.84	14.30
Pond 4	4D-Opt 2	BASE	Post 25-72	37.69	28.10	28.06	0.0050	116758	36.00	60.23	37.69	15.68





Basin 5

RUNOFF CURVE NUMBER CALCULATIONS

PROJECT: SR 710 PREPARED: LCS DATE: 2/11/2014

LOCATION OKEECHOBEE CO., FL CHECKED: GS DATE: 2/24/2014

Basin: BASIN 5 - PRE DEVELOPMENT - R/W Only

Drainage Area: From Station 685+00 to Station 703+40

Basin Length = 1840 feet (measured from roll plot)

R/W Width = 160 feet

1. Runoff curve number

Cover description	Soil name	Hydrologi c group	CN	Area (Acre)	CN x Area
Pavement - Existing Roadway			98	3.64	357
Open Space - Good Condition (Perv R/W)		D	80	4.85	388
Water Management (Existing - Largest Site (5C))		D	80	3.53	282
			Totals =	12.02	1027

Note: Assumed Type D Soil as soil types were predominantly Types B/D & C/D

Time of Concentration

PROJECT:		SR 710	BY:	LCS	DATE:	10/24/2013
LOCATION:	Oke	echobee County	CHECKED:	GSS	DATE:	10/24/2013
EXISTING	or	DEVELOPED / UN	DEVELOPED	BASIN:	5	
Tc	or	Tt (through subarea)				

NOTES: Space for as many as two segments per flow type can be used for each worksheet. Include map, schematic, or description of flow segments.

L=

Sheet flow (Applicable to Tc only)

Segment ID

- 1. Surface description (Table T-1, FDOT HB)
- 2. Mannings roughness coeff., n (Table T-1, FDOT HB) †
- 3. Flow length, L (total L \leq 100 ft.)
- 4. Design storm 72 hr. rainfall, P₇₂ (in.) ††
- 5. Land slope, s (ft./ft.)
- 6. Compute T_t in hr, $T_t = [0.007(nL)^{0.8}] / [P_{72hr}^{0.5} s^{0.4}] † †† Subtotal$

AB	
grass	
0.15	
100	
9.0	
0.005	
0.17	
	0.17

945 ft

Shallow concentrated flow

Segment ID

- 7. Surface description (Paved or Unpaved)
- 8. Flow length, L (ft)
- 9. Watercourse slope, s (ft/ft)
- 10. Average velocity, $V = k(S)^{0.5}$ (Equ. 5, FDOT HB)
- 11. Compute Tt in hr, $T_t = L / (3600*V)$

Subtotal

BC	
Unpaved	
845	
0.001	
0.39	
0.60	
	0.60

Channel Flow/Pipe Flow

Segment ID

- 12. Type of Flow
- 13. Diameter of Pipe (in.)
- 14. Cross sectional flow area, A (assumed d=0.5 ft)
- 15. Wetted perimeter, P_w
- 16. Hydraulic radius, r = A / P_w, Compute r
- 17. Channel slope, s (ft./ft.)
- 18. Manning's roughness coeff., n
- 19. $V = 1.486 (r)^{0.667} (s)^{0.50} / n$, Compute V ††††
- 20. Flow length, L
- 21. Tt = L/(3600*V)
- 22. Subtotal

	0.00
	0.00
	3.00
Hours	0.77
110015	0.77

Time of Concentration, hr. (summation of subtotals)

 Hours
 0.77

 Minutes
 46.1

 Total
 46.1

Ref. FDOT Hydrology Handbook 2012.

- † The use of Table T-1 is the "Overland Flow Manning's n Values" from FDOT Hydrology Handbook (2012).
- †† The design storm of the basin is a 25-year storm frequency with a duration of 72-hours. Values found in SFWMD ERP Information Manual Volume IV, Surface Water Management Design Aids Figure C-8 (2012).
- ††† This equation is derived from the FDOT Hydrology HB overland flow equation which uses intensity instead of precipitation. The original equation mandates a trial and error process of a Type II rainfall distribution to find the correct intensity with the actual time of concentration. This derivative was created to bypass the trial and error process and is inclusive to both Type II and Type III rainfall distributions.
- †††† Manning's Coefficient for Artifical Channels were found in FDOT Hydrology Handbook (2012) Table T-3. Manning's Coefficient for Natural Channels where calcuated with USGS Water-Supply Paper 2339.

Tcs-ABs-Firsts100feetacrossProposedPondsC;&C-845'fromPondsCstosroadsidexditchstosMosquitosCreek

RUNOFF CURVE NUMBER CALCULATIONS

PROJECT: SR 710 PREPARED: LCS DATE: 2/12/2014

LOCATION: OKEECHOBEE CO., FL CHECKED: GS DATE: 2/24/2014

Basin: BASIN 5A - POST DEVELOPMENT - R/W Only

Drainage Area: From Station 685+30 to Station 703+50

Basin Length = 1820 feet R/W Width = 160 feet

1. Runoff curve number

Cover description	Soil name	Hydrologic group	CN	Area (Acre)	CN x Area
Pavement - Proposed SR 710			98	4.03	395
Open Space - Good Condition (Perv R/W)		D	80	4.46	357
Water Management Area (Imperv.)			100	0.00	0
Water Management Area (Perv.)		D	80	2.62	210
			Totals =	11.12	962

Note: Assumed Type D Soil as soil types were predominantly Types B/D & C/D

TREATMENT VOLUME CALCULATIONS FOR PROPOSED CONDITION

PROJECT: SR 710 - Pond 5A PREPARED: LCS 2/12/2014

LOCATION: OKEECHOBEE COUNTY, FLORIDA CHECKED: GS 2/24/2014

Dry Retention Online Pond Treatment Calculations:

Proposed impervious area = 4.03 Ac

Total Drainage area = 11.12 Ac

75% of 2.5" runoff from impervious area = 0.63 Ac-Ft

75% of 1" runoff from drainage area = 0.69 Ac-Ft

Treatment Volume = Greater of 75% of 2.50" times percent imperviousness or 75% of 1.0" over drainage area.

*Note: Dry Detention Volume Used If Nutrient Loading Can Be Eliminated

Required Treatment Volume (T.V.) = **0.69** Ac-ft

= 30268 ft^3

Pond Storage Calculations (Dry Retention - Pond 5A):

Elev. (NAVD)	h	Area	Area	Inc. Volume	Cum. Volume	Cum. Volume
(ft)	ft	sf	ac	Ac-ft	Ac-ft	Cu-ft
27.00	1.0	59,949	1.376	1.317	3.597	156,685
26.00	1.0	54,765	1.257	1.198	2.280	99,317
25.00	1.0	49,643	1.140	1.082	1.082	47,132
24.00	0.0	44,650	1.025	0.000	0.000	0

SHWT EI - 21.75'

Overflow Weir Elevation (Top of storage volume) (Pond5A)

Elev.	Storage	Area
24.00	0.000	44,650
25.00	1.082	49,643

Elev. = 24.65 = 0.70 Ac-Ft 30636 Cu-Ft

Provided Treatment Volume (T.V.) =	0.703	Ac-ft
Treatment Depth =	0.650	ft

From Geotechnical Information (10/13):

Boring PB-5A:

Est. Ground Elevation (at boring location) = 23 feet Subtract SHGT Depth = -0.75-0.5 (variation) = 1.25 feet Estimated SHGT Elev. = 21.75 feet

Nodes
A Stage/Area
V Stage/Volume
T Time/Stage
M Manhole

Basins
O Overland Flow
U SCS Unit CN
S SBUH CN
Y SCS Unit GA
Z SBUH GA

Links
P Pipe
W Weir
C Channel
D Drop Structure
B Bridge
R Rating Curve
B Breach
E Percolation
F Filter
F Fitter
X Exfil Trench

T: Mosquito

```
..oue. rond 5A Status: Onsite
Type: SCS Unit Hydrograph CN
      Name: Basin 5
     Group: BASE
  Max Allowable Q(cfs): 999999.000
_____
______
                     Base Flow(cfs): 0.000
    Name: Mosquito Creek
                                              Init Stage(ft): 18.190
   Group: BASE
Type: Time/Stage
                                              Warn Stage(ft): 999.000
From DHW Memo - NWL = 19.36' NGVD (18.19' NAVD) from SR 710 over Mosquito Creek Bridge Plans (91050-3509).
               Stage(ft)
        0 00
      250.00
    Name: Pond 5A Base Flow(cfs): 0.000 Init Stage(ft): 24.000
   Group: BASE
                                              Warn Stage(ft): 27.000
    Type: Stage/Area
      Stage(ft)
      25.000
26.000
              1.2570
1.3760
      27.000
______
 ______
                                              Length(ft): 595.00
      Name: Pond 5A Outfall From Node: Pond 5A
     Group: BASE
                          To Node: Mosquito Creek
                                         Friction Equation: Automatic
Solution Algorithm: Most Restrictive
Flow: Both
Entrance Loss Coef: 0.500
Exit Loss Coef: 1.000
           UPSTREAM
                     DOWNSTREAM
   Geometry: Circular Span(in): 18.00
                     Circular
                     18.00
                    18.00
18.00
18.260
  Rise(in): 18.00
Invert(ft): 19.450
 Manning's N: 0.012000
Top Clip(in): 0.000
                     0.012000
0.000
                                           Outlet Ctrl Spec: Use dc or tw
Inlet Ctrl Spec: Use dc
Bot Clip(in): 0.000
                     0.000
                                             Solution Incs: 10
Upstream FHWA Inlet Edge Description:
Circular Concrete: Square edge w/ headwall
Downstream FHWA Inlet Edge Description:
Circular Concrete: Square edge w/ headwall
*** Weir 1 of 1 for Drop Structure Pond 5A Outfall ***
                                                            TABLE
             Count: 1
                                  Bottom Clip(in): 0.000
             Type: Horizontal
Flow: Both
                                  Top Clip(in): 0.000
Weir Disc Coef: 3.200
Orifice Disc Coef: 0.600
           Geometry: Rectangular
           Span(in): 37.00
                                        Invert(ft): 24.650
           Rise(in): 24.00
                                  Control Elev(ft): 24.650
______
Name: Post 5A 25-72 Filename: T:\00809.00\zTBG\drainage\ICPR\Post 5A - 25-72.R32
   Override Defaults: Yes
Storm Duration(hrs): 72.00
   Rainfall File: Flmod Rainfall Amount(in): 9.00
        Print Inc(min)
Time(hrs)
72.000
           15.00
```

---- Routing Simulations ------

Name: Post 25-72 Hydrology Sim: Post 5A 25-72 Filename: T:\00809.00\zTBG\drainage\ICPR\Pond 5A - 25-72.132

Execute: Yes Alternative: No Restart: No

 Max Delta Z(ft):
 1.00
 Delta Z Factor:
 0.00500

 Time Step Optimizer:
 10.000
 End Time(hrs):
 72.00

 Min Calc Time(sec):
 0.5000
 Max Calc Time(sec):
 60.0000

 Boundary Stages:
 Boundary Flows:

Print Inc(min)

10.000 15.000
72.000 15.000
Group Group Run BASE Yes

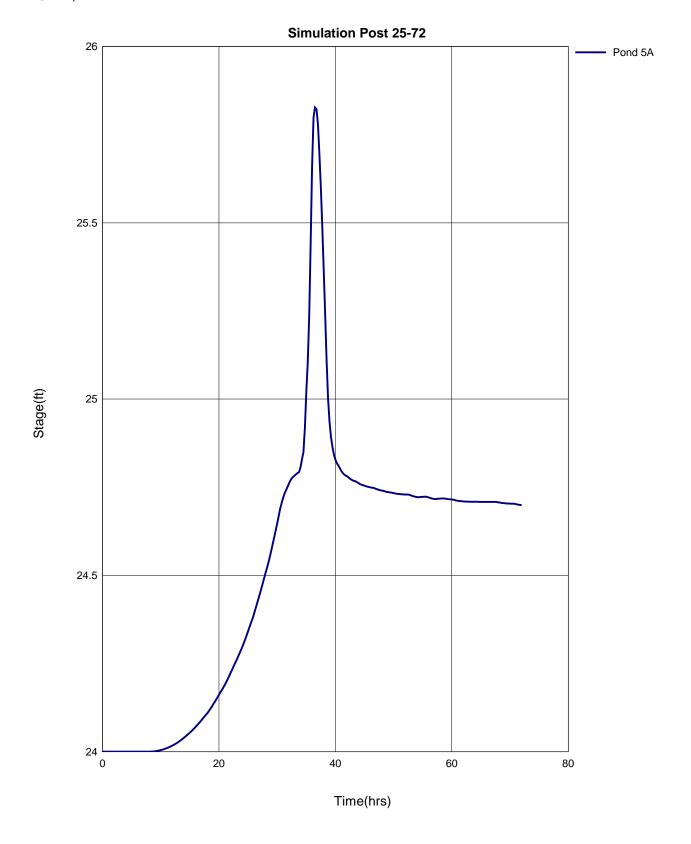
Basin Name: Basin 5
Group Name: BASE
Simulation: Post 5A 25-72
Node Name: Pond 5A
Basin Type: SCS Unit Hydrograph

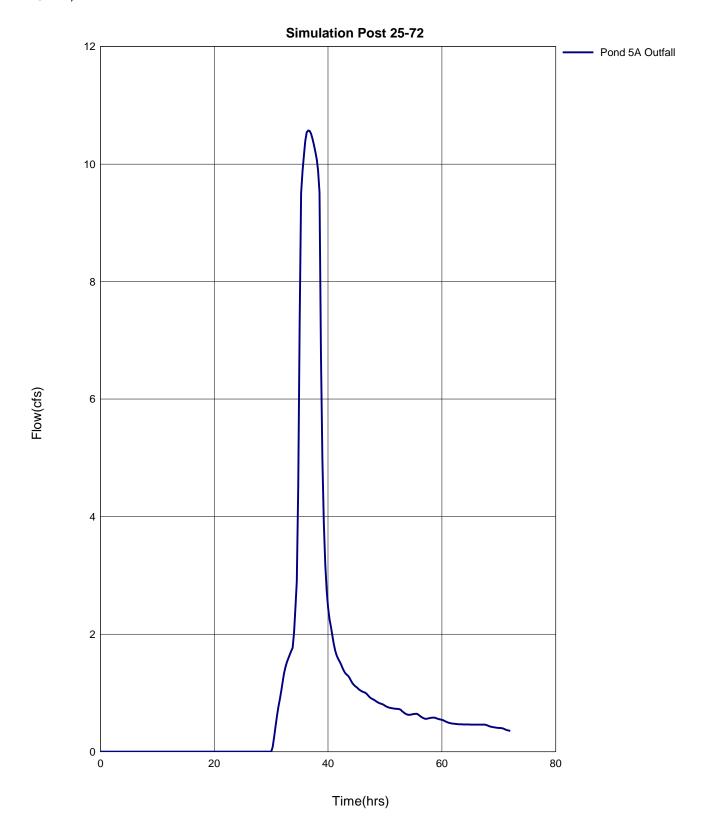
Unit Hydrograph: Uh223
Peaking Fator: 323.0
Spec Time Inc (min): 1.33
Comp Time Inc (min): 1.33
Rainfall File: Flmod
Rainfall Amount (in): 9.000
Storm Duration (hrs): 72.00
Status: Onsite
Time of Conc (min): 10.00
Time Shift (hrs): 0.00
Area (ac): 11.120
Vol of Unit Hyd (in): 1.001
Curve Number: 87.000
DCIA (%): 0.000

Time Max (hrs): 36.00
Flow Max (cfs): 23.70
Runoff Volume (in): 7.429
Runoff Volume (ft3): 299878

Pond 5A 25 Yr, 72 Hr

Name	Group	Simulation	Max Time Stage hrs	Max Stage ft	Warning M Stage ft	Max Delta Stage ft	Max Surf Area ft2	Max Time Inflow hrs	Max Inflow cfs	Max Time Outflow hrs	Max Outflow cfs
Mosquito Creek Pond 5A	BASE BASE	Post 25-72 Post 25-72	0.00 36.54	18.19 25.83	999.00 27.00	0.0000	0 53874	36.54 36.00	10.57 23.68	0.00 36.54	0.00





RUNOFF CURVE NUMBER CALCULATIONS

PROJECT: SR 710 PREPARED: LCS DATE: 2/12/2014

LOCATION: OKEECHOBEE CO., FL CHECKED: GS DATE: 2/24/2014

Basin: BASIN 5B - POST DEVELOPMENT - R/W Only

Drainage Area: From Station 685+30 to Station 703+50

Basin Length = 1820 feet R/W Width = 160 feet

1. Runoff curve number

Cover description	Soil name	Hydrologic group	CN	Area (Acre)	CN x Area
Pavement - Proposed SR 710			98	4.03	395
Open Space - Good Condition (Perv R/W)		D	80	4.46	357
Water Management Area (Imperv.)			100	0.00	0
Water Management Area (Perv.)		D	80	2.53	203
			Totals =	11.03	955

Note: Assumed Type D Soil as soil types were predominantly Types B/D & C/D

TREATMENT VOLUME CALCULATIONS FOR PROPOSED CONDITION

PROJECT: SR 710 - Pond 5B PREPARED: LCS 2/12/2014

LOCATION: OKEECHOBEE COUNTY, FLORIDA CHECKED: GS 2/24/2014

Dry Retention Online Pond Treatment Calculations:

Proposed impervious area = 4.03 Ac

Total Drainage area = 11.03 Ac

75 % of 2.5" runoff from impervious area = 0.63 Ac-Ft

75% of 1" runoff from drainage area = 0.69 Ac-Ft

Treatment Volume = Greater of 75% of 2.50" times percent imperviousness or 75% of 1.0" over drainage area.

*Note: Dry Detention Volume Used If Nutrient Loading Can Be Eliminated

Required Treatment Volume (T.V.) = **0.69** Ac-ft

: 30022 ft³

Pond Storage Calculations (Dry Retention - Pond 5B):

Elev. (NAVD)	h	Area	Area	Inc. Volume	Cum. Volume	Cum. Volume
(ft)	ft	sf	ac	Ac-ft	Ac-ft	Cu-ft
27.00	1.0	53,651	1.232	1.174	3.185	138,739
26.00	1.0	48,668	1.117	1.061	2.011	87,599
25.00	1.0	43,786	1.005	0.950	0.950	41,382
24.00	0.0	39,004	0.895	0.000	0.000	0

SHGT El. = 22.0'

Overflow Weir Elevation (Top of storage volume) (Pond5B)

Elev.	Storage	Area
24.00	0.000	43,786
25.00	0.950	48,668

Elev. = 24.73 = 0.69 Ac-Ft 30209 Cu-Ft

Provided Treatment Volume (T.V.) =	0.69	Ac-ft
Treatment Depth =	0.73	ft

From Geotechnical Information (10/13):

Boring PB-5B:

Est. Ground Elev. (at boring location) =	23 feet
Subtract SHGT Depth = -0.5-0.5 (variation)=	1 feet
Estimated SHGT Elev. =	22 feet

Nodes
A Stage/Area
V Stage/Volume
T Time/Stage
M Manhole

Basins
O Overland Flow
U SCS Unit CN
S SBUH CN
Y SCS Unit GA
Z SBUH GA

Links
P Pipe
W Weir
C Channel
D Drop Structure
B Bridge
R Rating Curve
B Breach
E Percolation
F Filter
X Exfil Trench

T: L-63N

```
..oue. rond 5B Status: Onsite Type: SCS Unit Hydrograph CN
       Name: Basin 5
      Group: BASE
   Max Allowable Q(cfs): 999999.000
_____
______
     Name: L-63N
                         Base Flow(cfs): 0.000
                                                    Init Stage(ft): 17.830
    Group: BASE
Type: Time/Stage
                                                    Warn Stage(ft): 28.830
From Bridge Plans for SR 70 over L-63N Canal: NHW in L-63N Canal = 19.0' NGVD = 17.83' NAVD
                Stage(ft)
        0.00 17.830
14.00 17.930
        40.00
                    17.950

        Name:
        Pond 5B
        Base Flow(cfs):
        0.000
        Init Stage(ft):
        24.000

        Group:
        BASE
        Warn Stage(ft):
        27.000

    Group: BASE
     Type: Stage/Area
    Stage(ft)
                  Area(ac)
       24.000
               0.8950
       25.000
26.000
                    1.0050
                    1.1170
       27.000
                   1.2320
______
______
       Name: Pond 5B Outfall From Node: Pond 5B
                                                     Length(ft): 125.00
      Group: BASE
                              To Node: L-63N
                                                          Count: 1
                        DOWNSTREAM
            UPSTREAM
                                                Friction Equation: Automatic
                       Circular
18.00
    Geometry: Circular
Span(in): 18.00
                                             Solution Algorithm: Most Restrictive
Flow: Both
                                              Flow: Both
Entrance Loss Coef: 0.500
Exit Loss Coef: 1.000
Outlet Ctrl Spec: Use dc or tw
Inlet Ctrl Spec: Use dc
Spain(in): 10:00
Rise(in): 18:00
Invert(ft): 19:730
Manning's N: 0.012000
Top Clip(in): 0.000
Bot Clip(in): 0.000
                        18.00
19.480
0.012000
                        0.000
                                                   Solution Incs: 10
                        0.000
Upstream FHWA Inlet Edge Description:
Circular Concrete: Square edge w/ headwall
Downstream FHWA Inlet Edge Description:
Circular Concrete: Square edge w/ headwall
*** Weir 1 of 1 for Drop Structure Pond 5B Outfall ***
            Count: 1 Bottom Clip(in): 0.000
Type: Horizontal Top Clip(in): 0.000
Flow: Both Weir Disc Coef: 3.200
Geometry: Rectangular Orifice Disc Coef: 0.600
                                                                    TABLE
            Span(in): 37.00
                                             Invert(ft): 24.730
            Rise(in): 24.00
                                      Control Elev(ft): 24.730
-----
Name: Post 5B 25-72
    Filename: T:\00809.00\zTBG\drainage\ICPR\Post 5B - 25-72.R32
   Override Defaults: Yes
Storm Duration(hrs): 72.00
Rainfall File: Flmod
   Rainfall Amount(in): 9.00
Time(hrs)
            Print Inc(min)
```

Pond 5B 25 Yr, 72 Hr

72.000 15.00

---- Routing Simulations ------

Name: Post 25-72 Hydrology Sim: Post 5B 25-72 Filename: T:\00809.00\zTBG\drainage\ICPR\Pond 5B - 25-72.132

Restart: No Execute: Yes Alternative: No

Max Delta Z(ft): 1.00
Time Step Optimizer: 10.000
Start Time(hrs): 0.000
Min Calc Time(sec): 0.5000

Delta Z Factor: 0.00500 End Time(hrs): 72.00 Max Calc Time(sec): 60.0000 Boundary Flows:

Boundary Stages:

Print Inc(min) Time(hrs)

15.000 15.000 10.000 72.000

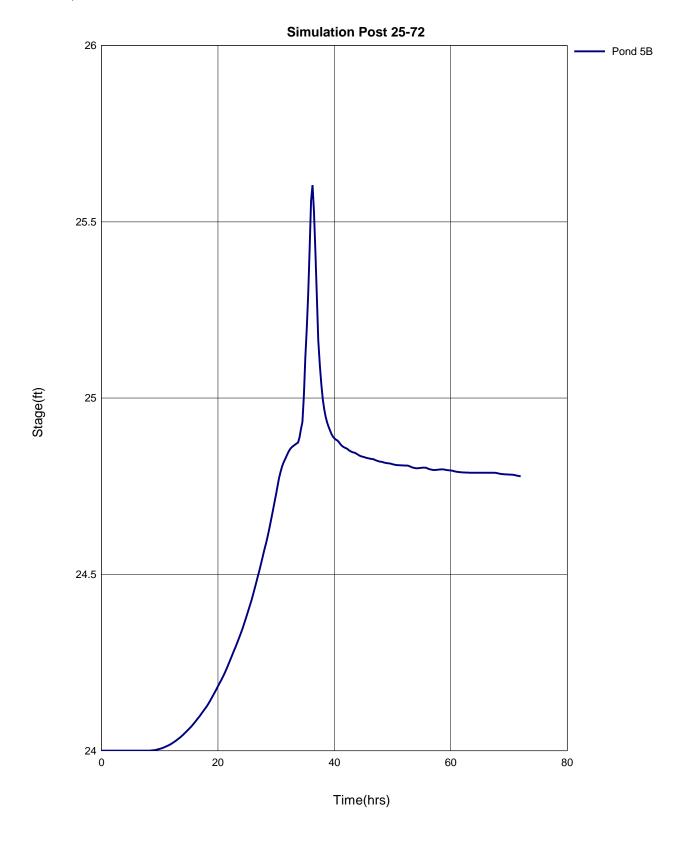
Group Run Yes BASE

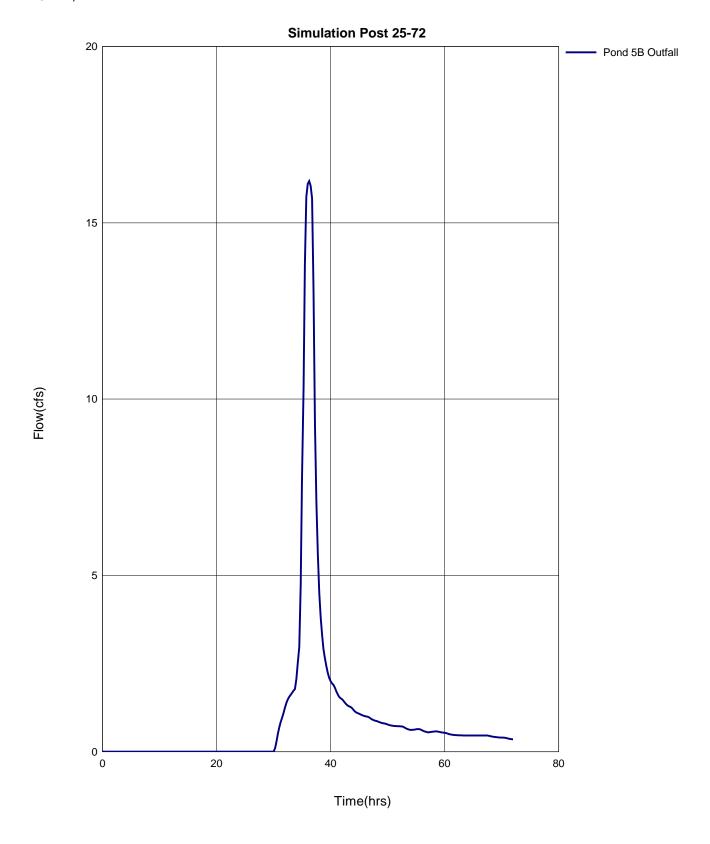
Basin Name: Basin 5
Group Name: BASE
Simulation: Post 5B 25-72
Node Name: Pond 5B
Basin Type: SCS Unit Hydrograph
Unit Hydrograph: Uh323
Peaking Fator: 323.0
Spec Time Inc (min): 1.33
Comp Time Inc (min): 1.33
Rainfall File: Flmod
Rainfall Amount (in): 9.000
Storm Duration (hrs): 72.00
Status: Onsite
Time of Conc (min): 10.00
Time Shift (hrs): 0.00
Area (ac): 11.030
Vol of Unit Hyd (in): 1.001
Curve Number: 87.000
DCIA (%): 0.000

Time Max (hrs): 36.00
Flow Max (cfs): 23.50
Runoff Volume (in): 7.429
Runoff Volume (ft3): 297451

Pond 5B 25 Yr, 72 Hr

Name	Group	Simulation	Max Time Stage hrs	Max Stage ft	Warning M Stage ft	ax Delta Stage ft	Max Surf Area ft2	Max Time Inflow hrs	Max Inflow cfs	Max Time Outflow hrs	Max Outflow cfs
L-63N	BASE	Post 25-72	40.00	17.95	28.83	0.0001	0	36.18	16.19	0.00	0.00
Pond 5B	BASE	Post 25-72	36.18	25.61	27.00	0.0050	46762	36.00	23.48	36.18	16.19





RUNOFF CURVE NUMBER CALCULATIONS

PROJECT: SR 710 PREPARED: LCS DATE: 2/12/2014

LOCATION: OKEECHOBEE CO., FL CHECKED: GS DATE: 2/24/2014

Basin: BASIN 5C - POST DEVELOPMENT - R/W Only

Drainage Area: From Station 685+30 to Station 703+50

Basin Length = 1820 feet R/W Width = 160 feet

1. Runoff curve number

Cover description	Soil name	Hydrologic group	CN	Area (Acre)	CN x Area
Pavement - Proposed SR 710			98	4.03	395
Open Space - Good Condition (Perv R/W)		D	80	4.46	357
Water Management Area (Imperv.)			100	0.00	0
Water Management Area (Perv.)		D	80	3.53	282
			Totals =	12.02	1034

Note: Assumed Type D Soil as soil types were predominantly Types B/D & C/D

TREATMENT VOLUME CALCULATIONS FOR PROPOSED CONDITION

PROJECT: SR 710 - Pond 5C PREPARED: LCS 2/12/2014

LOCATION: OKEECHOBEE COUNTY, FLORIDA CHECKED: GS 2/24/2014

Dry Retention Online Pond Treatment Calculations:

Proposed impervious area = 4.03 Ac

Total Drainage area = 12.02 Ac

75% of 2.5" runoff from impervious area = 0.63 Ac-Ft

75% of 1" runoff from drainage area = 0.75 Ac-Ft

Treatment Volume = Greater of 75% of 2.50" times percent imperviousness or 75% of 1.0" over drainage area.

*Note: Dry Detention Volume Used If Nutrient Loading Can Be Eliminated

Required Treatment Volume (T.V.) = 0.75 Ac-ft = 32729 ft³

Pond Storage Calculations (Dry Retention - Pond 5C):

Elev. (NAVD)	h	Area	Area	Inc. Volume	Cum. Volume	Cum. Volume
(ft)	ft	sf	ac	Ac-ft	Ac-ft	Cu-ft
27.00	1.0	97,339	2.235	2.165	6.091	265,324
26.00	1.0	91,300	2.096	2.029	3.926	171,017
25.00	1.0	85,452	1.962	1.897	1.897	82,633
24.00	0.0	79,794	1.832	0.000	0.000	0

SHGT EI = 22.5

Overflow Weir Elevation (Top of storage volume) (Pond5C)

Elev.	Storage	Area
24.00	0.000	79,794
25.00	1.897	85,452

Elev. = 24.40 = 0.76 Ac-Ft 33053 Cu-Ft

Provided Treatment Volume (T.V.) =	0.759	Ac-ft

Treatment Depth = 0.40 ft

From Geotechnical Information (10/13):

Boring PB-5C:

Est. Ground Elevation (at boring location) =	24 feet
Subtract SHGT Depth = -1.0-0.5 (variation)=	1.5 feet
Estimated SHGT Elev. =	22.5 feet

Nodes
A Stage/Area
V Stage/Volume
T Time/Stage
M Manhole

Basins
O Overland Flow
U SCS Unit CN
S SBUH CN
Y SCS Unit GA
Z SBUH GA

Links
P Pipe
W Weir
C Channel
D Drop Structure
B Bridge
R Rating Curve
B Breach
E Percolation
F Filter
F Fitter
X Exfil Trench

T: Mosquito

```
Noue. Fond 5C Status: Onsite
Type: SCS Unit Hydrograph CN
       Name: Basin 5
      Group: BASE
   Unit Hydrograph: Uh323 Peaking Factor: 323.0
Rainfall File: Storm Duration(hrs): 0.00
Rainfall Amount(in): 0.000 Time of Conc(min): 10.00
Area(ac): 12.020 Time Shift(hrs): 0.00
Curve Number: 86.00 Max Allowable Q(cfs): 999999
                                     Max Allowable Q(cfs): 999999.000
_____
______
                        Base Flow(cfs): 0.000
     Name: Mosquito Creek
                                                      Init Stage(ft): 18.190
    Group: BASE
Type: Time/Stage
                                                      Warn Stage(ft): 999.000
    Time(hrs)
                 Stage(ft)
         0 00
     Name: Pond 5C Base Flow(cfs): 0.000 Init Stage(ft): 24.000
Group: BASE Warn Stage(ft): 26.000
    Group: BASE
                                                      Warn Stage(ft): 26.000
     Type: Stage/Area
       age(ft)

24.000 1.8320

25.000 1.9620

2.0960
     Stage(ft)
       25.000
26.000
                   2.0960
       27.000
______
_____
                               To Node: Mosquito Creek Length(ft): 400.00
       Name: Pond 5C Outfall From Node: Pond 5C
      Group: BASE
                                                Friction Equation: Automatic
Solution Algorithm: Most Restrictive
Flow: Both
Entrance Loss Coef: 0.500
Exit Loss Coef: 1.000
            UPSTREAM
                         DOWNSTREAM
    Geometry: Circular Span(in): 18.00
                       Circular
18.00
18.00
18.600
  Rise(in): 18.00
Invert(ft): 19.400
                     18.600
0.012000
0.000
 Manning's N: 0.012000
Top Clip(in): 0.000
                                                  Outlet Ctrl Spec: Use dc or tw
Inlet Ctrl Spec: Use dc
 Bot Clip(in): 0.000
                                                    Solution Incs: 10
Upstream FHWA Inlet Edge Description:
Circular Concrete: Square edge w/ headwall
Downstream FHWA Inlet Edge Description:
Circular Concrete: Square edge w/ headwall
*** Weir 1 of 1 for Drop Structure Pond 5C Outfall ***
                                                                      TABLE
                Type: Horizontal Flow: Both metry: Rect
               Count: 1
                                        Bottom Clip(in): 0.000
                                       Top Clip(in): 0.000
Weir Disc Coef: 3.200
Orifice Disc Coef: 0.600
            Flow: Both
Geometry: Rectangular
             Span(in): 37.00
                                              Invert(ft): 24.400
             Rise(in): 24.00
                                        Control Elev(ft): 24.400
______
Name: Post 5C 25-72 Filename: T:\00809.00\zTBG\drainage\ICPR\Post 5C - 25-72.R32
   Override Defaults: Yes
Storm Duration(hrs): 72.00
   Rainfall File: Flmod Rainfall Amount(in): 9.00
         Print Inc(min)
Time(hrs)
72.000
             15.00
```

---- Routing Simulations ------

Name: Post 25-72 Hydrology Sim: Post 5C 25-72 Filename: T:\00809.00\zTBG\drainage\ICPR\Pond 5C - 25-72.132

Execute: Yes Alternative: No Restart: No

 Max Delta Z(ft):
 1.00
 Delta Z Factor:
 0.00500

 Time Step Optimizer:
 10.000
 End Time(hrs):
 72.00

 Min Calc Time(sec):
 0.5000
 Max Calc Time(sec):
 60.0000

 Boundary Stages:
 Boundary Flows:

Print Inc(min)

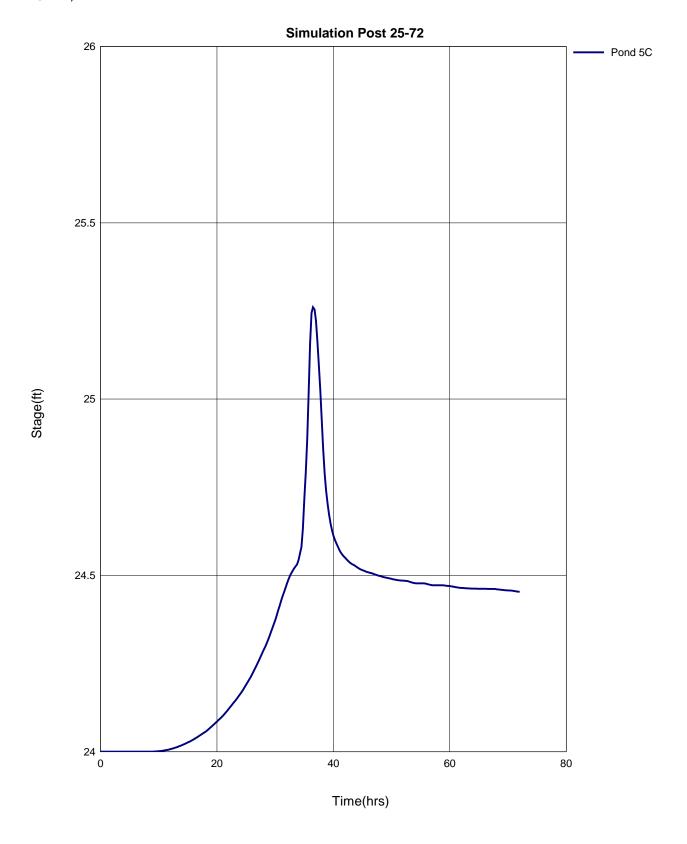
10.000 15.000
72.000 15.000
Group Group Run
---BASE Yes

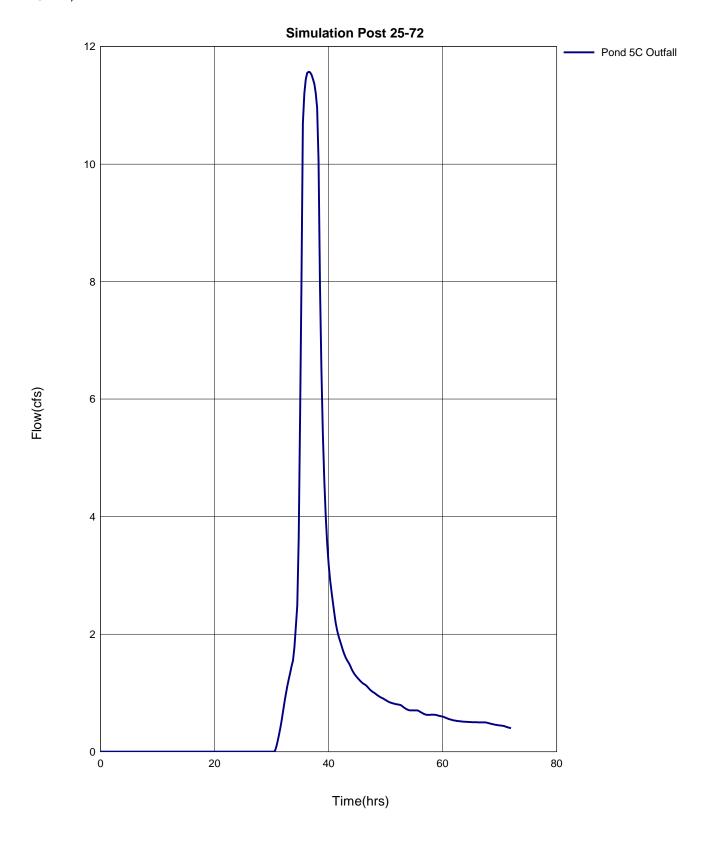
Basin Name: Basin 5
Group Name: BASE
Simulation: Post 5C 25-72
Node Name: Pond 5C
Basin Type: SCS Unit Hydrograph
Unit Hydrograph: Uh323
Peaking Fator: 323.0
Spec Time Inc (min): 1.33
Comp Time Inc (min): 1.33
Rainfall File: Flmod
Rainfall Amount (in): 9.000
Storm Duration (hrs): 72.00
Status: Onsite
Time of Conc (min): 10.00
Time Shift (hrs): 0.00
Area (ac): 12.020
Vol of Unit Hyd (in): 1.001
Curve Number: 86.000
DCIA (%): 0.000

Time Max (hrs): 36.00
Flow Max (cfs): 25.38
Runoff Volume (in): 7.307
Runoff Volume (ft3): 318817

Pond 5C 25 Yr, 72 Hr

Name	Group	Simulation	Max Time Stage hrs	Max Stage ft	Warning M Stage ft	ax Delta Stage ft	Max Surf Area ft2	Max Time Inflow hrs	Max Inflow cfs	Max Time Outflow hrs	Max Outflow cfs
Mosquito Creek Pond 5C	BASE BASE	Post 25-72 Post 25-72	0.00 36.49	18.19 25.26	999.00 26.00	0.0000	0 86985	36.49 36.00	11.57 25.36	0.00 36.49	0.00





Preliminary Storm Drain Tabulations

FLORIDA DEPARTMENT OF TRANSPORTATION STORM DRAIN TABULATION FORM

Financial Prj Id: 21151201.00 County: OKECHOBEE Network: POND1 Designed by AD Date: 2/18/2014
Description: NEW ALIGNMENT Organization WANTMAN GROUP State Road: SR 710 Checked by: PAT Date: 2/18/2014

LOCA	TION	STR.	TYPE	LEN.	AREA	S (Ac)	SUB-	TIME	TIME	INTEN	TOTAL	BASE	TOTAL	MINOR	INLET	HGL	HYDRA	ULIC GR	ADE	# P	IPE :	SLOPE	CTUAL	FULL	NOTES & REM	MARKS
OI	F	NO.	OF		C=	0.95	TOTAL	OF	OF		(C*A)	FLOW	FLOW	LOSS	ELEV.	CLEAR		ROWN		BS	IZE	%	VEL.	FLOW	ZONE:	8
UPPER	R END		STR.		C=	0.20	(C*A)	CONC	FLOW			SUMM					FL	OWLINE.		R (in.)	HGL	PHYS.	CAP.	FREQ. (Yrs):	3
ALIGNMEN	NT NAME	UPPER			C=	0.00			SECT.			BASE					UPPER	LOWER	FALL	LR	ISE	PHYS	VEL.		MANNINGS n:	0.0120
STATION	DIST S	DLOWER		(ft.)	INC	TOTAL		(min)	(min)	(in/hr)		(cfs)	(cfs)	(ft.)	(ft.)	(ft.)	(ft.)	(ft.)	(ft.)	SS	PAN	MIN.	(fps)	(cfs)	TAILW EL (ft):	19.64
CL7	10	S-1			0.67	0.67	0.64										21.67	21.52	0.15	18	8.00	0.144	2.44			
			P-4	102.00	0.10	0.10	0.02	10.00	0.70	6.58	0.66	0.00	4.32	0.00	23.85	2.18	21.24	21.09		1		0.147	_	4.43		
502+47	51.00 L	.t. S-2			0.00	0.00	0.00					0.00					19.74	19.59	0.15	18	8.00	0.150	2.51			
CL7	' 10	S-2			0.53	1.20	0.50										21.52	21.22	0.31	2	4.00	0.101	2.48			
		-	P-4	302.58	0.25	0.35	0.05	10.70	2.04	6.43	1.21	0.00	7.78	0.00	23.85	2.33	21.20	20.89		1	-	0.102		7.88		
502+47	51.00 R	Rt. S-4			0.00	0.00	0.00					0.00					19.20	18.89	0.31	2	4.00	0.102	2.51			
CL7	10	S-3			0.43	0.43	0.41										21.98	21.83	0.15	18	8.00	0.147	2.66			
			P-3	102.02	0.11	0.11	0.02	10.00	0.64	6.58	0.43	0.00	2.83	0.00	25.22	3.23	22.61	22.46		1		0.147		4.43		
505+47	51.01 L	.t. S-4			0.00	0.00	0.00					0.00					21.11	20.96	0.15	18	8.00	0.150	2.51			
CL7	10	S-4			0.40	2.03	0.38										21.22	20.99	0.23	3	0.00	0.078	2.52			
			P-3	293.36	0.15	0.61	0.03	12.73	1.94	6.03	2.05	0.00	12.38	0.00	25.22	4.00	21.39	20.99		1		0.136		16.49		
505+47	51.01 R	Rt. S-5			0.00	0.00	0.00					0.00					18.89	18.49	0.40	3	0.00	0.076	3.36			
CL7	CL710 S-5				0.00	2.03	0.00										20.65	20.59	0.06	_	0.00	0.070	2.39			
			MH-7	86.50	0.00	0.61	0.00	14.67	0.00	5.72	2.05	0.00	11.72	0.00	26.61	5.96	20.99	20.59		1		0.462		30.48		
508+36.72	45.50 R	Rt. POND1			0.00		0.00					0.00					18.49	18.09	0.40	3	0.00	0.076				_

Units: ENGLISH

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FLORIDA DEPARTMENT OF TRANSPORTATION STORM DRAIN TABULATION FORM

Financial Prj Id: 21151201.00 County: OKECHOBEE Network: POND2 Designed by AD Date: 2/18/2014
Description: NEW ALIGNMENT Organization WANTMAN GROUP State Road: SR 710 Checked by: PAT Date: 2/18/2014

Part	LOCAT	TION	STR.	TYPE	LEN.	AREA	S (Ac)	SUB-	TIME	TIME	INTEN	TOTAL	BASE	TOTAL	MINOR	INLET	HGL	HYDRA	ULIC GR	ADE	# PIPE	SLOPE	CTUAL	FULL	NOTES & REM	MARKS
ALTHON No. Part			NO.	OF															ROWN						ZONE:	8
STATION STATI	UPPER	END		STR.		C=	0.20	(C*A)	CONC	FLOW		` ′	SUMM					FL	OWLINE		R (in.)	HGL	PHYS.	CAP.	FREQ. (Yrs):	3
Figure F	ALIGNMEN	NT NAME	UPPER			C=	0.00			SECT.			BASE					UPPER	LOWER	FALL	L RISE	PHYS	VEL.		MANNINGS n:	0.0120
P-3 192-80 193-	STATION	DIST SD	LOWER		(ft.)	INC	TOTAL		(min)	(min)	(in/hr)		(cfs)	(cfs)	(ft.)	(ft.)	(ft.)	(ft.)	(ft.)	(ft.)	S SPAN	MIN.	(fps)	(cfs)	TAILW EL (ft):	21.50
51-24 51-2	CL7	10	S-200			0.34	0.65	0.32										23.76	23.65	0.11	24.00	0.029	1.34			1
C			-	P-3	372.82	0.08	0.20	0.02	10.85	3.11	6.39	0.66	0.00	4.21	0.00	25.63	1.87	21.14	20.76		1	0.102	-	7.86		
P-3 P-3	512+30	51.00 Lt.	S-202			0.00	0.00	0.00					0.00					19.14	18.76	0.38	24.00	0.102	2.50			
51-00 10 10 10 10 10 10 10	CL7	10	S-201			0.31	0.31	0.29										23.79	23.76	0.03	18.00	0.034	1.18			
State Stat				P-3	102.00	0.12	0.12	0.02	10.00	0.85	6.58	0.32	0.00	2.09	0.00	25.63	1.84	23.02	22.87		1	0.147	-	4.43		
Steholo	512+30	51.00 Rt.	S-200			0.00	0.00	0.00					0.00					21.52	21.37	0.15	18.00	0.150	2.51			
Sincol S	CL7	10	S-202			0.71	2.06	0.67										23.65	23.46	0.19	30.00	0.082	2.59			
S				P-4	227.95	0.46	1.10	0.09	13.96	1.47	5.83	2.18	0.00	12.69	0.00	24.03	0.38	21.26	21.09		1	0.075		12.22		
Signature Sign	516+00	51.00 Lt.	S-204			0.00	0.00	0.00					0.00					18.76	18.59	0.17	30.00	0.076	2.49			
Simple S	CL7	10	S-203			0.70	0.70	0.66										23.84	23.65	0.19	18.00	0.189	2.80			
CL710 S-204				P-4	102.00	0.44	0.44	0.09	10.00	0.61	6.58	0.75	0.00	4.95	0.00	24.03	0.19	21.42	21.22		1	0.196		5.11		
Mil-y Mil-	516+00	51.00 Rt.	S-202			0.00	0.00	0.00				L	0.00					19.92	19.72	0.20	18.00	0.150	2.89			
518+25	CL7	10	S-204			0.00	2.06	0.00										23.46	23.29	0.17	30.00	0.075	2.49			
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $				MH-7	227.92	0.00	1.10	0.00	15.43	1.53	5.60	2.18	0.00	12.20	0.00	24.91	1.44	21.09	20.92		1	0.075		12.22		
	518+25	50.20 Lt.	S-205			0.00	0.00	0.00					0.00					18.59	18.42	0.17	30.00	0.076	2.49			
520+50 50,20 Lt. 5205 S.20 Lt. 5205 S.20 Lt. 5206 S.20	CL7	10	S-205			0.00	2.06	0.00										23.29	23.13	0.16	30.00	0.070	2.39			_
520+50 50,20 Lt. 5205 S.20 Lt. 5205 S.20 Lt. 5206 S.20				MH-7	230.34	0.00	1.10	0.00	16.95	1.60	5.39	2.18	0.00	11.74	0.00	25.66	2.36	20.92	20.75		1	0.074		12.15		
S22+78 S	520+50	50.20 Lt.	S-206					0.00					0.00							0.17	30.00	0.076	2.48			
S22+78 S	CL7	10	S-206			0.00	2.06	0.00										23.13	23.00	0.13	30.00	0.065	2.30			
522+78 50.20 Lt S-207 S-207 S-207 S-207 S-207 S-208 S-207 S-208 S-207 S-208 S-209			_	MH-7	207.00	0.00		0.00	18.56	1.50	5.19	2.18	0.00	11.31	0.00	24.89	1.76	20.75	19.69		1	0.512		32.11		
S24+85 S1.00 L. S-208 S2-98	522+78	50.20 Lt.	S-207															18.25		1.06	30.00					
State Stat	CL7	10	S-207			0.93	3.91	0.88										23.00	22.88	0.12	42.00	0.037	2.18			
State Stat				J-4	318.00	0.60	2.27	0.12	20.06	2.43	5.02	4.17	0.00	20.94	0.00	24.17	1.17	20.69	20.54		1	0.047	_	23.86		
CL710	524+85	51.00 Lt.	S-209	_																0.15	42.00	0.048				
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $																										-
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $				P-4	102.00	0.58	0.58	0.12	10.00	0.82	6.58	0.99	0.00	6.51	0.00	24.17	1.10	19.30	19.19		1	0.108		8.21		
CL710 S-209 MH-7J 317.00 0.00 2.27 0.00 0.	524+85	51.00 Rt.	S-207																	0.11	24.00		2.61			
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $																										-
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $				MH-7J	317.00	0.00			22.49	2.55	4.77	4.17	0.00	19.90	0.00	25.01	2.13		20.39		1			23.90		
CL710 S-212	528+03	51.00 Lt.	S-212																	0.15	42.00					
Salt-20 Salt																										
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $					300.00				25.05	2.50	4.54	4.17	0.00	18.93	0.00	25.96	3.19				1			23.76		
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	531+20	51.00 Lt.	S-214												,					0.14	42.00			2 0		
Sign Sign																										
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $					220.00				27.55	1.72	4.34	4.73	0.00	20.51	0.00	25.08	2.40				1			23.53		
CL710 S-215 P-3 102.00 0.16 0.26 0.25 100 Rt. S-214 P-3 102.00 0.00 0.00 0.00 0.00 0.00 0.00 0.	534+20	51.00 Lt.	S-216																	0.10	42.00					
P-3 102.00 0.16 0.16 0.03 10.00 0.85 6.58 0.28 0.00 1.84 0.00 25.08 2.37 21.97 21.77 1 0.196 0.150													2.23													-
534+20 51.00 Rt. S-214 0 0.00 0.00 0.00 0.00 0.00 0.00 0.00	<u> </u>			P-3	102.00				10.00	0.85	6.58	0.28	0.00	1.84	0.00	25.08	2.37				1			5.15		
CL710 S-216 J-4 250.00 0.14 2.92 0.03 29.27 1.66 4.21 5.75 0.00 24.21 0.00 24.42 1.81 20.15 20.05 20.03 U 1 2.92 0.048 24.12	534+20	51.00 Rt.	S-214	. •	102.00					0.00	0.00	0.20			0.00					0.20	18.00		2.92	3		
J-4 250.00 0.14 2.92 0.03 29.27 1.66 4.21 5.75 0.00 24.21 0.00 24.42 1.81 20.15 20.03 1 0.048 24.12													2.23													
	<u> </u>			.1-4	250.00				29 27	1 66	4 21	5.75	0.00	24.21	0.00	24 42	1.81							24 12		
	536+40	51.00 l t	S-218									33			0.00					0.12	- 1					

Units: ENGLISH HGL method: Standard FDOT (Jump HGL to pipe crown).

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Financial Prj Id: 21151201.00 County: OKECHOBEE Network: POND2 Designed by AD Date: 2/18/2014
Description: NEW ALIGNMENT Organization WANTMAN GROUP State Road: SR 710 Checked by: PAT Date: 2/18/2014

LOCA	TION	STR.	TYPE	LEN.	AREA	S (Ac)	SUB-	TIME	TIME	INTEN	TOTAL	BASE	TOTAL	MINOR	INLET	HGL	HYDRA	ULIC GR	ADE	# PIPE	SLOPE	ACTUAL	FULL	NOTES & REM	//ARKS
OF		NO.	OF		C=		TOTAL		OF				FLOW					ROWN		B SIZE	%	VEL.		ZONE:	8
UPPER	REND		STR.		C=	0.20	(C*A)	CONC	FLOW		` ′	SUMM	1				FL	OWLINE		R (in.)	HGL	PHYS.	CAP.	FREQ. (Yrs):	3
ALIGNMEN	NT NAME	UPPER			C=	0.00			SECT.			BASE					UPPER	LOWER	FALL	L RISE	PHYS	VEL.		MANNINGS n:	0.0120
STATION	DIST SD	LOWER		(ft.)	INC	TOTAL		(min)	(min)	(in/hr)		(cfs)	(cfs)	(ft.)	(ft.)	(ft.)	(ft.)	(ft.)	(ft.)	S SPAN	MIN.	(fps)	(cfs)	TAILW EL (ft):	21.50
CL7	10	S-217			0.48	0.48	0.46										22.69	22.61	0.08	18.00	0.081	1.83			
			P-4	102.00	0.18	0.18	0.04	10.00	0.85	6.58	0.49	0.00	3.23	0.00	24.42	1.73	21.31	21.11		1	0.196	-	5.14		
536+40	51.00 Rt.	S-216			0.00	0.00	0.00					0.00					19.81	19.61	0.20	18.00	0.150	2.91			
CL7	10	S-218			0.00	5.44	0.00										22.48	22.37	0.12	42.00	0.047	2.45			
			MH-7J	250.00	0.00	2.92	0.00	30.92	1.70	4.09	5.75	0.00	23.55	0.00	25.17	2.69	20.03	19.91		1	0.048		24.12		
538+90	51.00 Lt.	S-219			0.00	0.00	0.00					0.00					16.53	16.41	0.12	42.00	0.048	2.51			
CL7	10	S-219			0.57	6.62	0.54										22.37	22.20	0.17	42.00	0.064	2.87			
			J-4	260.00	0.15	3.17	0.03	32.62	1.51	3.98	6.92	0.00	27.58	0.00	24.42	2.05	19.91	19.73		1	0.069		28.96		
541+40	51.00 Lt.	S-221			0.00	0.00	0.00					0.00					16.41	16.23	0.18	42.00	0.048	3.01			
CL7	10	S-220			0.61	0.61	0.58										22.49	22.37	0.12	18.00	0.121	2.24			
			P-4	102.00	0.11	0.11	0.02	10.00	0.76	6.58	0.60	0.00	3.95	0.00	24.42	1.93	21.31	21.11		1	0.196		5.14		
541+40	51.00 Rt.	S-219			0.00	0.00	0.00		·			0.00					19.81	19.61	0.20	18.00		2.91			
CL7	10	S-221			0.00	6.62	0.00										22.20	22.05	0.15	42.00	0.061	2.80			
			MH-7J	250.00	0.00	3.17	0.00	34.14	1.49	3.89	6.92	0.00	26.93	0.00	25.20	3.00	19.73	19.55		1	0.072		29.54		
544+00	51.00 Lt.	S-222			0.00	0.00	0.00					0.00					16.23	16.05	0.18	42.00	0.048	3.07			
CL7		S-222			0.56	7.78	0.53										22.05	21.95	0.10	48.00	0.039				
			J-4	250.00	0.15	3.42	0.03	35.62	1.71	3.80	8.08	0.00	30.71	0.00	24.45	2.40	20.05	19.87		1	0.072		42.18		
546+50	51.00 Lt.	S-224			0.00	0.00	0.00					0.00					16.05	15.87	0.18	48.00	$\overline{}$	3.36			
CL7	10	S-223			0.60	0.60	0.57										22.17	22.05	0.12	18.00	0.117	2.20			
		_	P-4	102.00	0.10	0.10	0.02	10.00	0.77	6.58	0.59	0.00	3.89	0.00	24.45	2.28	21.34	21.14		1	0.196		5.14		
546+50	51.00 Rt.	S-222			0.00	0.00	0.00		•			0.00					19.84	19.64	0.20	18.00		2.91			
CL7		S-224			0.00	7.78	0.00										21.95	21.86		48.00					
		_	MH-7J	250.00	0.00	3.42	0.00	37.33	1.75	3.71	8.08	0.00	29.94	0.00	25.20	3.25	19.87	19.69		1	0.072	_	42.18		
549+00	51.00 Lt.	S-225			0.00	0.00	0.00					0.00					15.87	15.69	0.18	48.00		3.36			
CL7		S-225			0.62	9.00	0.59										21.86	21.72		48.00		-			_
	1		J-4	300.48	0.16	3.75	0.03	39.08	1.87	3.62	9.30	0.00	33.62	0.00	24.45	2.59	19.69	19.51		1	0.060		38.44		
551+50	51.00 Lt.	S-227		0000	0.00	0.00	0.00	00.00		0.02	0.00	0.00	00.02	0.00			15.69	15.51	0.18	48.00		3.06			
CL7		S-226			0.60	0.60	0.57										21.98	21.86		18.00		-			-
-			P-4	102.00	0.17	0.17	0.03	10.00	0.76	6.58	0.60	0.00	3.97	0.00	24.45	2.47	21.34	21.14		1	0.196		5.14		
551+50	51.00 Rt.	S-225			0.00	0.00	0.00		3 3	0.00	0.00	0.00		0.00			19.84	19.64	0.20	18.00		2.91	J		
CL7		S-227			0.34	9.64	0.32					1					21.72	21.56		48.00		2.79			_
-	1		J-3	301.83		3.95	0.02	40 95	1.80	3.52	9.95	0.00	35.04	0.00	25.35	3.63	19.51	19.33		1	0.060	•	38.39		
554+50	51.40 Lt.	S-229			0.00	0.00	0.00			0.02	0.00	0.00		0.00			15.51	15.33	0.18	48.00		3.05	20.00		
CL7		S-228			0.30	0.30	0.29					0.00					22.07	22.04		18.00		-			-
<u> </u>	-		P-3	102.00	0.11	0.11	0.02	10.00	0.85	6.58	0.31	0.00	2.02	0.00	25.35	3.28	22.24	22.04		1	0.196		5.15		
554+50	50.60 Rt.	S-227	' "	102.00	0.00	0.00	0.00	10.00	0.00	0.50	0.01	0.00	2.02	0.00	20.00	0.20	20.74	20.54	0.20	18.00		2.92	0.10		
CL7		S-229			0.34	20.87	0.32					0.00					21.56	21.50	0.06	60.00					-
	1 1		J-3	94.62	0.09	7.60	0.02	42.75	0.00	3.44	21.35	0.00	73.36	0.00	26.25	4.69	20.33	20.23	0.00	1	0.106	<u> </u>	93.22		
557+50	51.30 Lt.	POND2		34.02	0.00	0.00	0.02	72.13	0.00	5.44	21.00	0.00	, 5.50	0.00	20.23	7.03	15.33	15.23	0.10	60.00		4.75	JJ.22		
CL7		S-230			0.30	0.30	0.00					0.00					22.61	21.91		18.00					-
OL7	1	3 200	P-3	102.00	0.30	0.11	0.23	10.00	0.39	6.58	0.31	0.00	2.02	0.00	26.25	3.64	23.64	22.94	0.70	1 10.00	0.686	7.00	9.64		
557+50	50.70 Rt.	S-220		102.00	0.00			10.00	0.59	0.56	0.51	0.00	2.02	0.00	20.23	3.04	22.14		0.70	18.00		5.46	3.04		
JJ1 TJU	30.70 KL	3-229	l		0.00	0.00	0.00				1	0.00	1	l	l	1	42.14	41.44	0.70	10.00	0.150	J.40			

Units: ENGLISH HGL method: Standard FDOT (Jump HGL to pipe crown).

Financial Prj Id: 21151201.00 County: OKECHOBEE Network: POND2 Designed by AD Date: 2/18/2014
Description: NEW ALIGNMENT Organization WANTMAN GROUP State Road: SR 710 Checked by: PAT Date: 2/18/2014

LOCA	TION	STR.	TYPE	LEN.	AREA	S (Ac)	SUB-	TIME	TIME	INTEN	TOTAL	BASE	TOTAL	MINOR	INLET	HGL	HYDRA	ULIC GR	ADE	# PIPE	SLOPEA	CTUAL	FULL	NOTES & REN	MARKS
OF	F	NO.	OF		C=		TOTAL		OF							CLEAR		ROWN		B SIZE	%	VEL.		ZONE:	8
UPPER	REND		STR.		C=	0.20	(C*A)	CONC	FLOW		, ,	SUMM					FL	OWLINE		R (in.)	HGL	PHYS.	CAP.	FREQ. (Yrs):	3
ALIGNMEN	NT NAME	UPPER			C=	0.00			SECT.			BASE					UPPER	LOWER	FALL	L RISE	PHYS	VEL.		MANNINGS n:	0.0120
STATION	DIST SD	LOWER		(ft.)	INC	TOTAL		(min)	(min)	(in/hr)		(cfs)	(cfs)	(ft.)	(ft.)	(ft.)	(ft.)	(ft.)	(ft.)	S SPAN	MIN.	(fps)	(cfs)	TAILW EL (ft):	21.50
CL7	10	S-231			0.34	10.59	0.32										23.45	23.23	0.22	48.00	0.072	3.33			
			J-3	301.83	0.09	3.45	0.02	34.11	1.51	3.89	10.75	0.00	41.83	0.00	27.15	3.70	23.43	23.23		1	0.066	-	40.46		
560+50	51.20 Lt.	S-229			0.00	0.00	0.00					0.00					19.43	19.23	0.20	48.00	0.041	3.22			
CL7	10	S-232			0.30	0.30	0.29										23.87	23.84	0.03	18.00	0.032	1.15			
			P-3	102.00	0.11	0.11	0.02	10.00	0.85	6.58	0.31	0.00	2.02	0.00	27.15	3.28	24.04	23.84		1	0.196		5.15		
560+50	50.80 Rt.	S-231			0.00	0.00	0.00					0.00					22.54	22.34	0.20	18.00	0.150	2.92			
CL7	10	S-233			0.00	9.95	0.00										23.65	23.45	0.20	48.00	0.067	3.21			
			MH-7J	301.83	0.00	3.24	0.00	32.54	1.57	3.99	10.10	0.00	40.29	0.00	28.05	4.40	23.63	23.43		1	0.066		40.43		
563+50	51.20 Lt.	S-231			0.00	0.00	0.00					0.00					19.63	19.43	0.20	48.00	0.041	3.22			
CL7	10	S-234			0.62	9.95	0.59										23.83	23.65	0.18	48.00	0.070	3.27			
			J-4	251.01	0.16	3.24	0.03	31.27	1.28	4.07	10.10	0.00	41.13	0.00	27.30	3.47	23.78	23.63		1	0.060		38.43		
566+00	51.00 Lt.	S-233			0.00	0.00	0.00					0.00					19.78	19.63	0.15	48.00	0.041	3.06			
CL7	10	S-235			0.55	0.55	0.52										24.10	23.99	0.11	18.00	0.107	2.11			
			P-4	102.00	0.22	0.22	0.04	10.00	0.81	6.58	0.57	0.00	3.72	0.00	27.30	3.20	24.19	23.99		1	0.196		5.14		
566+00	51.00 Rt.	S-234			0.00	0.00	0.00					0.00					22.69	22.49	0.20	18.00	0.150	2.91			
CL7		S-236			0.00	8.78	0.00										24.17	23.83	0.35	42.00	0.116				
			MH-7J	298.15	0.00	2.87	0.00	29.98	1.29	4.16	8.91	0.00	37.08	0.00	28.20	4.03	23.82	23.28		1	0.181	_	46.78		
569+00	51.00 Lt.	S-234			0.00	0.00	0.00					0.00					20.32	19.78	0.54	42.00		4.86			
CL7		S-237			0.73	8.78	0.69										24.47	24.17	0.30	42.00		3.92			-
				248.46	0.19	2.87	0.04	28.92	1.06	4.24	8.91	0.00	37.75	0.00	27.45	2.98	23.94	23.82		1	0.048		24.20		
571+50	51.00 Lt.	S-236			0.00	0.00	0.00					0.00					20.44	20.32	0.12	42.00		2.52			
CL7		S-238			0.65	0.65	0.62										24.62	24.47	0.15	18.00		2.49			-
			P-4	102.00	0.26	0.26	0.05	10.00	0.68	6.58	0.67	0.00	4.40	0.00	27.45	2.83	24.84	24.14		1	0.686		9.62		
571+50	51.00 Rt.	S-237		.02.00	0.00	0.00	0.00	10.00	0.00	0.00	0.0.	0.00		0.00			23.34	22.64	0.70	18.00		5.44	0.02		
CL7		S-239			0.00	7.40	0.00										24.83	24.47	0.36	42.00		3.42			-
				397.52	0.00	2.42	0.00	26.99	1.94	4.38	7.51	0.00	32.93	0.00	28.65	3.82	24.13	23.94		1	0.048		23.98		
575+50	51.00 Lt.	S-237		001.02	0.00	0.00	0.00	20.00				0.00	02.00	0.00	20.00	0.02	20.63	20.44	0.19	42.00		2.49	_0.00		
CL7		S-240			0.68	7.40	0.65					0.00					25.12	24.83		42.00	0.096	3.51			
<u> </u>			J-4	299.04	0.17	2.42	0.03	25 57	1.42	4.50	7.51	0.00	33.79	0.00	27.75	2.63	24.27	24.13		1	0.047		23.78		
578+50	51.00 Lt.	S-239	• .	-00.0	0.00	0.00	0.00					0.00	300	0.00	0		20.77	20.63	0.14	42.00		2.47	_0 0		
CL7		S-241			0.60	0.60	0.57					2.23					25.15	25.12	0.03	24.00		1.29			_
-			P-4	102.00	0.23	0.23	0.05	10.00	0.85	6.58	0.62	0.00	4.06	0.00	27.75	2.60	25.10	24.90		1	0.196		11.07		
578+50	51.00 Rt.	S-240			0.00	0.00	0.00		0.00	0.00	0.02	0.00		0.00	0		23.10	22.90	0.20	24.00		3.52			
CL7		S-242		 	0.34	6.12	0.32					0.00					25.33	25.12		42.00					
<u> </u>	_		J-3	300.00	0.09	2.01	0.02	23 90	1.67	4.64	6.22	0.00	28.86	0.00	28.65	3.32	25.17	24.27		1	0.300		60.25		
581+50	51.00 Lt.	S-240		300.00	0.00	0.00	0.02	20.00	1.07	7.04	0.22	0.00	_0.00	0.00	20.00	3.02	21.67	20.77	0.90	42.00		6.26	50.25		
CL7		S-243			0.30	0.30	0.29					0.00					25.37	25.34	0.03	18.00		1.15			-
		20	P-3	102.00	0.12	0.12	0.02	10.00	0.85	6.58	0.31	0.00	2.03	0.00	28.65	3.28	26.04	25.34	0.00	1	0.686		9.64		
581+50	51.00 Rt.	S-242	1 -3	102.00	0.12	0.12	0.02	10.00	0.03	0.55	0.51	0.00	2.03	0.00	20.00	3.23	24.54	23.84	0.70	18.00		5.46	3.04		
CL7		S-244		+ +	0.00	5.48	0.00					0.00				 	25.51	25.33		42.00		2.78			-
JE7		3 2 7 7	J-3	300.00	0.20	1.81	0.27	22 10	1.80	4.81	5.57	0.00	26.79	0.00	29.55	4 04	25.81	25.17	0.10	1 42.00	0.213		50.85		
584+50	51.00 Lt.	S-242		300.00	0.07		0.00	22.10	1.00	4.01	3.37	0.00	20.79	0.00	29.55	7.04	22.31	21.67	0.64				50.05		
JU4TJU	31.00 Lt.	3-242	l		0.00	0.00	0.00	1	l		1	0.00	l	l		1	44.01	21.07	0.04	42.00	0.040	5.23			

Units: ENGLISH HGL method: Standard FDOT (Jump HGL to pipe crown).

Financial Prj Id: 21151201.00 County: OKECHOBEE Network: POND2 Designed by AD Date: 2/18/2014
Description: NEW ALIGNMENT Organization WANTMAN GROUP State Road: SR 710 Checked by: PAT Date: 2/18/2014

LOCA	TION	STR.	TYPE	LEN.	AREA	S (Ac)	SUB-	TIME	TIME	INTEN	TOTAL	BASE	TOTAL	MINOR	INLET	HGL	HYDRA	ULIC GR	ADE	# PIPE	SLOPE	CTUAL	FULL	NOTES & REM	//ARKS
OF	F	NO.	OF		C=		TOTAL		OF				FLOW					ROWN		B SIZE	%	VEL.		ZONE:	8
UPPER	REND		STR.		C=	0.20	(C*A)	CONC	FLOW		` ′	SUMM	1				FL	OWLINE		R (in.)	HGL	PHYS.	CAP.	FREQ. (Yrs):	3
ALIGNMEN	NT NAME	UPPER			C=	0.00			SECT.			BASE					UPPER	LOWER	FALL	L RISE	PHYS	VEL.		MANNINGS n:	0.0120
STATION	DIST SD	LOWER		(ft.)	INC	TOTAL		(min)	(min)	(in/hr)		(cfs)	(cfs)	(ft.)	(ft.)	(ft.)	(ft.)	(ft.)	(ft.)	S SPAN	MIN.	(fps)	(cfs)	TAILW EL (ft):	21.50
CL7	'10	S-245			0.25	0.25	0.24		·								26.26	26.24	0.02	18.00	0.022	0.96			_
			P-3	102.00	0.10	0.10	0.02	10.00	0.85	6.58	0.26	0.00	1.69	0.00	29.55	3.29	26.94	26.24		1	0.686		9.64	l	
584+50	51.00 Rt.	S-244			0.00	0.00	0.00					0.00					25.44	24.74	0.70	18.00	0.150	5.46		l	
CL7		S-246			0.00	4.95	0.00										25.94	25.81	0.13	42.00	0.053	2.60			_
			MH-7.J	250.00	0.00	1.64	0.00	20.50	1 60	4.98	5.03	0.00	25.03	0.00	30.30	4.36	25.93	25.81		1	0.048		24.15	l	
587+00	51.00 Lt.	S-244			0.00	0.00	0.00					0.00					22.43	22.31	0.12	42.00		2.51		l	
CL7		S-247			0.67	4.95	0.64					0.00					26.11	25.94		42.00		2.71			-
		V =	J-4	290.00	0.17	1.64	0.03	18 72	1.79	5.18	5.03	0.00	26.03	0.00	29.54	3 44	26.07	25.93	0	1	0.048		24.16	l	
589+90	51.00 Lt.	S-246	0 4	230.00	0.00	0.00	0.00	10.72	1.75	0.10	0.00	0.00	20.00	0.00	25.54	0.44	22.57	22.43	0.14	42.00		2.51	24.10	l	
CL7		S-248			0.59	0.59	0.56					0.00					26.36	26.23	0.13	18.00		2.30			-
OL7	10	0-240	P-4	100.00				10.00	0.74	C EO	0.60	0.00	4.06	0.00	29.54	2 10			0.13	10.00	0.686	2.50	9.62	I	
500.00	54 00 D4	0.047	P-4	102.00	0.28	0.28	0.06	10.00	0.74	6.58	0.62	0.00	4.06	0.00	29.54	3.10	26.93	26.23	0.70	1 40.00		- 11	9.62	l	
589+90	51.00 Rt.				0.00	0.00	0.00					0.00					25.43	24.73	0.70	18.00		5.44			
CL7	10	S-249			0.34	3.69	0.32						40.00			4.00	26.70	26.11	0.59	30.00		8.80		l	
		0 0 1 =	P-3	300.00	0.09	1.18	0.02	18.15	0.57	5.24	3.74	0.00	19.62	0.00	30.73	4.03	28.04	25.07		1	0.990		44.51	l	
592+90	51.00 Lt.				0.00	0.00	0.00					0.00					25.54	22.57	2.97	30.00		9.07		<u> </u>	
CL7	'10	S-250			0.30	0.30	0.29										27.33	27.18	0.15	18.00		2.45		I	
			P-3	102.00	0.12	0.12	0.02	10.00	0.69	6.58	0.31	0.00	2.03	0.00	30.73	3.40	28.12	27.97		1	0.147		4.43	l	
592+90	51.00 Rt.	S-249			0.00	0.00	0.00					0.00					26.62	26.47	0.15	18.00	0.150	2.51		ļ	
CL7	'10	S-251			0.21	3.05	0.20										27.95	27.05	0.90	30.00		5.36		l	
			P-3	300.00	0.06	0.98	0.01	17.22	0.93	5.36	3.09	0.00	16.58	0.00	32.23	4.28	28.94	28.04		1	0.300		24.46	l	
595+90	51.00 Lt.	S-249			0.00	0.00	0.00					0.00					26.44	25.54	0.90	30.00	0.076	4.98		l	
CL7	'10	S-252			0.19	2.84	0.18										29.07	28.94	0.13	30.00	0.124	3.19			
		_	P-3	102.00	0.07	0.92	0.01	16.68	0.53	5.43	2.88	0.00	15.65	0.00	32.23	3.16	29.02	28.94		1	0.078	-	12.63	l	
595+90	51.00 Rt.	S-251			0.00	0.00	0.00					0.00					26.52	26.44	0.08	30.00	0.076	2.57		l	
CL7		S-253			0.00	2.65	0.00										29.28	29.07	0.21	30.00					_
			MH-7	183.90	0.00	0.85	0.00	15.68	1.01	5.57	2.69	0.00	14.96	0.00	32.70	3 42	29.16	29.02		1	0.076		12.36	l	
597+78	51.00 Rt.	S-252	1411 1 7	100.50	0.00	0.00	0.00	10.00	1.01	0.01	2.00	0.00	14.50	0.00	02.70	0.72	26.66	26.52	0.14	30.00		2.52	12.00	l	
CL7		S-254			0.65	0.65	0.62					0.00					29.74	29.60	0.15	18.00					
JE7		3 204	P-4	102.00	0.18	0.18	0.02	10.00	0.70	6.58	0.65	0.00	4.30	0.00	32.05	2 31	29.44	29.29	0.10	1 10.00	0.147	25	4.43	l	
600+50	51.00 Lt.	S-255	F -4	102.00	0.10	0.10	0.04	10.00	0.70	0.56	0.03	0.00	4.50	0.00	32.03	2.51	27.94	27.79	0.15	18.00		2.51	4.43	l	
CL7		S-255		+	0.57	2.65	0.54					0.00					29.60	29.28	0.13	30.00		3.16			-
J.	10	J-233	P-4	265.66		0.85		14 20	1 10	E 70	2.60	0.00	15 53	0.00	32.05	2 45			0.52	1 30.00	0.122	3.10	12.26	l	
600.50	51.00 Rt.	0.050	P-4	∠05.00	0.21		0.04	14.28	1.40	5.78	2.69	1	15.53	0.00	32.05	2.43	29.36	29.16	0.00	20.00		2.50	12.20	İ	
600+50				-	0.00	0.00	0.00					0.00					26.86	26.66		30.00		2.50			_
CL7	10	S-256	D. ^	400.00	0.34	0.34	0.32	40.00		0		0.00	0.0-	0.00	00.05	0.70	30.23	30.19	0.04	18.00	_	1.27	4	l	
	=4.00	0.055	P-3	102.00	0.09	0.09	0.02	10.00	0.85	6.58	0.34	0.00	2.25	0.00	32.95	2.72	30.34	30.19		1	0.147		4.43	l	
603+50	51.00 Lt.				0.00	0.00	0.00					0.00					28.84	28.69		18.00		2.51		 	_
CL7	10	S-257			0.30	1.43	0.29										29.98	29.60	0.38	24.00		2.80		l	
			P-3	292.96	0.11	0.46	0.02	12.53	1.74	6.07	1.45	0.00	8.80	0.00	32.95	2.97	30.30	28.86		1	0.492		17.27	l	
603+50	51.00 Rt.				0.00	0.00	0.00					0.00					28.30	26.86		24.00					
CL7	10	S-258		T	0.42	0.42	0.40										31.15	31.09	0.06	18.00		1.57			
		-	P-3	102.00	0.11	0.11	0.02	10.00	0.85	6.58	0.42	0.00	2.78	0.00	33.85	2.70	31.24	31.09		1	0.147		4.43	l	
606+50	51.00 Lt.	S-259			0.00	0.00	0.00					0.00					29.74	29.59	0.15	18.00	0.150	2.51		<u> </u>	

Units: ENGLISH HGL method: Standard FDOT (Jump HGL to pipe crown).

Financial Prj Id: 21151201.00 County: OKECHOBEE Network: POND2 Designed by AD Date: 2/18/2014
Description: NEW ALIGNMENT Organization WANTMAN GROUP State Road: SR 710 Checked by: PAT Date: 2/18/2014

LOCAT	TION		STR.	TYPE	LEN.	AREA	AS (Ac)	SUB-	TIME	TIME	INTEN	TOTAL	BASE	TOTAL	MINOR	INLET	HGL	HYDRA	ULIC GR	ADE	# PIPE	SLOPE	ACTUAL	FULL	NOTES & REN	MARKS
OF	=		NO.	OF		C=	0.95	TOTAL	OF	OF		(C*A)	FLOW	FLOW	LOSS	ELEV.	CLEAR	C	ROWN		B SIZE	%	VEL.	FLOW	ZONE:	8
UPPER	REND			STR.		C=	0.20	(C*A)	CONC	FLOW			SUMM					FL	OWLINE		R (in.)	HGL	PHYS.	CAP.	FREQ. (Yrs):	3
ALIGNMEN	NT NAME	ΕŪ	UPPER			C=	0.00			SECT.			BASE					UPPER	LOWER	FALL	L RISE	PHYS	VEL.	Ī	MANNINGS n:	0.0120
STATION	DIST	SDL	LOWER		(ft.)	INC	TOTAL		(min)	(min)	(in/hr)		(cfs)	(cfs)	(ft.)	(ft.)	(ft.)	(ft.)	(ft.)	(ft.)	SPAN	MIN.	(fps)	(cfs)	TAILW EL (ft):	21.50
CL7	10		S-259			0.37	0.79	0.35										30.93	30.34	0.59	18.00	0.203	2.90			
			_	P-3	292.96	0.14	0.25	0.03	10.85	1.68	6.39	0.80	0.00	5.12	0.00	33.85	2.92	31.09	30.34		1	0.256	-	5.79		
606+50	51.00	Rt.	S-257			0.00	0.00	0.00					0.00					29.59	28.84	0.75	18.00	0.150	3.27			

Units: ENGLISH

Financial Prj Id: 21151201.00 County: OKECHOBEE Network: POND3 Designed by AD Date: 2/18/2014
Description: NEW ALIGNMENT Organization WANTMAN GROUP State Road: SR 710 Checked by: PAT Date: 2/18/2014

LOCA	TION	STR.	TYPE	LEN.	AREA	S (Ac)	SUB-	TIME	TIME	INTEN	TOTAL	BASE	TOTAL	MINOR	INLET	HGL	HYDRA	ULIC GR	ADE	# PIPE	SLOPE	CTUAL	FULL	NOTES & REN	MARKS
OF	F	NO.	OF		C=		TOTAL		OF					LOSS				ROWN		B SIZE	%	VEL.		ZONE:	8
UPPER	REND		STR.		C=	0.20	(C*A)	CONC	FLOW		` ′	SUMM					FL	OWLINE		R (in.)	HGL	PHYS.	CAP.	FREQ. (Yrs):	2
ALIGNMEN	NT NAME	UPPER			C=	0.00			SECT.			BASE					UPPER	LOWER	FALL	L RISE	PHYS	VEL.		MANNINGS n:	0.0120
STATION	DIST SD	LOWER		(ft.)	INC	TOTAL		(min)	(min)	(in/hr)		(cfs)	(cfs)	(ft.)	(ft.)	(ft.)	(ft.)	(ft.)	(ft.)	S SPAN	MIN.	(fps)	(cfs)	TAILW EL (ft):	25.92
CL7	10	S-300			0.34	0.64	0.32										30.95	30.59	0.36	18.00	0.118	2.22			
		-	P-3	306.59	0.09	0.21	0.02	10.85	2.31	6.03	0.65	0.00	3.91	0.00	34.06	3.11	31.30	30.55		1	0.245	-	5.66		
613+20	51.00 Lt.	S-302			0.00	0.00	0.00					0.00					29.80	29.05	0.75	18.00	0.150	3.20			
CL7	10	S-301			0.30	0.30	0.29										31.33	31.30	0.03	18.00	0.028	1.08			
			P-3	102.00	0.11	0.11	0.02	10.00	0.85	6.21	0.31	0.00	1.91	0.00	34.06	2.73	31.45	31.30		1	0.147	-	4.43		
613+20	51.00 Rt.	S-300			0.00	0.00	0.00					0.00					29.95	29.80	0.15	18.00	0.150	2.51			
CL7	10	S-302			0.34	0.98	0.32										30.59	30.35	0.24	18.00	0.237	3.13			
			P-3	102.00	0.09	0.30	0.02	13.16	0.54	5.59	0.99	0.00	5.54	0.00	33.16	2.57	30.55	30.35		1	0.196		5.11		
616+20	51.00 Lt.	S-303			0.00	0.00	0.00					0.00					29.05	28.85	0.20	18.00	0.150	2.89			
CL7	10	S-303			0.30	1.28	0.29										30.05	29.87	0.18	24.00	0.085	2.27			
			P-3	208.08	0.11	0.42	0.02	13.70	1.53	5.50	1.30	0.00	7.14	0.00	33.16	3.11	30.51	29.87		1	0.308		13.69		
616+20	51.00 Rt.	S-305			0.00	0.00	0.00					0.00					28.51	27.87	0.64	24.00	0.102	4.36			
CL7	10	S-304			0.24	0.24	0.23										29.78	29.76	0.02	18.00	0.017	0.85			
			P-3	102.00	0.07	0.07	0.01	10.00	0.85	6.21	0.24	0.00	1.50	0.00	32.52	2.74	29.91	29.76		1	0.147		4.43		
618+33	51.00 Lt.	S-305			0.00	0.00	0.00					0.00					28.41	28.26	0.15	18.00	0.150	2.51			
CL7		S-305			0.22	1.74	0.21										29.43	29.14	0.29	24.00	0.143	2.95			
			P-3	202.22	0.07	0.56	0.01	15.22	1.14	5.26	1.76	0.00	9.28	0.00	32.52	3.09	29.87	28.17		1	0.841		22.64		
618+33	51.00 Rt.	S-307			0.00	0.00	0.00					0.00					27.87	26.17	1.70	24.00		7.21			
CL7		S-306			0.75	0.75	0.71										29.36	29.19	0.17	18.00		2.61			
		-	P-4	102.00	0.14	0.14	0.03	10.00	0.65	6.21	0.74	0.00	4.60	0.00	31.90	2.54	29.34	29.19		1	0.147		4.43		
620+40	51.00 Lt.	S-307			0.00	0.00	0.00					0.00					27.84	27.69	0.15	18.00		2.51			
CL7		S-307			0.46	2.95	0.44										29.14	29.03	0.11	36.00		2.15			-
			P-4	244.19	0.17	0.87	0.03	16 37	1.90	5.10	2.98	0.00	15.18	0.00	31.90	2.76	29.17	29.03		1	0.057		17.41		
620+40	51.00 Rt.	S-308			0.00	0.00	0.00			0	2.00	0.00		0.00	00		26.17	26.03	0.14	36.00		2.46			
CL7		S-308			0.00	2.95	0.00										28.98	28.88		36.00		2.05			
			MH-7	253.95	0.00	0.87	0.00	18.26	2.07	4.86	2.98	0.00	14.46	0.00	32.65	3.67	29.03	28.88		1	0.059		17.61		
622+90	51.00 Rt.	S-310		200.00	0.00	0.00	0.00	. 0.20				0.00		0.00	02.00	0.01	26.03	25.88	0.15	36.00		2.49			
CL7		S-309			0.57	0.57	0.54					0.00					29.21	29.11	0.10	18.00		2.02			_
<u> </u>	_		P-4	102.00	0.16	0.16	0.03	10.00	0.84	6.21	0.57	0.00	3.56	0.00	31.87	2.66	29.26	29.11		1	0.147		4.40		
625+50	51.00 Lt.	S-310	' '	. 52.55	0.00	0.00	0.00	. 5.55	0.01	J.2.	3.07	0.00		0.00	0		27.76	27.61	0.15	18.00		2.49	0		
CL7		S-310			0.51	4.03	0.48					0.00					28.85	28.68	0.17	36.00		2.67			_
<u> </u>	_		P-4	244.19	0.19	1.22	0.04	20.33	1.53	4.63	4.07	0.00	18.84	0.00	31.87	3.02	28.88	28.68		1	0.082		20.74		
625+50	51.00 Rt.	S-311			0.00	0.00	0.00	_0.00	1.00	1.00		0.00	.0.04	0.00	31.07	0.01	25.88	25.68	0.20	36.00		2.93	_0., +		
CL7		S-311			0.00	4.03	0.00					0.00					28.67	28.48		36.00		2.58			-
				292.96	0.00	1.22	0.00	21.86	1 90	4.47	4.07	0.00	18.21	0.00	32.62	3.95	28.68	28.48	05	1 33.30	0.068		18.98		
628+00	51.00 Rt.	S-313	IVII 1-7	232.30	0.00	0.00	0.00	21.00	1.30	7.7/	7.07	0.00	10.21	0.00	32.02	3.33	25.68	25.48	0.20	36.00		2.68	10.50		
CL7		S-312			0.34	6.24	0.32					0.00					27.15	26.95		42.00		5.22			_
J			P-3	101.23	0.09	2.52	0.02	24.39	0.00	4.24	6.43	0.00	27.28	0.00	31.62	4 47	28.78	28.58	0.20	1 -2.50	0.198		48.81		
631+00	51.00 Lt.	BUND3		101.23	0.09	0.00	0.02	24.39	0.00	4.24	0.43	0.00	21.20	0.00	31.02	7.7/	25.28	25.08	0.20	42 00	0.198		-0.01		
CL7		S-313		 	0.30	4.33	0.00					0.00					28.35	28.28		36.00		2.66			_
JE7		5 5 . 5	P-3	102.00		1.33	0.02	23.75	0.64	4.30	4.38	0.00	18 92	0.00	31 62	3 27	28.48	28.28	0.07	1 30.00	0.196		32.48		
631+00	51.00 Rt.	C 212		102.00	0.11			23.15	0.04	4.30	4.30	0.00	10.02	0.00	31.02	3.21	25.48		0.20	36.00			JZ.40		
031+00	31.00 Kl.	3-312			0.00	0.00	0.00					0.00	l	l	l		20.40	25.28	0.20	30.00	0.059	4.59			

Units: ENGLISH HGL method: Standard FDOT (Jump HGL to pipe crown).

Financial Prj Id: 21151201.00 County: OKECHOBEE Network: POND3 Designed by AD Date: 2/18/2014
Description: NEW ALIGNMENT Organization WANTMAN GROUP State Road: SR 710 Checked by: PAT Date: 2/18/2014

LOCAT	ION	STR.	TYPE	LEN.	AREA	S (Ac)	SUB-	TIME	TIME	INTEN	TOTAL	BASE	TOTAL	MINOR	INLET	HGL	HYDRA	ULIC GR	ADE	# PI	PE SLOI	PEACTUA	AL FULL	NOTES & REM	MARKS
OF		NO.	OF		C=	0.95	TOTAL	OF	OF		(C*A)	FLOW	FLOW	LOSS	ELEV.	CLEAR	С	ROWN		B SI	ZE %	VEL.	FLOW	ZONE:	8
UPPER	END		STR.		C=	0.20	(C*A)	CONC	FLOW			SUMM					FL	OWLINE		R (ir	.) HG	L PHYS	. CAP.	FREQ. (Yrs):	2
ALIGNMEN [*]	T NAME	UPPER			C=	0.00			SECT.			BASE					UPPER	LOWER	FALL	L RI	SE PHY	S VEL.		MANNINGS n:	0.0120
STATION	DIST	DLOWER		(ft.)	INC	TOTAL		(min)	(min)	(in/hr)		(cfs)	(cfs)	(ft.)	(ft.)	(ft.)	(ft.)	(ft.)	(ft.)	S SP	AN MIN	I. (fps)	(cfs)	TAILW EL (ft):	25.92
CL71	10	S-314			0.34	1.57	0.32										27.61	27.15	0.46	24	00 0.15	3.06	i		
			P-3	301.72	0.13	1.10	0.03	12.98	1.64	5.62	1.71	0.00	9.61	0.00	30.12	2.51	26.24	25.93		1	0.10)3	7.90		
634+00	51.00 L	t. S-312			0.00	0.00	0.00					0.00					24.24	23.93	0.31	24	00 0.10	2.51			
CL71	10	S-315			0.30	0.30	0.29										27.64	27.61	0.03	18	00 0.02	28 1.08	1		
			P-3	102.00	0.12	0.12	0.02	10.00	0.85	6.21	0.31	0.00	1.91	0.00	30.12	2.48	27.51	27.36		1	0.14	17	4.43		
634+00	51.00 F	Rt. S-314			0.00	0.00	0.00					0.00					26.01	25.86	0.15	18	00 0.15	2.51			
CL71	10	S-316			0.48	0.93	0.46										27.78	27.61	0.17	24	00 0.06	37 2.02	!		
			P-4	258.00	0.15	0.85	0.03	10.85	2.13	6.03	1.05	0.00	6.35	0.00	29.15	1.36	26.50	26.24		1	0.10)1	7.83		
636+58	51.00 L	.t. S-314			0.00	0.00	0.00					0.00					24.50	24.24	0.26	24	00 0.10	2.49)		
CL71	10	S-317			0.45	0.45	0.43										27.88	27.78	0.10	18	00 0.09	96 2.00)		
			P-4	102.00	0.70	0.70	0.14	10.00	0.85	6.21	0.57	0.00	3.53	0.00	29.15	1.26	26.54	26.39		1	0.14	17	4.43		
636+58	51.00 F	Rt. S-316			0.00	0.00	0.00					0.00					25.04	24.89	0.15	18	00 0.15	2.51			

Units: ENGLISH

Financial Prj Id: 21151201.00 County: OKECHOBEE Network: POND4 Designed by AD Date: 2/19/2014
Description: NEW ALIGNMENT Organization WANTMAN GROUP State Road: SR 710 Checked by: PAT Date: 2/19/2014

LOCA	TION	STR.	TYPE	LEN.	AREA	S (Ac)	SUB-	TIME	TIME	INTEN	TOTAL	BASE	TOTAL	MINOR	INLET	HGL	HYDRA	ULIC GR	ADE	# PIPE	SLOPE	ACTUAL	FULL	NOTES & REM	JARKS
OF		NO.	OF		C=	0.95	TOTAL	OF	OF		(C*A)	FLOW	FLOW	LOSS	ELEV.	CLEAR		CROWN		B SIZE	%	VEL.	FLOW	ZONE:	8
UPPER	REND		STR.		C=	0.20	(C*A)	CONC	FLOW		` ′	SUMM					FL	OWLINE		R (in.)	HGL	PHYS.	CAP.	FREQ. (Yrs):	3
ALIGNMEN	NT NAME	UPPER			C=	0.00			SECT.			BASE					UPPER	LOWER	FALL	L RISE	PHYS	VEL.		MANNINGS n:	0.0120
STATION	DIST SD	LOWER		(ft.)	INC	TOTAL		(min)	(min)	(in/hr)		(cfs)	(cfs)	(ft.)	(ft.)	(ft.)	(ft.)	(ft.)	(ft.)	S SPAN	MIN.	(fps)	(cfs)	TAILW EL (ft):	24.76
CL7	10	S-400			0.73	1.29	0.69										26.48	26.38	0.10	30.00	0.034	1.67		1	
			P-4	295.52	0.05	0.28	0.01	10.79	2.46	6.41	1.28	0.00	8.21	0.00	28.68	2.20	25.99	25.77		1	0.074	_	12.19	I	
641+00	51.00 Lt.	S-402			0.00	0.00	0.00					0.00					23.49	23.27	0.22	30.00	0.076	2.48		1	
CL7	10	S-401			0.56	0.56	0.53										26.59	26.48	0.11	18.00	0.111	2.15		 	
			P-4	102.00	0.22	0.22	0.04	10.00	0.79	6.58	0.58	0.00	3.80	0.00	28.68	2.09	26.07	25.92		1	0.147		4.43	I	
641+00	51.00 Rt.	S-400			0.00	0.00	0.00					0.00					24.57	24.42	0.15	18.00	0.150	2.51		1	
CL7	10	S-402			0.00	1.29	0.00										26.38	26.33	0.05	30.00	0.029	1.55		l	
			MH-7	167.93	0.00	0.28	0.00	13.25	1.40	5.94	1.28	0.00	7.61	0.00	29.45	3.07	25.77	25.64		1	0.077		12.48	I	
643+98	51.00 Lt.				0.00	0.00	0.00					0.00					23.27	23.14		30.00	0.076				
CL7	10	S-403			0.19	1.94	0.18										26.33	26.24	0.09	30.00	0.063	2.27		I	
			P-3	143.39	0.05	0.51	0.01	14.65	1.05	5.72	1.95	0.00	11.13	0.00	29.10	2.77	25.64	25.53		1	0.077		12.44	I	
645+69	51.00 Lt.				0.00	0.00	0.00					0.00					23.14	23.03	0.11	30.00				<u> </u>	
CL7	10	S-404			0.46	0.46	0.44										26.35	26.33	0.02	24.00	0.016	0.99		I	
			P-4	109.93		0.19	0.04	10.00	0.92	6.58	0.47	0.00	3.12	0.00	28.98	2.63	26.33	25.14		1	1.083		25.85	I	
646+10	51.00 Rt.				0.00	0.00	0.00					0.00					24.33	23.14		24.00				<u> </u>	
CL7	10	S-405			0.16	2.10	0.15										26.24	26.14	0.10	30.00		2.39		I	
			P-3	142.40		0.55	0.01	15.71	0.99	5.56	2.11		11.72	0.00	29.29	3.06	25.53	25.42		1	0.077		12.48	I	
647+15	51.00 Lt.				0.00	0.00	0.00					0.00					23.03	22.92	0.11	30.00	+			<u></u>	
CL7	10	S-406			0.00	2.10	0.00										26.14	26.01	0.13	30.00	_	1		I	
			MH-7	191.49		0.55	0.00	16.70	1.37	5.43	2.11		11.43	0.00	29.73	3.59	25.42	25.21		1	0.110	4	14.89	I	
648+60	51.00 Lt.				0.00	0.00	0.00					0.00					22.92	22.71	0.21	30.00					
CL7	10	S-407			0.20	0.20	0.19										26.03	26.01	0.01	18.00	0.014	1		I	
			P-3	102.00		0.08	0.02	10.00	0.85	6.58	0.21	0.00	1.35	0.00	29.14	3.12	26.54	25.84		1	0.686		9.64	I	
650+55	51.00 Rt.				0.00	0.00	0.00					0.00					25.04	24.34		18.00					
CL7	10	S-408			0.22	2.52	0.21										26.01	25.95	0.06	36.00		1.88		I	
			J-3	191.49		0.69	0.01	18.07	1.60	5.25	2.53	0.00	13.30	0.00	29.14	3.13	25.71	25.13		1	0.303		40.35	I	
650+55	51.00 Lt.				0.00	0.00	0.00					0.00					22.71	22.13							
CL7	10	S-409			0.50	3.47	0.47										25.90	25.75	0.15	36.00	0.058	-		I	
	54 00 D		J-4	254.37		0.99	0.04	20.46	1.72	4.98	3.49	0.00	17.40	0.00	28.56	2.66	25.07	24.92		1	0.059		17.72	I	
652+50	51.00 Rt.				0.00	0.00	0.00					0.00					22.07	21.92	0.15	36.00	+				
CL7	10	S-410			0.45	2.97	0.43									0.04	25.95	25.90	0.04	36.00				I	
		0 400	J-4	102.00		0.81	0.02	19.67	0.80	5.07	2.98	0.00	15.11	0.00	28.56	2.61	25.13	25.07		1	0.059	4	17.97	I	
652+50	51.00 Lt.				0.00	0.00	0.00					0.00					22.13	22.07	0.06	36.00					
CL7	10	S-411			0.00	3.47	0.00										25.75	25.73	0.03	36.00	0.054	-		I	
055.00	54.00 5:	l I	MH-7J	50.99		0.99	0.00	22.19	0.36	4.80	3.49	0.00	16.78	0.00	29.31	3.55	24.92	24.89	0.00	1 00.00	0.059	-	18.56	I	
655+00	51.00 Rt.				0.00	0.00	0.00				-	0.00					21.92	21.89	0.03	36.00					
CL7	10	S-412		00.0-	0.05	3.52	0.05	00.5	0.46	4	0.5.	0.00	40.00	0.00	00.46	2.42	25.73	25.69	0.03	36.00		-	40.00	I	
055.50.40	54 00 D:	0.440	J-3	60.97		1.00	0.00	22.54	0.43	4.77	3.54	0.00	16.90	0.00	29.16	3.43	24.89	24.86	0.00	1 20.00	0.049		16.88	I	
655+50.10 CL7	51.00 Rt.	S-413 S-413			0.00	0.00	0.00				-	0.00					21.89 25.69	21.86 25.67		36.00	0.059				
CL/	10	3-413	1.0	40.04	0.06	3.58	0.06	22.07	0.22	4 70	2.64	0.00	17.05	0.00	20.00	2 20			0.03	30.00		4	15 77	I	
656.00	64 50 54	C 44.4	J-3	48.01		1.02	0.00	22.97	0.33	4.73	3.61		17.05	0.00	28.98	3.29	24.86	24.84	0.00	36.00	0.042	4	15.77	I	
656+09	61.50 Rt.	J-414			0.00	0.00	0.00					0.00					21.86	21.84	0.02	36.00	0.059	2.23			

Units: ENGLISH HGL method: Standard FDOT (Jump HGL to pipe crown).

Financial Prj Id: 21151201.00 County: OKECHOBEE Network: POND4 Designed by AD Date: 2/19/2014
Description: NEW ALIGNMENT Organization WANTMAN GROUP State Road: SR 710 Checked by: PAT Date: 2/19/2014

C	LOCA	TION	STR.	TYPE	LEN.	AREA	S (Ac)	SUB-	TIME	TIME	INTEN	TOTAL	BASE	TOTAL	MINOR	INLET	HGL	HYDRA	ULIC GR	ADE	# PIPE	SLOPE	ACTUAL	FULL	NOTES & REM	JARKS
ALTON DIT DI			NO.			C=	0.95	TOTAL	OF	OF		(C*A)	FLOW	FLOW	LOSS	ELEV.	CLEAR				B SIZE	%	VEL.	FLOW	ZONE:	8
STATION STATI	UPPER	REND		STR.		C=	0.20	(C*A)	CONC	FLOW		` ′	SUMM					FL	OWLINE		R (in.)	HGL	PHYS.	CAP.	FREQ. (Yrs):	3
Chi Chi	ALIGNMEN	NT NAME	UPPER			C=	0.00			SECT.			BASE					UPPER	LOWER	FALL	L RISE	PHYS	VEL.		MANNINGS n:	0.0120
1	STATION	DIST SD	LOWER		(ft.)	INC	TOTAL		(min)	(min)	(in/hr)		(cfs)	(cfs)	(ft.)	(ft.)	(ft.)	(ft.)	(ft.)	(ft.)	S SPAN	MIN.	(fps)	(cfs)	TAILW EL (ft):	24.76
Section Sect	CL7	10	S-414			0.07	3.65	0.07										25.67	25.64	0.03	36.00	0.057	2.44			
C			_	J-3	48.01	0.01	1.04	0.00	23.30	0.33	4.70	3.67	0.00	17.26	0.00	28.84	3.17	24.84	24.82		1	0.042		15.77	I	
Strology Strology	656+56	61.50 Rt.	S-415			0.00	0.00	0.00					0.00					21.84	21.82	0.02	36.00	0.059	2.23			
Strong S	CL7	10	S-415			0.07	3.72	0.07										25.64	25.61	0.03	36.00	0.058	2.47			
CL710				J-3	48.01	0.01	1.05	0.00	23.63	0.32	4.67	3.74	0.00	17.47	0.00	28.70	3.06	24.82	24.58		1	0.500		54.29	I	
Section Sect	657+03	61.50 Rt.	S-416			0.00	0.00	0.00					0.00					21.82	21.58	0.24	36.00	0.059	7.68			
Section Sect	CL7	10	S-416			0.14	4.41	0.13										25.61	25.59	0.02	42.00	0.036	2.14			
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$				J-4	48.01	0.02	1.22	0.00	23.95	0.37	4.64	4.43	0.00	20.56	0.00	28.56	2.95	25.08	25.06		1	0.042		23.64	I	
State Stat	657+50	61.50 Rt.	S-418			0.00	0.00						0.00					21.58	21.56	0.02	42.00	0.048	2.46			
Strock S	CL7	10	S-417			0.55	0.55	0.52										25.73	25.61	0.11	18.00	0.102	2.06			
CL710 S-418 J.3 R.0 0.01 1.2 2.0 0.00 2.43 0.07 0.00 0.				P-4	112.50	0.15	0.15	0.03	10.00	0.91	6.58	0.55	0.00	3.64	0.00	28.56	2.83	25.95	25.25		1	0.622		9.14	I	
State Stat	657+50	51.00 Lt.	S-416			0.00	0.00	0.00					0.00					24.45	23.75	0.70	18.00	0.150	5.17		<u> </u>	
65+44	CL7	10	S-418			0.07	4.48	0.07										25.59	25.58	0.02	42.00	0.036	2.15			
CL710				J-3	48.01	0.01	1.23	0.00	24.33	0.37	4.60	4.50	0.00	20.72	0.00	28.70	3.11	25.06	25.04		1	0.042		23.78	I	
Second Personal Per	657+97	61.50 Rt.	S-419			0.00	0.00	0.00					0.00					21.56	21.54	0.02	42.00	0.048	2.47		I	
688+44 61.5 Rt	CL7	10	S-419			0.06	4.54	0.06										25.58	25.43	0.15	42.00	0.037	2.17			
CL71 S-420 S-420 S-420 S-420 S-420 S-421 S-42				J-3	414.37	0.00	1.23	0.00	24.70	3.19	4.57	4.56	0.00	20.84	0.00	28.84	3.26	25.04	24.84		1	0.048		24.11	I	
S S S S S S S S S S	658+44	61.50 Rt.	S-420			0.00	0.00	0.00					0.00					21.54	21.34	0.20	42.00	0.048	2.51		I	
662+50	CL7	10	S-420			0.75	5.29	0.71										25.43	25.38	0.05	42.00	0.044	2.39			
CL710			_	J-4	112.50	0.25	1.48	0.05	27.89	0.79	4.31	5.32	0.00	22.95	0.00	28.56	3.13	24.84	24.79		1	0.044		23.51	I	
State Stat	662+50	61.50 Rt.	S-421			0.00	0.00	0.00					0.00					21.34	21.29	0.05	42.00	0.048	2.44		I	
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	CL7	10	S-421			0.72	6.01	0.68										25.38	25.18	0.19	42.00	0.056	2.69			
CL710			_	J-4	343.56	0.40	1.89	0.08	28.67	2.13	4.25	6.09	0.00	25.89	0.00	28.56	3.18	24.79	24.63		1	0.047		23.69	I	
MH-7J MH-7	662+50	51.00 Lt.	S-422			0.00	0.00	0.00					0.00					21.29	21.13	0.16	42.00	0.048	2.46		I	
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	CL7	10	S-422			0.00	6.01	0.00										25.18	25.07	0.12	42.00	0.053	2.60			
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $			_	MH-7J	220.94	0.00	1.89	0.00	30.80	1.42	4.10	6.09	0.00	24.97	0.00	29.61	4.43	24.63	24.53		1	0.045		23.45	l	
Californ Californ	666+00	51.00 Lt.	S-423			0.00	0.00	0.00					0.00					21.13	21.03	0.10	42.00	0.048	2.44		I	
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	CL7	10	S-423			0.62	6.63	0.59										25.07	25.00	0.07	42.00	0.061	2.79			
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $			_	J-4	107.52	0.15	2.04	0.03	32.22	0.64	4.01	6.71	0.00	26.89	0.00	29.05	3.98	24.53	22.80		1	1.609	_	141.59	I	
State Stat	668+25	51.00 Lt.	S-424					0.00												1.73	42.00	0.048	14.72		I	
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	CL7	10	S-424			0.56	9.43	0.53										25.00	24.76	0.24	42.00	0.124	3.99			
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $			_	J-4	194.00	0.28	3.57	0.06	32.86	0.00	3.97	9.68	0.00	38.40	0.00	29.05	4.05	22.57	23.50		1	-0.479	_	-75.96	I	
CL710 S-425 P-3 327.11 0.06 1.25 0.01 20.98 2.28 4.92 2.38 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0	668+27	56.50 Rt.	POND4				0.00	0.00					0.00					19.07	20.00	-0.93	42.00	0.048	-7.89		l	
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	CL7	10	S-425			0.15		0.14										25.23			30.00	0.070	2.39			
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $			_	P-3	327.11	0.06	1.25	0.01	20.98	2.28	4.92	2.38	0.00	11.73	0.00	30.36	5.13	22.05	21.80		1	0.076		12.36	I	
CL710 S-426 P-3 102.00 0.04 0.04 0.01 10.00 0.81 6.58 0.17 0.00 1.12 0.00 1.12 0.00 10.00	671+50	51.00 Rt.	S-424				l													0.25	30.00				l	
P-3 102.00 0.04 0.04 0.04 0.01 10.00 0.81 6.58 0.17 0.00 1.12 0.00 1.12 0.00 3.60 27.75 27.60 0.15 18.00 0.15 0.167 0.15 0.167 0.15 0.167 0.15 0.167 0.15 0.167 0.15 0.167 0.15 0.167 0.15 0.167 0.15 0.167 0.15 0.167 0.15 0.167 0.15 0.167 0.15 0.167 0.15 0.167 0.15 0.167 0.15 0.167 0.15 0.167 0.16																										-
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			_	P-3	102.00	0.04	0.04	0.01	10.00	0.81	6.58	0.17	0.00	1.12	0.00	30.36	3.60	27.75	27.60		1		1	4.43	I	
CL710 S-427 MH-7 150.17 0.00 1.92 0.00 1.15 0.00 19.80 1.18 5.05 2.06 0.00 10.39 0.00 30.73 5.42 22.16 22.05 1 30.00 0.055 2.12 0.073	671+50	51.00 Lt.	S-425		. 52.50		l			0.01	0.00	3			0.00	30.00	2.03			0.15	18.00			5	1	
MH-7 150.17 0.00 1.15 0.00 19.80 1.18 5.05 2.06 0.00 10.39 0.00 30.73 5.42 22.16 22.05 1 0.073 12.15																										
			-	MH-7	150.17				19.80	1.18	5.05	2.06	0.00	10.39	0.00	30.73	5.42	1					4	12.15	Ì	
	673+00	58.13 Rt.	S-425													333				0.11	- 1		4		1	

Units: ENGLISH HGL method: Standard FDOT (Jump HGL to pipe crown).

Financial Prj Id: 21151201.00 County: OKECHOBEE Network: POND4 Designed by AD Date: 2/19/2014
Description: NEW ALIGNMENT Organization WANTMAN GROUP State Road: SR 710 Checked by: PAT Date: 2/19/2014

LOCA	TION	STR.	TYPE	LEN.	AREA	S (Ac)	SUB-	TIME	TIME	INTEN	TOTAL	BASE	TOTAL	MINOR	INLET	HGL	HYDRA	ULIC GR	ADE	# PIPE	SLOPE	ACTUAL	FULL	NOTES & REN	MARKS
	F	NO.	OF	[C=	0.95	TOTAL	OF	OF		(C*A)	FLOW	FLOW	LOSS	ELEV.	CLEAR	С	ROWN		B SIZE	%	VEL.	FLOW	ZONE:	8
UPPE	R END		STR.		C=	0.20	(C*A)	CONC	FLOW		` ′	SUMM					FL	OWLINE		R (in.)	HGL	PHYS.	CAP.	FREQ. (Yrs):	3
ALIGNME	NT NAME	UPPER			C=	0.00			SECT.			BASE					UPPER	LOWER	FALL	L RISE	PHYS	VEL.		MANNINGS n:	0.0120
STATION	DIST SD	LOWER		(ft.)	INC	TOTAL		(min)	(min)	(in/hr)		(cfs)	(cfs)	(ft.)	(ft.)	(ft.)	(ft.)	(ft.)	(ft.)	S SPAN	MIN.	(fps)	(cfs)	TAILW EL (ft):	24.76
CL.	710	S-428			0.81	1.92	0.77	` ′	` ′	,		, ,	` ′	` '	` ′	` '	25.58	25.31	0.27	30.00	0.063	2.28	` ′	. ,	
		-	P-4	432.01	0.43	1.15	0.09	16.64	3.16	5.44	2.06	0.00	11.18	0.00	28.63	3.04	22.49	22.16		1	0.076	-	12.32		
677+32	61.50 Rt.	S-427			0.00	0.00	0.00					0.00					19.99	19.66	0.33	30.00	0.076	2.51			
CL.	710	S-429			0.75	1.11	0.71										25.67	25.58	0.08	24.00	0.074	2.13			
			P-4	113.85	0.49	0.72	0.10	15.75	0.89	5.56	1.20	0.00	6.68	0.00	28.63	2.96	22.10	21.99		1	0.097	-	7.72		
677+32	52.35 Lt.	S-428			0.00	0.00	0.00					0.00					20.10	19.99	0.11	24.00	0.102	2.46			
CL.	710	S-430			0.00	0.37	0.00										25.84	25.67	0.17	18.00	0.044	1.36			
			MH-7	388.25	0.00	0.22	0.00	12.51	3.24	6.07	0.39	0.00	2.40	0.00	29.72	3.88	22.18	21.60		1	0.149		4.42		
681+20	66.16 Lt.	S-429			0.00	0.00	0.00					0.00					20.68	20.10	0.58	18.00	0.150	2.50			
CL.	710	S-431			0.19	0.37	0.18										25.93	25.84	0.09	18.00	0.049	1.42			
			P-3	187.04	0.11	0.22	0.02	10.96	1.56	6.37	0.39	0.00	2.51	0.00	31.10	5.17	22.46	22.18		1	0.150		4.44		
683+07	62.45 Lt.	S-430			0.00	0.00	0.00					0.00					20.96	20.68	0.28	18.00	0.150	2.51			
CL.	710	S-432			0.18	0.18	0.17										25.95	25.93	0.01	18.00	0.012	0.70			_
			P-3	114.72	0.11	0.11	0.02	10.00	0.96	6.58	0.19	0.00	1.24	0.00	29.96	4.01	22.63	22.46		1	0.148		4.44		
683+24	51.00 Rt.	S-431			0.00	0.00	0.00					0.00					21.13	20.96	0.17	18.00	0.150	2.51			

Units: ENGLISH

Appendix 9 Correspondence

MEETING MINUTES



DRAINAGE KICK-OFF MEETING SR 710 from US 441 to the L-63 Canal FPID No. 419344-3-52-01

February 18, 2013, 9:00 am; FDOT, District 1, Bartow Office

Attendees:

Amy Setchell –FDOT, Project Management
Carl Spirio – FDOT, Drainage
Brent Setchell –FDOT, Permitting
Martin Horwitz – FDOT, Permitting
Joel Hobbs – FDOT, PE Trainee
Brian Kirwan – The Wantman Group, PM - Design
Eric Lanning – The Wantman Group, Roadway
Greg Griffith – The Wantman Group, Permitting
Greg Seidel – The Balmoral Group, Drainage
Lori Stanfill – The Balmoral Group, Drainage

- 1. Brian Kirwan began by giving an overview of the proposed SR 710 project limits and proposed typical sections.
- 2. Greg Seidel described the proposed drainage design and the potential pond sites. When asked if potential pond sites should be discussed more in-depth at this time, Brent Setchell advised that a Pre-Pond Siting Meeting be scheduled with the R/W Department. Prior to this, a Pre-Application Meeting with SFWMD should also be scheduled. Brent would like to be notified and/or attend this meeting.

The first drainage basin and the potential pond locations within this area were reviewed. Pond Alternate 1A is located before (800' west) of the Begin Project station). Carl Spirio remarked that it would be more desirable to use the Pond Alternate 1B site which is adjacent to Taylor Creek (west side). The 1A site is adjacent to an existing FDOT pond.

In proposed Basin 4, look at the remnant parcels (owned by Berman Ranch) for use as an alternate pond site.

In proposed Basin 5, the parcel on the northeast side of SR 710 was investigated as a potential pond site. Owned by Okeechobee County, this parcel is the Front Entrance to the Agriculture Center. The FDOT has been in recent negotiations with Okeechobee County regarding use of this parcel for a bridge widening project at SR 70 and L-63 N Canal. It is advised that use of this parcel should be avoided. Amy Setchell will search for the plans/BHR for the bridge widening project. Due to R/W issues, the project required 8

months to acquire the SFWMD permit. An access permit was given to the SFWMD.

Brent Setchell noted that for the PSR, pond treatment estimates should continue to incorporate the additional 50% treatment when discharging to impaired water bodies.

3. Permit issues for the project were discussed. Due to the project being located within a pumped basin, the project criterion consists of the Basin S-133 allowable discharge of 15.6 csm (0.024 cfs per acre). This equates to 1.5 cfs for the entire project. Greg Seidel mentioned investigating an outfall to the L-63N Canal which would allow for higher discharge rates.

Brent mentioned that the first Lake Okeechobee BMAP Meeting is starting on Wednesday, February 20 which he is planning to attend.

Carl discussed that other options should be explored for this project. As the project progresses, opportunities to receive credit for improving the basin may present themselves. This may include improving pump systems or improving Taylor Creek. Other options may include design of a regional pond instead of multiple ponds under House Bill 599 (Regional Treatment). If there are communities flooding downstream, maybe an option for the FDOT to improve the basin will present itself. TMDL removal should be documented as an opportunity to gain credit also.

The difficulties with TMDL removal and the proposed typical section were discussed. For the TMDL calculations with the urban typical section, the existing condition DCIA will be 0% while the proposed condition DCIA will be 100% requiring bigger treatment volumes. The wet detentions pond max out at approximately 43% Nitrogen removal and 70% Phosphorus removal. Dry treatment swales are currently proposed on one side of the project to aid in meeting the reduction requirements.

For seasonal high water determination, Brent mentioned to request that the FDOT Geotechnical Department install piezometers. Also, it will be necessary to scrutinize the seasonal highs as old indicators may be perched, and never achieve this elevation again due to the canal.

As the existing pond at intersection of SR 70 and proposed SR 710 has been recently modified (weir raised), check the SFWMD website for permit information. Balmoral will research the SFWMD permitting website for this permit.

4. Greg Griffith presented the environmental and permitting concerns for the project. A wetlands discussion ensued. Greg Griffith mentioned that he is awaiting the full R/W to be staked out before delineating wetlands. Brent stated he would like to be notified and/or present when the wetlands are

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flagged. Greg Griffith will investigate which mitigation banks are to be used. Bluefield Ranch was mentioned. Endangered Species surveys are currently ongoing for the PD&E and will be updated/revised at within the appropriate timeframe when the actual permitting has begun.

5. Potential R/W issues regarding the bridge crossings were discussed at this time. The SFWMD owns the R/W for Taylor Creek so R/W permitting will go through the West Palm Office. Initial bridge hydraulics work has been completed for Taylor Creek and a box culvert was analyzed along with a bridge due to the proximity of the location to a hospital. The pile driving needed for bridge construction might be disturbing, therefore, a proposed 8 – 12' x 14' box culvert was analyzed. Carl Spirio thought that a Conspan structure should be further investigated. Although possibly a little more expensive, less boxes could be used. The box culvert option should be discussed with the SFWMD. The SFWMD has a 0.1' head loss criteria. As the crossing is located within a lock area, large boat navigation is not an issue.

Brent Setchell recommended that the L-63N Canal crossing be purchased as a fee simple transaction and then return an easement to the SFWMD for the canal and canal access requirements. This will be similar to what occurred on the recent SR 70 project.

The Drainage Kick-Off Meeting ended, and the Roadway Design Meeting started.

c. Attendees Peter Rogas, RS&H





MEETING NOTES

SFWMD PRE-APPLICATION MEETING SR 710 from US 441 to L-63N Canal FPID Number 419344-3-52-01

May 29, 2013 10:00 a.m., SFWMD Okeechobee Service Center

The purpose of the meeting is to present the project, present and discuss the approach for the stormwater management facilities and review the permitting requirements. The potential stormwater pond sites will also be presented for review and discussion. The following are highlights of the conversation.

- 1. Brian Kirwan provided a description of the project which consist of new construction of SR 710 from US 441 to L-63N. The typical section will be a four-lane suburban section with curb and gutter. A sidewalk will be included on the north side of the project and a treatment ditch is currently proposed on the south side
- 2. Greg Seidel provided a review of the drainage basins utilizing the board from the Wantman presentation which shows the presentation pond sites and the PD&E Pond Sites.
- 3. A discussion of stormwater management ensued the following items were noted:
 - a. The project is located in the S-133 Basin which has an allowable discharge of 15.6 CSM. It was agreed that the SR 710 project could utilize a pre-post method. Kelly Cranford added the pre-development calculations needed to be reasonable and to review the permit for North Shore Village for additional information. Likewise, the Industrial Park at the beginning of the project has a permitted discharge through the Industrial Park project which would be considered the allowable discharge at that outfall location.
 - b. 2 ½ inches over the impervious area will be the controlling factor for water quality. The additional 50% requirements for impaired water bodies will not be needed as the pre-post nutrient loading calculations will show that there are no offsite water quality impacts. Basin will be top of slope to top of slope for the Typical Section.
 - c. Pasture is acceptable for EMC values for the areas that are currently pasture.
 - d. Drawdown in the wet ponds will be ½" of runoff over the basin in 24 hours. It is expected that the minimum 3" bleeder will be utilized on the control structures.
 - e. Mr. Seidel inquired if a new outfall to the L-63N canal would be permittable given that both the L-63N canal and Taylor Creek discharge to Lake Okeechobee. Kelly Cranford responded that coordination with the SFWMD operations would be required to determine if the canal had the available capacity and, if so, the approach would be reasonable. Mr .Seidel mentioned that this would help reduce the

- nitrogen and phosphorous loading to Taylor Creek while still meeting pre-post phosphorous loading in Lake Okeechobee. Brent Setchell asked the Balmoral Group to inquire if the outfall permit could be included in the R/W modification permit for the L-63N bridge work.
- f. It was mentioned that reduced discharges to Pine Ridge Park would be beneficial and Cypress Quarter had undertaken several retrofit projects.
- g. Mr. Seidel noted the floodplain maps had not been updated and were vague representations, at best, as the impacts of the canals was not included. It was noted that Taylor Engineering was in the process of updating the flood maps. If new maps are not available, Mr. Seidel proposed to evaluate floodplain impacts based on updated modeling based on LiDAR contours of the surrounding area and show no increase in to existing flood stages. This approach was considered reasonable. Carl Spirio added that the roadway should be checked for evacuation route status.
- 4. A discussion of environmental considerations ensued the following items were noted:
 - a. Ponds needed to maintain a 75 foot setback from private wells.
 - b. A minimum 25 foot buffer should be located between any ponds and wetlands, otherwise, secondary impacts will need to be included. Discharges to the wetland should be low velocity or impacts will be accessed. Secondary impact distances will vary for associated roadway impacts. Wantman Group (WGI) staff conducted a wetland delineation of the proposed alignment on May 22nd and 23rd. At the time of the meeting these wetland lines were being surveyed so an acreage of impacts is not yet available. Wetlands locations depicted in the National Wetlands Inventory (NWI) are fairly consist with actual field conditions. Through the southern and middle sections of the alignment wetland impacts will be mostly depressional features while some Cypress/Cabbage Palm hammocks will be impacted in the middle and western sections. There are some minor Other Surface Waters (OSW) impacts located throughout the pasture and near the SR-710/Mosquito Creek bridge as well.
 - c. No Threatened & Endangered (T&E) Species were observed while WGI staff were in the field, however more in depth surveys will be conducted prior to construction. It was noted that a Crested Caracara (*Caracara cheriway*) nest was observed at the southern end of the project.
 - d. The Modified WRAP (M-WRAP) assessment method shall be used for primary and secondary impacts due to the regional mitigation banks being permitted in WRAP and banking being FDOT's preferred mitigation option.
 - e. It was noted that a conservation easement was recently recorded west of Mosquito Creek and north of SR 710. Additionally, a wetland line was surveyed to the west on a private parcel to evaluate filling operations in the area. The SFWMD will provide this wetland line to the FDOT.
- 5. The following items from miscellaneous discussion were noted:
 - a. Carl Spirio inquired about any regional stormwater management projects that my under consideration in the area. The SFWMD was not aware of any and suggested checking with the FDEP. Carl mentioned a possible filter marsh on

Taylor Creek. Mr. Seidel added that a control structure could be constructed as part of the proposed culvert crossing of Taylor Creek.

- b. The ditch north of the proposed Taylor Creek crossing is referred to as the "City Limits Ditch" and has a history of erosion issues.
- c. Brent Setchell relayed some of the requirement for the L-63N canal bridge would include a survey of the channel at all faces of the existing and proposed bridge and the original canal width design would need to be restored during construction. He added that 1 method of construction will need to be shown in the plans and to include mixing zones.

ACTION ITEMS

- Balmoral Group to follow up with Taylor Engineering on the status of the updated FEMA maps.
- Balmoral Group to contact SFWMD Operations to determine available capacity in the L-63N canal.
- SFWMD to provide wetland survey of property near Agricultural Center entrance.
- Wantman to schedule a meeting with Brent Setchell to discuss approaches for the SFWMD ROW permit based on the nearby SR 70 Widening project.

ATTACHMENTS

Sign in Sheet

c. Attendees

Amy Setchell, P.E., Project Manager, FDOT



SIGN IN SHEET

SFWMD PRE-APPLICATION MEETING SR 710 from US 441 to L-63N Canal FPID Number 419344-3-52-01

Location: Okeechobee Service Center

Date: May 29, 2013 Time 9:30 am

NAME	FIRM/AGENCY	OFFICE / RESPONSIBILITY	EMAIL ADDRESS
GREG SEIDER	BAINORKE GROUP	PROJECT DRAINAGE ENGINEER	aseidel Chalmoralgroup. US
BRIAN KIRWAN	WANTMAN GROUP	DESIGN PROJECT MUR	brian. Kirwan ewantmangrayp. COM
GREG GRIFFITH	WANTMAN GROWP	ENV. PERMITTIME	area griffill Lunartmangroup. con
Root GHUI	FDOT		brent setch 40 dot. state flux
CARL SPIRIO	FDOT	DRAINAGE PERMITTING	carlton. spirio@dof. state. Flus
Keur CRANFARD	MARK SFUND		REGULATION - SECTION LEADER KORANTER CE STUMO. GOV
EVe Raymond	SFWMD	Regulation - Enu Review	Staymona stumd, gov
Carolin Mercedin	STWHD	Revolution - Son face Water	Concreed a Shorn d. gor
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MEETING MINUTES

PRE-POND SITING REPORT / RIGHT-OF-WAY MEETING SR 710 from US 441 to the L-63N Canal FPID No. 419344-3-52-01

September 9, 2013, 9:30 am; FDOT, District 1, Bartow Office

Attendees:

Amy Setchell –FDOT, Project Management
Kevin Ingle – FDOT, Project Management
Joe Harper – FDOT, Right-of-Way
Brent Setchell –FDOT, Permitting
Carl Spirio – FDOT, Drainage
Brian Kirwan – The Wantman Group, PM - Design
Alfredo Rodriguez – The Wantman Group, Roadway
Greg Griffith – The Wantman Group, Permitting
Greg Seidel – The Balmoral Group, Drainage
Jennifer Nunn – The Balmoral Group, Drainage
Lori Stanfill – The Balmoral Group, Drainage

- 1. Brian Kirwan began by giving an overview of the proposed SR 710 project limits.
- 2. Greg Seidel described the proposed pond alternative locations and impacted parcels. Seventeen potential sites within five basins were reviewed. Based on the discussion, four pond alternatives will require minor adjustments. One potential pond site will be removed. After the potential sites have been updated, the geotechnical, cultural resource, contamination, biological, wetland, and economic (right-of-way cost) assessments can be conducted.
- 3. As time was limited, Brian Kirwan briefly discussed SR 710 road right-of-way impacts before the meeting concluded.
- c. Attendees



Memo

To: Bob Hindman, Okeechobee Maintenance

From: Lori Stanfill, Balmoral Group

CC:

Date: January 22, 2014

Re: SR 710 PSR & BHR – Okeechobee County

I spoke with Bob Hindman regarding any flooding or maintenance issues in the vicinity of the SR 710 project. I inquired about specific areas of interest including:

- 1. The existing pond located west of US 441 and south of the City Ditch Mr. Hindman stated that he is not aware of any problems with this ponds function. However, there are erosion issues with the City Ditch which is frequently flowing full after heavy rainfall events. He stated that there is not flooding problems in this area, mostly just erosion. He is not aware of any issues with Taylor Creek to the east, but does not maintain Taylor Creek R/W.
- 2. Existing pond at SE corner of SR 70 & NE 34th Avenue. No problems with this pond, but there has been flooding problem in outfall ditch along SR 70 just east of the Agricultural Park Area. He has had to have crews clean out the outfall ditch.
- 3. SR 710 from west of L-63N Canal to Mosquito Creek. He is not aware of any flooding issues even adjacent to Mosquito Creek or at the L-63N Canal. He noticed that rubble riprap was installed as channel protection against scour within the L-63N Canal several years ago.

SR 710 Stormwater Treatment Area/Regional Pond Feasibility Study Stakeholder Meeting Minutes FPID No. 432644-1-32-01 - D1 DW Drainage

Location: SFWMD Okeechobee Service Center, Okeechobee

Date: July 31, 2014 Time 10:30 am

The purpose of the meeting is to introduce the SR 710 Stormwater Treatment Area/Regional Pond Feasibility Study as an investigation being undertaken by the FDOT District One as a part of the SR 710 new alignment project in Okeechobee.

Attendees: See attached Sign-In Sheet

- 1. Mr. Brent Setchell gave an introduction on the SR 710 Feasibility Study.
- 2. Mr. Greg Seidel gave a brief project history explaining how the SR 710 Feasibility Study has progressed to this point.
- 3. Mr. Greg Seidel introduced the regional pond alternative that is to be constructed by the FDOT for the SR 710. This option would incorporate offsite areas associated with Lower Taylor Creek.
 - a. Representatives from Okeechobee County confirmed the airport ditch is owned by the County from Taylor Creek up to airport property.
 - b. Mr. Setchell voiced his concern about conveying water from the airport ditch to the regional pond. He mentioned the preferred option on behalf of the FDOT would be to provide the required 1-inch of treatment for the SR 710 roadway and demonstrate that the nutrient removal shows a net benefit to the community.
 - c. Mr. Seidel mentioned that a lower treatment depth could be provided. He also indicated that a control structure could be located at Taylor Creek and securing flood rights from the property owners could be an option.
 - d. Mr. Setchell explained the SR 710 Regional Pond approach in that Basins 1 and 2 would be treated by the Regional Pond, Basin 3 and a portion of Basin 4 would pre-treat via the existing pond and that the remaining runoff would discharge directly to the L-63N Canal.
- 4. Ms. Janet Hearn introduced the Stormwater Treatment Area (STA) alternatives which would require interagency cooperation and be hydraulically connected to the L63-N canal and Upper Taylor Creek.
 - a. Ms. Hearn said that for planning purposes a 100-acre STA is being evaluated. This is comparable to the Taylor Creek STA which has a treatment area of 118 acres. A 100 acre STA could remove about 1,500 to 1,600 kg of TP per year. An overview of three potential locations for a 100 acre STA within the Hamrick property was presented. These three sites were selected to avoid wetlands.

- b. The Lake Okeechobee TMDL requires an in-lake concentration of 40 parts per billion (ppb) TP.
- FDEP added that the existing Taylor Creek STA provides approximately 1520 kg of removal.
- d. The STA 2 option would require some rehabilitation of the existing wetland in order to retain runoff from the surrounding property. This would provide additional storage and remove approximately 180 kg TP per year without additional flow from the L-63N Canal or Upper Taylor Creek.
- e. The STA 2 option could provide up to 1000 kg of removal if inflow was augmented with flow from L-63N Canal.
- f. Mr. Morris Crady asked if a combination of STA 1 and STA 2 would be possible in order to still use the property (i.e. for walking trails) in the winter. Mr. Seidel responded by saying the final STA choice is not part of the feasibility study and would be coordinated under final design.
- g. Mr. Setchell liked the fact that the STA 2 option would provide some treatment and attenuation. However, he expressed some concern for the STA 2 option since the restored wetlands would be limited on the treatment volume depth (storage) provided. Would this option still require a control structure and how would the western bank of Lower Taylor Creek be affected?
- h. If an STA option is chosen, FDOT would still need to obtain fill for the SR 710 project and this could be coordinated through agreements.
- i. Mr. Hamrick asked if an STA option would impact ranch operations. Ms. Bonnie Wolff Pelaez confirmed that the BMAP manual does not restrict cattle from the wetlands.
- j. Mr. Hamrick mentioned that the wetland portion of his property is the emotional piece, and the upland portion of his property is the economic piece.
- 5. Mr. Seidel mentioned that if an STA option was selected, FDOT would not be taking the lead on this design and this would most likely fall to the FDEP or SFWMD.
- 6. Mr. Jim Threewits reiterated his concerns with ponds adjacent to the right-of-way. The County has requested from FDOT that the new SR 710 alignment be a main corridor to attract development. The County wants this gateway to be pretty and attractive for development and does not want unattractive ponds or ponds along the roadway frontage. Mr. Threewits feels this is a chance to do something good and doesn't want to miss out and added that this is a very valuable piece of the land to the county.
 - a. Mr. Setchell responded by saying that FDOT is evaluating the need for pond fencing. FDOT is open to providing drainage easements for property owners to provide pond maintenance.
 - b. Mr. Setchell stated that FDOT does not want to move ponds away from the right-of-way due to the hydraulics and increase in cost.
- 7. Mr. Seidel commented that the current schedule calls for a decision to be reached by the end of the year.
 - a. Ms. Amy Setchell responded that the draft Feasibility report is due Sept. 22nd with the final report due Oct. 22nd.

- b. The next step is to review the information presented today individually with the stakeholders and obtain feedback as necessary.
- c. Final calculations need to be performed.

End of Minutes

c. Attendees Carl Spirio, P.E., FDOT Drainage Alfredo Rodriguez, P.E., Wantman

SR 710 Stormwater Treatment Area/Regional Pond Feasibility Study Stakeholder Meeting Sign-In Sheet FPID No. 432644-1-32-01 - D1 DW Drainage

Location:

SFWMD Okeechobee Service Center Auditorium

3800 NW 16th Boulevard, Suite A, Okeechobee, FL 34972

Date:

July 31, 2014

Time

10:30 am

NAME	FIRM/AGENCY	OFFICE / RESPONSIBILITY	EMAIL ADDRESS	Initials
Carlton Spirio	FDOT	Drainage	Carlton.Spirio@dot.state.fl.us	
Brent Setchell	FDOT	Permitting	Brent.Setchell@dot.state.fl.us	Bal
Amy Setchell	FDOT	PM	Amy.Setchell@dot.state.fl.us	955
Kevin Inlge	FDOT		Kevin.Ingle@dot.state.fl.us	K51
Jeffrey Mednick	FDOT		Jeffrey.Mednick@dot.state.fl.us	JLM
Michael Hamrick	Property Owner	Hamrick & Sons	MHamrick@manateelegal.com	My
Morris Crady	Lucido & Assoc.	Hamrick & Sons	mcrady@lucidodesign.com	MAC
Maryann Hamrick	Property Owner	Hamrick & Sons	Annie4UF@aol.com	mah
Regina Hamrick	Property Owner	Hamrick & Sons		
Gregory Seidel	The Balmoral Group	Project Drainage Engineer	gseidel@balmoralgroup.us	9M
Jennifer Nunn	The Balmoral Group	Project Drainage Engineer	inunn@balmoralgroup.us	89
Janet Hearn	ATM	STA Designer	jhearn@appliedtm.com	jh
Henri Belrose	Wantman Group	Consultant PM	Henri.belrose@wantmangroup.com	
Alfredo Rodriguez	Wantman Group	Consultant Asst. PM	Alfredo.rodriguez@wantmangroup.com	AN
Kathy Scott	Okeechobee Co.	Kathy Airport/TDC	kscott@co.okeechobee.fl.us	KS
Lee Evett	Okeechobee Co.	0	levett@co.okeechobee.fl.us	100
Jim Threewits	Okeechobee Co.	Adora	jthreewits@co.okeechobee.fl.us	21
Kelly Baney	Okeechobee Co.		kbaney@co.okeechobee.fl.us	/
Katie Hallas	FDEP	PHONE	Katie.Hallas@dep.state.fl.us	
Elizabeth Alvi	FDEP	PHONE	Elizabeth.Alvi@dep.state.fl.us	
Jim Jeffords	USACE		jim.w.jeffords@usace.army.mil	
David Allen	City of Okeechobee		dallen@cityofokeechobee.com	
Lesley Bertolotti	SFWMD		lbertolo@sfwmd.gov	
Drie Wolf Bela	er FDACS		Bonie Wolff Pelase @ freshfor	MIM
Regina Hann				

SR 710 Stormwater Treatment Area/Regional Pond Feasibility Study Stakeholder Meeting Sign-In Sheet

FPID No. 432644-1-32-01 - D1 DW Drainage

Location:

SFWMD Okeechobee Service Center Auditorium

3800 NW 16th Boulevard, Suite A, Okeechobee, FL 34972

Date:

July 31, 2014

Time

10:30 am

NAME	FIRM/AGENCY	OFFICE / RESPONSIBILITY	EMAIL ADDRESS	Initials
GARY RITTER	SFWMD	INTER GOV	gritter @ Stwmd.gov	(4)
		2		



MEETING NOTES

SFWMD PRE-APPLICATION MEETING #2 SR 710 from US 441 to L-63N Canal FPID Number 419344-3-52-01

March 24, 2015 10:00 a.m., SFWMD Okeechobee Service Center

The purpose of the meeting is to review the SFWMD comments on the regional pond approach clarify SFWMD permitting requirements and discuss the approach for the stormwater management facilities. The following are highlights of the conversation.

- 1. Greg Seidel provided a project description showing an overview of the project limits and the current typical section. The project consists of new construction of SR 710 from US 441 to L-63N. The typical section will be a four-lane suburban section with curb and gutter. An asphalt path will be included on the north side of the project and sidewalk on the south side. The previously proposed treatment swale on the south side has been eliminated.
- 2. Mr. Seidel noted that the 1st Pre-Application meeting was held on May 29, 2013.
- 3. Mr. Seidel provided a quick overview of drainage basins, flow patterns and water resources issues and summary of Regional Pond/STA study. It was noted that the FDOT had added another option to the study which included a wet detention pond with the water being pumped from the adjacent L-63N canal to the regional pond for treatment and gravity discharge back into the canal.
- 4. It was noted that the upon completion of the final Pond Siting Report, FDOT will proceed with the preferred option which will likely be the regional pond option to address new SR 710 alignment runoff water quality/quantity requirements Brent Setchell indicated in order for the STA option to move forward an agreement or MOU of participating funds from other stakeholders would be needed by September 4, 2015 in order to meet FDOT's schedule.
- 5. At FDOT's request, regional pond option B was moved closer to L-63N canal for the following reasons
 - a) Locates the pond outside 10,000-ft range of airport
 - b) Eliminates need for costly rubble riprap on pond slopes
 - c) Shortens length of pipe needed to pump from L-63N canal



d) Eliminates the mixing of basins. The pumped water from the L-63N will discharge back to the L-63N rather than discharging into Lower Taylor Creek.

However, this change also caused:

- a) The regional pond location to move higher ground
- b) Lost capability to send large portion of SR 710 runoff to the new pond location due to higher SHWE at new pond location.

Greg Seidel noted that remaining portion of SR 710 not directed to the regional pond would employ minimal Best Management Practices prior to discharge to Lower Taylor Creek or the L-63N.

- 6. Brent Setchell asked if the reduction of SR 710 runoff being directed to the regional pond without formal treatment would be acceptable. Jesse Markle indicated this would be acceptable since compensatory treatment is provided in the regional pond (ie Ac-ft) and FDOT will demonstrate via Nutrient loading calculations that there is a significant improvement treating water from L-63N canal versus treating runoff from SR 710.
- 7. It was also confirmed with operations (Zhiming Chen) that the new discharge locations into the L-63N would not impact the capacity of the canal to pass flood discharges. It was noted that the expected discharge rates from the roadway would be around 50 cfs and the canal design flow rates are around 7,000 cfs. Additionally, the roadway discharge would peak well before the canal would reach peak stage. The project will be able to demonstrate that no additional runoff volume will be added to the Lower Taylor Creek pumped discharge to Lake Okeechobee.
- 8. FDOT will consider bringing the regional pond closer to SR 710 and will weigh this against property access considerations for current property owner (Hamrick).
- 9. SFWMD will require min 15-ft from toe of levee to top of bank for regional pond.
- 10. Location of pump station should be coordinated with SFWMD Operations to ensure no impediment to levee access or regional pond access.
- 11. SFWMD will provide plans/specs for pump station layout constructed along levees.
- 12. The nutrient loading reduction calculations uses Harper wet detention methodology based on residence time, but using pumping rather than rainfall.



- 13. Pumping is less efficient than rainfall (shorter residence time), but significantly higher volume results in greater overall benefit.
- 14. Size of regional pond (26 ac) equates to estimated amount of fill material needed for SR 710 construction. It was noted that the size of pond far exceeds water quality/quantity and nutrient removal requirements for runoff from SR 710.
- 15. The FDOT is not planning to use vegetative treatment, residence time only. It was suggested that the SFWMD take over maintenance and operation of the pond and the performance of the regional pond should be monitored post-construction (potential pilot project) to determine ideal flow rate. FDOT would prefer to transfer O&M of the proposed pump station to SFWMD or FDEP. The Operation schedule will need to take into consideration dry season water levels in L-63N canal. The nutrient removal estimate was based on the annual average and should be investigated. A variable speed pump should be considered to increase flow rate during wet season, reduce flow rate (or stop pumping operation) during dry season, to meet annual average targets. Brent Setchell will determine if FDOT will accept pump station O&M as fallback position if SFWMD will not accept O&M.
- 16. Leslie Bertolotti inquired what FDOT was specifically requesting from SFWMD by the Sept 4, 2015 deadline. Brent Setchell stated that FDOT needed to compile the remaining estimated costs and present a proposal to SFWMD (and/or FDEP) to consider.
- 17. The intake and outfall structures which impact the L-63N canal/levee will require a SFWMD ROW permit and ACOE Section 408 approval.
- 18. Tom Colios noted that removal of water from L-63N canal will require Water Use permit or MOU from Governing Board. He recommended considering pursuing MOU since regional pond is a potential pilot project and, that once in operation, the pond would switch to a Water Use permit. SFWMD will provide a template MOU. It was added that the Regional Pond Pump Option would not need a consumptive water use permit until operational parameters were determined during the MOU.
- 19. SFWMD Operations will provide guidance on low water elevation in L-63N canal to determine if/when pumping should stop during certain times of year.
- 20. Greg Seidel noted that the estimated pump station cost \$500,000 was based on 5 cfs flow rate pump from the 2011 SFWMD documents.
- 21. FDOT is requesting final decision from SFWMD by September 4, 2015 on participation in STA option. The FDOT R/W acquisition is funded over 3 years beginning FY 2017 (July 2016) with final signed & sealed R/W Maps



complete June 2016. SR 710 is not funded for construction yet. July 2019 is the earliest construction funds could be programmed based on R/W acquisition schedule.

- 22. SFWMD participating funds for STA option could be applied to R/W costs, acceptance of pump station O&M costs or additional construction costs. It was noted that the larger STA option will need the property owner to be willing seller if additional R/W is not subject to eminent domain.
- 23. A complete review of initial comments from SFWMD on STA/Regional Pond Feasibility Study was not completed as the commenting parties were not all available. It was noted by Kevin Carter that the SFWMD preferred the Regional Pond Option A as presented in the report. However, the cost of the modification to US 441 and the riprap for the airport have made this option not favored by FDOT. It should be noted that the comments are not considered resolved and discussions are ongoing.
- 24. FDOT will prepare a summary of costs to present to SFWMD for determining if participating funds will be applied. This will include Research and Design costs typically associated with STAs.

Action Items

- 1. FDOT to prepare final presentation to FDEP and SFWMD with expected costs and proposed alternative.
- 2. Brent Setchell to determine if FDOT will agree to long term maintenance of pumps.
- 3. Greg Seidel to check with Janet Hearn for the Research & Design costs for STA facilities.
- 4. Leslie Bertolotti to provide long term monitoring costs of water quality.
- c. Attendees (Via Email)
 Amy Setchell, FDOT Project Manager
 Carl Spirio FDOT, Drainage
 Greg Griffith The Wantman Group, Permitting
 Jennifer Nunn The Balmoral Group, Drainage

Attachments – Agenda, Agenda Exhibits



SIGN IN SHEET

SFWMD PRE-APPLICATION MEETING 2 SR 710 from US 441 to L-63N Canal FPID Number 419344-3-52-01

Okeechobee Service Center March 24, 2015 10:00 am Location:

Date: Time

EMAIL ADDRESS	Henri. Belose O wantmen gould in	Octobes Med Paters Marion Went Orderson But and	SANTERED OF WAY CON	asside (a halmone browners	Wreicher Stwmo. ror	brent. Setch 11 @ dot. 544 fl. 115			I hertolo a Stumb. and	Kearter @ Stunn on!		coolate Octumbor		1	
OFFICE / RESPONSIBILITY	Temper / Porcet Maryer	October 1 Rect. Parch Mouren	OKOS COMPRES / OSR >	ON WINTER PARK / DIMINAGE	OKFS / Right of Way	FOOT - Permits			PhinchAL SciENTIST	LEMO SCIENTIST	SECTION LEADER (CUP)	LEMO ENEMBER	PRINCIPA ENGROSER WATER		
FIRM/AGENCY	Wastman Grown	Wastman Goup	Shumis	barmona broup	SFWMD	FOOT			SFWMD	SFWMD	SFWMD	SAUMD	STWMO		
NAME	Henri Belose	Alfredo Rodriguez	Losse MARINE	CREG SGIOGZ	Michelle Reichert	Brant Settell	Cotos of Les and	a distribution of the state of	LESLEY BERTOLOFF	KEVIN CARTER	TOM COLLOS	Ceyda Pointer	Zhimma Chen)	



MEETING NOTES

SR 710 REGIONAL POND PRESENTATION TO SFWMD SR 710 from US 441 to L-63N Canal FPID Number 419344-3-52-01

July 7, 2015, 1:00 P.M., SFWMD Headquarters, West Palm Beach - Building B1; Room 3B

The purpose of the meeting is for the FDOT to present a proposed Regional Pond alternative to the traditional FDOT "postage stamp" ponds. FDOT requested SFWMD to take over operation and maintenance of the regional treatment facility after construction. The following are highlights of the conversation.

- 1. Brent Setchell provided the introduction and background for the project. This included discussions of sizing and locating the proposed Regional Stormwater Pond in its current location. Brent noted that the pond was shown with 4 cells but could be configured differently as long as enough fill material was generated for the roadway project.
- 2. Brent Setchell presented the cost estimates developed for the standard pond sites versus the regional pond site. He noted that the FDOT was not interested in maintaining the pond site due to the required pump station and long term maintenance costs that exceed that of the postage stamp ponds. He indicated that the FDOT would maintain ownership but have a maintenance agreement with the entity that would maintain the facility.
- 3. Discussion ensued regarding the cost estimates. SFWMD will review and provide comment. Brent noted that the cost estimate did not include water quality sampling and testing which would likely be a condition of FDOT's ERP permit to demonstrate net improvement.
- 4. The effectiveness of the facility for removal of phosphorous was discussed. It was noted that the Dr. Harper/Permanent Pool calculations were used based on pumping flow rates for 21 day residence time and a 150 day residence time. It was also noted that the flow and concentrations in the L63-N canal are very seasonal. Greg Seidel added that Janet Hearn with ATM, Inc. had researched the available data and provided the data to Balmoral. It was agreed that Balmoral would share the spreadsheets with the SFWMD to review the calculated removal efficiencies. Beth Alvi noted that there may be a Thirsty Duck project in Pinellas County that utilized continuous flow in a wet detention facility and would check for information on effectiveness.



- 5. Brent Setchell indicated that a decision was needed by Sept 4, 2015 and that the current R/W funding is for fiscal year 2018 but no construction funding is programmed.
- 6. Greg Seidel noted that the required phosphorous removal for the project was minimal and that the pond could be constructed as a test facility with multiple cells and still meet the project requirements for nutrient removal.

Action Items

- 1. Balmoral to provide nutrient loading calculations and phosphorous testing information to the SFWMD.
- 2. SFWMD to provide comments on cost estimate and removal estimates.
- 3. Beth Alvi to check into Pinellas County project for data.
- 4. SFWMD and FDEP to determine if they will be able to provide maintenance for the proposed facility.
- c. Attendees (Via Email)
 Carl Spirio FDOT, Drainage
 Kevin Carter, SFWMD
 Greg Griffith The Wantman Group, Permitting
 Jennifer Nunn The Balmoral Group, Drainage

Attachments – Sign in Sheet, Agenda, Agenda Exhibits



SIGN IN SHEET

SR 710 REGIONAL POND PRESENTATION TO SFWMD SR 710 from US 441 to L-63N Canal FPID Number 419344-3-52-01

SFWMD Headquarter, West Palm Beach July 7, 2015 1:00 pm

Location: Date: Time

NAME	FIRM/AGENCY	OFFICE / RESPONSIBILITY	EMAIL ADDRESS
SKEG SEIDER	BACMORKE GROUP	PROJECT DRAINAGE ENG	956 dol Oct/1000
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PHONE -			
AMY SETCHEZL	FDOT	PROJECT MANGER	April Sorcher a date conto 5/10
Beth ALUI	FDEP	PROGRAM ADMINISTRATOR	ELIZABETH, MUST Plante 61.15
SARA DAVIS	FOEP	GAMMES SPECIALIST	Sara , davic O Ada cente II.
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MEETING MINUTES

PSR POND ALTERNATIVE REVIEW MEETING SR 710 from US 441 to the L-63 Canal FPID No. 419344-3-52-01

April 7, 2016 at 1:00 pm; FDOT, District 1, Bartow Office

Attendees:

Brent Setchell –FDOT, Permitting
Nicole Monies– FDOT, Permitting
David Turley – FDOT, Project Management
Alfredo Rodriguez– The Wantman Group, Assistant PM
Greg Seidel – The Balmoral Group, Drainage
Lori Stanfill – The Balmoral Group, Drainage

Greg Seidel described the proposed pond sites from the Draft Pond Siting Report (PSR) (dated March, 2014). During the process of addressing FDOT comments and investigation of the regional pond, these pond sites were updated. The original pond recommendations from the Draft PSR were Ponds 1B, 2C (Option1), 3C, 4B (Option 2), and 5B. Based upon the discussion during this meeting and other project updates, the recommended pond sites remained the same as the original estimates except in Basins 3 and 5. For Basin 3, Pond Site 3B is now preferred, and further investigation is needed in Basin 5 to determine the recommended site.

- 1. For Basin 1, the costs of Pond 1A (\$291,167) and Pond 1B (\$301,023) are relatively close. Pond 1B is located closer and just adjacent to the Taylor Creek outfall. It is also in a better location than Pond 1A for conveyance of roadway runoff to the site. Therefore, Pond 1B is still the recommended option in this basin.
- 2. In Basin 2, Pond Site 2C (Option 1) is still the recommended pond site, however, it is within 10,000 feet of the local airport. Due to this, Brent Setchell suggested that riprap be added to the pond cost estimate and reevaluate.
- 3. In Basin 3, Pond 3B is now recommended as compared to Pond 3C. FDOT will expect suitable landscaping on this site particularly due to its location adjacent to the roadway.
- 4. For Basin 4, Pond 4B (Option 2) remains the recommended option.
- 5. In Basin 5, all three options are very close in all reviewed parameters including cost, although 5A is now the lowest cost. The costs are \$444,696, \$466,083 and \$461,723 for Ponds 5A, 5B, and 5C, respectively. Further investigation will be needed to determine the best alternative considering the possible extension of the basin to Mosquito Creek and outfall of the pond to

Mosquito Creek. Use of wet or dry ponds will need to be explored. In addition, the use of the access road as the berm for Pond Site 5B should be further examined before final determination of recommended option in this basin.

Greg asked if permitting would be more difficult if proposed ponds outfall to the L-63N Canal, but Brent indicated that it should not as the proposed bridge crossing the L-63N Canal will require the Section 408 USACE review and this was completed in a straightforward fashion on the SR 70 project to the north of this crossing.

Brent also mentioned that it would not be necessary to add 20% to the pond sizes for our pond size estimates for landscaping. In addition, we do not need to include curvilinear pond design into the estimation of site size. However, each potential site should be examined for mature trees which are in good condition, and ponds should be configured around the perimeter trees if possible.

Greg asked if it would be prudent to get updated R/W costs since the initial cost estimates are 2 years old, and Brent agreed that it would. Our team will submit the request to the FDOT R/W Department to receive updated cost estimates.

cc. Attendees Henri Belrose, Wantman Group PM

File: T:\00809.00\zTBG\admin\Correspondence\SR 710 PSR Alt Review Minutes 2016 4 7.pdf

Appendix 10 SR 710 Regional Pond Feasibility Study

SR 710 Stormwater Treatment Area/Regional Pond Feasibility Study Final Submittal

Financial Project ID 432644-1-32-01

Okeechobee County, Florida

Prepared For: Florida Department of Transportation

District 1 801 North Broadway Avenue Bartow, Florida 33830

Prepared By:

The Balmoral Group 165 Lincoln Avenue Winter Park, Florida 32789

Applied Technology & Management, Inc. 5550 NW 111th Boulevard Gainesville, Florida 32653

Dewberry | Bowyer-Singleton 520 South Magnolia Avenue Orlando, Florida 32801

November 10, 2015

PROFESSIONAL ENGINEER CERTIFICATION

I hereby certify that I am a registered professional engineer in the State of Florida practicing engineering with **The Balmoral Group** and that I have supervised the preparation of and approve the analysis, findings, opinions, conclusions and technical advice hereby reported for:

PROJECT: SR 710 Stormwater Treatment Area/Regional Pond Feasibility Study

Financial Project ID: 432644-1-32-01

Okeechobee County, Florida

The engineering work represented by this document was performed through the following duly authorized engineering business:

The Balmoral Group 165 Lincoln Avenue Winter Park, Florida 32789 Telephone: (407) 629-2185

Certificate of Authorization No. 26123

This report provides the results of the analysis required for the feasibility study of the SR 710 Regional Pond and Stormwater Treatment Area (STA) in Okeechobee County. I acknowledge that the procedures and references used to develop the results contained in this report are standard to the professional practice of hydrologic analysis and hydraulic engineering as applied through professional judgment and experience.

Any engineering analysis, documents, conclusions or recommendations relied upon from other professional sources or provided with responsibility by the client are referenced accordingly in the following report.

FLORIDA REGISTERED ENGINEER:	
Gregory Seidel, P.E. Name	-
REGISTRATION NUMBER: FL #47571	
SIGNATURE: DATE:	

Executive Summary

The proposed Florida Department of Transportation (FDOT) new alignment for State Road (SR) 710 in Okeechobee County and the City of Okeechobee is currently under design by the FDOT. During the development of the Pond Siting Report, Pond Site Location 2B and the surrounding area were identified as a possible location for a regional stormwater treatment facility that could provide greater stormwater treatment benefits to the local area, as opposed to meeting only FDOT's needs. Two teleconferences were held between the FDOT, the Florida Department of Environmental Protection (FDEP) and South Florida Water Management District (SFWMD) to brainstorm the feasibility of regional treatment and possible cooperation between the agencies. At the last meeting, it was decided that the FDOT would perform a feasibility study for two options -

- 1. A <u>Regional Pond</u> constructed by the FDOT for SR 710 that would incorporate offsite areas associated with Lower Taylor Creek.
- 2. A <u>Stormwater Treatment Area</u> (STA) with interagency cooperation connected to the L-63N Canal and Upper Taylor Creek.

The goal of the study was to research these two options, including limited data collection, reaching out to stakeholders and discussing the willingness to participate with the property owner. A statement from the property owner is included in the correspondence section (Appendix E) as a supplement to the August 12, 2014 Meeting Minutes. The Regional Pond Option was researched as an FDOT-only facility with regard to design and construction and does not require financial assistance from other stakeholders. The STA options were developed for review by the other stakeholders to determine their willingness to participate in the facility. The FDOT would not be the lead agency for the design or construction of the STA facility.

The Regional Pond Option will require a 26-acre pond. There are two proposed sources for offsite water to be treated. The first source is from the Airport Ditch and would require an additional cross drain under US 441. The other source would be from L-63N Canal that would require a pumped connection. The first option reduces the nutrient loading by 496 kilograms per year (kg/yr) within Lower Taylor Creek and Lake Okeechobee, while the second option reduces the nutrient loading by up to 221 kg/yr to Lake Okeechobee. The costs are expected to be similar, since the first option is gravity flow but requires an additional 10-ft-by-6-ft cross drain and right-of-way (ROW) for the Airport Ditch Extension. The STA Option will require a pump station that will have long-term operating and maintenance costs.

Three options for the STA were evaluated. These options included a Stormwater Treatment Area (Option 1), a Biosorption Activated Media (BAM) (Option 2) and Wetland Rehydration Conservation Easement (Option 3). A 50-acre STA will reduce phosphorous by up to 727 kg/yr. The reduction of phosphorous by the BAM is based on the amount used. For this study, the reduction is up to 176 kg/yr for an initial cost of \$1.1M. Option 3 may reduce the phosphorous loading by up to 144 kg/yr and includes the purchase of a conservation easement over the wetland areas that will have increased stored water.

Summary of Options

Facility	Area	FDOT to provide Design,	Phosphorous
	(Acres)	Const. and Maintenance	Removal (kg/yr)
Regional Pond Opt A	26	Yes	496
Regional Pond Opt B	26	Yes/No	31-221
STA - Option 1	60	No	Up to 727
Biosorption - Option 2	0*	No	Up to 176
Rehydration - Option 3	162.5	No	Up to 144

^{*}May be located in existing SFWMD Easement

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1. GENERAL INFORMATION

1.1 PROJECT BACKGROUND

The State Road (SR) 710 new alignment project is located in Okeechobee County, Florida. The project is a segment of the larger SR 710 upgrade project that stretches from U.S. Highway (US) 441 in Okeechobee County to County Road (CR) 714 (S.W. Martin Highway) in Martin County. The upgrading of SR 710 is required to meet the needs of the local community in terms of improved rural connectivity, enhanced emergency capabilities and to accommodate future population and traffic growth [Florida Department of Transportation (FDOT) Project Development and Environment (PD&E) Worksheet, 2010].

The SR 710 new alignment Project in Okeechobee County and the City of Okeechobee is currently under design by the FDOT. During the development of the Pond Siting Report, Pond Site Location 2B and the surrounding area were identified as a possible location for a regional stormwater treatment facility that could provide greater stormwater treatment benefits to the local area. Two teleconferences were held between the FDOT, Florida Department of Environmental Protection (FDEP) and South Florida Water Management District (SFWMD) to brainstorm the feasibility of the regional treatment and possible cooperation between the agencies (See **Appendix E** for minutes). At the last meeting, it was decided that the FDOT would perform a feasibility study for two options:

- 1. A Regional Pond constructed by the FDOT for SR 710 that would treat offsite areas associated with either Lower Taylor Creek or the L-63N Canal.
- 2. A Stormwater Treatment Area (STA) with interagency cooperation connected to the L-63N Canal and Upper Taylor Creek.

1.2 Purpose of Report

FDOT contracted with The Balmoral Group to prepare a STA/Regional Pond Feasibility Study for the proposed construction of the SR 710 [Financial Project Identification (FPID) 419344-3-32-01].

The purpose of the study is to research whether these two options for stormwater management of SR 710 would provide a significantly greater improvement in water quality than the standard FDOT ponds. The study included limited data collection, reaching out to stakeholders and discussing the willingness to participate with the property owner.

1.3 PROJECT LOCATION AND AREA OF STUDY

The proposed SR 710 will cross Lower Taylor Creek just east of US 441 and north of NW 13th Street located in Okeechobee County, Florida. **Plate 1** shows this specific location and **Figure 1** in **Appendix A** shows the area of study. The project uses the North American Vertical Datum of 1988 (NAVD88), and the horizontal datum for the project is Florida State Plane [North American Datum (NAD) 1983], East Zone. To convert to

NAVD88, 1.17 feet (ft) was subtracted from all National Geodetic Vertical Datum (NGVD) 29 elevations

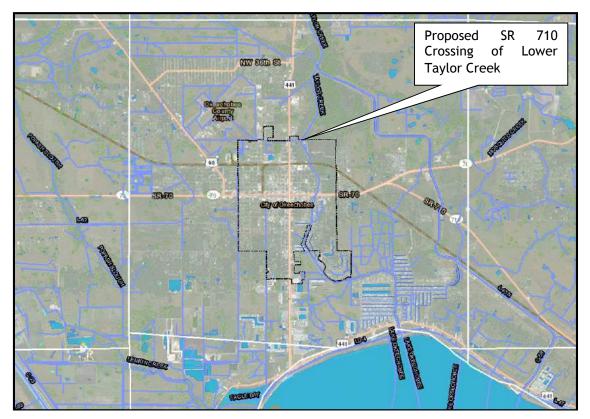


Plate 1: Taylor Creek and the City of Okeechobee

1.4 Existing Drainage Overview

Taylor Creek is part of the Lake Okeechobee watershed (See Figure 3 in Appendix A), which drains to both the Everglades and the Gulf of Mexico through a number of canals and the Caloosahatchee River. Taylor Creek is divided by S-192 into two distinct sections - Upper Taylor Creek, north of S-192, and Lower Taylor Creek, south of S-192. Lower Taylor Creek drains a smaller area than it did historically, due to the construction of the Taylor Creek Levee (referred to as L64). The U.S. Army Corps of Engineers (USACE) built the levee in the 1960s for flood control and to divert flow into L-63N Canal. Both Lower Taylor Creek and the L-63N Canal flow into Lake Okeechobee by means of further canals, pumps and control structures. Figure 5 in Appendix A is an aerial photograph taken in 1953 before canal construction.

Upper Taylor Creek drains an area of approximately 110 square miles (to the start of the L-63N borrow canal) and predominantly drains in a north-to-south direction. Upper Taylor Creek has headwaters in central-west Okeechobee County in the White Hammock locality and flows from there through a number of artificially constructed drainage lines until a natural channel forms. At the intersection with CR 68 (NW 160th St), the creek flows into the Upper Taylor Creek Canal to the point of the Taylor Creek Levee, (S-192), where flow is diverted along the L-63N Canal. Downstream of the Taylor Creek Levee, Lower Taylor Creek, the creek is again an artificial channel to the point of the proposed SR 710 bridge crossing. At this point, Lower Taylor Creek takes the form of a natural channel until it meets structure S-133/S-193 (lock and pump station) at Lake

Okeechobee. Plate 2 shows the location of the pumps and control structures associated with this system.



Plate 2: Location of USACE Structures

The Upper Taylor Creek basin contains a number of tributaries, namely Otter Creek, Wolff Creek and Williamson Ditch, which are primarily artificial drainage channels used for irrigation. Stages are maintained in all canals by controlling the stage in the L-63N Canal at Structure S-191 (the outlet of the L-63N Canal at Lake Okeechobee).

The normal operational drainage scenario for the Taylor Creek basin involves the diversion of flow from Upper Taylor Creek to the L-63N Canal at the location of the Upper Taylor Creek Levee and S-192 structure. S-192 prevents flow of water through the Upper Taylor Creek Levee to Lower Taylor Creek. The diverted flow then travels along the L-63N Canal to the C-59 Canal, where Structure S-191 controls discharge to Lake Okeechobee. Structure S-191 is operated to maintain a lake stage of 18.62 ft NAVD (19 ft NGVD) in the canals. S-191, C-59 Canal and L-63N Canal were designed for the 10-year storm event with a flow of 7440 cubic feet per second (cfs).

S-192 is a gated culvert and pump station at the Upper Taylor Creek Levee and start of the L-63N Canal. Its purpose is to divert flow from Upper Taylor Creek along L-63N Canal. It is opened only for maintenance activity on L-63N Canal or to dilute low quality water in Lower Taylor Creek when Lake Okeechobee is below 12.83 ft NAVD (14 ft NGVD), allowing for gravity flow. S-192 permits back pumping from the Lower Taylor Creek into L-63N Canal in extreme flooding events. The S-192 is not designed to convey flood flows.

Lower Taylor Creek begins downstream of S-192 and flows in a southerly direction to its ultimate control structure of S-193, located 6 miles southeast of the City of Okeechobee. Structure S-192 was previously called HGS No. 6 and was left open to permit unrestricted navigation between Lake Okeechobee and Lower Taylor Creek. It was later modified to a lock structure to allow navigation when the lake regulation schedule was raised to the 15.5 to 17.5 ft NGVD range. This structure also acts as a hurricane control structure preventing hurricane tides from entering Lower Taylor Creek. There is no design flood for this structure since flood flows are discharged through adjacent pump station S-133. If the lake stage is below 12.83 ft NAVD (14 ft NGVD), S-193 is opened to allow tailwater flow from the lake to Lower Taylor Creek. The quantity introduced is pumped into the L-63N Canal at S-192 to maintain consistent stages. No standard practice of opening this structure occurs during flood conditions.

Adjacent to S-193, S-133 is a pump station with five 48-inch steel pipes that are designed to remove three-quarters of an inch of runoff per day from its tributary drainage area of 16,190 acres (25.3 square miles), resulting in a discharge of 625 cfs into Lake Okeechobee.

1.5 Drainage Basin History

A review of historical flood information was completed during the bridge hydraulics report (BHR) development for the proposed SR 710 crossing of Lower Taylor Creek. Significant flooding occurred around the lower-lying areas of Lake Okeechobee during the early 1900s. This flooding, mainly as a result of lake surges from hurricane wind forces, caused significant damage and claimed the lives of thousands of local residents. As a result, the USACE was engaged to build a system of canals, levees and locks to control water movement, as well as protect the areas surrounding the lake from storm surges.

Since USACE completed the works in the 1960s, and with strict operational standards, flooding in the area has declined in both frequency and magnitude. However, the 2013 Preliminary FEMA Flood Insurance Study (FIS) states that the existing creeks and sloughs in the area have inadequate capacities to drain local and upland areas during periods of heavy rainfall and ponding of floodwaters in those areas can be expected.

The Okeechobee 2010 Local Mitigation Strategy (LMS) noted that a number of low-lying or poorly drained areas regularly experience flooding with or without a storm. One such area is the southern portion of Okeechobee County adjacent to Lake Okeechobee. Floods have been experienced and regularly affect hundreds of homes and several roads for many days every few years (Okeechobee 2010 LMS). Available information indicates that the canals, structures and levees significantly influence the flooding problems.

1.6 Previous Flood Studies

FEMA Flood Insurance Study - Okeechobee County Florida Unincorporated Areas, August 4, 1980

The Federal Emergency Management Agency (FEMA) has published an FIS report for Okeechobee County and the incorporated areas. FEMA Federal Insurance Administration (FIA) staff with the assistance of USACE, investigated the major sources of flooding in the area of interest and the flood protection measures that were inexistent at the time of the report. Two methods were used to compute the flood stages for the S-133 basin since it presented riverine characteristics, but also acted as a large storage basin controlled by pump. The first method, a Hec-1 model, was created for the S-133 drainage basin, and peak discharges were calculated. Pumps were assumed to be operating at peak capacity with the lake level at 18.5 ft NGVD (17.33 ft NAVD). The second approach was to use a volumetric approach that compared the volume of rainfall for the design storms to the volume of water that could be pumped for a period of time. The resultant volume to be ponded was compared to a stage-storage curve and resulted in a peak stage. The results of the Hec-1 model produced slightly lower stages and were selected as the flood elevations for the S-133 basin. It was found that no 'floodways' existed due to the predominance of ponding as the primary cause of flooding.

Preliminary FEMA Flood Insurance Study - Okeechobee County Florida Unincorporated Areas, 2013 (prepared by Taylor Engineering Inc.)

Although preliminary in status, the information provided in this FIS (Taylor Engineering, Inc., 2013) is assumed to revise and supersede the information presented in the 1980 FIS for Okeechobee County. All vertical elevations presented in this study are in NAVD88. As part of this analysis, a detailed hydrologic and hydraulic study was performed for Lower Taylor Creek; this included the S-133 drainage basin previously studied under the 1980 FIS. Lower Taylor Creek was defined as from the S-193 to the L-63N. HEC-HMS was used to update the hydrologic data that was calibrated using U.S. Geological Survey (USGS) gage data and rainfall from tropical storms. Cross-section geometry was based on digital terrain data and field survey. Hydraulic analysis utilized the HEC-RAS step-backwater computer program, which employed a normal depth downstream boundary condition.

Technical Memorandum - An Atlas of Martin County Surface Water Management Basins, Richard M. Cooper and Ray Santee, (DRE-266) November 1988

This SFWMD-sponsored publication summarizes the events leading to USACE constructing these canals, levees and control structures and the uses of these canals. Of particular interest to this investigation is the detail contained for the C-59 (Taylor Creek-Nubbin Slough) Basin. A description of the flow routing and control structure operation is provided (**Plate** 3), along with a figure to show the basin, the location of the control structures and main channel alignments (**Plate** 4).

Structure	Туре	Design HW Stage (ft NGVD)	Design TW Stage (ft NGVD)	Optimum Stage (ft NGVD)	Design Discharge (cfs)	Peak Stage (ft NGVD) Peak Discharge (cfs)	Date of Peak
S-191 Stage divide	Gated Spillway, 3-gates 17.6ft high x 27.8 ft wide NetCrest lgth = 81.0ft Crest elev = 7.4.ft NGVD	19.2	18.6	19.0 19.2 ≥ HW ≥ 18.8 (Gate closed if TW > HW)		HW = 23.08 Q = 3236	7/18/74 6/25/87
S-192 Divide structure and pump station, Water supply from L-63N borrow canal to Taylor Creek	Gated Culvert 1-48in x 112ft CMP Invert elev = 8.0ft NGVD Pump Station, 1 unit: 13500 GPM	21.6 (water supply)	13.0 (water supply)	HW = 19.0 TW = 14.0 (water supply)	Normally Closed, open only for water supply		
G-106 Divide Structure and water supply from L- 63N borrow canal to S-133 basin	Gated Culvert 1-36in x 90ft CMP Invert elev = 15 0ft NGVD				Ocassionally lopen for water supply		
in = inches ft = feet elev = elevation	lgth = Length TW = Tail water Q = discharge in cfs	RCP = Reinfe	igated metal pipe orced concrete pipe eet relative to Natior	HW ≈ Head with CFS ≈ Cubic fe al Geodetic Vertical D	et per second	ds = downstre ups = upstrea	

Plate 3: C-59 Design Information

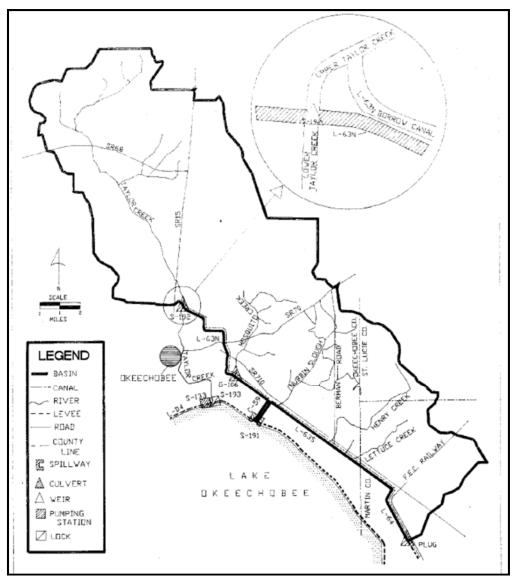


Plate 4: C-59 Control Structure Location

1.7 WETLAND FIELD REVIEW AND INFORMATION GATHERING

A preliminary ecological field review was performed to evaluate wetlands and species listed as threatened or endangered within the project vicinity. Current PD&E documents and biological evaluations currently underway under FPID 419344-3-32-01 were reviewed. A desktop review of available published information from federal and state online databases was performed to evaluate listed species that may occur in the project area. Data collection consisted of literature review of existing sources for information useful in identifying the occurrence or potential occurrence of wildlife species listed as threatened or endangered or as species of special concern (collectively recognized as listed species), as defined by U.S. Fish and Wildlife Service (USFWS) and/or the Florida Fish and Wildlife Conservation Commission (FWC). In addition, the presence of designated critical habitat and/or vegetative communities and land uses with the potential to support listed species was evaluated.

The literature review included the following sources: Natural Resources Conservation Service (NRCS) (formerly known as the Soil Conservation Service [SCS]) Soil Survey of Okeechobee County, Florida; USGS topographic quadrangle maps; FWC bald eagle and waterbird colony databases; Florida Natural Areas Inventory (FNAI) Okeechobee County tracking list; previous studies available; and false-color infrared and true-color aerial photography of the project corridor. Additional resources, such as the FNAI Field Guides and Rare and Endangered Biota of Florida Series, were used to evaluate habitat and vegetative community requirements for those species potentially occurring within the proposed project corridor.

Land use types located within the proposed project were identified through color aerial photograph interpretation and compared to land uses identified by FDOT Florida Land Use, Cover and Forms Classification System (FLUCFCS) (FDOT, 1999). Estimated wetland limits were identified on an aerial exhibit. A preliminary qualitative evaluation of the onsite wetlands system(s) was conducted. The wetlands were identified in general accordance with the USACE October 2008 Regional Supplement to the Corps of Engineers Wetland Delineation Manual: Atlantic and Gulf Coastal Plain Region and the State of Florida's Delineation of the Landward Extent of Wetlands and Surface Waters (Chapter 62-340, Florida Administrative Code). Seasonal high water elevations were marked at six locations within the proposed STA and surveyed to better understand the normal water and allowable peak stage. Three Seasonal High Water Elevation (SHWE) nails were set at each location and the average elevation was used.

The wetland and wildlife evaluation is provided in **Appendix D**.

1.8 STAKEHOLDER COORDINATION

The project team contacted local stakeholders including the property owners, pump operators, City of Okeechobee, Okeechobee County, FDEP, SFWMD and USACE, etc. An introductory stakeholder meeting was held on July 31, 2014 in Okeechobee to discuss the proposed project. The meeting focused on providing project background and gauging the willingness of the stakeholders to participate via funding, design, construction, and maintenance. The data gathering included obtaining actual costs and nutrient load reductions on recently constructed water quality improvement projects.

Input was solicited for ideas and options, as well. The project team conducted follow-up meetings with various stakeholders. A summary of the meetings held in reference to the Regional Pond and STA feasibility study are as follows and the meeting minutes are included in **Appendix E**:

- Initial Brainstorming Meeting September 13, 2013
- Second Brainstorming Meeting April 4, 2014
- Introductory Meeting with the Hamrick property owners July 11, 2014
- Introductory Stakeholder Meeting July 31, 2014
- Goto Coordination Meeting with the Hamricks August 12, 2014
 - o Includes Response from Mike Hamrick
- AVCON Meeting to discuss airport interests August 14, 2014
- Email Coordination with the SFWMD Pump Operators September 12, 2014

In addition to meetings, a telephone log was kept to document and track project calls.

2. REGIONAL POND ANALYSIS

2 GENERAL

The Regional Pond analysis evaluated two separate sources of runoff for the same proposed pond area. Option A treats runoff already within the Lower Taylor Creek basin. Option B diverts runoff from the L-63N Canal into Lower Taylor Creek basin for treatment in the Regional Pond.

2.1 OPTION A

2.1.1 General

A preliminary HEC-RAS model was developed based on the draft Taylor Creek BHR model submitted for FPID 419344-3-32-01 (SR 710 New Alignment in Okeechobee). The predevelopment model was based on the existing conditions model and flow rates developed during the BHR with the addition of adding to the HEC-RAS Model the portion of the Airport Ditch from US 441 back to the west to NW 9th Avenue. This would allow an analysis of the channel response to raising the tailwater levels where the Airport Ditch intersects Lower Taylor Creek. Limited survey data was obtained for areas along the Airport Ditch and the Lower Taylor Creek to verify critical elements.

The analysis includes nutrient loading calculations, preliminary design, and construction cost estimates. Permitted facilities within the Airport Ditch basin were reviewed to establish the treated areas versus untreated areas. Treatment calculations were performed to demonstrate compensatory treatment for a portion of SR 710. A large wet detention pond will be utilized for water quality and attenuation and will provide a source of fill material for the SR 710 project. All files developed during the current SR 710 project were utilized, including survey, ROW and the current design files. The pond was designed with 1:2 slopes to meet the Federal Aviation Administration (FAA) requirements for wildlife attractants since it is located within the 10,000-foot buffer shown in **Appendix A, Figure 4.**

2.1.2 Drainage Basin Specific Documents

FEMA Flood Insurance Rate Map (FIRM), Okeechobee County, Florida, Unincorporated Areas, Panel 200 of 275, February 4, 1981

The FIRM provides details of the design 100-year flood extent, as well as flood zones for the area adjacent to Taylor Creek and the City of Okeechobee. This will provide details of the expected flood extent and any limitations on bridge design to account for regulated floodways. Lower Taylor Creek was not included in this information. **Plate 5** shows the available floodplain data for the area.

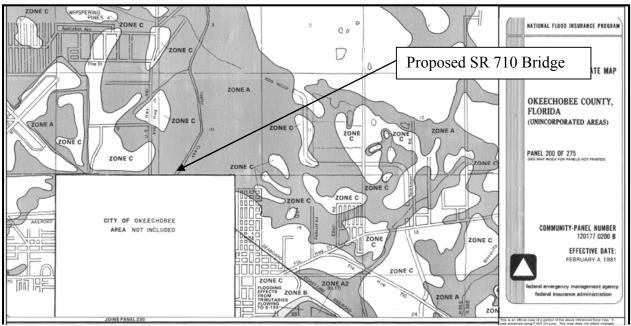


Plate 5: FIRM Panel 200 of 275, 2/4/1981

The Preliminary 2013 FEMA Maps became available in May 2013; however, these maps are not scheduled to become effective until March 20, 2015. See **Plate 6** for Preliminary 2013 FEMA FIRM.

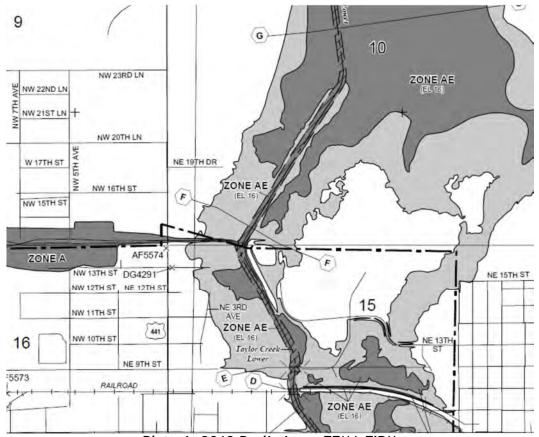


Plate 6: 2013 Preliminary FEMA FIRM

Central and Southern Florida Project for Flood Control and Other Purposes System Operating Manual - Lake Okeechobee and Everglades Agricultural Area Volume 3 DRAFT, Department of the Army Corps of Engineers, Jacksonville District, December 2005

This manual provides operational instruction to both the SFWMD and USACE in the operation of the various structures controlling water movement around and into Lake Okeechobee, as well as its tributaries and the Everglades Agricultural Area. This manual will provide guidance on how the structures around the proposed SR 710 bridge site will operate and, hence, allow impacts of the operation to be considered within this BHR, ensuring appropriate design is achieved for all operational conditions.

Okeechobee County Local Mitigation Strategy 2010, Okeechobee LMS Working Group, 2010

This report was prepared to assist in mitigation planning, enhancing public awareness, providing a decision-making tool for management, complying with state and federal program requirements, and allowing mitigation coordination between agencies. The report provides detailed and comprehensive data and discussion for all potential natural disasters, including flooding. As a result, flood history can be extracted from this report and used to verify design floods and areas susceptible to inundation. Flood history was not extracted from this report since the areas susceptible to inundation appeared to be outside of the impacts of the L-63N Canal hydraulic model. Plate 7 shows the extents of the 100-year event expected flood hazards.

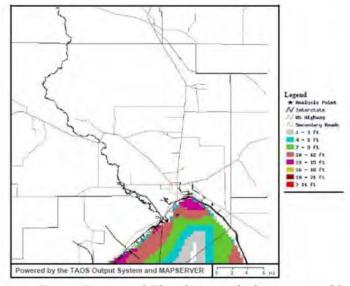


Plate 7- 100-year Event Expected Flood Hazards from 2010 Okeechobee LMS

2.1.3 Drainage Basin

Lower Taylor Creek drains a 5.46 square mile basin to the proposed SR 710 bridge. **Figure 7** in **Appendix A** shows the extent of the Lower Taylor Creek basin draining to SR 710. Lower Taylor Creek generally drains in a southerly direction towards the project site and consists primarily of manmade channels and tributaries that have a confluence immediately upstream of the proposed bridge site where the Airport Ditch meets Lower Taylor Creek. The existing Airport Ditch is a manmade channel that conveys flow west to east toward

Lower Taylor Creek. The Airport Ditch conveys runoff through SR 15 (US 441) via a 10-ft-by-6-ft box culvert just prior to draining into the main channel of Lower Taylor Creek immediately upstream of the proposed SR 710 crossing.

The Lower Taylor Creek basin area was delineated using light detection and ranging (LiDAR) data, existing permit information, and field information. This basin was divided into two sub-basins consisting of the sub-basin for the main channel of Lower Taylor Creek and the sub-basin for the Airport Ditch. **Table I** shows the breakdown of the two drainage areas flowing to the proposed crossing.

Table 1: Lower Taylor Creek at Proposed SR 710 Basin Summary

Basin	Area (sq. mi.)	10 YR Flow (CFS)	25 YR Flow (CFS)	50 YR Flow (CFS)	100 YR Flow (CFS)
Taylor Creek	2.20	201	281	346	417
Airport Ditch	3.26	437	570	699	838

The basin varies in elevation from approximately 40 ft (NAVD88) at the northern basin boundary to about 7.0 ft NAVD (bottom of the channel) at the project site. The upper and middle portion of the basin consists mostly of wetlands and rural properties (beef and dairy farmland), and the lower portion consists mostly of the low-density residential areas of Northern Okeechobee as well as the Okeechobee County Airport.

The proposed SR 710 crossing at Lower Taylor Creek is influenced by local surface water runoff and backwater flows from Lake Okeechobee (during certain operational circumstances).

The SR 710 Regional Pond is located within SFWMD jurisdiction, which will be responsible for review and issuing the environmental resource permit (ERP) for the project. The Regional Pond would be constructed as part of the new alignment construction of SR 710, and these improvements will be included in the roadway ERP permit.

2.1.4 HEC-RAS Analysis

The pre-development versus post-development HEC-RAS analysis was based on comparing the existing conditions to a proposed condition that extended the Airport Ditch over Lower Taylor Creek to the Regional Pond, a distance of approximately 1,000 ft east of Lower Taylor Creek. See **Figure 10** in **Appendix A** for the proposed modifications at the confluence of the Airport Ditch and Lower Taylor Creek. The concept diverts the Airport Ditch flow over Lower Taylor Creek in a ditch parallel to SR 710 into the proposed Regional Pond. The proposed Regional Pond has a control elevation at 18.0 ft NAVD. The existing 10-ft by-6-ft box culvert capacity at US 441 was expanded until the increase in tailwater would not cause an increase in the upstream stage. The existing headloss across the culvert for the 50-year storm event is 4.66 ft. By adding a culvert of the same size, the head loss is dramatically reduced. A tailwater in the Regional Pond of 21.0 ft NAVD was utilized for the post-construction conditions, which assumes 2.5 ft over the treatment weir at elevation 18.5 ft NAVD. The HEC-RAS model shows no rise in the stages in the Airport Ditch upstream of the proposed double 10-ft by-6-ft box culverts under US 441. Survey information was collected for cross sections further west of US 441 and includes the culvert

under NW 9th Avenue. The HEC_RAS calculations are included in **Appendix B** and the results are provided in **Table 2**.

Table 2: Airport Ditch Pre-Post HEC-RAS Analysis

UEC DAC	10-Year Water	Surface Elevation	Difference	25-Year Water	Surface Elevation	Difference	50-Year Wat	er Surface Elevation	Difference	100-Year Wate	er Surface Elevation	Difference
HEC-RAS Model Cross	(feet	NAVD88)	(feet)	(feet N	IAVD88)	(feet)	(fee	et NAVD88)	(feet)	(feet	: NAVD88)	(feet)
Section	Exist	Proposed Double Culvert		Exist	Proposed Double Culvert		Exist	Proposed Double Culvert		Exist	Proposed Double Culvert	
4430.000	27.83	27.83	0.00	29.10	29.10	0.00	29.70	29.70	0.00	29.84	29.85	0.01
4330.000	27.77	27.77	0.00	29.05	29.05	0.00	29.64	29.64	0.00	29.76	29.77	0.01
Culvert	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
4280.000	24.36	24.34	-0.02	25.16	25.02	-0.14	25.97	25.58	-0.39	26.99	26.10	-0.89
3550.000	23.74	23.71	-0.03	24.60	24.36	-0.24	25.52	24.89	-0.63	26.62	25.38	-1.24
2780.000	23.39	23.34	-0.05	24.29	23.97	-0.32	25.26	24.49	-0.77	26.43	24.96	-1.47
2100.591	23.05	22.99	-0.06	24.00	23.60	-0.40	25.05	24.10	-0.95	26.30	24.55	-1.75
1527.972	21.80	20.97	-0.83	23.15	21.55	-1.60	24.52	21.98	-2.54	26.25	22.38	-3.87
1344.355	21.85	20.78	-1.07	23.12	21.72	-1.40	24.50	22.10	-2.40	26.20	22.45	-3.75
Culvert	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
1218.437	18.55	20.47	1.92	19.26	21.26	2.00	19.86	21.38	1.52	20.43	21.39	0.96
972.498	17.83	20.31	2.48	18.48	21.08	2.60	19.00	21.11	2.11	19.50	21.30	1.80
648.236	16.46	20.33	3.87	17.46	21.15	3.69	17.99	21.22	3.23	18.50	21.30	2.80
267.180	14.24	20.30	6.06	16.66	21.12	4.46	17.19	21.18	3.99	17.69	21.25	3.56
-232.820		20.24	20.24		21.06	21.06		21.09	21.09		21.13	21.13
-732.820		20.17	20.17		21.00	21.00		21.00	21.00		21.00	21.00

2.1.5 Treatment Volume Calculations

Option A is designed to treat the required presumptive runoff for the proposed SR 710 improvements only. Figure 9 in Appendix A shows the location of the Regional Pond. The total area for proposed SR 710 Basin 1 through Basin 5 is 77.78 acres. The required treatment volume is 1 inch over this drainage area for wet detention ponds and results in 6.48 acre-feet (ac-ft) of treatment volume. Only SR 710 Basin 1 and Basin 2 will be routed to the pond. Compensating treatment volume will be provided for SR 710 Basin 3, Basin 4, and Basin 5 by treating a portion of the Airport Ditch drainage area. The proposed SR 710 Basin 1 and Basin 2 were delineated in the Draft Pond Siting Report and total 40.37 acres. The SR 710 Possible Regional Pond Brainstorming Meeting 2 Minutes in Appendix E show the proposed drainage basins for SR 710 for this option.

The proposed design provides 9.98 ac-ft of treatment with the weir elevation set at 18.5 ft NAVD. The treatment volume calculations are included in **Appendix B.**

2.1.6 Nutrient Loading Calculations

Option A is designed to provide nutrient loading reduction for total phosphorous (TP) and total nitrogen (TN) outflow to Lower Taylor Creek. The nutrient loading calculations were performed in accordance with the current basin management action plan (BMAP) land use designations and applied event mean concentration (EMC) values. Figure 8 in Appendix A identifies the land uses utilized for the nutrient loading calculations.

The Airport Ditch drains a 2,086-acre area. A review of the permitted treatment areas within the drainage area determined that 231.78 acres of the basin have permitted treatment facilities. Thus, 1,855 acres remain untreated and discharge through The Airport Ditch to Lower Taylor Creek. The permitted treatment facilities are shown on **Figure 7** in **Appendix A**. Although the Regional Pond provides additional pollutant removal for those permitted treatment areas, those areas are excluded from the nutrient loading basin to provide a conservative estimate.

The total area included in the nutrient removal calculations for the Regional Pond is 1,895 acres, which includes the untreated areas of the Airport Ditch drainage basin and the proposed SR 710 Basin 1 and Basin 2.

The proposed SR 710 alignment provides a reduction in phosphorous and nitrogen compared to the pre-development loading due to the change in land use from pasture to highway. The Lower Taylor Creek basin will also have a reduction in post-development loading since the Regional Pond area will not generate a phosphorous or nitrogen loading.

With 227 ac-ft of permanent pool, the Regional Pond provides a TN removal of 34.7 percent and a TN removal of 63.0 percent across the total drainage area of 1,894.59 acres. This is a net benefit to Lake Okeechobee, with a TP removal of 39.7 percent and a TN removal of 25.0 percent for the 5.46 square miles draining to the SR 710 crossing of Lower Taylor Creek. **Table 3** summarizes the nutrient loading reductions.

Table 3: Option A Regional Pond Nutrient Loading Reductions

Nutrient	Pre-Dev (kg/yr)	Post-Dev (kg/yr)	Reduction (kg/yr)	Reduction (%)
Phosphorous	1250	754	496	39.7
Nitrogen	7489	5616	1873	25.0

The nutrient loading calculations are included in Appendix B.

2.1.7 Floodplain Impact Estimates

The 2013 Preliminary Flood Insurance Rate Map prepared for Taylor Creek shows that Lower Taylor Creek is a regulatory floodway. However, according to information obtained from Okeechobee County, the 2013 FEMA Flood Maps are not scheduled to be adopted until March 20, 2015. The FEMA FIRM Maps currently in effect do not show Lower Taylor Creek, and the FEMA FIS states that Lower Taylor Creek is not within a floodway.

No floodplain impacts are associated with the Regional Pond option.

2.2 OPTION B

Option B will utilize the same Regional Pond area and shape but will include only Basins 1 and 2 of the roadway basins as well as flows being diverted from the L-63N Canal. A pump system will be required to divert flow from the L-63N Canal to the Regional Pond. A pump system may also be needed to discharge treated stormwater back into the L-63N Canal.

The calculations in Appendix B for the SR 710 Regional Pond withdrawing L-63N water were performed by working the nutrient removal calculations backwards to determine an appropriate inflow rate. The nutrients from the roadway runoff were ignored. The calculations are based on the Harvey Harper methodology presented in the Evaluation of Current Stormwater Design Criteria within the State of Florida Final Report, June 2007 prepared by Harvey Harper and David Baker for the FDEP. The flow rate was controlled by the assumed residence time for the permanent pool. The residence time then determined the removal efficiency. The flow rate controlled the volume of the high concentration

runoff to be extracted from the L-63N Canal. Two residence times were evaluated to determine a range for the phosphorous removal: 21 days and 150 days. Once the removal rate was determined, the depth to anoxic conditions was calculated and the removal rate reduced for the reduction in permanent pool volume. These calculations utilized TP concentrations and TP removal rates provided by SFWMD, which were based on observed concentrations at the S-133 structure. The results are summarized in Table 4.

Table 4: Phosphorous Reduction for the Regional Pond Option B

Residence Time	Flow Rate (cfs)	Flow Rate (GPM)	Yearly Volume (Ac-Ft)	Reduction (kg/yr)	Depth to Anoxic Conditions (ft)
21 Days	5.44	2440	3940	221	8.8
150 Days	0.76	340	522	31	8.8

The results indicate that the higher flow rate would increase the reduction but it would also increase the cost of pumping. The water would need to be pumped out of the canal and into the pond and, if the discharge remains in the Lower Taylor Creek basin, it will need to be pumped to Lake Okeechobee at S-133. If the pond were relocated closer to the L-63N Canal, the pond may be able to gravity discharge back into the L-63N but would not be able to treat as much of the roadway runoff. Alternatively, the treated stormwater could be pumped back into L63-N, which would further increase the pumping costs.

3. STORMWATER TREATMENT AREA ANALYSIS

3.1 GENERAL

Three different types of alternative water quality treatment systems were evaluated. They include 1) a 60-acre STA, 2) use of BAM either within or beside Lower Taylor Creek downstream of S-192 to enhance nutrient removal, and 3) onsite retention of stormwater runoff in existing wetlands on the portion of the property lying east of Lower Taylor Creek. Estimates of both TN and TP load reduction were calculated for each of the alternatives, and estimates of design, construction and maintenance costs are provided.

3.2 LITERATURE AND EXPERT PANEL REVIEW

In preparation for development of the three alternative water quality treatment options, ATM interviewed experts from FDEP, SFWMD, USACE, and industry for background information on STA and alternative system experiences, costs, treatment effectiveness and design considerations. Literature supporting previous STA projects and outcomes was reviewed, and salient points are summarized in this section. Other items considered throughout these discussions include:

- Feedback from SFWMD staff on how an STA at this site could fit in to the water management district's overall water quality improvement plan for the Lake Okeechobee basin.
- 2. Willingness of the property owner to participate in some fashion, either as a seller or other mode of participation, and identification of opportunities to work with Florida Department of Agriculture and Consumer Services (FDACS) and the property

owner to develop additional water storage on the property or to help fund structural agricultural best management practices (BMPs).

3. Incorporation of alternative technologies into the STA (e.g., BAM).

As part of this background review, three existing or planned STAs)were reviewed to provide information on STA experience, costs, treatment effectiveness and design considerations. STAs reviewed are all located in the Taylor Creek-Nubbin Slough sub-watershed of the Lake Okeechobee basin and include the Taylor Creek STA, the Nubbin Slough STA, and the Lakeside Ranch STA. See **Figure 11 in Appendix A** for STA locations. Results of this review are presented in the following sections.

Taylor Creek STA

The Taylor Creek STA was constructed in April 2006 and began flow-through operations on June 26, 2008. The STA has an effective treatment area of 118 acres, which is small compared to the STAs operated by SFWMD south of Lake Okeechobee. The total site area is 142 acres. Up to four pumps, each with a discharge capacity of 6 cfs, divert water into the STA. Diverted water flows through two treatment cells and discharges back into Upper Taylor Creek approximately 1.2 miles downstream. Pumps operate automatically based on the stage in Upper Taylor Creek. Normal operational water depths average 1.5 ft, but during the dry season, a minimum water depth of 0.5 ft is maintained to prevent the treatment cells from drying out. Water levels in the treatment cells are regulated via adjustable gates between the two treatment cells and at the downstream discharge point.

This STA was designed to remove 2.08 metric tons (mt) of phosphorus annually, or about 9 percent of the TP load at that point in Upper Taylor Creek. The design removal efficiency is 38 percent (Goforth, 2005b). Since commencement of operations in June 2008 through the end of water year 2013 (April 30, 2013), phosphorus removal has ranged from 0.58 to 1.11 mt annually. This represents 37 months of flow-through operations over a total of 58 months. Operation statistics and water quality and loading information are presented in Table 5. The STA performed reasonably well during the first 2 years of operation, removing 31 percent and 64 percent of input load in WY2009 and WY2011, respectively. For the most recent 2 water years, however, measured load reductions were only 20 and 22 percent. This is attributed to reversals in TP concentration, i.e., the outflow concentration of phosphorus is higher than the inflow concentration, and is discussed below in more detail.

Table 5: Summary of calculated operational parameters and performance metrics for the Taylor Creek STA by water year (Source: 2014 South Florida Environmental Report)

Parameter	WY2009	WY2011	WY2012	WY2013
Period of operation, days	244	235	366	276
Total inflow, ac-ft	9,218	6,988	13,188	5,810
Hydraulic loading rate, cm/d	10.04	7.70	9.31	5.44
Inflow TP, μg/L	408	167	341	368
Total Load In, MT	4.64	1.44	5.51	2.64
TP mass load rate, g/m²/d	0.038	0.013	0.032	0.020

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Parameter	WY2009	WY2011	WY2012	WY2013
Total outflow, ac-ft	8,767	6,257	12,208	5,762
Outflow TP, µg/L	295	68	292	289
Total Load Out, MT	3.12	0.52	4.40	2.05
HRT, d	6.34	7.75	6.52	9.72
TP mass removed, MT	1.44	0.91	1.15	0.58
TP Conc reduction	27.5%	59.3%	14.4%	21.5%
TP Load Reduction	31.1%	63.6%	20.2%	22.0%

The Taylor Creek STA has experienced a number of operational challenges. In February 2009, the culvert at the STA outlet failed, and the STA was inoperable for 20 months, resuming normal operations in September 2010. In addition, for the past 2 water years, TP load removal efficiency was only about 20 percent. The poor performance is attributed to a large number of reversals in weekly outflow TP concentrations. Fifteen reversals occurred during WY2012, nine of which happened between November 10, 2011 and February 15, 2012. The average difference between inflow and outflow TP concentrations during these reversals was 43 parts per billion (ppb). In WY2013, a pattern of reversals was observed between October 2012 and January 2013, and flow-through operations were discontinued on February 1, 2013. During the 4-month period in which flow reversals were occurring, 309 kilograms (kg) of TP were released into Upper Taylor Creek. The STA remained offline through the end of the water year, April 30, 2013. Minimal pumping into the STA occurred during this time so that the desired water levels were maintained. One theory about the reason these flow reversals are occurring is that when the Grassy Island Hybrid Wetland Treatment Facility is functioning well, the inflow concentrations of phosphorus to Taylor Creek STA are low enough that to establish equilibrium, phosphorus is transferred from the sediments to the water column instead of the reverse (Joe Albers, personal communication). The Grassy Island facility is located on Upper Taylor Creek, approximately 1.2 miles upstream of the intake to the Taylor Creek STA.

Nubbin Slough STA

The Nubbin Slough STA was designed and built in conjunction with the Taylor Creek STA. Although construction was completed in 2006, the facility is not yet operational due to a number of issues, including mechanical problems discovered during pump tests. There have also been problems with accumulation of sediment in the pump basin. The final repair to a damaged outfall structure is expected to be completed by the end of October 2014, with responsibility transferred from USACE to SFWMD shortly thereafter.

Nubbin Slough STA is a two-cell system, with a total treatment area of 773 acres. SFWMD recognized a significant operational constraint in that the system cannot pump sufficient water to keep the entire STA wet. If the STA goes dry, there can be a net export of phosphorus from the system. To help maintain a more consistent water supply, the Nubbin Slough design includes a 30-acre pond that can store up to 90 ac-ft of water to be released as needed into the STA. Even with this additional storage, the STA is expected to go dry, and SFWMD will be monitoring the system for the occurrence of TP export once the system is operational.

Lakeside Ranch STA

The Lakeside Ranch STA is located on a 2,700-acre property in western Martin County and adjacent to Lake Okeechobee. The project was designed in two phases. Phase I is on the north side of the property and includes 1,200 acres of treatment. Phase II will provide an additional 788 acres of effective treatment. Construction of Phase I was completed in 2012 and flow-through operations commenced in July 2013. The 2015 South Florida Environmental Report will include the first year of water quality reporting under operational conditions for the period between July 2013 and April 30, 2014.

Initial TP reduction estimates for Lakeside Ranch based on modeled results totaled 25.8 mt, including 15.4 mt in Phase I and 10.4 mt in Phase II (Hazen and Sawyer, 2011). Current reductions for both phases are 19 mt (Odi Villapando, personal communication). The total load reduction estimate included in the draft Lake Okeechobee BMAP for both phases is 21.6 mt, 14 mt for Phase I and 7.6 mt for Phase II.

Summary of Existing and Planned STA Costs

Costs for these three STAs are summarized in Table 6. Except for the costs for the Lakeside Ranch Phase II and design, permitting and construction costs for Taylor Creek STA, costs were obtained from the draft Lake Okeechobee BMAP document. Initial costs for Phase II of Lakeside Ranch are based on personal communication with SFWMD staff and initial capital costs for Taylor Creek STA were obtained from Hazen and Sawyer (2011).

Table 6: Summary of Existing STA Costs

Facility	Design, Permitting,	Annual Operation	Initial Cost per
Facility	and Construction (\$)	and Maintenance (\$)	Treatment Acre (\$)
Taylor Creek	5,642,293	50,000	47,816
Nubbin Slough	21,257,707	100,000	27,500
Lakeside Ranch Phase I	22,800,000	341,000	19,000
Lakeside Ranch Phase II	25,000,000	Not available	31,726

<u>Alternative Technologies</u>

Permeable Reactive Barriers (PRBs)

SFWMD recently completed a pilot study to assess the feasibility of using PRBs to reduce TP loads to Lake Okeechobee (IFAS 2014). The configuration of PRBs for this study consisted of trenches dug perpendicular to the direction of groundwater flow and filled with a medium that is capable of reacting to and binding the pollutant of concern. The medium used in this study was potable water treatment residuals produced from aluminum salts (Al-WTRs). Al-WTRs are capable of long-term sequestration of phosphorus, and they are readily available at little to no cost. Two study sites were selected. The first site was at an abandoned dairy and the second was at an active dairy. The first site selected did not have sufficient topography to provide adequate groundwater flow through the PRBs for phosphorus removal. In addition, the placement of the PRBs was too far from the water bodies of interest, and the benefit of the PRB was lost because the groundwater picked up phosphorus from the soil before discharge into the surface water. The up-gradient and

down-gradient TP concentrations were not statistically different. The conclusion was that placement of PRBs in the middle of highly impacted areas is not a good idea. The PRBs should be placed down-gradient of the impacted soils. The second site had much better hydraulic conditions, i.e., greater flow through the PRB, but the amount of phosphorus removed was low because the concentration of phosphorus in the groundwater was lower than expected.

Floating Aquatic Vegetation Treatment

The potential use of a new technology called Floating Aquatic Vegetation Treatment (FAVT) is being evaluated concurrent with this study. FDACS is providing funding this fiscal year for the development of an FAVT system in conjunction with a willing property owner. FAVT is a type of wetland treatment system that uses a combination of floating and submerged vegetation for phosphorus removal. Floating vegetation, typically water hyacinth, is used in the top one third of the water column. Water hyacinth is efficient at nutrient removal, but will eventually stop growing and need to be removed. The FAVT system consists of a deep zone treatment area and a shallow zone treatment area. To remove the vegetation, the shallow zone is allowed to dry out during the dry season, and the vegetation is tilled into the soil. Based on results of a pilot-scale study and work done for a dissertation at the University of Florida, FAVTs are estimated to be eight times more efficient than conventional STAs (Tony Federico, personal communication). An FAVT project in the Fisheating Creek sub-basin is included in the draft Lake Okeechobee BMAP. The annual removal of TP and TN for that project is estimated to be 8.6 mt and 29.2 mt, respectively.

3.3 OPTION 1 - STORMWATER TREATMENT AREA

The subject 684-acre property between Lower Taylor Creek and the L-63N Canal includes approximately 305 acres of wetland. Because of the high cost of mitigating for wetland impacts, potential STAs in the wetland areas of the property were eliminated from consideration early in the study. In addition, the proposed location of the STA on the east side of the property is outside the 10,000-ft airport buffer requirement. The Taylor Creek STA was used as the basis for development of the performance efficiencies of Option 1 because it is the most similar in size and because it is the only facility of the three evaluated for which operational data are available.

The total STA footprint shown in **Figure 13** in **Appendix A** is 60 acres and is configured to avoid impacts to wetlands. Of this total area, it is estimated that 50 acres will be available for treatment. This is consistent with the ratio of treatment area to non-treatment area for the Taylor Creek STA. This option would require establishment of a pump system on the north end of the STA with gravity outflow back into the L-63N Canal at the south end. Initially, consideration was given to pumping water from S-192 to hydrate the STA. This would require a major modification in the way the pump at S-192 is operated currently. The required pumping distance along the L-63N Canal from S-192 to the north end of the STA is approximately 1.2 miles. To facilitate adaptive management for the STA and to provide for a constant inflow of water, it will be necessary for the STA to have an independent pump system. To achieve average hydraulic loading rates of 5 to 10 centimeters per day (cm/day), the pump system will need to pump an average of 4 to 8 cfs on an annual basis. At these pumping rates, the hydraulic residence time in the STA for an average operating depth of 2.0 ft ranges from 6.1 to 12.2 days.

The annual removal of TP will vary depending upon the total load into the STA. The average annual measured inflow TP concentration to the Taylor Creek STA for water years 2009, 2011, 2012, and 2013 was 321 ppb (range 167 to 408 ppb) (SFER, 2014). This compares well with the average annual geometric mean of TP in Upper Taylor Creek at Cemetery Road for calendar years 2008 through 2011 of 354 ppb (range 298 to 439 ppb). See **Figures 11** and **12** in **Appendix A** for the basin map and land use map. For purposes of calculating an estimated average annual removal rate for TP, an inflow concentration of 354 ppb was used because the Cemetery Road site is downstream of the existing Taylor Creek STA and closer to the site under consideration. The assumed removal efficiency is 28.7 percent, which is the average TP removal efficiency for the Taylor Creek STA since the start of operations. For a hydraulic loading rate ranging from 5 to 10 cm/day over 50 treatment acres, Option 1 is expected to yield TP reductions of 465 to 727 kg/yr.

This relatively small facility is expected to cost more on a per-acre basis than the larger STAs discussed in Section 3.2 because there is no economy of scale. Taylor Creek STA is the most similar in size to Option 1 of the three STAs evaluated, and the initial cost per acre of treatment is \$47,816. The Powell Creek Filter Marsh in Lee County has 40 treatment acres and is even closer in size to the Option 1 STA. Powell Creek Filter Marsh was completed in 2013 at a cost of \$2,100,000 for design, permitting, and construction, or at an initial cost per treatment acre was \$52,500. The Powell Creek system includes the cost of a pump station. Because it is comparable in size to the proposed STA and was completed more recently, costs from the Powell Creek project are used to calculate the estimated initial cost for Option 1 of \$2,650,000. Operating and maintenance costs are assumed to be similar to Taylor Creek STA, at \$50,000 annually.

3.4 OPTION 2 - BIOSORPTION ACTIVATED MEDIA (BAM)

Option 2 considers the use of BAM for nutrient removal. Marion County is using BAM in several stormwater retention basins to reduce nitrate leaching to groundwater in karst areas. Monitoring data from the springshed sites indicates that BAM is also effective at removing orthophosphate, with reductions of greater than 70 percent in the unsaturated soil zone beneath the BAM layer. The BAM removes nitrogen through biological processes in an anaerobic environment. Phosphorus is reduced by sorption onto the BAM. The BAM used for the retention pond in the springsheds consists of a 1.0:1.9:4.0 mixture of tire crumb, silt+clay, and sand. The tire crumbs increase the sorption capacity of the BAM, the silt+clay layer increases water retention and sorption capacity, and the sand promotes infiltration. To be effective at removing phosphorus, the minimum contact time with the BAM is 15 minutes.

BAM could be used downstream of S-192 in either an in-stream system or an offline swale system adjacent to Lower Taylor Creek. Both concepts require the diversion of water from the L-63N Canal into Lower Taylor Creek and would require a modification in the current manner in which the gate and/or the pump are operated. S-192 consists of a manually operated sluice gate and a pump with a design rating of 30 cfs. The gate is normally closed and opened for two reasons:

1. To divert flows from the L-63N Canal for maintenance purposes, and

2. When water quality is degraded in Lower Taylor Creek and Lake Okeechobee is sufficiently low to permit gravity flow into the lake (below elevation 14.0).

The pump is operated only when the water quality in Lower Taylor Creek is degraded and when the water level in Lake Okeechobee is too high to permit gravity flow. When the pump is discharging, S-193 is opened enough to discharge about the same amount of water as S-192 is pumping (SFWMD Operations Control Center Structure Book, Structure S-192, Revised 8/15/1994). Pump operations would not require modification if water was only supplied to the system when water levels in the L-63N Canal and lake allow for gravity flow.

For the 3,300 ft offline swale shown in **Figure 14** in **Appendix A**, diverted water flows through a swale with a bottom width of 50 ft and underlain with BAM to a depth of 1 ft. To maintain a minimum depth of 1 ft in the swale, a control berm is installed on the downstream end of the swale. The approximate volume in the swale at a depth of 1 ft is 4.1 ac-ft. Assuming an infiltration rate of 0.25 inches per hour (in/hr), this volume would have to be replaced every 48 hours, requiring an average flow from the structure of approximately 1 cfs. Assuming an average TP concentration of 354 ppb, the annual TP load to the BAM system is 316 kg/yr. Orthophosphorus is almost 80 percent of the TP in Taylor Creek water (2013, SFER), so the load of orthophosphorus is estimated at 253 kg/yr. Using a range of removal efficiency for orthophosphorus of 35 to 70 percent, this configuration can be expected to remove at least 88 to 176 kg/yr of orthophosphorus. The TN removal rate observed in the Marion County study was up to about 50 percent.

For planning purposes, in-place costs for the BAM system are estimated at \$180 per cubic yard (Wanielista, personal communication). Costs could be reduced if soils onsite can be used to mix the BAM. For the swale system shown, 6,111 cubic yards are required, and the estimated cost is \$1,100,000. This is likely conservative, because for a project of this size, it is expected that there would be economies of scale.

The second BAM concept that was considered, but in less detail, is an in-stream application, in which a structure is used to increase the water elevation on the structure's upstream side, forcing water downward and through a BAM layer installed under the streambed to a depth of 2 ft. The minimum downstream length of the layer is determined based on the rate of flow through the layer to maintain a minimum contact time of 15 minutes. This concept is untested, but the Stormwater Management Academy at the University of Central Florida recently received a grant from FDOT to test an in-line system for nitrate removal in a springshed. An in-stream system would not require as much land acquisition as the offline system, but the lack of demonstration projects make functional parameters less well known.

Many factors are involved with the development of a BAM system, and the needs of each site are unique and require site-specific detailed design. The numbers presented are conceptual but believed to be achievable. An important design factor to consider is the phosphorus removal design life of the BAM. Because phosphorus is removed by sorption onto the BAM, eventually the BAM will become saturated and need replacement. This is not a problem for nitrogen removal because nitrogen is removed using biological processes. Ease and cost of future maintenance is a consideration.

3.5 STA OPTION 3

Option 3 considers increasing water storage in the existing onsite wetlands to contain runoff from the property. A 162.5-acre wetland area is proposed for improvement (Figure 15 in Appendix A) by installation of risers or other structures to restore seasonal high water lines (SHWLs) to levels more indicative of pre-disturbance. Nutrient reduction benefits are calculated for this option by assuming that whatever load from the property would have entered Lower Taylor Creek will be contained onsite. The TP and TN loads for the entire 684-acre property between Lower Taylor Creek and the L-63N Canal based on the Lake Okeechobee BMAP Load Estimation Tool are 180 and 858 kg/yr, respectively. The SHWLs and water levels in Lower Taylor Creek shown in Appendix A Figure 6 indicate that there is an additional 1 to 2 ft of storage available in this wetland area. One foot of extra storage will completely contain runoff from an 8-inch storm event. This corresponds to the 50-year return period, 1-day maximum rainfall for the area (Pathak, 2001). During the wet season, it is unlikely that all runoff can be fully contained without some discharge into Lower Taylor Creek. Therefore, the load reduction benefit is reduced by whatever load eventually makes it to Lower Taylor Creek. Without more detailed modeling of specific rainfall events over time, it is difficult to estimate how much water will actually be discharged. For purposes of this study, a range of 50 to 80 percent retention will by assumed, resulting in TP reductions of 90 to 144 kg/yr and TN reductions of 429 to 686 kg/yr.

A secondary benefit of Option 3 is restoration of some of the wetland functions. A quantification of the potential environmental lift that could be realized by rehydration of this wetland was determined using the Uniform Mitigation Assessment Method (UMAM). The UMAM calculated the potential environmental lift per acre, known as the relative functional gain (RFG), for the 338 acres of cypress wetland contained within the property to be 0.076. The functional gain for the 162.5-acre wetland area placed in a conservation easement based on the UMAM is 12.35. Restoration of larger or smaller wetland acres would correspondingly increase or decrease the environmental lift achieved.

Potential costs for Option 3 can vary considerably depending upon the type and number of structures required to restore water levels in the wetlands and the contract with the property owners for the use of their properties. For the purposes of this discussion, initial costs would include payment to the landowner for the cost of acquiring a conservation easement over the wetland areas that are being rehydrated.

3.6 STA DISCUSSION AND SUMMARY

Estimated nutrient reductions for each of the three options iare summarized in Table 7.

Table 7: STA Estimated Nutrient Loading Reductions

	Estimated TP	Estimated TN
	Reduction (kg/yr)	Reduction (kg/yr)
Option 1 - Stormwater Treatment Area	465 - 727	Not calculated
Option 2 - Biosorption Activated Media	88 - 176	50 percent
Option 3 - Increased Wetland Storage	90 - 144	429 - 686

Each option presented has advantages and disadvantages. Option 1 has the potential to provide substantial nutrient reductions, but requires a large amount of privately owned land. SFWMD would be the most logical entity to operate this facility, but the agency already has a backlog of projects that lack funding, including Lakeside Ranch STA Phase II. STA operation in the northern Everglades is relatively new to the agency, and the systems function differently than the STAs in the southern Everglades. SFWMD is still working through substantive operational issues at the Taylor Creek STA related to the periodic net export of phosphorus. The Nubbin Slough STA, despite being completed in 2006, has never been operational due to a number of mechanical problems and needed repairs that should be completed by the end of October. Once Nubbin Slough is online, the SFWMD already understands that it is likely to have problems with insufficient flow to operate the STA and will have to address those issues as they arise. Since the start of flow-through operations in July 2013, Lakeside Ranch Phase I seems to be working well but is still in its stabilization phase. The first year of nutrient reduction calculations for Lakeside Ranch Phase II will be included in the 2015 South Florida Environmental Report. Given its funding constraints as well as its efforts to work through operational difficulties with existing STAs, SFWMD is likely unable to commit to managing another STA.

Option 2 can achieve reasonable nutrient reductions within a small footprint, thus minimizing land acquisition requirements. Although a number of projects have been constructed throughout the state, this is still a relatively new technology for which new applications and uses are continually being investigated. In addition, much of the effort has been focused on the use of BAM in karst areas because of its ability to reduce nitrate loads to groundwater, with less research focused on reducing phosphorus. While a relatively simplistic model was presented as part of this analysis, there are many factors involved in design of a successful system. This may be a good opportunity, however, to investigate the use of BAM in the Lake Okeechobee watershed for phosphorus removal on a larger scale.

Option 3 provides estimated reductions comparable to Option 2 but, unlike BAM, reduction estimates are not based on research data. Rehydration of the wetland will improve a disturbed wetland habitat so Option 3 has an additional ecological benefit. SFWMD funds water storage and restoration projects but is more interested in larger scale projects that have a higher benefit-to-cost ratio. In addition, SFWMD has no money available for additional water storage projects that are not already planned, in progress, or completed. Implementation of this option would require acquisition of a permanent conservation easement from the property owner. For purposes of this discussion, initial project costs are the costs to acquire the easement.

4. CONCLUSIONS

The feasibility report has presented several options worthy of investigation for both the FDOT Regional Pond and the multi-agency STA. It is recommended that the report be shared with the property owner, SFMWD, FDEP and FDACS for consideration of the alternatives to determine if partners are available to pursue the STA option.

5. REFERENCES

- 1. Federal Emergency Management Agency (May 2013). Flood Insurance Rate Maps, Okeechobee County, Florida and Incorporated Areas. Community-Panel Number 12093C0415C.
- 2. Federal Emergency Management Agency (May 2013). <u>Preliminary Flood</u> Insurance Study: Okeechobee County, Florida and Incorporated Areas.
- 3. Gary Goforth, Inc. 2005a. Operation Plan Nubbin Slough/New Palm Stormwater Treatment Area. Submitted to South Florida Water Management District.
- 4. Gary Goforth, Inc. 2005b. Operation Plan Taylor Creek/Grassy Island Stormwater Treatment Area. Submitted to South Florida Water Management District.
- 5. Hazen and Sawyer. 2011. Compilation of Benefits and Costs of STA and Reservoir Projects in the South Florida Water Management District. Submitted to the World Wildlife Fun acting on behalf of the Florida Ranchlands Environmental Services Project.
- 6. Institute of Food and Agricultural Sciences (IFAS). 2014. Permeable Reactive Barriers for Passive Management of Phosphorus in the Lake Okeechobee Basin: Final Report. Submitted to South Florida Water Management District, West Palm Beach, FL. Environmental Hydrology Laboratory, Soil and Water Science Department, Gainesville FL.
- 7. South Florida Water Management District. 2014. 2014 South Florida Environmental Report.
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- 9. South Florida Water Management District. 2012. 2012 South Florida Environmental Report.
- 10. Stanley Consultants, Inc. 2003. Lake Okeechobee Water Retention/Phosphorus Removal Project Design Analysis Final Submittal. Submitted to Department of the Army Corps of Engineers, Jacksonville District.
- 11. Stanley Consultants, Inc. 2003. Lake Okeechobee Water Retention/Phosphorus Removal Project Design Documentation Final Submittal. Submitted to Department of the Army Corps of Engineers, Jacksonville District.

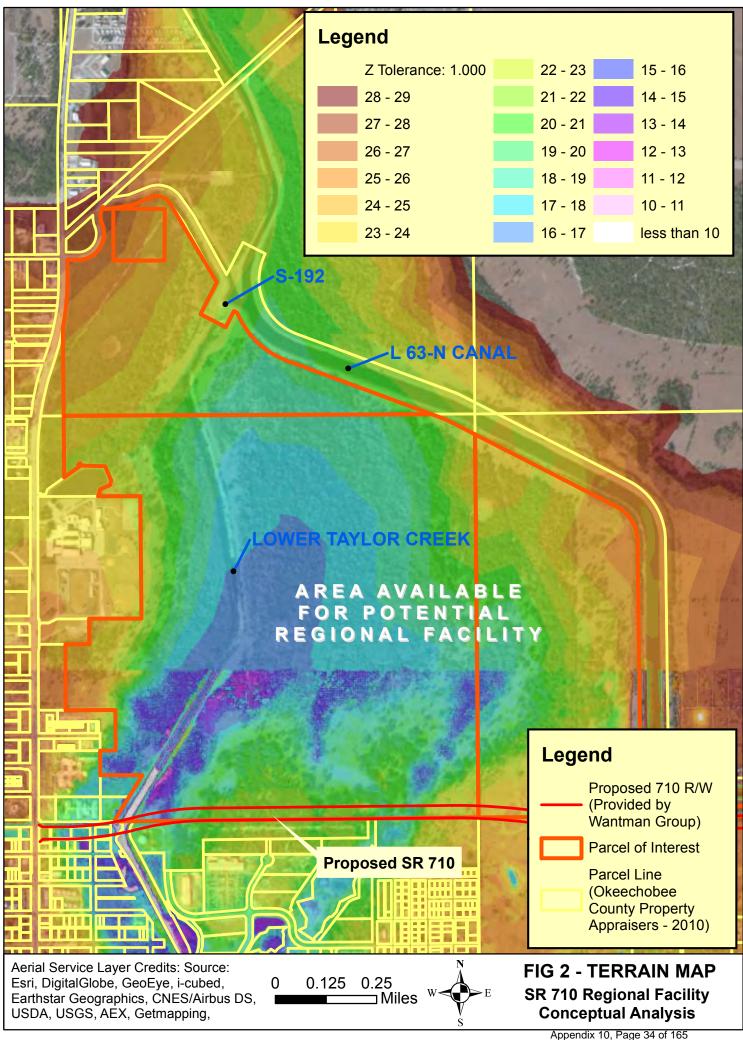
Appendix A: Figures

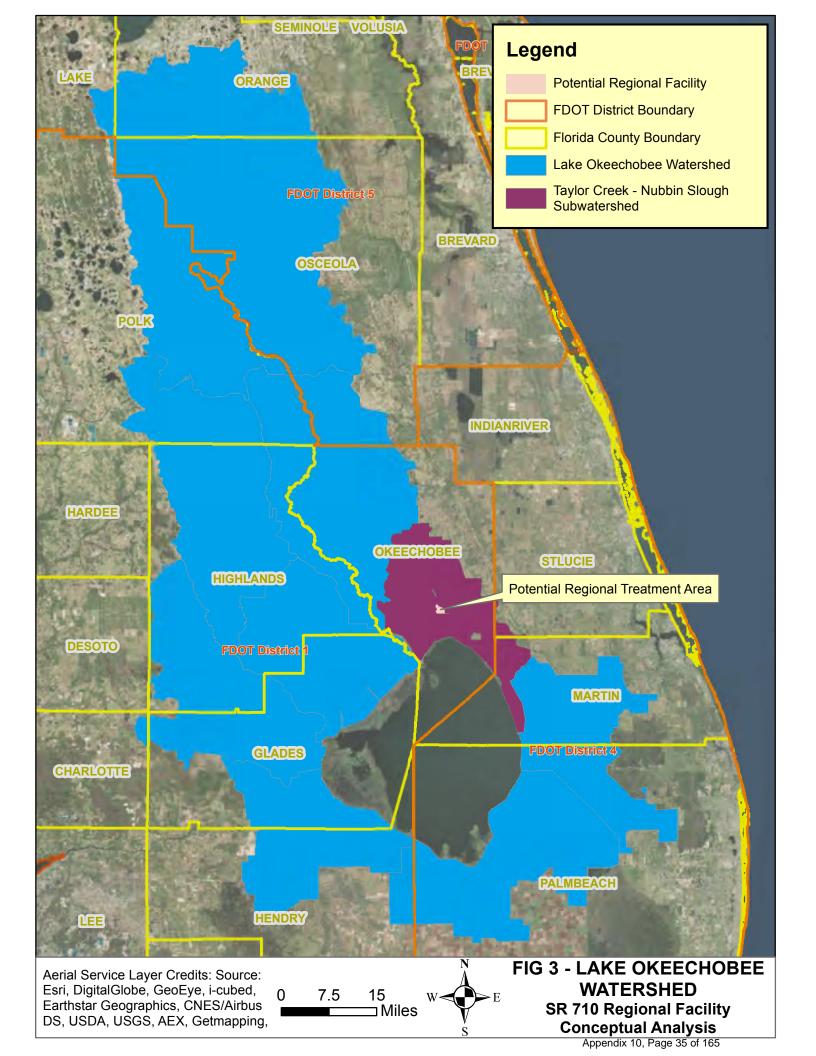
SR 710 Stormwater Treatment Area/Regional Pond Feasibility Study Final Submittal

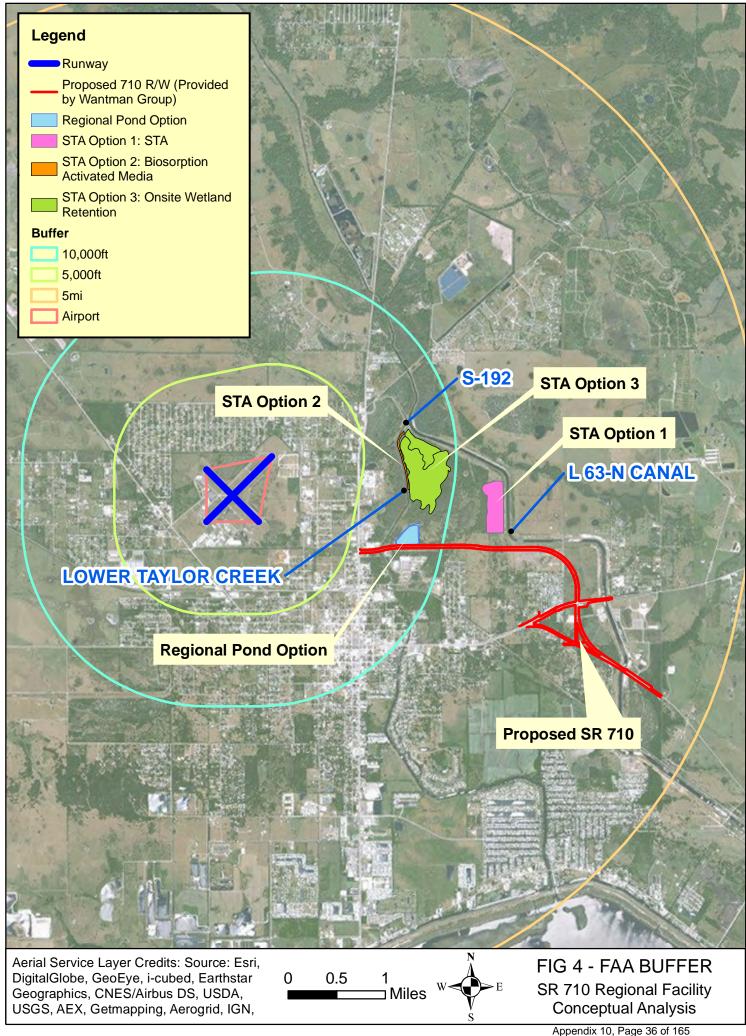
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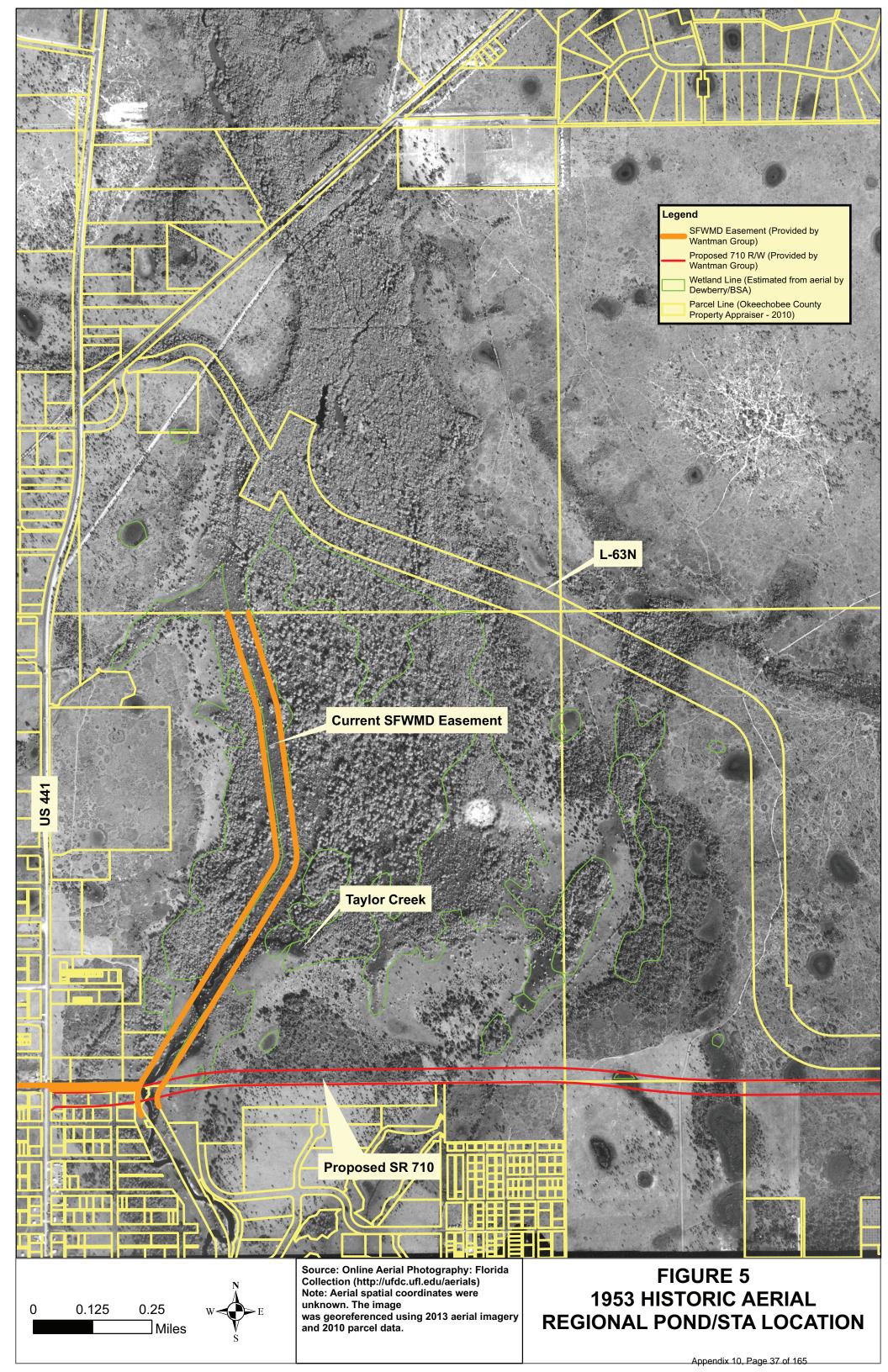
Okeechobee County, Florida



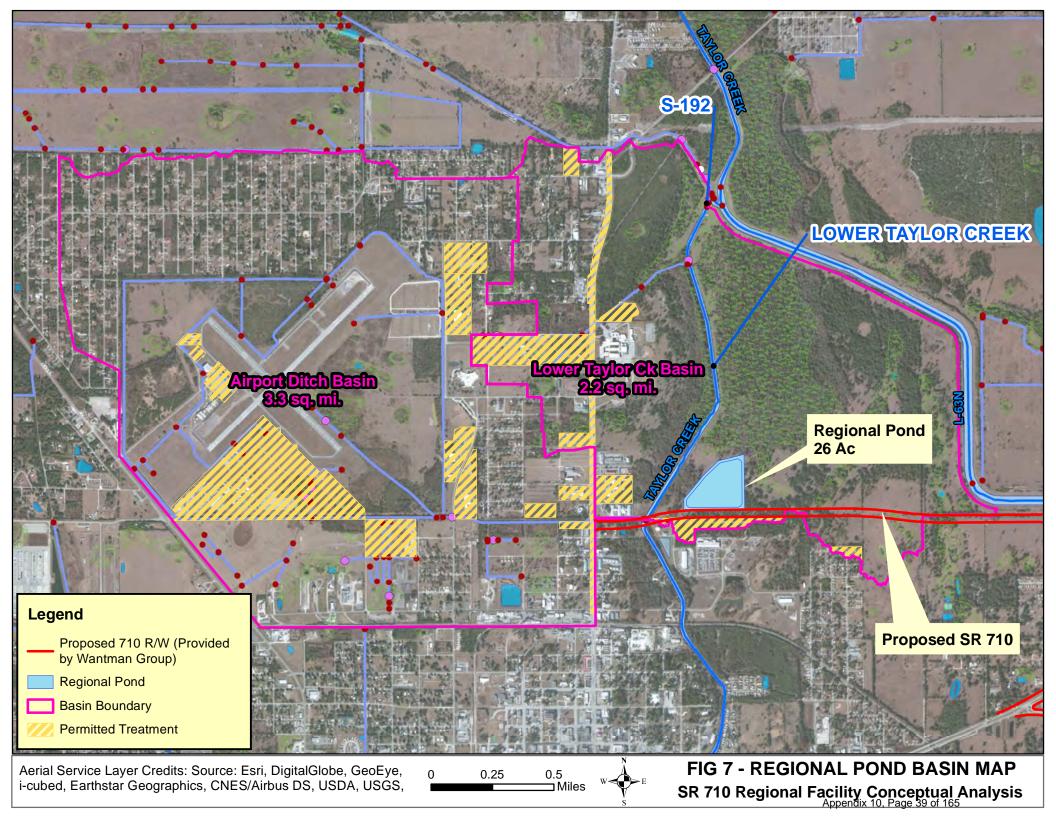


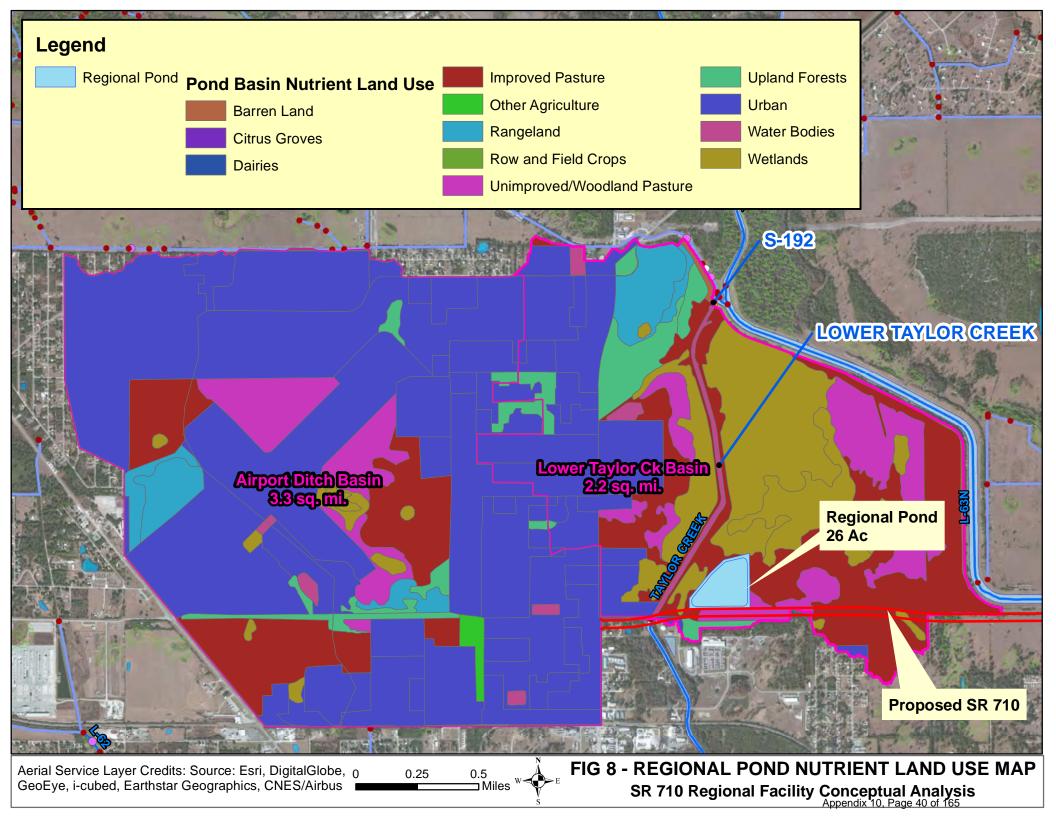


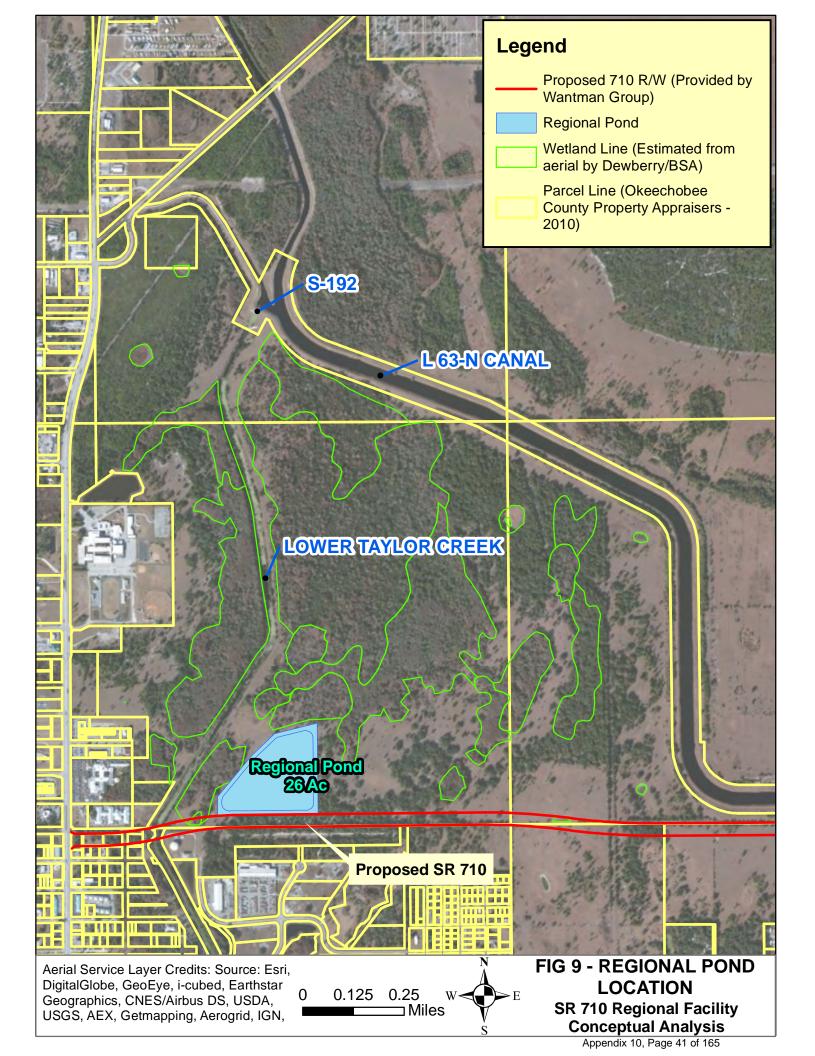


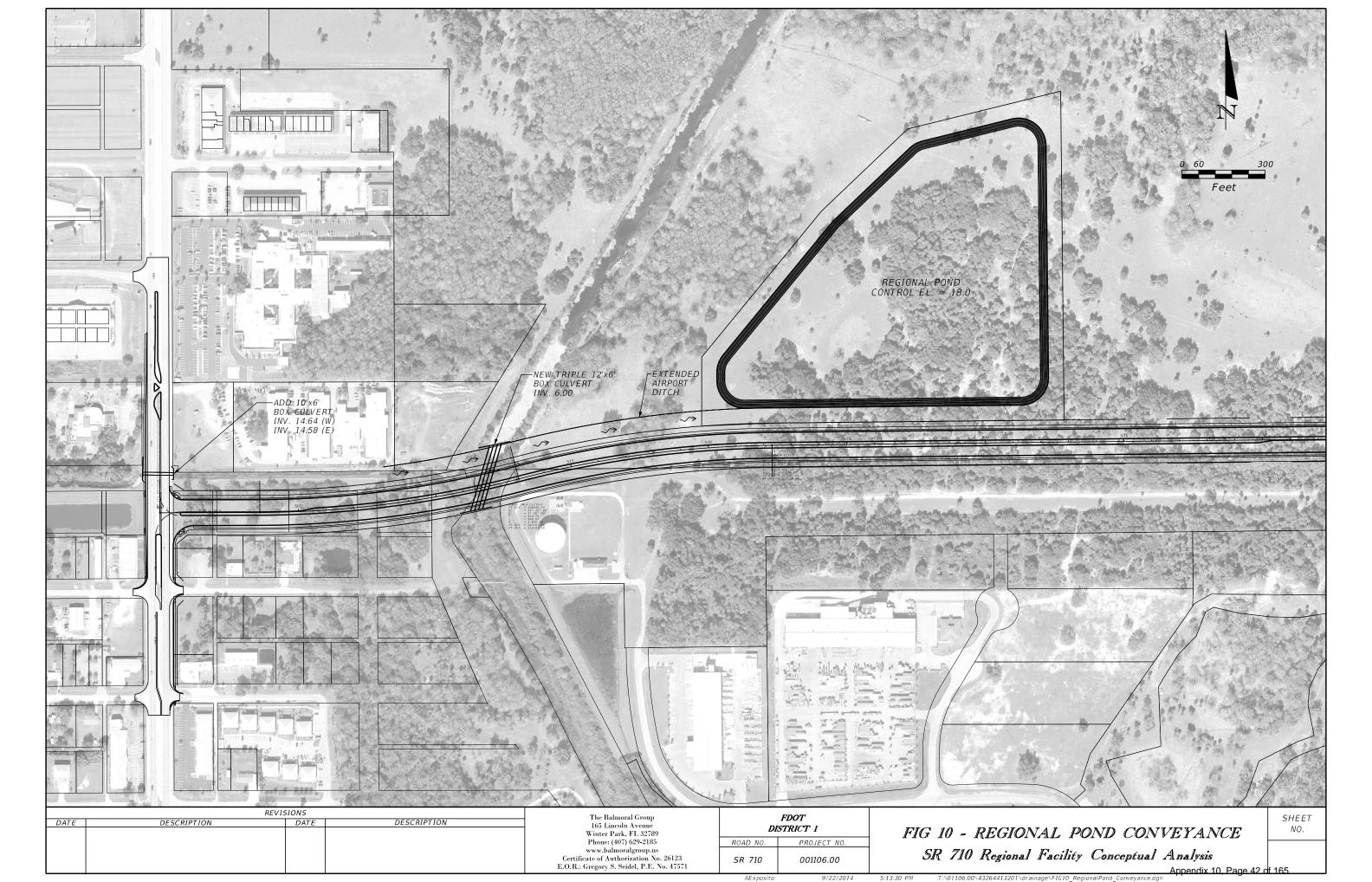


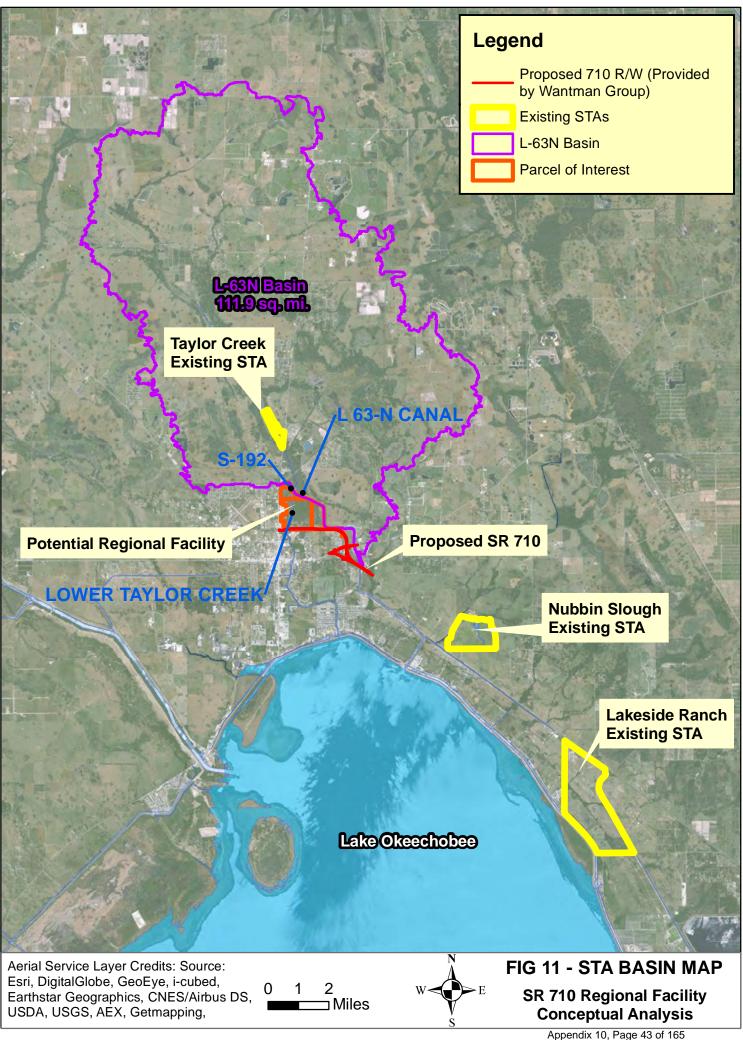


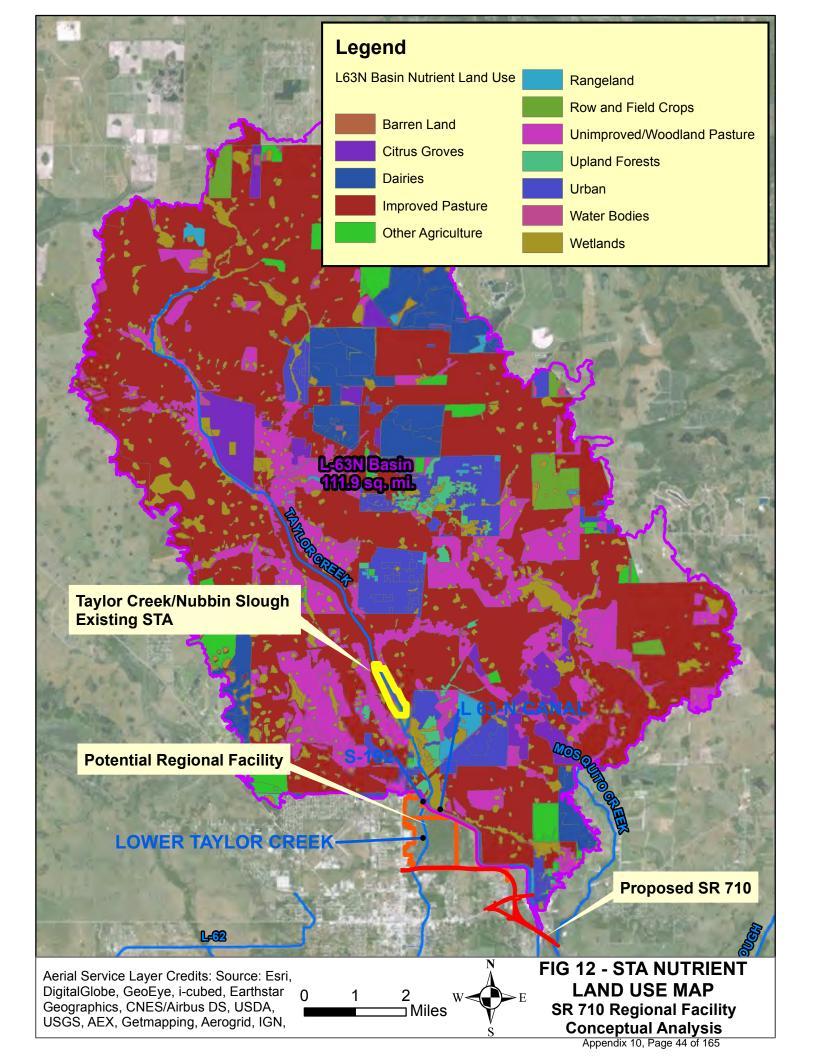


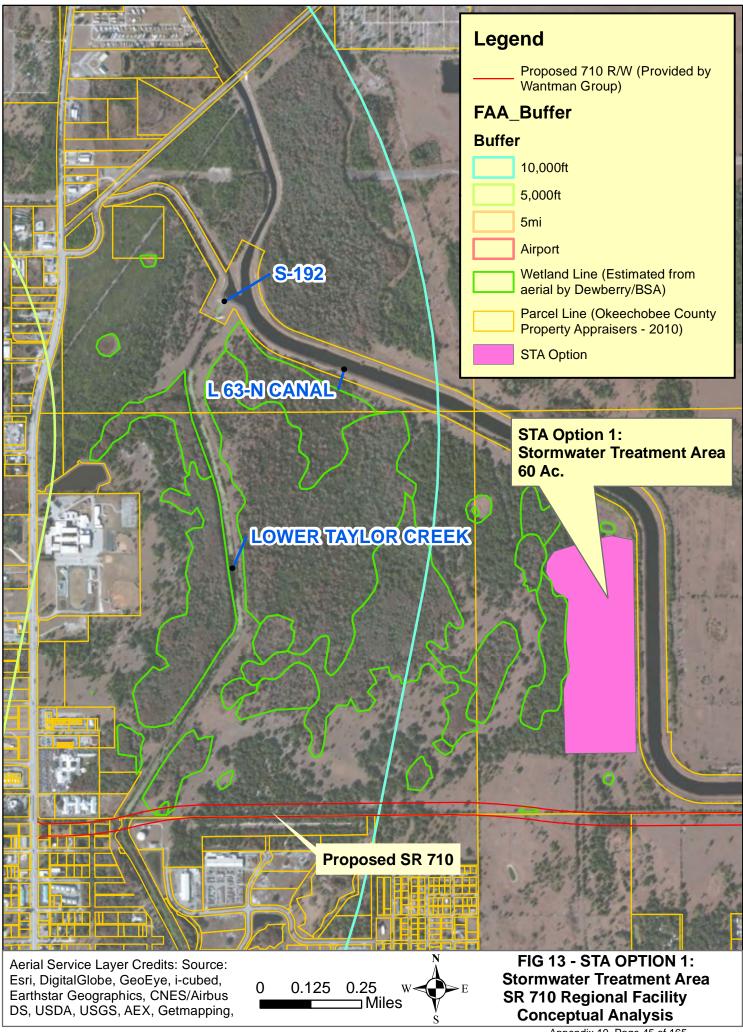


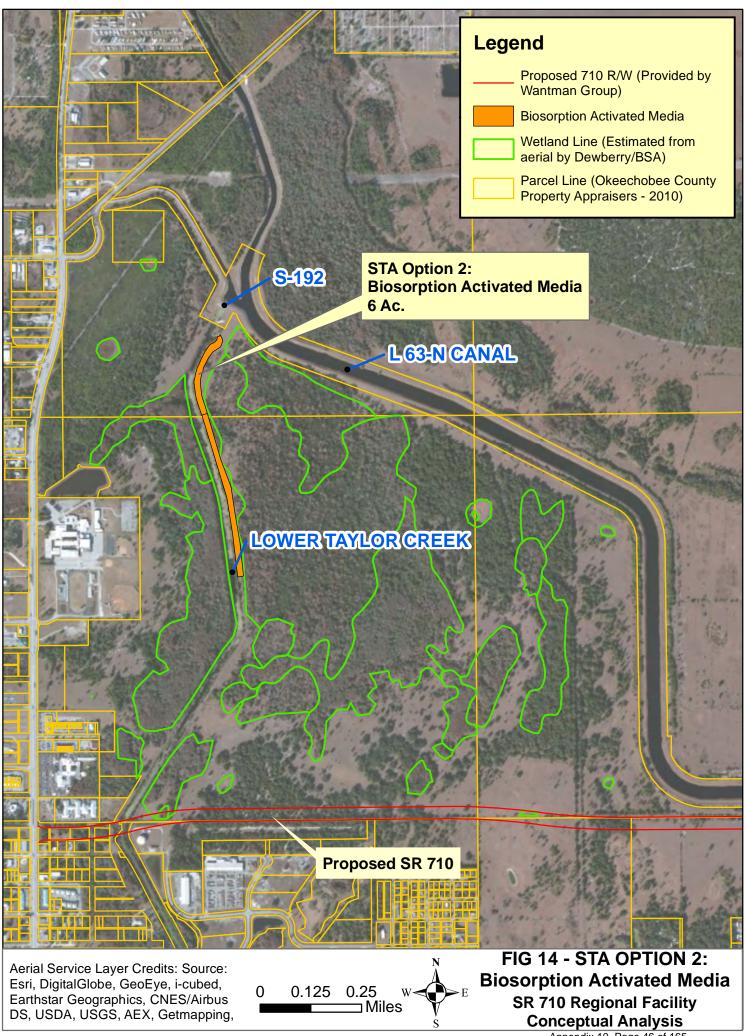




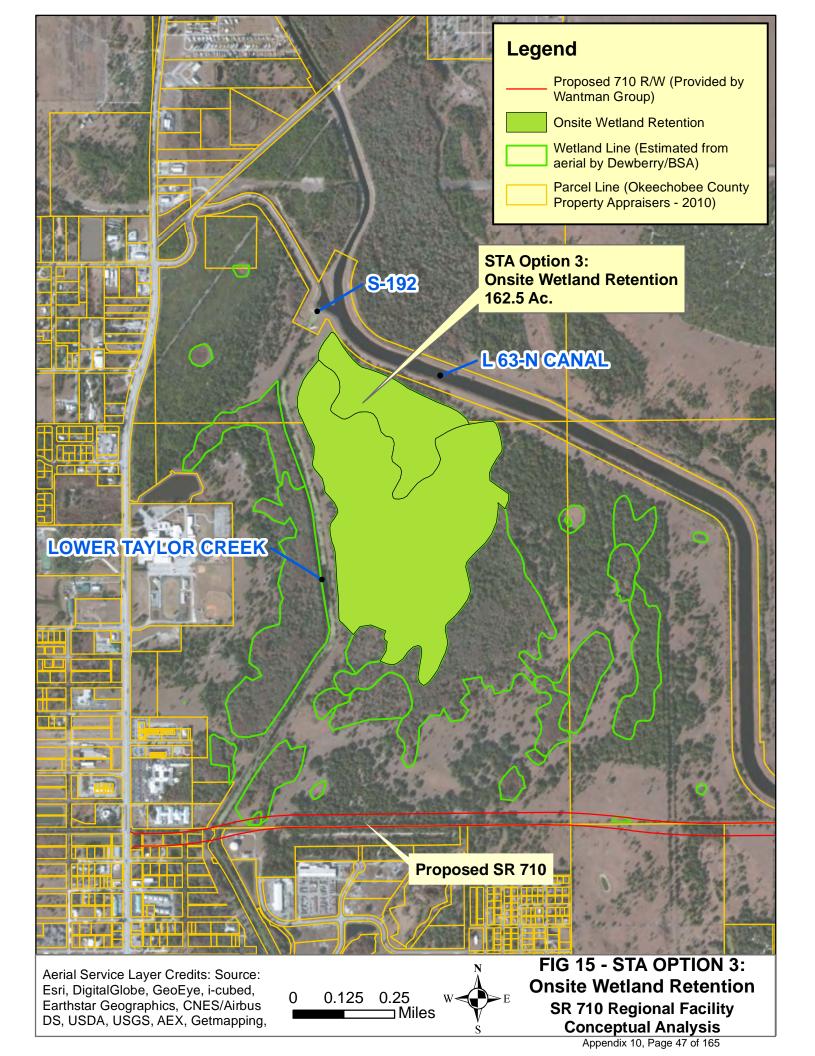








Appendix 10, Page 46 of 165



Appendix B: Regional Pond Analysis

SR 710 Stormwater Treatment Area/Regional Pond Feasibility Study Final Submittal

Financial Project ID 432644-1-32-01

Okeechobee County, Florida

TREATMENT VOLUME CALCULATIONS FOR REGIONAL POND

PROJECT: SR 710 - Regional Pond Option A PREPARED: JAN 7/24/2014

LOCATION: OKEECHOBEE COUNTY, FLORIDA CHECKED: GSS 7/30/2014

Wet Detention Online Pond Treatment Calculations:

Total Airport Ditch Drainage area = 2086.00 Ac

Total Treated within Airport Ditch Drainage Area = 231.78 Ac

Remaining Area of Airport Basin Untreated = 1854.22 Ac

SR 710 Drainage area (Basin 1 and Basin 2) = 40.37 Ac

SR 710 Drainage area (Basin 3, Basin 4, and Basin 5) = 37.41 Ac

2126.37 Ac (Includes Airport and SR 710 Basins 1 and 2 only) Total Drainage Area Draining to Regoinal Pond =

77.78 Ac (Includes only SR 710 Basins) Total Area to be treated =

1" runoff from drainage area = 6.48 Ac-Ft

> Required Treatment Volume (T.V.) = 6.48 Ac-ft

282,341 ft³

STAGE-STORAGE FOR PROPOSED CONDITION

9/21/2014 9/22/2014 PREPARED: GSS CHECKED: JAN OKEECHOBEE COUNTY, FLORIDA SR 710 - Regional Pond LOCATION: PROJECT:

Shrinkage Factor = 10% = 413,721 CY
Shrinkage Factor = 10% = 41,372 CY
Required Pond Excavation = 282 Ac-Ft

Pond Storage Calculations (Wet Detention):

1:2 Slopes

			12,513,612 Top of Berm = App Exist Ground															Bottom of Pond
me			12 Top	17	02	IMN 0	4	7,	33	5	5	46	32	7.	72	_	m	Bott
Total Volu	Cn-ft		12,513,6	11,626,817	10,747,602	9,876,010 NWL	9,011,954	8,155,434	7,306,493	6,465,045	5,631,045	4,804,494	3,985,392	3,173,651	2,369,272	1,572,211	782,468	0
Total Volume Total Volume	Ac-ft		287.273	266.915	246.731	226.722	206.886	187.223	167.734	148.417	129.271	110.296	91.492	72.857	54.391	36.093	17.963	0.000
Cum. Volume	Cu-ft		2,637,602	1,750,807	871,592	0				-	1	1	1	1	1	1	1	
Cum. Volume	Ac-ft		60.551	40.193	20.009	0.000					1	:	:	:	:	:	:	-
Inc. Volume	Ac-ft		20.358	20.184	20.009	19.836	19.663	19.489	19.317	19.146	18.975	18.804	18.635	18.466	18.298	18.130	17.963	0.000
Area	ac	25.864	20.445	20.271	20.096	19.922	19.750	19.575	19.403	19.231	19.061	18.889	18.719	18.551	18.382	18.214	18.046	17.879
Area	sf	1,126,640	009'068	883,000	875,400	867,800	860,300	852,700	845,200	837,700	830,300	822,800	815,400	808,100	800,700	793,400	786,100	778,800
h	ft		1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	0.0
Elev. (NAVD)	(ft)	Parcel	21.00	20.00	19.00	18.00	17.00	16.00	15.00	14.0	13.0	12.0	11.0	10.0	0.6	8.0	7.0	0.9

PPV = Cum. Vol - Total = 227

Ac-Ft

NUTRIENT LOADING CALCULATIONS FOR REGIONAL POND

PROJECT: SR 710 - Regional Pond Option A PREPARED: JAN 7/24/2014

LOCATION: OKEECHOBEE COUNTY, FLORIDA CHECKED: GSS 9/21/2014

Annual Runoff & Calculation b

Basin	C*	AnnualsRunoffs (in.)	BasinsAreas(ac)**
Regional P ond	0.6156	51	1894.59

^{*}SAssumesNonDCIAS-S61&DCIAS-S75%,susingZoneScTablesfromSQAH

RegionalbPondbNutrientbRemovalbCalculation

Dasin	AnnualsRunoffs	PermanentsPools	ResidencesTimes	WetsDetentions	WetsDetentionsTNs
Basin	(ac/ft/yr)	(ac-ft)	(days)	TPsRemovals(%)	Removals(%)
Regional £ ond	4956.8	227.00	16.7	63.0	34.7

Pre-Development Loading Summary

Basin	TDeOutflowdka/vr)	TNsOutflows		
Basili	TPsOutflows(kg/yr)	(kg/yr)		
AirportsBasin	762.09	4971.29		
LowersTaylorsCreeksBasin	460.75	2353.67		
SRs710sBasinss1-2	14.16	78.85		
SRs710sBasinss3-5	12.53	84.70		
TotallOutflow	1249.53	7488.51		

Post-Development Loading TPL ummary

· ·									
Basin	TPs(kg/yr)	%sRemoval	TPsOutflows(kg/yr)						
AirportsBasin	762.09	62.99	282.05						
LowersTaylorsCreeksBasin***	456.47	N/A	456.47						
SRs710sBasins1-2	10.15	62.99	3.76						
SRs710sBasins3-5	11.52	N/A	11.52						
Totalibe	TotallPostlTPlDutflow								

^{***}PostsLowersTaylorCreekBasindoadingsisdesssthanPresduestosthesregionalpondsareas(~20sac)

Post-Developmentboadingb Nb ummary

Basin	TNs(kg/yr)	%sRemoval	TNsOutflows(kg/yr)						
AirportsBasin	4971.29	34.67	3247.93						
LowersTaylorsCreeksBasin***	2321.50	N/A	2321.50						
SRs710sBasins1-2	26.21	34.67	17.12						
SRs710sBasins3-5	29.72	N/A	29.72						
Totalbo	TotallPostlTNlDutflow								

^{***}PostsLowersTaylor©reek&asindoadingssdesssthanPresduestostheregionalpondsareas(~20sc)

TotalbTPbRemoved	495.7 b kg/yr
Totalb TNb Removed	1872.2 l kg/yr

^{**}Basinareas=\$Rs710PostBasinss1-2andAirportDitchBasinssTreatedportionofAirportBasin

SFWMD Provided TP Removal Rate and Concentration

PROJECT: SR 710 - Regional Pond Option B PREPARED: JAN 11/9/2015

LOCATION: OKEECHOBEE COUNTY, FLORIDA CHECKED: GSS 11/10/2015

Scenario - SFWMD Data

1. Provided Data from SFWMD

Literature Cited:

- 1. ERD (Environmental Research & Design, Inc.), 2004. Lake Okeechobee Tributary Sediment Removal Demonstration Project SFWMD Contract No. C-11205. Final report submitted to South Florida Water Management District.
- 2. Bottcher, A.B. 2006. Phosphorus Reduction Performance and Implementation Costs under BMPs and Technologies in the Lake Okeechobee Protection Plan Area. Letter report provided to the South Florida Water Management District. West Palm Beach, FL.

Average TP concentration at S-133 = 0.203 mg/L SFWMD recommended TP removal rate = 25.0 %

2. Wet Detention Pond Characteristics

a. Calculate annual runoff inputs to pond:

226.70 ac-ft = Permanent Pool Volume

For a 21-day residence time, the allowable volume of runoff into the pond will be:

Allowable Volume = 365 days/ 1 Year / 21 days = 3940 Ac-Ft

Flow Rate from L63-N = 5.44 cfs (Assumes 0 roadway runoff)

- b. Estimate Max. Allowable Pond Depth:
 - 1. Estimate runoff characteristics:

TP = 0.203 mg/l (from above)

2. Calculate TP loading to wet detention pond and Reduction:

TP loading to wet det. Pond = 986 kg TP/yr Allowable Volume x TP x $43560 \times 7.48 \times 3.785 \times 10^{-6}$

TP Removal Rate = 25.00 %

TP removal by Wet Det. Pond = 247 kg TP/yr

3. Calculate TP concentration in pond:

TP removal = 25.0 % (from above)

Annual mass of TP remaining in water column = TP load to pond X (1 - TP removal) = 739.50 kg TP/ yr

This phosphorous mass will be distributed within the pond permanent pool and the pond outflow. Assuming that inflow and outflow are approx. equal, the

Outflow = 3940.00 ac-ft/yr

Mean Pond Concentration = 0.14391 mg TP/liter $\frac{Altitude Mids of TP}{Outflow Vol. + PPV} \frac{10}{43560x7.48x3.785}$

SFWMD Provided TP Removal Rate and Concentration

PROJECT: SR 710 - Regional Pond Option B PREPARED: JAN 11/9/2015

LOCATION: OKEECHOBEE COUNTY, FLORIDA CHECKED: GSS 11/10/2015

Scenario - SFWMD Data

4. Calculate mean chlorophyll-a concentration in pond:

ln (chyl-a) = 1.058 ln (TP) - 0.934

In (chyl-a) = 4.32

chyl-a = 75.44 mg/cu. Meter

5. Calculate mean Secchi disk depth:

SD = (24.2386 + (0.3041)(chyl-a))/(6.0632 + chyl-a)=

SD = 0.579 m= 1.90 feet

6. Calculate depth of anoxic conditions in pond:

Depth of DO<1 = 3.035*SD + 0.02164 x (chyl-a) - 0.004979 x Total P

Depth of DO<1 = 2.67 m 8.8 feet

7. Adjust Volume Reduction for Permanent Pool

Permanent Pool Volume = 226.70 Ac-Ft
Permanent Pool Above Anoxic Conditions = 203.70 Ac-Ft

Actual Estimated TP Removal = 221 kg TP/yr

SFWMD Provided TP Removal Rate and Concentration PROJECT: SR 710 - Regional Pond Option B PREPARED: JAN 11/9/2015 LOCATION: OKEECHOBEE COUNTY, FLORIDA CHECKED: GSS 11/10/2015 Scenario - SFWMD Data 1. Provided Data from SFWMD Literature Cited: 1. ERD (Environmental Research & Design, Inc.), 2004. Lake Okeechobee Tributary Sediment Removal Demonstration Project SFWMD Contract No. C-11205. Final report submitted to South Florida Water Management District. 2. Bottcher, A.B. 2006. Phosphorus Reduction Performance and Implementation Costs under BMPs and Technologies in the Lake Okeechobee Protection Plan Area. Letter report provided to the South Florida Water Management District. West Palm Beach, FL. Average TP concentration at S-133 = 0.203 mg/L SFWMD recommended TP removal rate = 25.0 % 2. Wet Detention Pond Characteristics a. Calculate annual runoff inputs to pond: 226.70 ac-ft = Permanent Pool Volume For a 150-day residence time, the allowable volume of runoff into the pond will be: Allowable Volume = 365 days/ 1 Year / 150 days = 552 Ac-Ft Flow Rate from L63-N = 0.76 cfs (Assumes 0 roadway runoff) b. Estimate Max. Allowable Pond Depth: 1. Estimate runoff characteristics: 0.203 mg/l (from above) 2. Calculate TP loading to wet detention pond and Reduction: TP loading to wet det. Pond = 138 kg TP/yr Allowable Volume x TP x $43560 \times 7.48 \times 3.785 \times 10^{-6}$ TP Removal Rate = TP removal by Wet Det. Pond = 3. Calculate TP concentration in pond: TP removal = 25.0 % (from above) Annual mass of TP remaining in water column = TP load to pond X (1 - TP removal) 103.50 kg TP/ yr This phosphorous mass will be distributed within the pond permanent pool and the pond outflow.

Assuming that inflow and outflow are approx. equal, the

552.00 ac-ft/yr

0.10777 mg TP/liter

Outflow =

Mean Pond Concentration =

SFWMD Provided TP Removal Rate and Concentration

PROJECT: SR 710 - Regional Pond Option B PREPARED: JAN 11/9/2015

LOCATION: OKEECHOBEE COUNTY, FLORIDA CHECKED: GSS 11/10/2015

Scenario - SFWMD Data

4. Calculate mean chlorophyll-a concentration in pond:

ln (chyl-a) = 1.058 ln (TP) - 0.934

In (chyl-a) = 4.02

chyl-a = 55.56 mg/cu. Meter

5. Calculate mean Secchi disk depth:

SD = (24.2386 + (0.3041)(chyl-a))/(6.0632 + chyl-a)=

SD = 0.668 m= 2.19 feet

6. Calculate depth of anoxic conditions in pond:

Depth of DO<1 = 3.035*SD + 0.02164 x (chyl-a) - 0.004979 x Total P

Depth of DO<1 = 2.69 m 8.8 feet

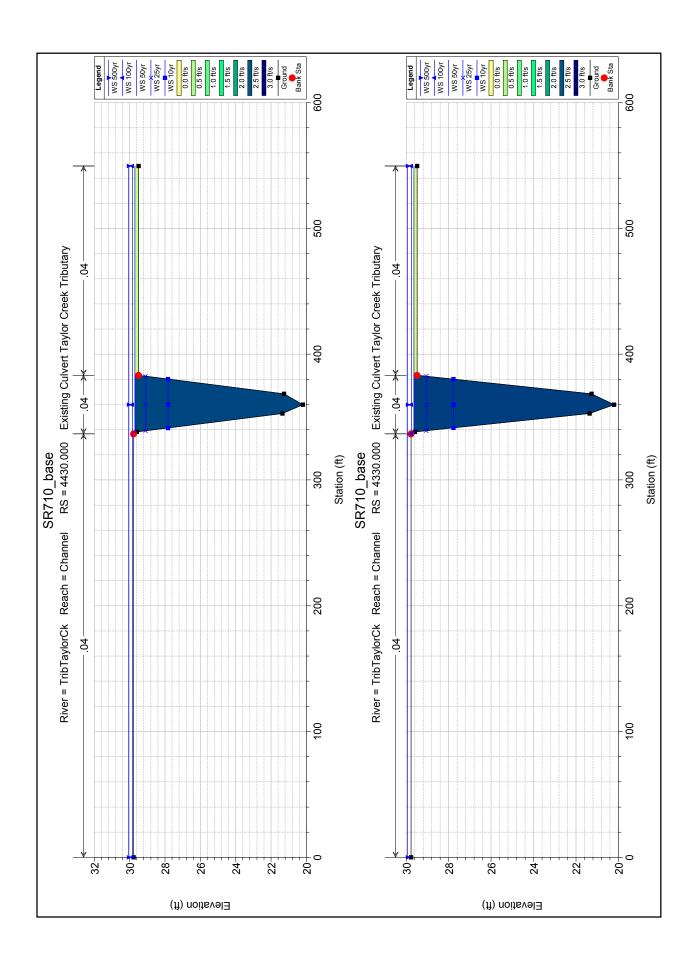
7. Adjust Volume Reduction for Permanent Pool

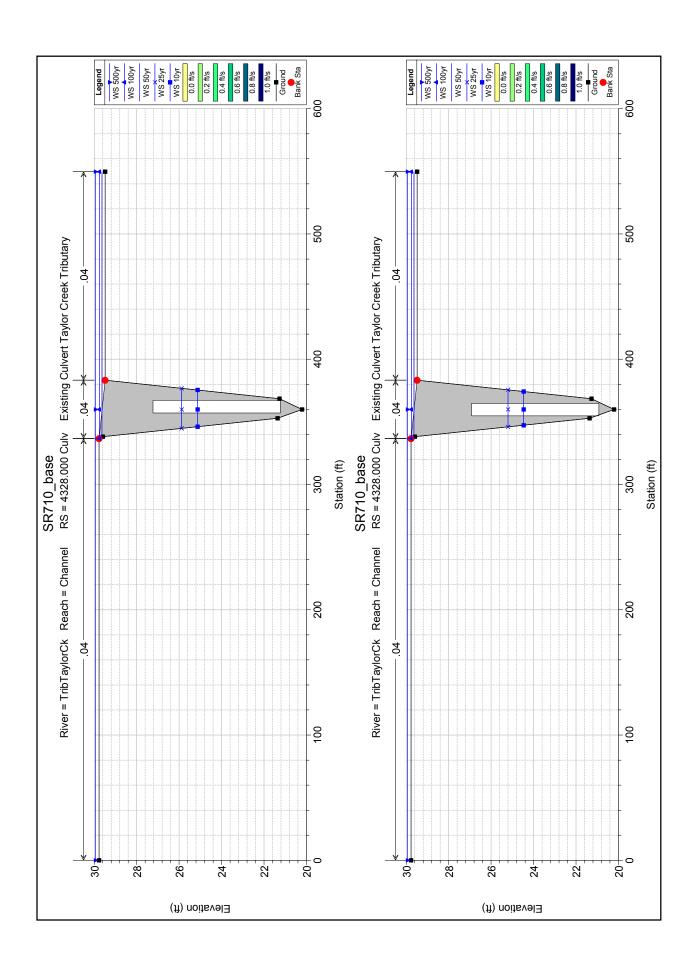
Permanent Pool Volume = 226.70 Ac-Ft
Permanent Pool Above Anoxic Conditions = 203.70 Ac-Ft

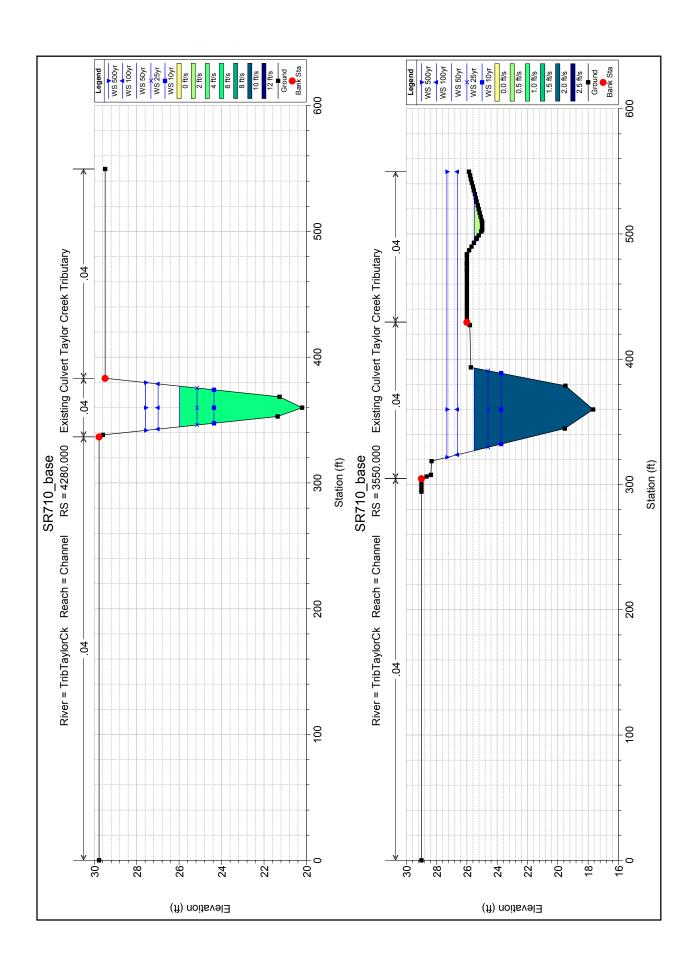
Actual Estimated TP Removal = 31 kg TP/yr

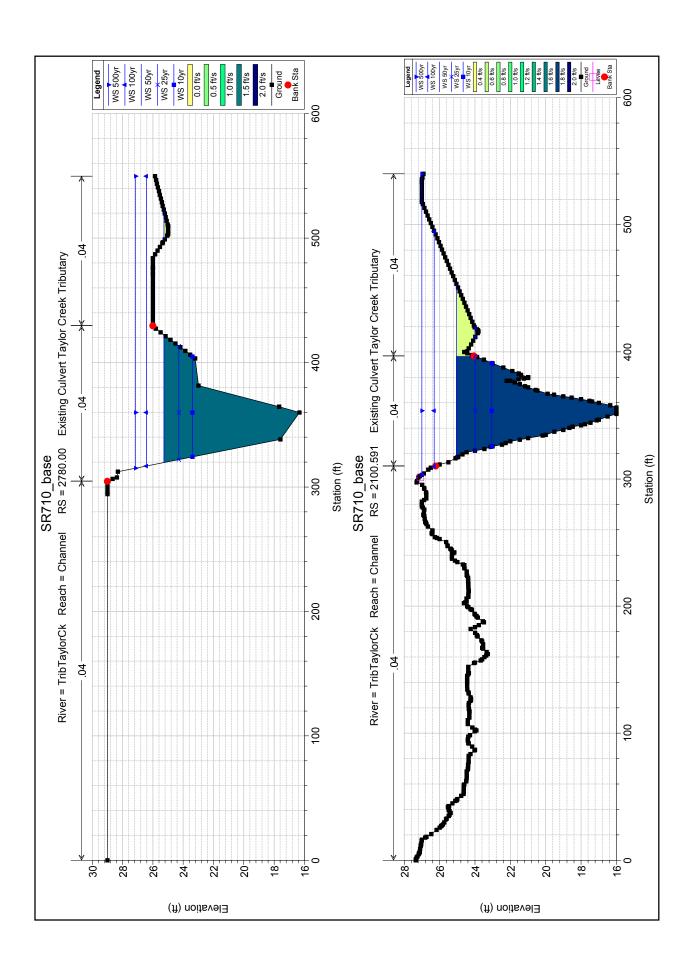
HEC-RAS Plan: Exist_US&DSnew River: TribTaylorCk Reach: Channel

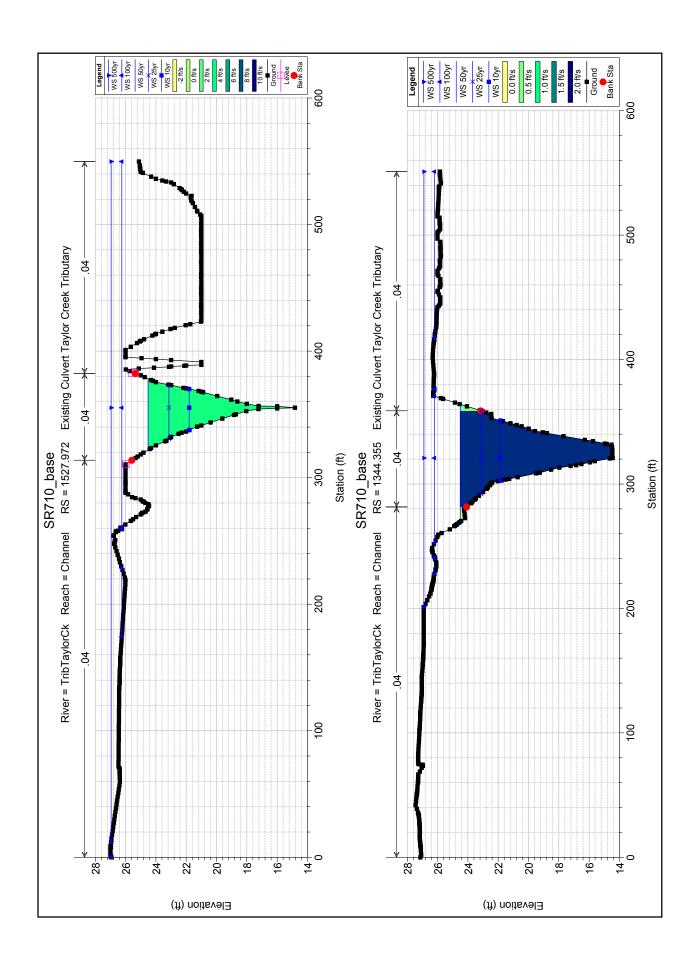
				Reach: Chann				:				
Reach	River Sta	Profile	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chnl	Flow Area	Top Width	Froude # Chl
01 1	1100.000	50	(cfs)	(ft)	(ft)	(ft)	(ft)	(ft/ft)	(ft/s)	(sq ft)	(ft)	0.44
Channel	4430.000	50yr	699.00	20.20	29.70		29.80	0.000531	2.59	300.69	212.44	0.19
Channel	4430.000	100yr	838.00	20.20	29.84		29.97	0.000680	2.96	355.78	549.69	0.22
Channel	4430.000	500yr	1080.00	20.20	30.07		30.23	0.000844	3.38	482.53	549.69	0.24
Channel	4430.000	25yr	570.00	20.20	29.10		29.19	0.000479	2.38	239.22	43.47	0.18
Channel	4430.000	10yr	437.00	20.20	27.83		27.92	0.000551	2.34	186.73	38.93	0.19
Channel	4330.000	50yr	699.00	20.20	29.64	24.38	29.75	0.000548	2.63	288.30	211.93	0.19
Channel	4330.000	100yr	838.00	20.20	29.76	24.78	29.90	0.000735	3.05	313.74	212.97	0.22
Channel	4330.000	500yr	1080.00	20.20	29.95	25.42	30.14	0.000999	3.63	412.48	549.69	0.26
Channel	4330.000	25yr	570.00	20.20	29.05	23.98	29.14	0.000491	2.40	237.04	43.29	0.18
Channel	4330.000	10yr	437.00	20.20	27.77	23.50	27.86	0.000570	2.37	184.47	38.72	0.19
Channel	4328.000		Culvert									
Channel	4280.000	50yr	699.00	20.20	25.97		26.49	0.004668	5.80	120.53	32.30	0.53
Channel	4280.000	100yr	838.00	20.20	26.99		27.45	0.003340	5.39	155.46	35.95	0.46
Channel	4280.000	500yr	1080.00	20.20	27.58		28.16	0.003894	6.10	177.02	38.02	0.50
Channel	4280.000	25yr	570.00	20.20	25.16		25.71	0.005911	5.97	95.45	29.40	0.58
Channel	4280.000	10yr	437.00	20.20	24.36		24.91	0.007313	5.98	73.08	26.55	0.64
Channel	3550.000	50yr	699.00	17.67	25.52		25.59	0.000386	2.09	344.27	106.63	0.16
Channel	3550.000	100yr	838.00	17.67	26.62		26.67	0.000342	1.74	551.91	225.94	0.15
Channel	3550.000	500yr	1080.00	17.67	27.31		27.36	0.000296	1.77	708.40	227.98	0.14
Channel	3550.000	25yr	570.00	17.67	24.60		24.67	0.000445	2.08	273.79	61.13	0.17
Channel	3550.000	10yr	437.00	17.67	23.74		23.80	0.000443	1.96	223.20	56.57	0.17
J. Idi II ICI	0000.000	.0,1	757.00	17.07	23.14		25.00	0.000404	1.00	223.20	30.31	0.17
Channel	2780.00	50yr	699.00	16.33	25.26		25.30	0.000271	1.59	443.92	126.52	0.14
Channel	2780.00	100yr	838.00	16.33	26.43		26.46	0.000271	1.41	657.90	232.87	0.12
			1080.00				27.17					
Channel Channel	2780.00 2780.00	500yr 25yr	570.00	16.33 16.33	27.14 24.29		24.33	0.000169 0.000347	1.50 1.65	822.17 345.04	234.56 91.15	0.11
Channel	2780.00	10yr	437.00	16.33	23.39		23.43	0.000405	1.63	267.72	80.71	0.16
01 1	0400 504	50	200.00	40.00	05.05	22.22	05.40	0.00000	1.01	110.07	407.00	0.44
Channel	2100.591	50yr	699.00	16.00	25.05	20.02	25.10	0.000320	1.81	413.67	137.00	0.15
Channel	2100.591	100yr	838.00	16.00	26.30	20.38	26.34	0.000190	1.57	615.58	184.88	0.12
Channel	2100.591	500yr	1080.00	16.00	27.00	20.94	27.04	0.000198	1.73	754.95	236.93	0.12
Channel	2100.591	25yr	570.00	16.00	24.00	19.63	24.06	0.000458	1.94	294.96	82.10	0.17
Channel	2100.591	10yr	437.00	16.00	23.05	19.19	23.11	0.000538	1.92	227.57	65.70	0.18
Channel	1527.972	50yr	699.00	14.82	24.52	21.83	24.72	0.001986	3.58	195.41	56.29	0.34
Channel	1527.972	100yr	838.00	14.82	26.25	22.19	26.26	0.000084	0.88	1018.85	342.74	0.07
Channel	1527.972	500yr	1080.00	14.82	26.96	22.75	26.97	0.000077	0.93	1350.22	537.54	0.07
Channel	1527.972	25yr	570.00	14.82	23.15	21.43	23.45	0.003813	4.45	128.21	42.62	0.45
Channel	1527.972	10yr	437.00	14.82	21.80	20.97	22.28	0.008360	5.59	78.13	32.48	0.64
Channel	1344.355	50yr	699.00	14.44	24.50	18.35	24.56	0.000306	1.83	387.24	94.33	0.15
Channel	1344.355	100yr	838.00	14.44	26.20	18.75	26.24	0.000151	1.57	603.26	265.03	0.11
Channel	1344.355	500yr	1080.00	14.44	26.91	19.38	26.95	0.000153	1.69	837.85	349.91	0.11
Channel	1344.355	25yr	570.00	14.44	23.12	17.92	23.19	0.000478	2.04	278.98	66.69	0.18
Channel	1344.355	10yr	437.00	14.44	21.85	17.46	21.92	0.000496	2.10	207.69	48.27	0.18
Channel	1281.855		Culvert									
Channel	1218.437	50yr	699.00	13.50	19.86		20.12	0.001086	4.11	169.89	39.43	0.35
Channel	1218.437	100yr	838.00	13.50	20.43		20.72	0.001099	4.34	193.74	46.81	0.36
Channel	1218.437	500yr	1080.00	13.50	21.33		21.66	0.001079	4.61	242.74	59.87	0.36
Channel	1218.437	25yr	570.00	13.50	19.26		19.50	0.001079	3.87	147.17	37.06	0.34
Channel	1218.437	10yr	437.00	13.50	18.55		18.75	0.001057	3.59	121.75	34.20	
	12.10.407	,.	407.50	10.50	10.00		10.70	3.001007	0.00	121.70	J-1.20	0.5-
Channel	972.498	50yr	699.00	13.10	19.00	17.37	19.60	0.002969	6.25	111.82	27.92	0.55
Channel	972.498	100yr	838.00	13.10	19.50	17.81	20.18	0.002909	6.64	126.23	29.45	0.57
Channel	972.498	500yr	1080.00	13.10	20.29	18.51	21.09	0.003072	7.17	150.63	31.87	0.58
Channel	972.498	25yr	570.00	13.10	18.48	16.91	19.00	0.003166	5.84	97.67	26.34	0.53
		-		13.10				0.002851	5.84			0.52
Channel	972.498	10yr	437.00	13.10	17.83	16.38	18.28	0.002761	5.37	81.35	24.38	0.52
Channel	648.236	50vr	699.00	12.60	17.99	16.66	18.60	0.002240	6.24	110.05	31.57	0.50
Channel		50yr						0.003249		112.05		0.58
Channel	648.236	100yr	838.00	12.60	18.50	17.07	19.16	0.003218	6.52	128.54	33.59	0.59
Channel	648.236	500yr	1080.00	12.60	19.28	17.71	20.02	0.003323	6.91	156.32	38.41	0.60
Channel	648.236	25yr	570.00	12.60	17.46	16.24	18.01	0.003312	5.95	95.74	29.43	0.58
Channel	648.236	10yr	437.00	12.60	16.46	15.74	17.10	0.004858	6.38	68.51	25.46	0.69
		l										
Channel	267.180	50yr	699.00	7.17	17.19	12.29	17.29	0.002826	2.58	270.65	58.65	0.21
Channel	267.180	100yr	838.00	7.17	17.69	12.81	17.81	0.003014	2.79	300.51	60.87	0.22
Channel	267.180	500yr	1080.00	7.17	18.52	13.65	18.65	0.002935	3.01	389.35	167.49	
	267.180	25yr	570.00	7.17	16.66	11.81	16.74	0.002656	2.38	239.93	56.27 38.02	0.20
Channel	267.180		437.00	7.17			14.45	0.009574	3.65	119.75		0.36

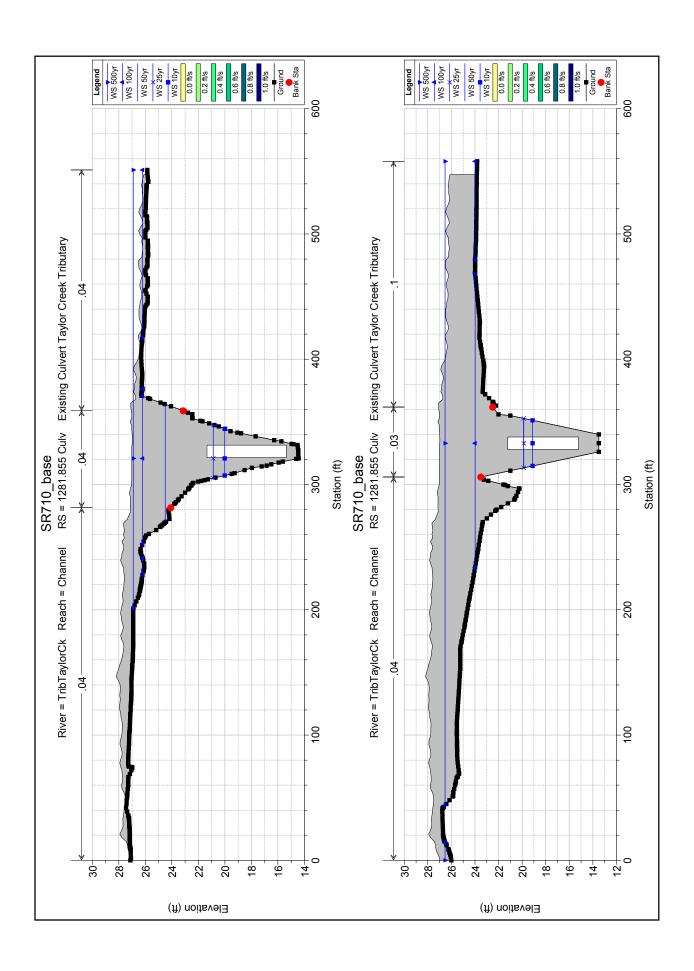


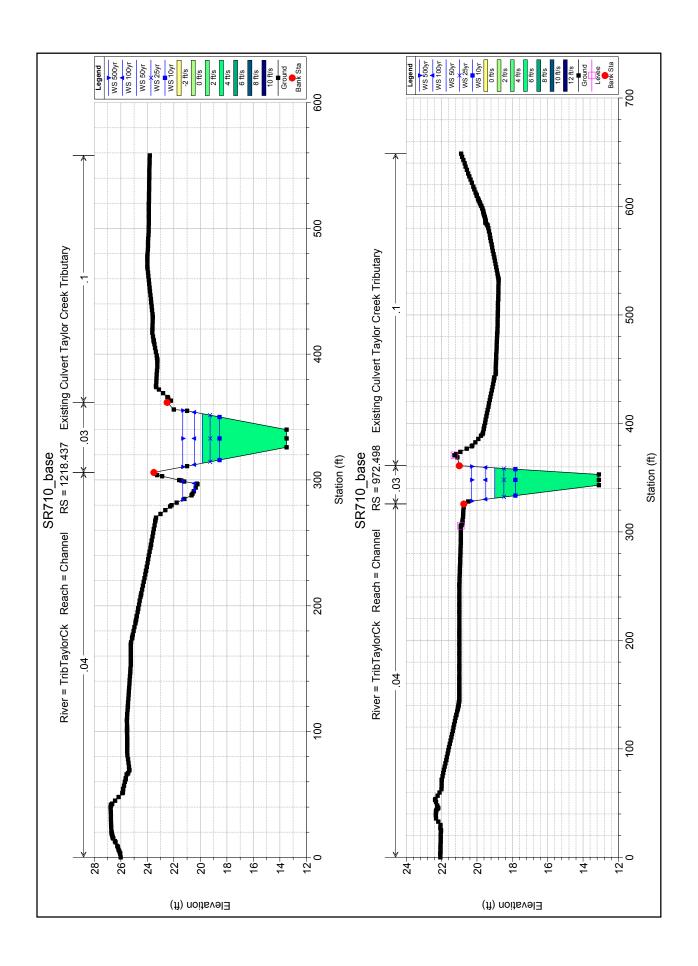


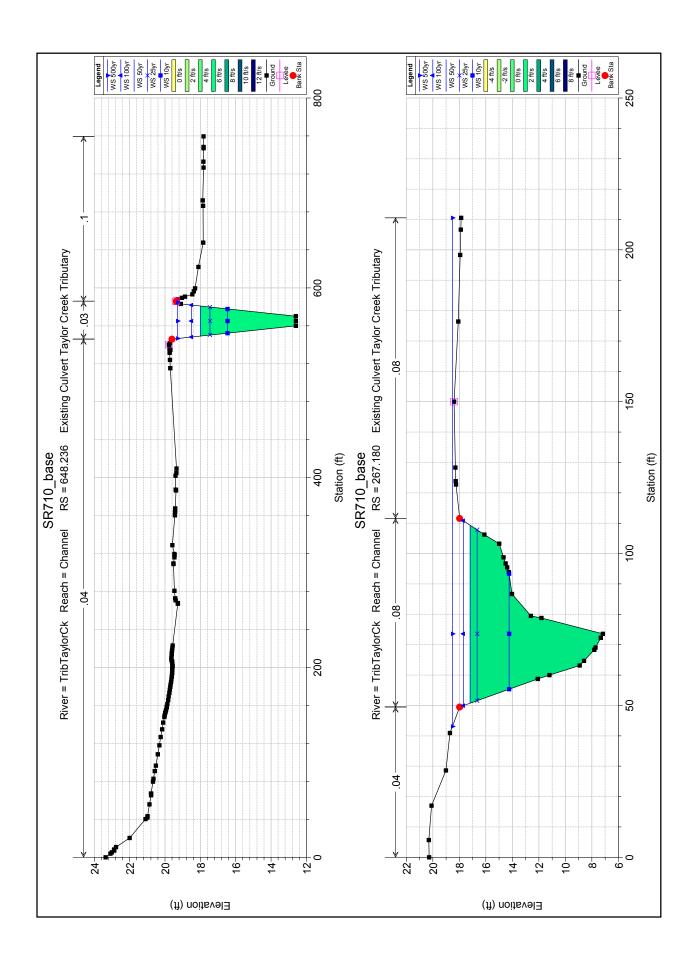


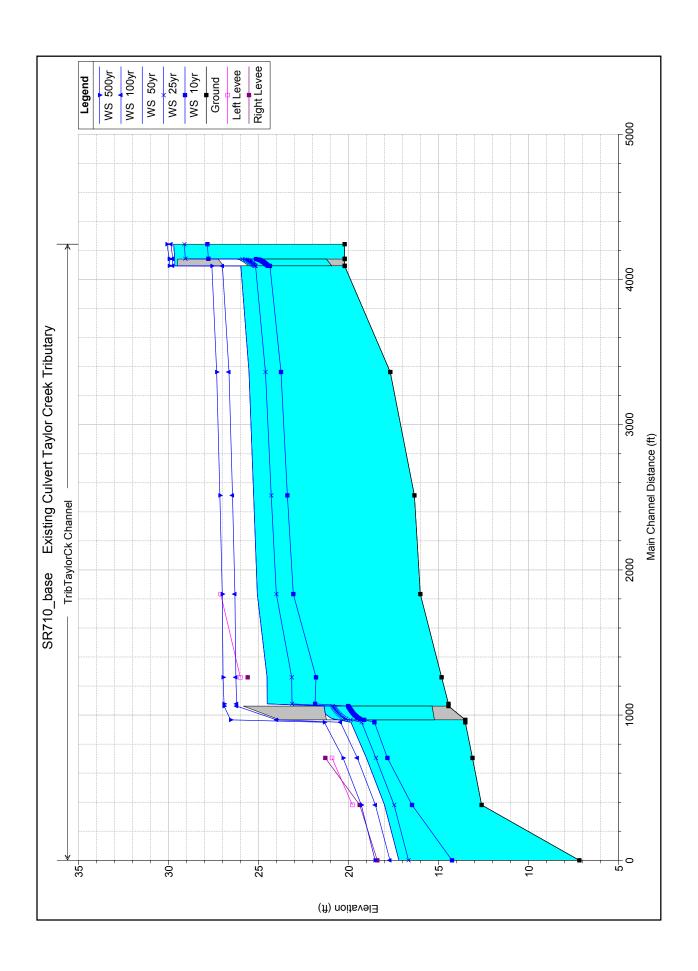










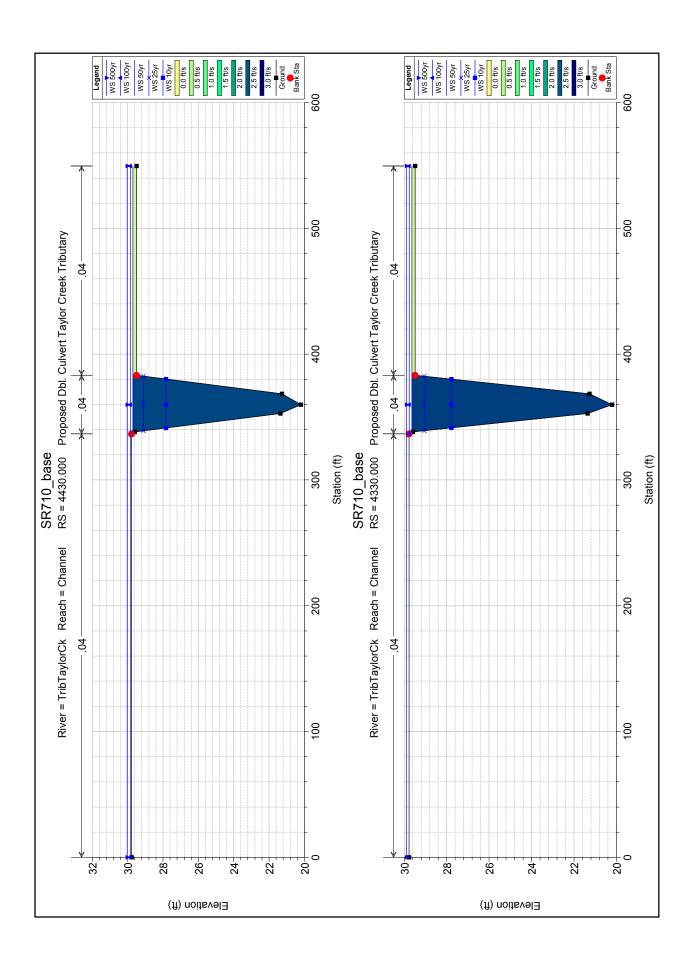


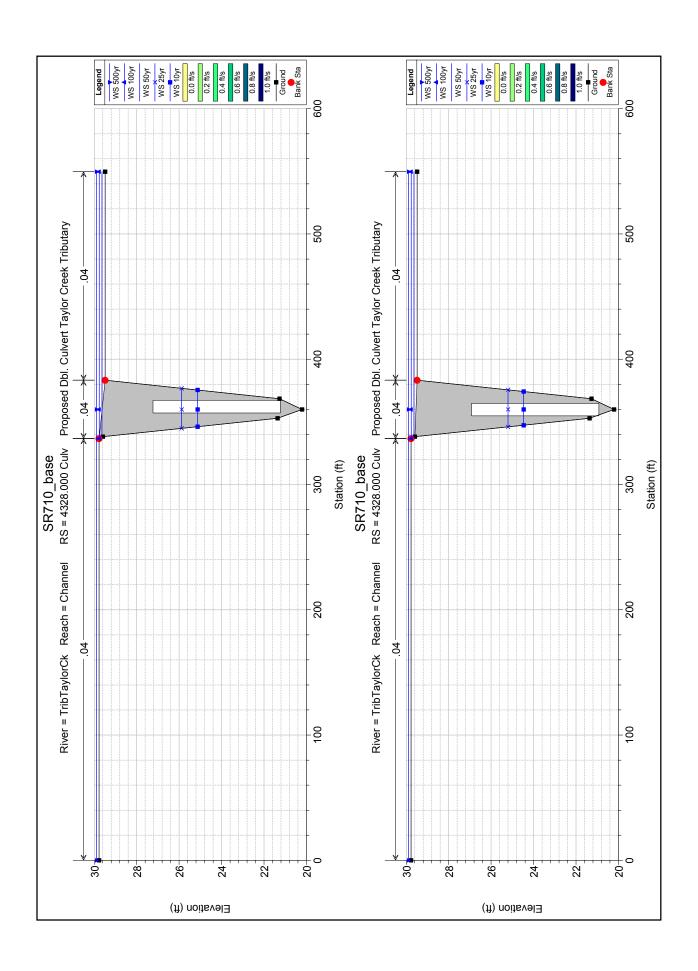
HEC-RAS Plan: US&DS River: TribTaylorCk Reach: Channel

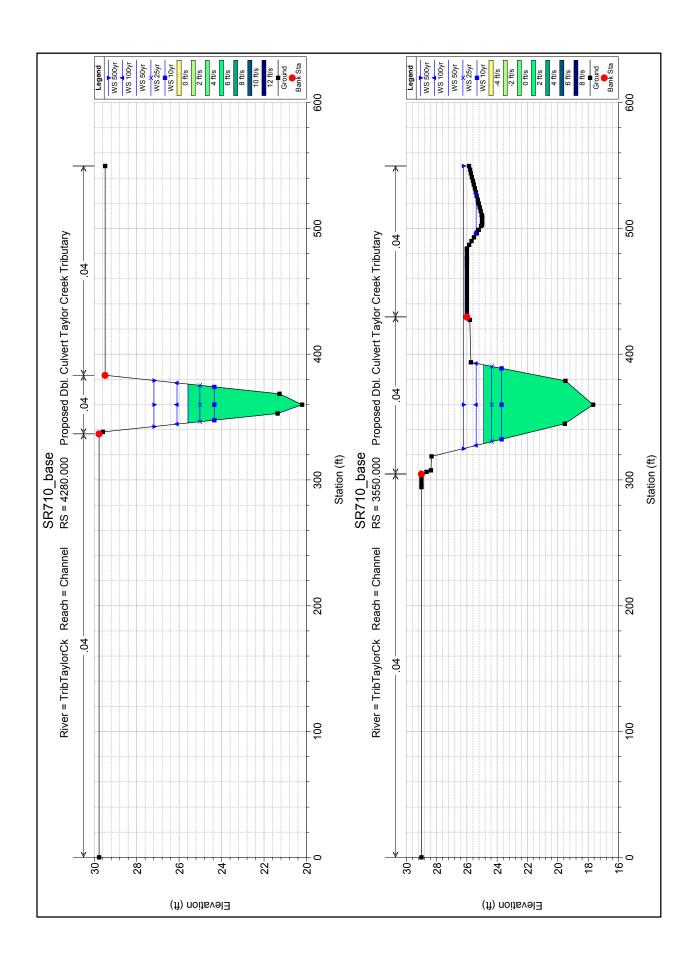
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Channel 4330.000 Channel 4328.000 Channel 4280.000 Channel 4280.000 Channel 4280.000 Channel 4280.000 Channel 4280.000 Channel 3550.000 Channel 3550.000 Channel 3550.000 Channel 3550.000 Channel 2780.000 Channel 2780.000 Channel 2780.000 Channel 2780.000 Channel 2780.000 Channel 2100.591 Channel 2100.591 Channel 2100.591 Channel 1527.972 Channel 1527.972 Channel 1527.972 Channel 1527.972 Channel 1344.355 Channel 1344.355 Channel 1344.355 Channel 128.835 Channel 1218.437 Channel 1218.437	3.000 3.000 3.000 3.000 3.000 3.000 3.000 3.000 3.000	50yr 100yr 500yr 500yr 25yr 10yr	437.00 Culvert 699.00 838.00 1080.00 570.00	20.20				0.000491	2.40	237.04	43.29	0.18
Channel 4328.000 Channel 4280.000 Channel 4280.000 Channel 4280.000 Channel 4280.000 Channel 3550.000 Channel 3550.000 Channel 3550.000 Channel 3550.000 Channel 2780.000 Channel 2780.000 Channel 2780.000 Channel 2780.000 Channel 2780.000 Channel 2780.000 Channel 2100.591 Channel 2100.591 Channel 2100.591 Channel 2100.591 Channel 1527.972 Channel 1527.972 Channel 1527.972 Channel 1344.355 Channel 1344.355 Channel 1344.355 Channel 128.437 Channel 1218.437 Channel 1218.437 Channel 1218.437	6.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	50yr 100yr 500yr 25yr 10yr	Culvert 699.00 838.00 1080.00 570.00	20.20		20.00		0.000570	2.37	184.47	38.72	0.19
Channel 4280.000 Channel 4280.000 Channel 4280.000 Channel 4280.000 Channel 4280.000 Channel 3550.000 Channel 3550.000 Channel 3550.000 Channel 3550.000 Channel 2780.000 Channel 2780.000 Channel 2780.000 Channel 2780.000 Channel 2780.000 Channel 2100.591 Channel 2100.591 Channel 2100.591 Channel 2100.591 Channel 1527.972 Channel 1527.972 Channel 1527.972 Channel 1527.972 Channel 1344.355 Channel 1344.355 Channel 1344.355 Channel 128.437 Channel 1218.437 Channel 1218.437 Channel 12218.437	0.000 0.000 0.000 0.000 0.000 0.000 0.000	100yr 500yr 25yr 10yr	699.00 838.00 1080.00 570.00				21.00	0.000070	2.07		00.72	0.10
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Channel 3550.000 Channel 3550.000 Channel 3550.000 Channel 3550.000 Channel 3550.000 Channel 3550.000 Channel 2780.000 Channel 2780.000 Channel 2780.000 Channel 2780.000 Channel 2100.591 Channel 2100.591 Channel 2100.591 Channel 1527.972 Channel 1527.972 Channel 1527.972 Channel 1527.972 Channel 1344.355 Channel 1344.355 Channel 1344.355 Channel 1281.835 Channel 1281.835 Channel 1218.437 Channel 1218.437 Channel 1218.437 Channel 1218.437 Channel 1218.437	0.000 0.000 0.000			20.20	25.02		25.62	0.006656	6.23	91.45	28.91	0.62
Channel 3550.000 Channel 3550.000 Channel 3550.000 Channel 3550.000 Channel 2780.000 Channel 2780.000 Channel 2780.000 Channel 2780.000 Channel 2780.000 Channel 2100.591 Channel 2100.591 Channel 2100.591 Channel 2100.591 Channel 1527.972 Channel 1527.972 Channel 1527.972 Channel 1527.972 Channel 1344.355 Channel 1344.355 Channel 1344.355 Channel 1284.835 Channel 1284.835 Channel 1218.437 Channel 1218.437 Channel 1218.437 Channel 1218.437 Channel 1218.437	0.000	50yr	437.00	20.20	24.34		24.90	0.007441	6.02	72.63	26.49	0.64
Channel 3550.000 Channel 3550.000 Channel 3550.000 Channel 3550.000 Channel 2780.000 Channel 2780.000 Channel 2780.000 Channel 2780.000 Channel 2780.000 Channel 2100.591 Channel 2100.591 Channel 2100.591 Channel 2100.591 Channel 1527.972 Channel 1527.972 Channel 1527.972 Channel 1527.972 Channel 1344.355 Channel 1344.355 Channel 1344.355 Channel 1284.835 Channel 1284.835 Channel 1218.437 Channel 1218.437 Channel 1218.437 Channel 1218.437 Channel 1218.437	0.000	50yr										
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Channel 3550.000 Channel 3550.000 Channel 2780.000 Channel 2780.000 Channel 2780.000 Channel 2780.000 Channel 2780.000 Channel 2100.591 Channel 2100.591 Channel 2100.591 Channel 2100.591 Channel 1527.972 Channel 1527.972 Channel 1527.972 Channel 1527.972 Channel 1344.355 Channel 1344.355 Channel 1344.355 Channel 1281.835 Channel 1281.835 Channel 1218.437 Channel 1218.437 Channel 1218.437 Channel 1218.437 Channel 1218.437	.000	100yr	838.00	17.67	25.38		25.49	0.000601	2.58	330.72	97.00	0.20
Channel 3550.000 Channel 2780.000 Channel 2780.000 Channel 2780.000 Channel 2780.000 Channel 2780.000 Channel 2100.591 Channel 2100.591 Channel 1527.972 Channel 1527.972 Channel 1527.972 Channel 1527.972 Channel 1344.355 Channel 1344.355 Channel 1344.355 Channel 1344.355 Channel 1281.855 Channel 1281.835 Channel 1218.437		500yr	1080.00	17.67	26.23		26.33	0.000857	2.60	463.40	224.78	0.24
Channel 2780.000 Channel 2780.000 Channel 2780.000 Channel 2780.000 Channel 2780.000 Channel 2780.000 Channel 2100.591 Channel 2100.591 Channel 2100.591 Channel 1527.972 Channel 1527.972 Channel 1527.972 Channel 1527.972 Channel 1344.355 Channel 1344.355 Channel 1344.355 Channel 1344.355 Channel 1281.835 Channel 1281.835 Channel 1218.437 Channel 1218.437 Channel 1218.437 Channel 1218.437 Channel 1218.437 Channel 1218.437	0.000	25yr	570.00	17.67	24.36		24.43	0.000519	2.20	259.12	59.84	0.19
Channel 2780.000 Channel 2780.000 Channel 2780.000 Channel 2780.000 Channel 2780.000 Channel 2100.591 Channel 2100.591 Channel 2100.591 Channel 1527.972 Channel 1527.972 Channel 1527.972 Channel 1527.972 Channel 1344.355 Channel 1344.355 Channel 1344.355 Channel 1281.855 Channel 1281.835 Channel 1218.437 Channel 1218.437 Channel 1218.437 Channel 1218.437 Channel 1218.437 Channel 1218.437		10yr	437.00	17.67	23.71		23.77	0.000476	1.97	221.27	56.39	0.18
Channel 2780.000 Channel 2780.000 Channel 2780.000 Channel 2780.000 Channel 2780.000 Channel 2100.591 Channel 2100.591 Channel 2100.591 Channel 1527.972 Channel 1527.972 Channel 1527.972 Channel 1527.972 Channel 1344.355 Channel 1344.355 Channel 1344.355 Channel 1281.855 Channel 1281.835 Channel 1218.437 Channel 1218.437 Channel 1218.437 Channel 1218.437 Channel 1218.437 Channel 1218.437	_											
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Channel 2780.000 Channel 2780.000 Channel 2780.000 Channel 2100.591 Channel 2100.591 Channel 2100.591 Channel 1527.972 Channel 1527.972 Channel 1527.972 Channel 1527.972 Channel 1344.355 Channel 1344.355 Channel 1344.355 Channel 1344.355 Channel 1281.855 Channel 1281.835 Channel 1218.437 Channel 1218.437 Channel 1218.437 Channel 1218.437 Channel 1218.437 Channel 1218.437		100yr	838.00	16.33	24.96		25.02	0.000475	2.05	409.07	98.97	0.18
Channel 2780.000 Channel 2100.591 Channel 2100.591 Channel 2100.591 Channel 2100.591 Channel 1527.972 Channel 1527.972 Channel 1527.972 Channel 1527.972 Channel 1344.355 Channel 1344.355 Channel 1344.355 Channel 1344.355 Channel 1344.355 Channel 1281.855 Channel 1218.437	0.000	500yr	1080.00	16.33	25.71		25.79	0.000485	2.20	508.28	161.06	0.18
Channel 2100.591 Channel 2100.591 Channel 2100.591 Channel 2100.591 Channel 2100.591 Channel 2100.591 Channel 1527.972 Channel 1527.972 Channel 1527.972 Channel 1344.355 Channel 1344.355 Channel 1344.355 Channel 1344.355 Channel 1281.835 Channel 1218.437 Channel 1218.437 Channel 1218.437 Channel 1218.437 Channel 1218.437 Channel 1218.437		25yr	570.00	16.33	23.97		24.02	0.000436	1.80	317.04	87.53	0.17
Channel 2100.591 Channel 2100.591 Channel 2100.591 Channel 2100.591 Channel 1527.972 Channel 1527.972 Channel 1527.972 Channel 1527.972 Channel 1344.355 Channel 1344.355 Channel 1344.355 Channel 1344.355 Channel 1281.855 Channel 1281.855 Channel 1218.437	0.000	10yr	437.00	16.33	23.34		23.38	0.000420	1.66	264.02	80.19	0.16
Channel 2100.591 Channel 2100.591 Channel 2100.591 Channel 2100.591 Channel 1527.972 Channel 1527.972 Channel 1527.972 Channel 1527.972 Channel 1344.355 Channel 1344.355 Channel 1344.355 Channel 1344.355 Channel 1281.855 Channel 1281.855 Channel 1218.437												
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Channel 2100.591 Channel 2100.591 Channel 1527.972 Channel 1527.972 Channel 1527.972 Channel 1527.972 Channel 1344.355 Channel 1344.355 Channel 1344.355 Channel 1344.355 Channel 1281.855 Channel 1218.437		100yr	838.00	16.00	24.55	20.38	24.65	0.000650	2.48	350.08	116.06	0.21
Channel 2100.591 Channel 1527.972 Channel 1527.972 Channel 1527.972 Channel 1527.972 Channel 1344.355 Channel 1344.355 Channel 1344.355 Channel 1344.355 Channel 1281.855 Channel 1218.437		500yr	1080.00	16.00	25.30	20.94	25.41	0.000642	2.62	449.31	147.26	0.21
Channel 1527.972 Channel 1527.972 Channel 1527.972 Channel 1527.972 Channel 1527.972 Channel 1344.355 Channel 1344.355 Channel 1344.355 Channel 1281.855 Channel 1218.437		25yr	570.00	16.00	23.60	19.63	23.67	0.000612	2.15	265.08	71.22	0.20
Channel 1527.972 Channel 1527.972 Channel 1527.972 Channel 1527.972 Channel 1344.355 Channel 1344.355 Channel 1344.355 Channel 1344.355 Channel 1281.855 Channel 1218.437).591	10yr	437.00	16.00	22.99	19.19	23.05	0.000564	1.95	223.62	65.08	0.19
Channel 1527.972 Channel 1527.972 Channel 1527.972 Channel 1527.972 Channel 1344.355 Channel 1344.355 Channel 1344.355 Channel 1344.355 Channel 1281.855 Channel 1218.437												
Channel 1527.972 Channel 1527.972 Channel 1527.972 Channel 1344.355 Channel 1344.355 Channel 1344.355 Channel 1344.355 Channel 1281.855 Channel 1218.437		50yr	699.00	14.82	21.98	21.83	23.05	0.017666	8.32	84.05	33.91	0.93
Channel 1527.972 Channel 1527.972 Channel 1344.355 Channel 1344.355 Channel 1344.355 Channel 1344.355 Channel 1281.855 Channel 1218.437		100yr	838.00	14.82	22.38	22.19	23.51	0.016473	8.54	98.15	36.29	0.91
Channel 1527.972 Channel 1344.355 Channel 1344.355 Channel 1344.355 Channel 1344.355 Channel 1281.855 Channel 1218.437 Channel 1218.437 Channel 1218.437 Channel 1218.437 Channel 1218.437 Channel 1218.437		500yr	1080.00	14.82	23.56	22.75	24.40	0.009702	7.35	146.97	46.63	0.73
Channel 1344.355 Channel 1344.355 Channel 1344.355 Channel 1344.355 Channel 1344.355 Channel 1281.855 Channel 1218.437 Channel 1218.437 Channel 1218.437 Channel 1218.437 Channel 1218.437		25yr	570.00	14.82	21.55	21.43	22.57	0.018835	8.12	70.19	30.49	0.94
Channel 1344.355 Channel 1344.355 Channel 1344.355 Channel 1281.855 Channel 1218.437	.972	10yr	437.00	14.82	20.97	20.97	21.99	0.022534	8.11	53.85	26.43	1.00
Channel 1344.355 Channel 1344.355 Channel 1344.355 Channel 1281.855 Channel 1218.437	255	F0	000.00	44.44	00.40	40.05	00.00	0.004000	0.40	222.22	40.70	0.07
Channel 1344.355 Channel 1344.355 Channel 1281.855 Channel 1218.437 Channel 1218.437 Channel 1218.437 Channel 1218.437 Channel 1218.437 Channel 1218.437		50yr	699.00	14.44	22.10	18.35	22.26	0.001089	3.18	220.00	49.72	0.27
Channel 1344.355 Channel 1344.355 Channel 1281.855 Channel 1218.437 Channel 1218.437 Channel 1218.437 Channel 1218.437 Channel 1218.437		100yr	838.00	14.44	22.45	18.75	22.64	0.001306	3.53	237.64	52.70	0.29
Channel 1344.355 Channel 1281.855 Channel 1218.437 Channel 1218.437 Channel 1218.437 Channel 1218.437 Channel 1218.437		500yr	1080.00	14.44	23.47	19.38	23.67 21.85	0.001402 0.000915	3.57 2.83	303.05	71.82 47.54	0.30
Channel 1281.855 Channel 1218.437 Channel 1218.437 Channel 1218.437 Channel 1218.437		25yr	570.00 437.00	14.44 14.44	21.72	17.92 17.46	20.90	0.000915	2.63	201.45	42.09	0.24
Channel 1218.437 Channel 1218.437 Channel 1218.437 Channel 1218.437		10yr	437.00	14.44	20.78	17.40	20.90	0.001003	2.75	159.18	42.09	0.25
Channel 1218.437 Channel 1218.437 Channel 1218.437 Channel 1218.437	055		Culvert									
Channel 1218.437 Channel 1218.437 Channel 1218.437	.000		Culvert									
Channel 1218.437 Channel 1218.437 Channel 1218.437	1437	50vr	699.00	13.50	21.38		21.52	0.000439	2.95	245.91	60.51	0.23
Channel 1218.437 Channel 1218.437		50yr 100yr	838.00	13.50	21.39		21.52	0.000439	3.53	245.91	60.53	0.23
Channel 1218.437		500yr	1080.00	13.50	21.58		21.87	0.000939	4.38	257.70	62.62	0.27
		25yr	570.00	13.50	21.26		21.36	0.000939	2.47	238.71	59.04	0.33
1210.437		10yr	437.00	13.50	20.47		20.55	0.000313	2.47	195.42	47.78	0.19
	101	.031	757.00	10.00	20.71		20.00	5.500295	2.24	100.42	71.70	0.10
Channel 972.498	498	50yr	699.00	13.10	21.11	17.37	21.34	0.000834	3.87	207.71	234.00	0.30
Channel 972.498		100yr	838.00	13.10	21.11	17.81	21.34	0.000834	3.00	781.44	526.92	0.30
Channel 972.498		500yr	1080.00	13.10	21.47	18.51	21.60	0.000477	3.54	873.04	539.76	0.23
Channel 972.498		25yr	570.00	13.10	21.08	16.91	21.24	0.000572	3.19	199.64	229.62	0.27
Channel 972.498		10yr	437.00	13.10	20.31	16.38	20.44	0.000515	2.89	151.02	31.91	0.23
0.200		-,-	107.50	.50	20.01		20.74	2.3000.0	2.00	.052	001	
Channel 648.236		50yr	699.00	12.60	21.22	16.66	21.23	0.000061	1.20	1538.04	721.85	0.09
Channel 648.236	236	100yr	838.00	12.60	21.30	17.07	21.32	0.000079	1.37	1600.40	723.76	0.10
Channel 648.236		500yr	1080.00	12.60	21.48	17.71	21.49	0.000106	1.62	1725.34	727.56	0.12
Channel 648.236	236	25yr	570.00	12.60	21.15	16.24	21.16	0.000045	1.01	1487.81	720.31	0.07
Channel 648.236	236 236	10yr	437.00	12.60	20.33	15.74	20.35	0.000048	1.26	927.50	642.78	0.10
	236 236 236											
Channel 267.180	236 236 236	50yr	699.00	7.17	21.18	12.29	21.19	0.000172	0.94	904.97	210.57	0.06
Channel 267.180	236 236 236 236	100yr	838.00	7.17	21.25	12.81	21.27	0.000235	1.11	920.37	210.57	0.07
Channel 267.180	236 236 236 236 236	500yr	1080.00	7.17	21.40	13.65	21.43	0.000353	1.38	951.69	210.57	0.08
Channel 267.180	236 236 236 236 236 180	25yr	570.00	7.17	21.12	11.81	21.13	0.000119	0.78	892.69	210.57	0.05
Channel 267.180	236 236 236 236 236 180 180		437.00	7.17	20.30	11.24	20.31	0.000125	0.75	719.30	210.28	0.05
	236 236 236 236 236 180 180 180	10yr	· · · · ·									

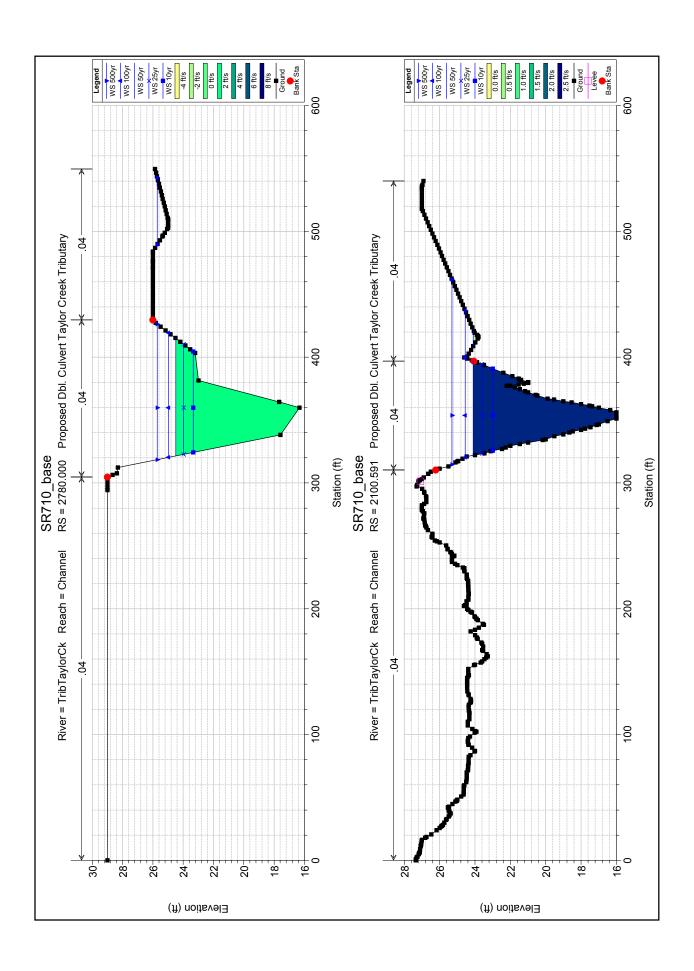
HEC-RAS Plan: US&DS River: TribTaylorCk Reach: Channel (Continued)

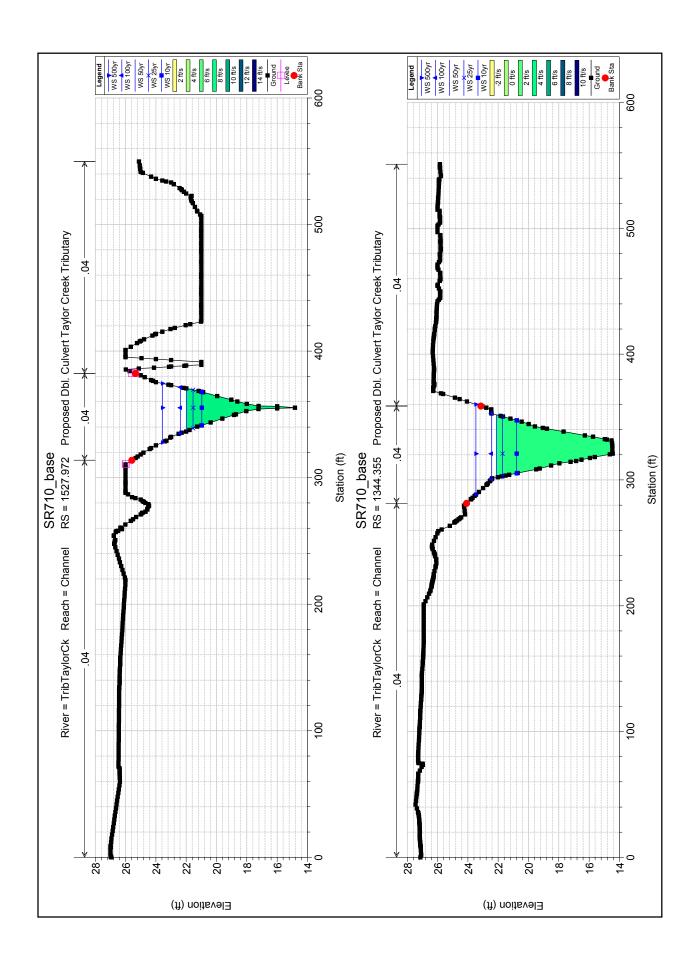
Reach	River Sta	Profile	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chnl	Flow Area	Top Width	Froude # Chl
			(cfs)	(ft)	(ft)	(ft)	(ft)	(ft/ft)	(ft/s)	(sq ft)	(ft)	
Channel	-232.82	50yr	699.00	6.67	21.09	12.02	21.10	0.000179	0.96	891.16	210.57	0.06
Channel	-232.82	100yr	838.00	6.67	21.13	12.51	21.15	0.000251	1.14	899.37	210.57	0.07
Channel	-232.82	500yr	1080.00	6.67	21.21	13.41	21.24	0.000395	1.44	916.65	210.57	0.09
Channel	-232.82	25yr	570.00	6.67	21.06	11.52	21.07	0.000122	0.79	884.74	210.57	0.05
Channel	-232.82	10yr	437.00	6.67	20.24	10.95	20.24	0.000128	0.75	711.04	201.38	0.05
Channel	-732.82	50yr	699.00	6.17	21.00	11.73	21.01	0.000188	0.98	876.64	210.57	0.06
Channel	-732.82	100yr	838.00	6.17	21.00	12.24	21.02	0.000271	1.17	876.64	210.57	0.07
Channel	-732.82	500yr	1080.00	6.17	21.00	13.13	21.03	0.000449	1.51	876.64	210.57	0.09
Channel	-732.82	25yr	570.00	6.17	21.00	11.22	21.01	0.000125	0.80	876.64	210.57	0.05
Channel	-732.82	10yr	437.00	6.17	20.17	10.62	20.18	0.000131	0.76	702.98	197.86	0.05

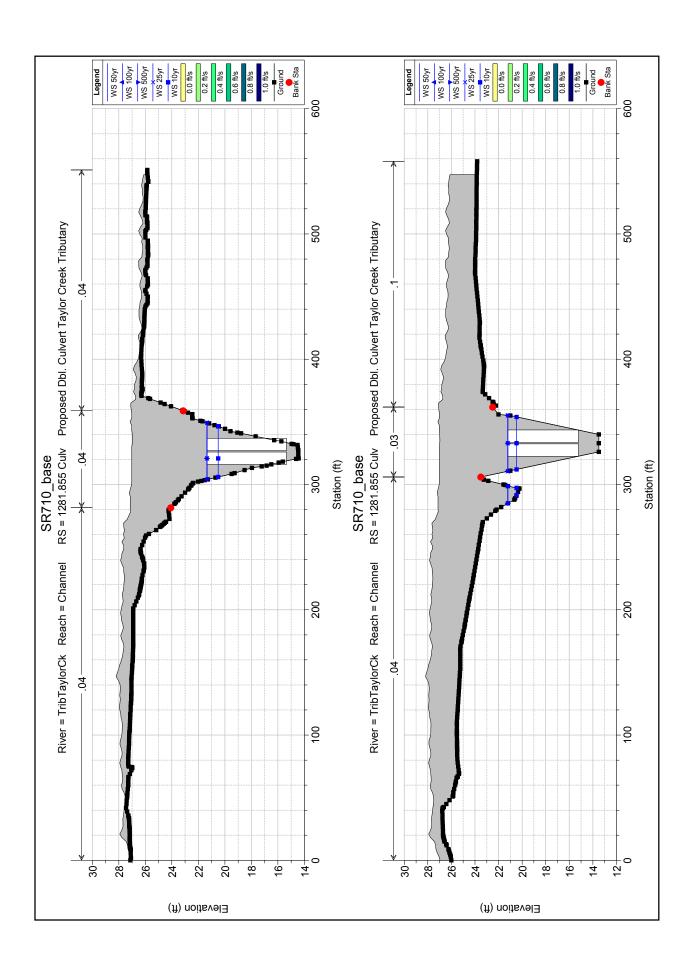


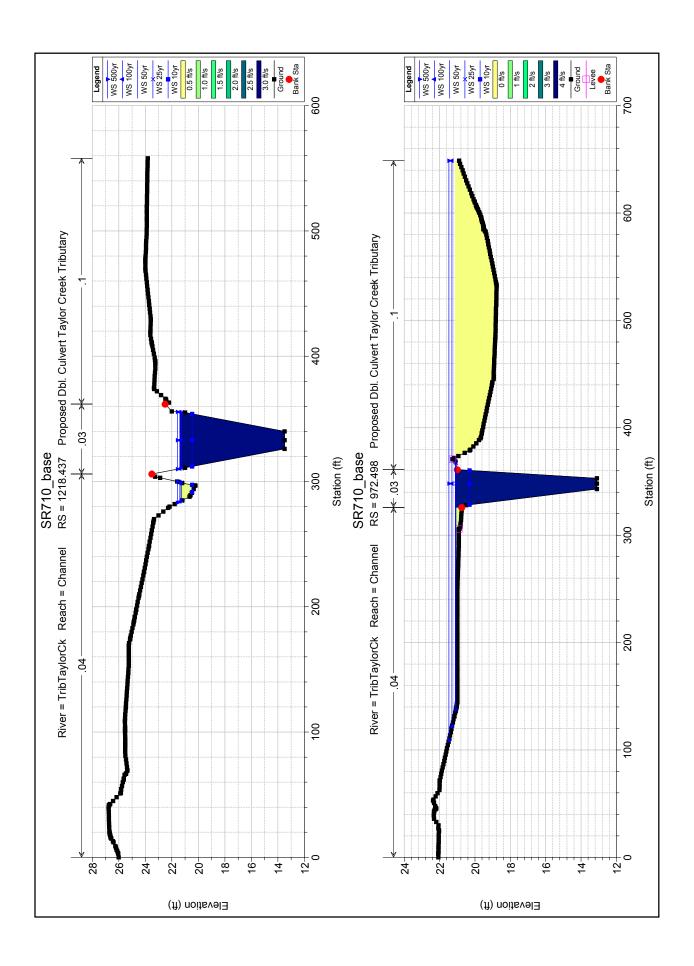


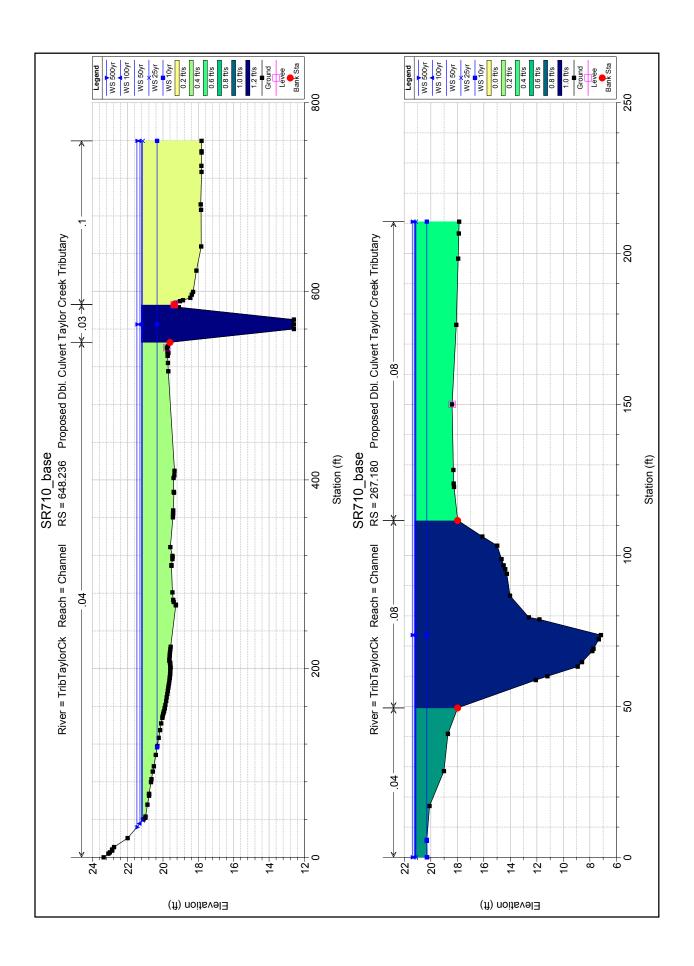


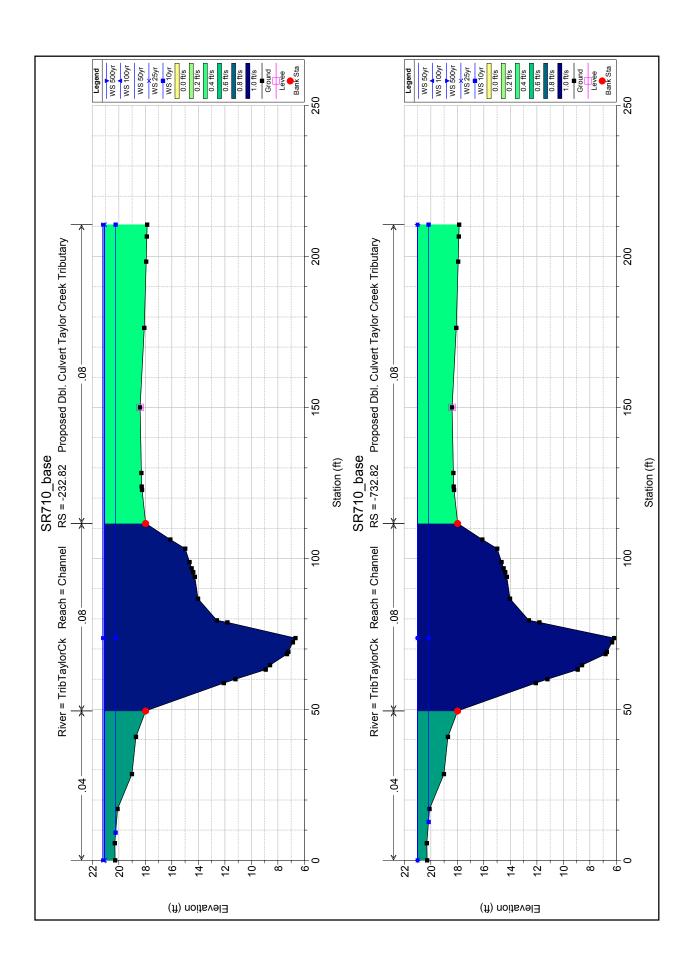


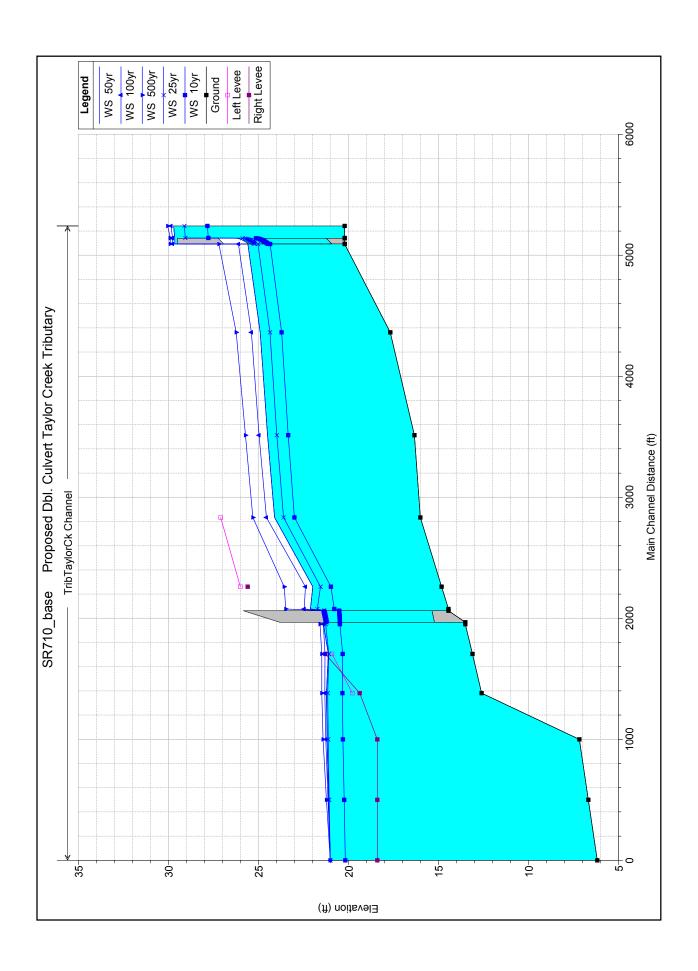












380 330		10-Year Water Surface Elevation	rface Elevation	Difference	25-Year Water Surface Elevation	urface Elevation	Difference	50-Year Water S.	50-Year Water Surface Elevation	Difference	100-Year Water	100-Year Water Surface Elevation	Difference	500-Year Water	500-Year Water Surface Elevation	Difference
	,0110	(feet NAVD88)	VD88)	(feet)	(feet NAVD88)	4VD88)	(feet)	(feet N,	(feet NAVD88)	(feet)	(feet N	(feet NAVD88)	(feet)	(feet N	(feet NAVD88)	(feet)
Section		Exist	Proposed Double		Exist	Proposed Double		Exist	Proposed Double		Exist	Proposed Double		Exist	Proposed Double	
4430.000 TribTa	TribTaylor Ck	27.83	27.83	0.00	29.10	29.10	0:00	29.70	29.70	0.00	29.84	29.85	0.01	30.07	30.03	-0.04
4330.000 TribTay	TribTaylor Ck	77.72	77.72	0.00	29.05	29.05	0.00	29.64	29.64	0.00	29.76	29.77	0.01	29.95	29.89	-0.06
Culvert TribTay	TribTaylor Ck	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	A/N	N/A	N/A	N/A	N/A	N/A	N/A
4280.000 TribTay	TribTaylor Ck	24.36	24.34	-0.02	25.16	25.02	-0.14	25.97	25.58	-0.39	26.99	26.10	-0.89	27.58	27.18	-0.40
3550.000 TribTay	TribTaylor Ck	23.74	23.71	-0.03	24.60	24.36	-0.24	25.52	24.89	-0.63	26.62	25.38	-1.24	27.31	26.23	-1.08
2780.000 TribTay	TribTaylor Ck	23.39	23.34	-0.05	24.29	23.97	-0.32	25.26	24.49	-0.77	26.43	24.96	-1.47	27.14	25.71	-1.43
2100.591 TribTay	TribTaylor Ck	23.05	22.99	-0.06	24.00	23.60	-0.40	25.05	24.10	-0.95	26.30	24.55	-1.75	27.00	25.30	-1.70
1527.972 TribTay	TribTaylor Ck	21.80	20.97	-0.83	23.15	21.55	-1.60	24.52	21.98	-2.54	26.25	22.38	-3.87	26.96	23.56	-3.40
1344.355 TribTay	TribTaylor Ck	21.85	20.78	-1.07	23.12	21.72	-1.40	24.50	22.10	-2.40	26.20	22.45	-3.75	26.91	23.47	-3.44
Culvert TribTay	TribTaylor Ck	N/A	N/A	N/A	N/A	W/N	N/A	N/A	N/A	N/A	W/A	N/A	N/A	N/A	N/A	N/A
1218.437 TribTay	TribTaylor Ck	18.55	20.47	1.92	19.26	21.26	2.00	19.86	21.38	1.52	20.43	21.39	96:0	21.33	21.58	0.25
972.498 TribTay	TribTaylor Ck	17.83	20.31	2.48	18.48	21.08	2.60	19.00	21.11	2.11	19.50	21.30	1.80	20.29	21.47	1.18
648.236 TribTay	TribTaylor Ck	16.46	20.33	3.87	17.46	21.15	3.69	17.99	21.22	3.23	18.50	21.30	2.80	19.28	21.48	2.20
267.180 TribTay	TribTaylor Ck	14.24	20.30	90'9	16.66	21.12	4.46	17.19	21.18	3.99	17.69	21.25	3.56	18.52	21.40	2.88

Appendix C: STA Costs

SR 710 Stormwater Treatment Area/Regional Pond Feasibility Study Final Submittal

Financial Project ID 432644-1-32-01

Okeechobee County, Florida

Cost information for STAs reviewed

Facility	Permitting, and	Annual Operation and Maintenance (\$)	Treatment Acres	Initial Cost per Treatment Acre (\$)
Taylor Creek	5,642,293	50,000	118	47,816
Nubbin Slough	21,257,707	100,000	773	27,500
Lakeside Ranch Phase I	22,800,000	341,000	1,200	19,000
Lakeside Ranch Phase II	25,000,000	Not available	788	31,726
Powell Creek Filter Marsh - Lee County	2,100,000	45,000	40	52,500
Option 1	2,625,000	50,000	50	52,500

Option 2 - Cost based	l on in place unit pr	ice per cubic yar	d	
Depth of Coverage (ft)	Width of Coverage (ft)	Length of coverage(ft)	In Place Cost per CY (\$)	Estimated Initial Cost (\$)
1	50	3,300	180	1,100,000

Option 3 - Initial costs include payment to the landowner for the cost of acquiring a conservation easement over the wetland areas that are being rehydrated.

Appendix D: Wetland and Wildlife Site Evaluation

SR 710 Stormwater Treatment Area/Regional Pond Feasibility Study Final Submittal

Financial Project ID 432644-1-32-01

Okeechobee County, Florida



September 15, 2014

File No. SR-710 STA (50063866)

Mr. Gregory S. Seidel, P.E. The Balmoral Group 165 Lincoln Ave Winter Park, FL 32789



Dewberry | Bowyer-Singleton 520 South Magnolia Avenue Orlando, Florida 32801 407.843.5120 407.649.8664 fax www.dewberry.com

Subject: State Road 710 – Stormwater Treatment Area (STA)

City of Okeechobee, Okeechobee, Florida

Parcel ID Nos.: 1-03-37-35-0A00-00002-0000, 1-10-37-35-0A00-00001-

0000, 1-11-37-35-0A00-00001-0000

Dear Mr. Seidel:

The purpose of this letter is to summarize our site evaluation for the approximately 895-acre referenced property. A qualified biologist of Dewberry Bowyer Singleton (DBS) reviewed the referenced property to evaluate general site conditions and environmental conditions that may influence the use of the site as a stormwater treatment area. Specifically, the site was evaluated for identifying the presence of wildlife species listed as threatened (T), endangered (E) or species of special concern (SSC) as defined by the United States Fish and Wildlife Service (FWS) and/or the Florida Fish and Wildlife Conservation Commission (FWC) and their habitat. Land use types located within the proposed project were identified via vehicular and pedestrian transects and through color aerial photograph interpretation and compared to land uses identified by the Florida Department of Transportation (FDOT) *Florida Land Use, Cover and Forms Classification System* (FLUCFCS) (FDOT 1999) utilizing the South Florida Water Management District (SFWMD) aerial interpretation of these codes available in Geographic Information System (GIS).

PROJECT DESCRIPTION

The overall subject Property consists of approximately 895-acres located within Okeechobee County, Florida. Specifically, the subject property includes the all or portions of the following parcels:

1-03-37-35-0A00-00002-0000 1-10-37-35-0A00-00001-0000 1-11-37-35-0A00-00001-0000

The Property is located north of State Road 70E, east of U.S. Highway 441 N approximately 3 miles north of Lake Okeechobee within the City of Okeechobee. The surrounding areas consists of commercial development, Okeechobee High School, the Okeechobee County Airport, channelized Taylor Creek and other agricultural use specifically cattle ranching.

The SR 710 New Alignment Project in Okeechobee County and the City of Okeechobee is currently under design by the FDOT. During the development of the Pond Siting Report, the Pond Site location 2B and the surrounding area were identified as a possible location for a regional stormwater treatment facility that could provide greater stormwater treatment benefits to the local area. Two teleconferences were held between the FDOT, FDEP and SFWMD to brainstorm the feasibility of the site and possible cooperation between the agencies. At the last meeting, it was decided that the FDOT would perform a feasibility study for two options —

1. A Stormwater Treatment Area (STA) with interagency cooperation connected to the L63-N canal and Upper Taylor Creek.

Mr. Greg Seidel The Balmoral Group SR 710 – Stormwater Treatment Area September 15, 2014 Page 2 of 9

2. A Regional Pond constructed by the FDOT for the SR 710 that would incorporate offsite areas associated with Lower Taylor Creek.

Dewberry | Bowyer-Singleton was contracted to perform the evaluation of onsite wetlands to assist in determining the ability to restore the wetlands using stormwater treatment and attenuation. Qualified environmental scientists with Dewberry | Bowyer-Singleton performed a preliminary ecological field review to evaluate onsite wetlands and listed species within the project vicinity. Dewberry reviewed the current PD&E documents and biological evaluations currently underway by the Wantman Group, Inc. We conducted a desktop review of available published information from federal and state online databases to evaluate listed species that may occupy the project area. Data collection consisted of literature review of existing sources for information useful in identifying the occurrence or potential occurrence of wildlife species listed as T, E or SSC (collectively recognized as listed species), as defined by FWS and/or the FWC. The literature review included the following sources: Natural Resources Conservation Service (f/k/a Soil Conservation Service [SCS]) Soil Survey of Okeechobee County, Florida, U.S. Geological Survey Topographic Quadrangle Maps, FWC Bald Eagle and Waterbird Colony databases, Florida Natural Areas Inventory (FNAI) Okeechobee County Tracking List, previous studies available, and false-color infrared and true color aerial photography of the project corridor, FNAI Field Guides and Rare and Endangered Biota of Florida Series.

Land use types located within the proposed project were identified through color aerial photograph interpretation and compared to land uses identified by the Florida Department of Transportation (FDOT) Florida Land Use, Cover and Forms Classification System (FLUCFCS) (FDOT 1999). Estimated wetland limits were identified on an aerial exhibit. A preliminary qualitative evaluation of the on-site wetlands system(s) was conducted. The wetlands were identified in general accordance with the U.S. Army Corps of Engineers (USACOE) October 2008 Regional Supplement to the Corps of Engineers Wetland Delineation Manual: Atlantic and Gulf Coastal Plain Region and the State of Florida's Delineation of the Landward Extent of Wetlands and Surface Waters (Chapter 62-340, Florida Administrative Code). Seasonal High Water Elevations were marked at six (6) locations in the field adjacent to Taylor Creek (east) within the proposed STA and surveyed to better understand the normal water and allowable peak stage. Three (3) SHWE nails were set at each location and the elevation at each is provided.

ENVIRONMENTAL CONSIDERATIONS

Soils

The *Soil Surveys of Okeechobee County, Florida* (Exhibit 1 - SCS Soils Map) were reviewed and mapped on-site soil types as follows:

Identification	Soil Name	Permeability	Native Vegetation
Number Ph	Placid, Pamlico and Delray soils, ponded	Placid (Rapid); Pamlico (N/A); Delray (Rapid)	Sweetbay, sweetgum, cypress, bracken fern, sawgrass and other hyrophytes
Pn	Pompano fine sand	Rapid	Grassy sloughs and depressions
Ad	Adamsville fine sand	Rapid	Pine trees, saw-palmetto, cabbage palms, other native grasses and shrubs
Fr	Ft. Drum fine sand	Rapid	Open growth pines, scattered cabbage palm, saw palmetto, native grasses
Pf	Placid fine sand	Rapid	Pickerelweed and maidencane
Bm	Basinger and Pompano	Basinger (Rapid);	Maidencane, St. Johnswort, water





Mr. Greg Seidel The Balmoral Group SR 710 – Stormwater Treatment Area September 15, 2014 Page 3 of 9

	fine sands, ponded	Pompano (Rapid)	lilies, pickerelweed and other
			hydrophytic grasses
Im	Immokalee fine sand	Rapid	Native flatwoods, saw palmetto,
		scattered pines and grasses	
Mo	Manatee, Delray and	Manatee (Rapid);	Dense pickerelweed, iris,
	Okeelanta soils	Delray (Rapid);	smartweed, maidencane, black
		Okeelanta (N/A) willow and other aquatic si	
			and grasses
*N/A listed when perme	ability is not provided in the	Soil Survey.	

General site review found soil types to be generally consistent with the mapped soil types.

Land Use

The SFWMD maintains a GIS database with a land use layer covering the entire SFWMD area. This land use layer was overlain on an aerial map using ArcGIS software. Land use types located within the proposed project were verified and/or modified through color aerial photograph interpretation and field reconnaissance. Each on-site land use form was classified using the Florida Department of Transportation (FDOT) *Florida Land Use, Cover and Forms Classification System* (FLUCFCS) as defined in the FDOT handbook, 1999 (**Exhibit 2 – FLUCFCS Map**).

The SR 710 STA project site supports six (6) land use type/vegetative communities within its boundaries. The illustration provided in **Exhibit 2** depicts the locations of all wetlands and the vegetative cover and community types for all wetlands, surface waters and uplands within the project boundaries. The uplands on the subject property consist of Improved Pasture (2110), Upland Hardwood Forest (4200) and Pine Flatwoods (4110). The wetlands and surface waters include Taylor Creek (5120), Mixed Wetland Hardwood (6170) and Cypress (6210). The following provides a brief description of the land use type/vegetative communities identified on the site:

UPLANDS

Improved Pasture – 310 acres FLUCFCS 2110

The majority of the subject site is most consistent with the Improved Pasture classification. This area is dominated by bahia grass (*Paspalum notatum*) and dog fennel where management has not been recently intensive. This area is actively maintained under a cattle management plan so very little other vegetation is present. Those vegetative species that do exist in the less managed areas are opportunistic, weed-type species, including dog fennel (*Eupatorium capillifolium*), broomsedge (*Andropogon virginicus*), blackberry (*Rubus betulifolius*), soda apple (*Solanum capsicoides*), and Caesar weed (*Urena lobata*). Widely scattered and mostly solitary longleaf pines (*Pinus palustris*) are present.

Upland Hardwood Forest – 185 acres FLUCFCS 4200

There are four large oak hammocks located within the property and these are located adjacent to cypress wetlands. These areas (including "Wetland 6") were likely mixed hardwood wetlands serving as floodplain storage prior to the onsite drainage feature construction. Historical aerials depict these areas as part of the historic Taylor Creek flow way and the cypress and freshwater marsh mosaic. These areas currently consist of a mature canopy of water oak (*Quercus nigra*), cabbage palm, sweetgum and elm.

Pine Flatwoods - 60 acres FLUCFCS 4110

The on-site pine flatwoods community is located in the northwest portion of the project, on the west side of Taylor Creek. This upland community contains a canopy of slash pine (*Pinus elliotti*).





Mr. Greg Seidel The Balmoral Group SR 710 – Stormwater Treatment Area September 15, 2014 Page 4 of 9

The groundcover is dominated by saw palmetto, wiregrass (*Aristida stricta*), bracken fern (*Pteridium aquilinum*), prickly pear cactus, shiny blueberry (*Vaccinium myrsinites*), gallberry (*Ilex glabra*) and runner oak (*Quercus pumila*). The soils are well drained and sandy throughout. The pines throughout the flatwoods system have died from unknown cause.

WETLANDS/OTHER SURFACE WATERS

The wetlands and surface waters illustrated in **Exhibit 3** (**Wetlands and Seasonal High Water Level Map**) were approximated using aerial photography and the National Wetlands Inventory (NWI) by qualified biologists from Dewberry | Bowyer Singleton in general accordance with the U.S. Army Corps of Engineers (USACOE) *October 2008 Regional Supplement to the Corps of Engineers Wetland Delineation Manual: Atlantic and Gulf Coastal Plain Region* and the State of Florida's *Delineation of the Landward Extent of Wetlands and Surface Waters* (Chapter 62-340, Florida Administrative Code). Seasonal High Wetland Levels were also set within the 6 wetland areas and are shown on **Exhibit 3**.

Wetlands 1, 2, 3, 4, 5 FLUCFCS 6210 Cypress - 338 acres

The wetland types are similar and contain a mature canopy of bald cypress (Taxodium ascendens), with a heterogenous mixture of sweet bay (*Magnolia virginiana*), red bay (*Persea palustris*) and water oak (*Quercus nigra*) with a subcanopy dominated in some areas by Brazilian pepper and a mixture of cabbage palm.

Groundcover includes wild coffee, cabbage palm, grapevine (*Vitis* spp.), smilax, blackberry (*Rubus* spp.), broomsedge (*Andropogon virginicus*), chain fern (*Woodwardia virginica*), air potato, and lizards tail (*Saururus cernuus*).

Seasonal High Water Elevations set within wetlands 1, 3 and 5 were established at flow ways (either an excavated ditch within the wetland or a historic tributary leading into Taylor Creek) which is the only location standing water was found in the wetlands. Seasonal high water indicators used to set these elevations were primarily lichen lines and the moss collar lowest extent (where present) which generally corresponded to an elevation near the top of the creek/ditch bank. These lichen lines generally maintained a relationship to the cypress knees and also a slight inflection point on the cypress trunk. Individually, these indicators are not considered the strongest; however, cumulatively they appear to be consistent and reliable for establishing a wet season peak elevation.

The cypress trees within most of the wetlands exhibit alteration to varying degrees. Cypress roots are exposed at numerous trunk bases and there is multiple inflection points present on the cypress. The USDA Soil Survey mentions that soil oxidation and subsidence can be observed in the onsite soils when water level controls are installed. Soil subsidence occurs throughout the wetlands, indicated prolonged muck exposure to oxygen, uncharacteristic for the system prior to anthropogenic manipulation.

Identifier	Elevation (ft)
Wetland 1	
SHWL 1-1	13.30
SHWL 1-2	12.96
SHWL 1-3	13.54
Wetland 2	
SHWL 2-1	14.48
SHWL 2-2	14.05
SHWL 2-3	14.52
Wetland 3	





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SHWL 3-1	15.98
SHWL 3-2	16.66
SHWL 3-3	16.91
Wetland 4	
SHWL 4-1	14.30
SHWL 4-2	14.03
SHWL 4-3	14.46
Wetland 5	
SHWL 5-1	19.55
SHWL 5-2	19.20
SHWL 5-3	19.14
Wetland 6	
SHWL 6-1	22.34
SHWL 6-2	22.38
SHWL 6-3	21.95

6410 Freshwater Marsh - 2 acres

This wetland type is present in a flatwoods depression in the northern section of the property and along the southern boundary where agricultural activities have altered drainage and this area is a low pasture. Freshwater marshes are described by the Florida Natural Areas Inventory (FNAI) as "having the outer, or driest, zone often occupied by sparse herbaceous vegetation consisting of longleaf threeawn (Aristida palustris), beaksedges (Rhynchospora microcarpa, R. cephalantha, R. tracyi, R. filifolia, etc.), Elliott's yellow-eyed grass (Xyris elliottii), the subshrub, myrtleleaf St. John's wort (Hypericum myrtifolium), and patches of blue maidencane (Amphicarpum muhlenbergianum) or sand cordgrass (Spartina bakeri). This sparse zone may be followed downslope by a sparse to dense zone of peelbark St. John's wort (Hypericum fasciculatum), water toothleaf (Stillingia aquatica) and scattered herbs, such as fringed yellow-eyed grass (Xuris fimbriata), pipeworts (Eriocaulon compressum and E. decangulare), narrowfruit horned beaksedge (Rhynchospora inundata), and Baldwin's spikerush (Eleocharis baldwinii). The innermost, deepest zone is occupied by maidencane (Panicum hemitomon), pickerelweed (Pontederia cordata), bulltongue arrowhead (Sagittaria lancifolia), or sawgrass (Cladium jamaicense). Floating-leaved plants, such as white waterlily (Nymphaea odorata), may be found in open water portions of the marsh."

FISH, WILDLIFE, LISTED SPECIES AND THEIR HABITAT

Data collection consisted of a literature review of existing sources for information useful in identifying the occurrence or potential occurrence of wildlife species listed as T, E or SSC (collectively recognized as listed species), as defined by the United States Fish and Wildlife Service (USFWS) and/or the Florida Fish and Wildlife Conservation Commission (FWC). In addition, the presence of designated critical habitat and/or vegetative communities and land uses with the potential to support listed species was evaluated. The literature review included, but was not limited to, the following sources: Natural Resources Conservation Service (f/k/a Soil Conservation Service [SCS]) Soil Survey of Okeechobee County, Florida, U.S. Geological Survey Topographic Quadrangle Maps, FWC Bald Eagle and Waterbird Colony databases, previous studies available, and false-color infrared and true color aerial photography of the project corridor.

Following the initial assessment, limited pedestrian and vehicular transects were conducted throughout all habitat types to determine the presence of protected wildlife species (**Tables 1 - Listed Species Occurrence in Okeechobee County, Florida**). Special attention was given to the following species: Everglades snail kite (*Rostrhamus sociabilis plumbeus*), crested caracara, gopher tortoise (*Gopherus polyphemus*) (T), sandhill crane (*Grus Canadensis pratensis*), Sherman's fox squirrel (*Sciurus niger*)





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shermani), wood stork (**Mycteria americana**) and bald eagle (**Haliaeetus leucocephalus**), recently delisted by FWC and FWS due to recovery, though all appropriate species were considered.

The potential occurrence of listed species to be identified within the proposed project is based on the vegetative communities present, as well as, surrounding land uses.

Everglades Snail Kite

The Everglades snail kite (*Rostrhamus sociabilis plumbeus*) is listed as endangered by the USFWS. The project corridor falls within the USFWS CA for the species. The nearest Everglades snail kite observation occurred 3 miles south of the project area on Lake Okeechobee. Very small areas of suboptimal habitat (ditches) exist within the project limits. No evidence of the Everglades snail kite was detected during field surveys, no historic sightings of this species were documented near the project area, and suitable habitat is limited.

Audubon's Crested Caracara

The Audubon's crested caracara (*Caracara cheriway*) is listed as threatened by the USFWS. In Florida, the caracara historically occupied native dry prairies with some wet areas and scattered cabbage palms (*Sabal palmetto*), but fire suppression has caused widespread conversion of prairies to open brushland. Currently, the majority of Florida's caracara population inhabits large cattle ranches with improved pastures and scattered cabbage palms. Caracaras also occur in some improved pasturelands and even in lightly wooded areas with limited stretches of open grassland. Within these habitats, caracaras exhibit a propensity for nesting in cabbage palms, followed by live oaks (*Quercus virginiana*).

The entire project is located within the CA for the Audubon's crested caracara. The surrounding land use consists of agriculture and since cabbage palms also exist within the upland hardwoods within the project limits, caracara habitat is classified as optimal. During the two field visits, no individuals were observed flying overhead, foraging or perching in the project area. The USFWS caracara survey protocol should be undertaken to determine presence or absence of the species on site.

Indigo Snake

The eastern indigo snake is listed by the USFWS as threatened. The species inhabits a wide variety of habitats present within the project, including pine flatwoods, hardwood forests, as well as wet and dry prairies. The nearest recorded eastern indigo snake observation was approximately 5 miles to the southeast of the project in 2005. No individuals were observed during the two site visits.

Sherman's fox squirrel

The Sherman's fox squirrel (*Sciurus niger shermani*) is listed as an SSC by the FWC. The optimal habitat for this species includes pine forests which are limited within the project area and oak hammocks which are found throughout the project area. No Sherman's fox squirrels were observed during field surveys and no nests were identified. The nearest Sherman's fox squirrel observation, documented in 2011, occurred approximately 1 mile east of the project.

Gopher Tortoise

The gopher tortoise (*Gopherus polyphemus*) is listed as threatened by FWC. The gopher tortoise occurs in sandhill (pine-turkey oak associations), sand pine scrub, xeric hammock, pine flatwoods, dry prairie, coastal grasslands and dunes and mixed hardwood pine communities. These burrows are known to serve as refuge to many species, some of which are protected (eastern indigo snake, Florida mouse, gopher frog, and Florida pine snake).

Gopher tortoise burrows were identified in the project's uplands adjacent to the large canal on the project's northern end.

Florida Sandhilll Crane





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The Florida sandhill crane (*Grus canadensis pratensis*) is listed as threatened by FWC and is protected under the Federal Migratory Bird Treaty Act. The Florida sandhill crane is commonly found in wet prairies, marshy lake regions, low-lying pastures (including improved pastures), and shallow water open areas. Nesting occurs in marshy depressional ponds vegetated by pickerelweed, arrowhead, fireflag, maidencane, and other herbaceous vegetation.

There were no nests or species identified on the project site during the two inspections, although suitable freshwater marsh habitat and low pasture occurs on the site.

Wood Stork

The wood stork (*Mycteria americana*) is listed as endangered by FWS and FWC. This species is typically found in freshwater marshes, swamps, lagoons, ponds, flooded fields, depressions in marshes and brackish wetlands. The critical foraging areas for this species include areas of very shallow water, generally six (6) to ten (10) inches in depth, where there is an abundance of small fishes and other aquatic life.

The project does fall within the Wood Stork Core Foraging area for two (2) wood stork colonies: 616108 Wescott Grove Reservoir and 616047A Cypress Creek. During site reviews, wood storks were observed foraging within the shallow portions of Taylor Creek.

Bald Eagle

The Bald Eagle (Haliaeetus leucocephalus) was previously listed as Threatened by the FWC and is now provided species protection by the State. Bald eagles are generally associated with large bodies of water where their dietary requirements (fish) are readily available. Bald eagles in Florida have also been observed consuming various types of waterfowl, carrion, and occasionally mammals and snakes (Scott 2004). Bald eagles prefer to roost in conifers or other sheltered sites in winter, usually selecting large, more accessible trees.

Initial research of databases containing information from the Florida Fish and Wildlife Conservation Commission (FWC), the U.S. Fish and Wildlife Service (FWS), and other agencies identifies that the project corridor is located near bald eagle habitat. The 2012 FWC database of known bald eagle nest sites identified two documented nest sites within a one (1) mile radius of the project, OK028 is located within the project and was active during the last survey period and OK022 which was last active in 2003.

Federal and state guidelines for the bald eagle require that certain activities may be conducted outside a 660-foot radius distance outward from a nest tree (FWS 2007). Per the 2007 FWS Bald Eagle Monitoring guidelines, monitoring of the active nest is required if construction activities are to take place within the 660-foot radius during the nesting season (October 1 – May 15).

FWC's 1999 Waterbird Colony Locator database of documented colonies was queried and yielded no documented occurrences within one (1) mile of the proposed project and is the only published data available to the public.

Other wildlife observed on-site includes the limpkin, little blue heron (SCC), mourning dove, anhinga, snowy egret (SSC), tri-colored heron (SSC), white ibis (SSC), cattle egret, turkey vulture, white tailed deer, red shouldered hawk, and armadillo.





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Mr. Seidel, we thank you for the opportunity of providing our services. Dewberry | Bowyer Singleton looks forward to working with you in the near future. Should you have any questions or require additional information, please contact our office at 321.354.9640.

Sincerely,

Matthew P. Miller, P.W.S. Environmental Scientist Dewberry | Bowyer-Singleton

MPM SR710/Env Enclosures

c: Alexis Preisser



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Table 1 <u>Listed Species Occurrence-Okeechobee County, Florida</u>

Table 1: Summary table of those federal and state listed species known to be present in Okeechobee County, Florida as documented by the FWS and FWC and their potential for occurrence within the SR 710 STA project area.

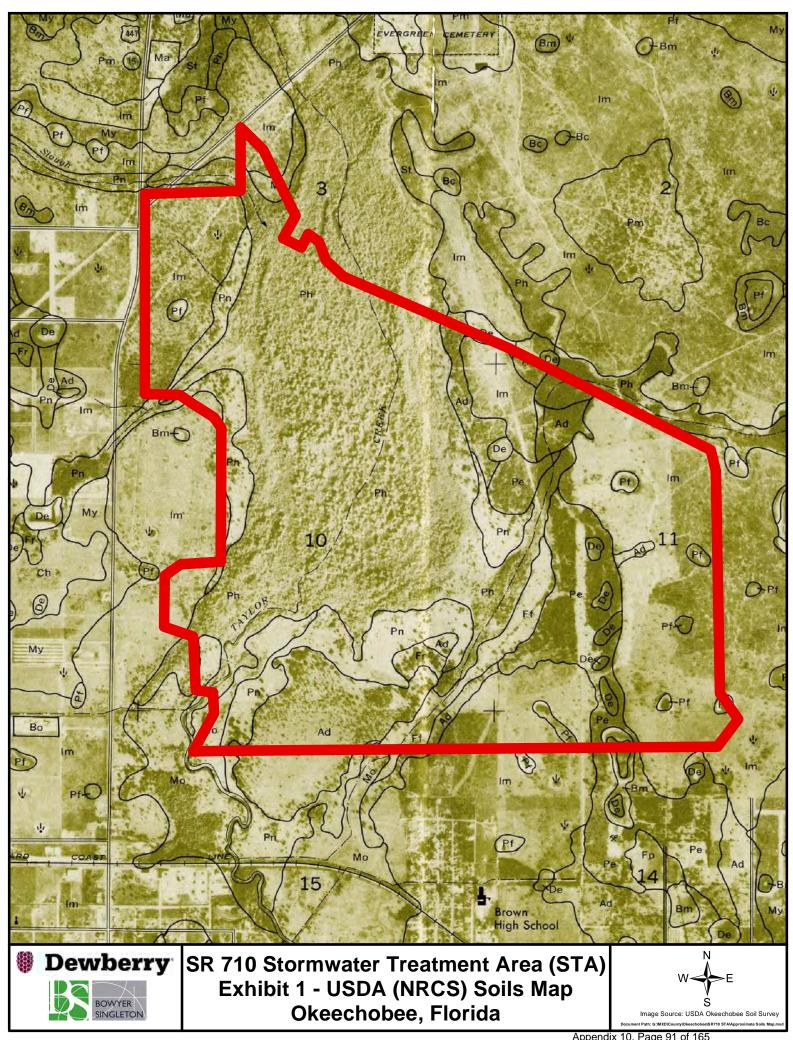
Code Key: E = Endangered, T = Threatened, P = Proposed, SSC = Species of Special Concern S/A = Similar in Appearance

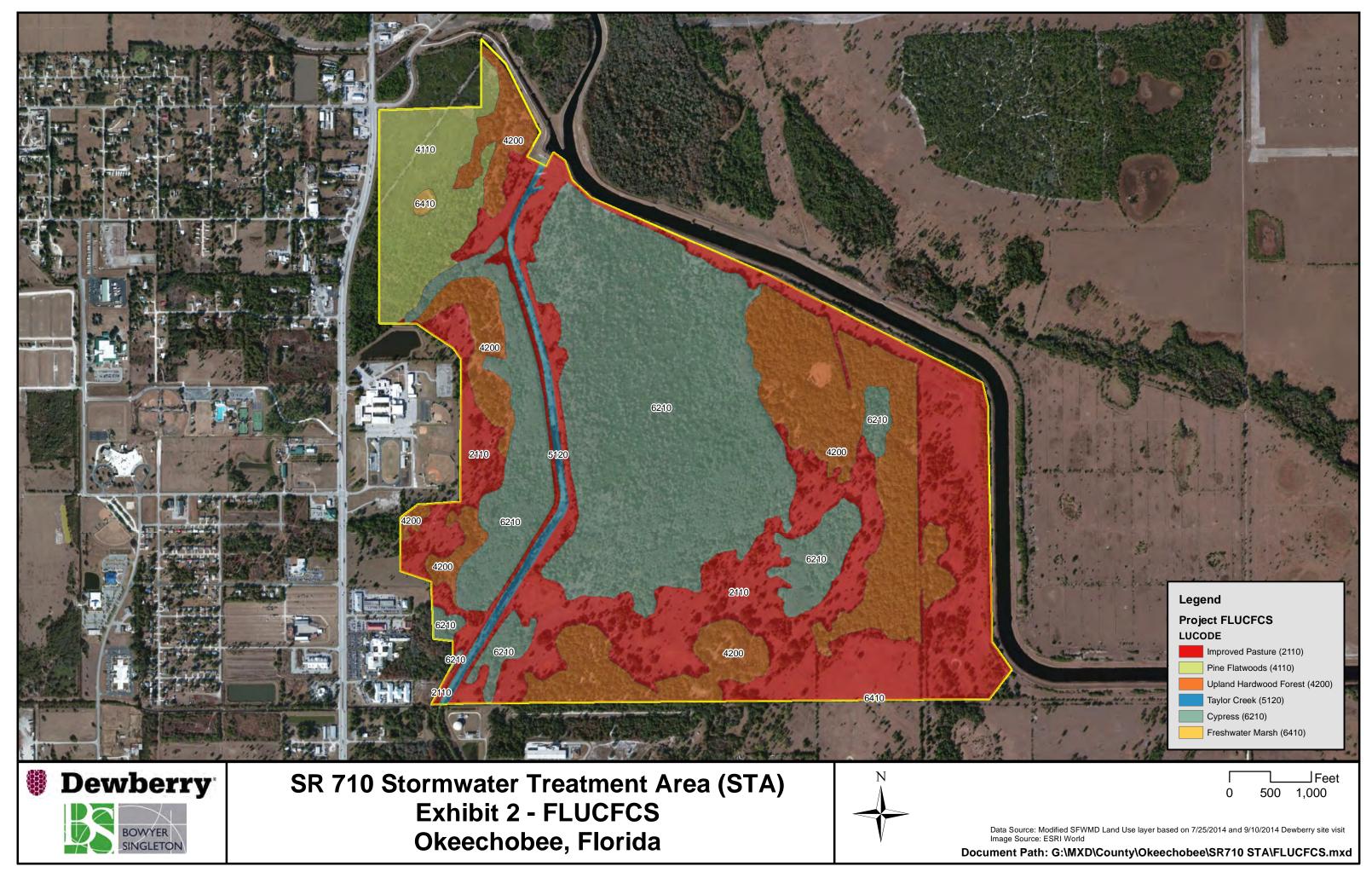
		FWS	FWC	Occurrence
Scientific Name	Common Name	Status	Status	Potential
Amphibians				
Rana capito	gopher frog	N/A	SSC	Low
Reptiles				
Alligator mississippiensis	American alligator	T(S/A)	SSC	Observed
Drymarchon corais couperi	eastern indigo snake	N/A	Т	Moderate
Gopherus polyphemus	gopher tortoise	N/A	SSC	Moderate
Birds				
Ammodramus savannarum floridanus	Florida grasshopper sparrow	Ε	Ε	Low
Aramus guarauna	limpkin	N/A	SSC	Moderate
Aphelocoma coerulescens	Florida scrub-jay	Т	Т	Low
Athene cunicularia floridana	Florida burrowing owl	N/A	SSC	Low
Egretta caerulea	little blue heron	N/A	SSC	Observed
Egretta thula	snowy egret	N/A	SSC	Observed
Egretta tricolor	tricolored heron	N/A	SSC	Moderate
Eudocimus albus	white ibis	N/A	SSC	Observed
Falco sparverius paulus	southeastern American kestrel	N/A	Τ	Low
Grus canadensis pratensis	Florida sandhill crane	N/A	Τ	Low
Haliaeetus leucocephalus	bald eagle	Т	Т	Observed
Mycteria americana	wood stork	Ε	Ε	Observed
Pandion haliaetus	osprey	N/A	SSC	Low
Rostrhamus sociabillis plumbeus	Snail Kite	Ε	Ε	Low
Sterna antillarum	least tern	N/A	Т	Low
Mammals				
Eumops floridanus	Florida bonneted bat	Ε	Ε	Low
Sciurus niger shermani	Sherman's fox squirrel	N/A	SSC	Moderate

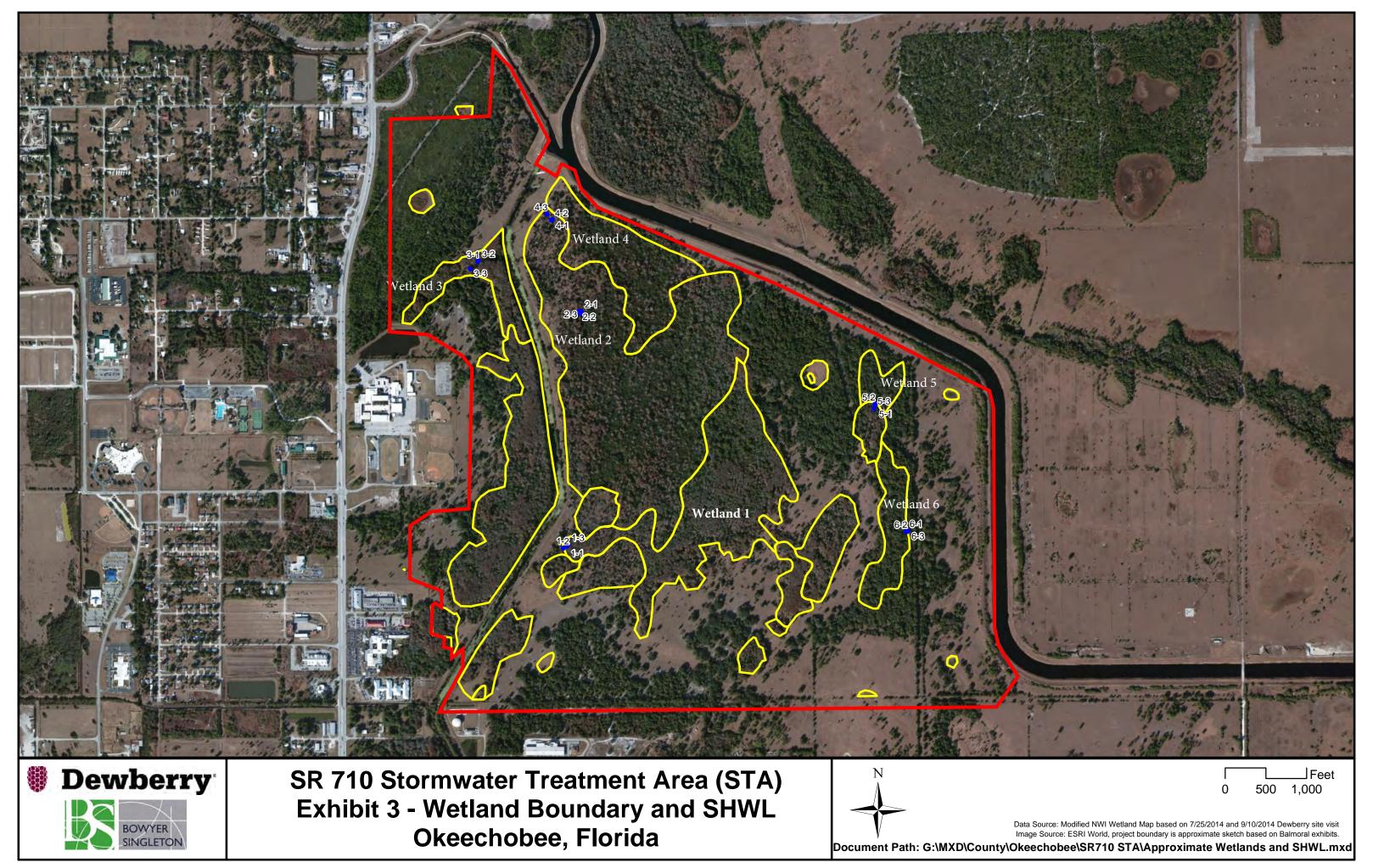
Data Source: URL: http://southeast.fws.gov/es/county%20lists.htm. Last modified on August 7, 2000 and URL: http://floridaconservation.org/pubs/endanger.html and Florida Natural Areas Inventory (FNAI). Occurrence Potential represents the likelihood of that particular species to be found within the project area. Occurrence Potential = Observed, High, Medium and Low.















Photograph 1. Wetland 1 facing North



Photograph 2. Wetland 1 facing East



Photograph 3. Wetland 1 facing South



Photograph 4. Wetland 1 facing West



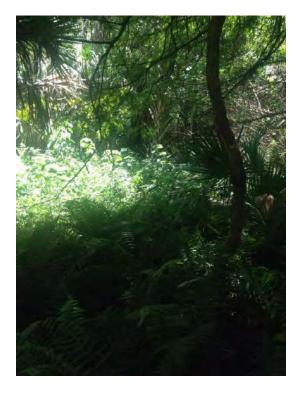
Photograph 5. Wetland 2 facing North



Photograph 6. Wetland 2 facing East



Photograph 7. Wetland 2 facing South



Photograph 8. Wetland 2 facing West



Photograph 9. Wetland 3 facing North



Photograph 10. Wetland 3 facing East



Photograph 11. Wetland 3 facing South



Photograph 12. Wetland 3 facing West



Photograph 13. Wetland 4 facing North



Photograph 14. Wetland 4 facing East



Photograph 15. Wetland 4 facing West



Photograph 16. Wetland 4 facing West



Photograph 17. Wetland 5 facing North



Photograph 18. Wetland 5 facing East



Photograph 19. Wetland 5 facing South



Photograph 20. Wetland 5 facing West



Photograph 21. Wetland 6 facing North



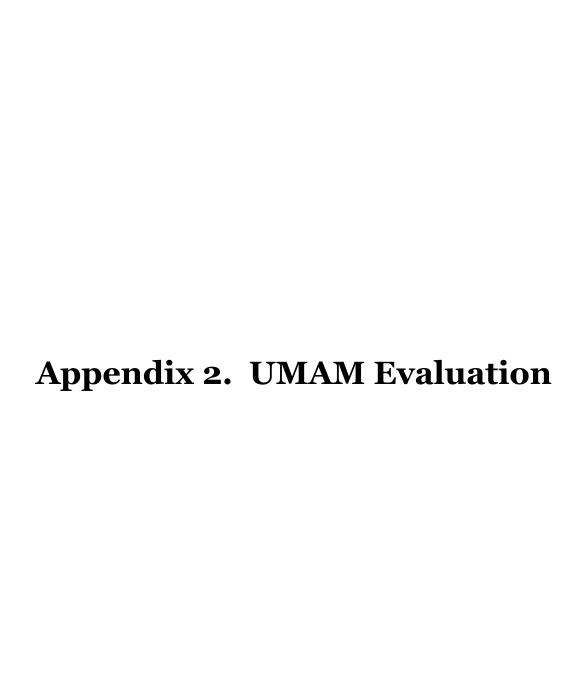
Photograph 22. Wetland 6 facing East



Photograph 23. Wetland 6 facing South



Photograph 24. Wetland 6 facing West



PART I – Qualitative Description (See Section 62-345.400, F.A.C.)

Site/Project Name			Application Numbe	er		Assessment Area Name	or Number
State Road 71	10					Сур	press
FLUCCs code		Further classification	tion (optional)		Impac	et or Mitigation Site?	Assessment Area Size
621 - Cypress						Mitigation	338 acres
Basin/Watershed Name/Number	Affect	ted Waterbody (Clas	ss)	Special Classificati	on (i.e.C	OFW, AP, other local/state/federa	I designation of importance)
Lake Okeechobee						OFW	
Geographic relationship to and hyd	rologi	c connection with	wetlands, other su	urface water, uplai	nds		
The cypress wetlands onsite are h	ydrolo	ogically connected	to the Taylor Cre- in the agricultura		both g	roundwater flow and su	rface water connection
Assessment area description The wetland types are similar an (Magnolia virginiana), red bay (Pe and a mixture of cabbage palm broomsedge (Androp	ersea n. Gro	palustris) and wate oundcover includes	er oak (Quercus r s wild coffee, cabl	nigra) with a subca bage palm, grape\	nopy o	dominated in some area	as by Brazilian pepper berry (Rubus spp.),
Significant nearby features				Uniqueness (co landscape.)	nsider	ing the relative rarity in	relation to the regional
Taylor Creek Canal, Lake Okeechobee, Okeechobee County Airport				The relative we		size in close proximity that is a close this wetland uniqu	
Functions				Mitigation for pre	vious _l	permit/other historic use	9
providing cover, substrate, and refuge; breeding, nesting, denning, and nursery areas; corridors for wildlife movement; food chain support; and natural water storage, natural flow attenuation, and water quality improvement, which enhances fish, wildlife, and listed species utilization						None	
Anticipated Wildlife Utilization Based on Literature Review (List of species that are representative of the assessment area and reasonably expected to be found)			(List of species		T, SS	by Listed Species (List s C), type of use, and inte	
Cypress swamps provide important and Ewel 1998). They provide salamanders (Ambystoma cingulimportant roosting sites for wadir albus) and wood stork (Mycteria an limpkin, american alligator, little blisnowy egre	critica atum ng biro nerica ue he	al breeding habitat and Ambystoma b ds such as white ib ana). Other species	for flatwoods pishopi) and are pis (Eudocimus s may include the	Woodstork (E), heron (SSC), o	restec	n (SSC), american alligd d caracara (T), snowy e ron (SSC), white ibis (S	gret (SSC), tricolored
Observed Evidence of Wildlife Utiliz	zation	(List species dire	ctly observed, or o	other signs such a	s tracl	ks, droppings, casings,	nests, etc.):
Woodstork, Lim	pkin,	American Alligator	, Little Blue Heror	n, Snowy Egret, Ca	attle E	gret, Red Shouldered H	ławk
Additional relevant factors:							
The Cypress wetlands have been h	neavil	y impacted by agri	cultural drainage	and the creation o	f the T	aylor Creek canal for fl	ood control purposes.
Assessment conducted by:				Assessment date	(s):		
MPM				9.15.2014			

Form 62-345.900(1), F.A.C. [effective date 02-04-2004]

PART II – Quantification of Assessment Area (impact or mitigation) (See Sections 62-345.500 and .600, F.A.C.)

		(- ,			
Site/Project Name			Application Number		ea Name or Number		
	ate Road 7	10 - STA		Су	press Wetlands		
Impact or Mitigation			Assessment conducted by:	Assessment dat	te:		
	Enhance	ment	MPM		9.15.2014		
Scoring Guidance		Optimal (10)	Moderate(7)	Minimal (4)	Not Present (0)		
The scoring of each indicator is based on whould be suitable for the type of wetland or surfawater assessed	ne	Condition is optimal and fully supports wetland/surface water functions	Condition is less than optimal, but sufficient to maintain most wetland/surface waterfunctions	Minimal level of support of wetland/surface water functions	Condition is insufficient to provide wetland/surface water functions		
.500(6)(a) Location Landscape Supp		The "Loca	ition" score will not be impacte	ed or enhanced with the proje	ect design.		
w/o pres or current	with						
5	5						
.500(6)(b)Water Envi (n/a for upland: w/o pres or current		ditch within the wetland or was found in the wetlands. and the moss collar lowest e creek/ditch bank. These I inflection point on the cyp cumulatively they ap The cypress trees within monumerous trunk bases and design these wetlands may due to the low control elevation.	tions set within wetlands 1, 3 a a historic tributary leading into Seasonal high water indicator extent (where present) which g ichen lines generally maintaine ress trunk. Individually, these pear to be consistent and relia ost of the wetlands exhibit alter d there is multiple inflection po y receive a lift from either increation from nearby drainage dit	Taylor Creek) which is the case used to set these elevation generally corresponded to an ed a relationship to the cypres indicators are not considereable for establishing a wet se ration to varying degrees. Coints present on the cypresseased surface water input, deches, or a combonation of the	only location standing water as were primarily lichen lines elevation near the top of the less knees and also a slight did the strongest; however, ason peak elevation. The property of the system ecreased groundwater loss e two restoration methods.		
.500(6)(c)Community	structure	heterogenous mixture of swe	The wetland types are similar and contain a mature canopy of bald cypress (Taxodium ascendens), with a terogenous mixture of sweet bay (Magnolia virginiana), red bay (Persea palustris) and water oak (Quercus nigra with a subcanopy dominated in some areas by Brazilian pepper and a mixture of cabbage palm.				
Vegetation an Enthic Comm w/o pres or current		broomsedge (Andropogoi cernuus). The wetlan outcompeting native wetla obtained in community struct sufficient to terminate upla levels may only need to	oundcover includes wild coffee, cabbage palm, grapevine (Vitis spp.), smilax, blackberry (Rubus spp.), insedge (Andropogon virginicus), chain fern (Woodwardia virginica), air potato, and lizards tail (Saururus ernuus). The wetland edges are particularly invaded by upland and invasive vegetation, presumably impeting native wetland vegetation due to the change in hydrologic conditions. Functional gains may be in community structure, if the design allows water to rehydrate the system to the edges for a period of time ent to terminate upland vegetation. Hydrologic indicators such as historic inflection points suggest water less may only need to acheive the historic seasonal high for a duration of 2-3% of the year (Carr 2006, MPARISON OF SIX BIOLOGIC INDICATORS OF HYDROLOGY AND THE LANDWARD EXTENT OF				
5	7	HYDRIC	SOILS IN WEST-CENTRAL I	FLORIDA, USA CYPRESS [OOMES).		
		,					
Score = sum of above sco uplands, divide by	,	If preservation as mitig	ation,	For impact asses	ssment areas		
current	-,	Preservation adjustme	nt factor =	El - dolto y coros			
or w/o pres	with	Adjusted mitigation del	ta =	FL = delta x acres =			
0.5	0.63	<u> </u>					
		If mitigation		Formition	agament grass		
Delta = [with-curr	rent]	Time lag (t-factor) = 1.	14	For mitigation ass	essment areas		
0.13		Risk factor = 1.5		RFG = delta/(t-factor x	x risk) = 0.076		

Form 62-345.900(2), F.A.C. [effective date 02-04-2004]

Appendix E: Correspondence

SR 710 Stormwater Treatment Area/Regional Pond Feasibility Study Final Submittal

Financial Project ID 432644-1-32-01

Okeechobee County, Florida



MEETING MINUTES &

SRb710bPossiblebRegionalbPondbBrainstormingbMeetingb SRb710bfrombUSb441btobthebb63-NbCanalb FPIDbNo.b419344-3-52-01b

b

Septembers13, 2013, s11:00 sam; sGoToMeetingss

Attendees:s

Lesley&ertolottis-SFWMD,&rincipal&cientists

KevinsCarters-SFWMD,sLeadsScientists

KellysCranfords-sFWMD, Permittingsections Leaders

OrlandosDiazs-SFWMD, Sr. Environmental Scientists

EricsGonzalezs-SFWMD, ProjectsManager Principals

SusansMartins-SFWMD.SeniorSpecialistsAttornevs

JohnsMorgans-SFWMD, Lead Policy Analysts

Gary Ritters-SFWMD, Intergovernmental & Outreach Representatives

SteveSentess-SFWMD, Regulatory Professional Leads

TonysWaterhouses-SFWMD, Assistant Executive Director, Regulations

MistysAldermans-sFDEP,sNonpointsSourcesManagements

ElizabethsAlvis-sFDEP,sEnvsConsultants

KensKuhls-sFDEP, sEnvsConsultants

TrinasVielhauers-&FDEP, &nv. &Assessment and &Restorations

BonniesWolffsPelaezs-sFDACS, sEnvsSpecialists

BrentSetchells-&DOT, Permittings

Carlspirios-sFDOT, sDrainages

AmySetchells-FDOTs-ProjectsManagers

BriansKirwanss-sThesWantmansGroup, \$PMs sDesigns

AlfredosRodriguezs-sThesWantmansGroup, Roadways

GregsGriffiths-sThesWantmansGroup, Permittings

GregsSeidels-sThesBalmoralsGroup,sDrainages

JennifersNunns-sThesBalmoralsGroup,sDrainages

TimsDesmarais—sThesBalmoralsGroup,sDrainages

Purpose:ssThespurposesofsthesmeetingswasstospresentsthesSRs710sprojectsandspossibles regionals ponds opportunitys tos thes SFWMDs ands FDEP, s brainstorms ons ideas, s discusss feasibilityandadevelopagoforwardatrategy. Beloware highlights of the meetings a

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- 1. GregsSeidelsbegansthesmeetingswithsintroductions.ssParticipantssannounceds whos theys represents ands whats roles theys woulds presumablys plays ins thiss concept.sss
 - a) FDOTs –s regionals ponds approachs has costs savings benefits and iss ins alignmentswithsBMAPseffortss
 - b) SFWMDs-spermittingsandsalsosinvolvedsinsBMAPsprocesss
 - c) FDEPs-sBMAPscoordinators
 - d) FDACSs-slandswinersofthespotentialsitesenrolledsinthesBMPsprograms

Mr. Seidelsaddedsthatshesissthesdrainagesengineersofs ecordsforsthes Rs710 snews alignments projects from s USs441 stos Easts of sthes L-63 Ns Canal.ss Asssuch, she siss responsibles for sdevelopings the sstormwaters managements plans for sthe sprojects and shass been saked to evaluate segional sopportunities by the FDOT.s

S

Brents Setchells stated sthes FDOTs positions of slookings for sbetters way sstoss pends stormwaters managements dollars \$thats would \$provides more \$treatment\$ than \$justs the sroad ways and shelps reduces costs stos the sFDOTs whiles providings as betters "product" \$to \$the \$public.s

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S

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3. Mr.s Seidels begans thes brainstormings sessions withs ans overviews ofs thes proposeds roads alignments ands overviews ofs thes local/regionals hydrology.s (Pleaseseesttachedexhibitssfromshesmeetingsgenda)s

S

- a) WaterslevelssgovernedsbysoperationsofsS-133sandsS-191.ssTaylorsCreeksiss pumpedsintosLakesOkeechobee.ssThisspumpsstationswassnotsdesignedstos pumpsbothsways.s
- b) MostsofsthesrunoffsinsTaylorsCreeksissfromsurbanizedsareas.ssFlowssfromsthes largesagriculturalsareasstosthesnorthsbypasssTaylorsCreeksandsflowsarounds thescitysviasthesL-63sCanal.ssMuchsofsthesag-basedsrunoffsisstreatedsviasans existingSFWMDStormwatersTreatmentsareastosthesnorth.s
- c) Discussedsongoingstormwatersimprovementsandsneedsinsthearea:s
 - i. OaksParks-sreconstructedsswaless
 - ii. SWs32ndsAvesditchs
 - iii. TMDL-relatedsmprovementss
 - iv. E-Wsconveyancesprojects
 - v. MiscellaneoussetrofitssforsdirectsconnectionsstosTaylorsCreeks
- d) OnesoptionsisstosreversesthestypicalsflowswatersinsTaylorsCreek,sroutsits throughsthesproposedsregionalsfacilitysforstreatment,sandsdischargingsbacks tosTaylorsCreeks(orspossiblysL-63N).ssRoutingswatersnorthwardsintosL-63Ns mayscreatesasproblemswithssepticstankssinsthessouth,swhichshavesreporteds toshavesissuesswheneverstheswatersreachess13.8'.s
- e) AnotherssuggestionswasstosroutessomesofstheswatersflowingsinsL-63Nsintos thesproposedsegionalsfacilitysforstreatmentsandsreleasesisbackstost-63N.sss
- f) The dandowners shave sbeen scontacted sabout sthe so adways project.s

S

4. ItswasssuggestedstoscontactsUSACEsaboutsthissconcept,sasstheysmayshaves interestssfromsaspermittingsperspectivesandspossiblescost-sharing.ssltswass agreedsosthisatadatersdatesfollowinganadditionalscoordinationsmeeting.s

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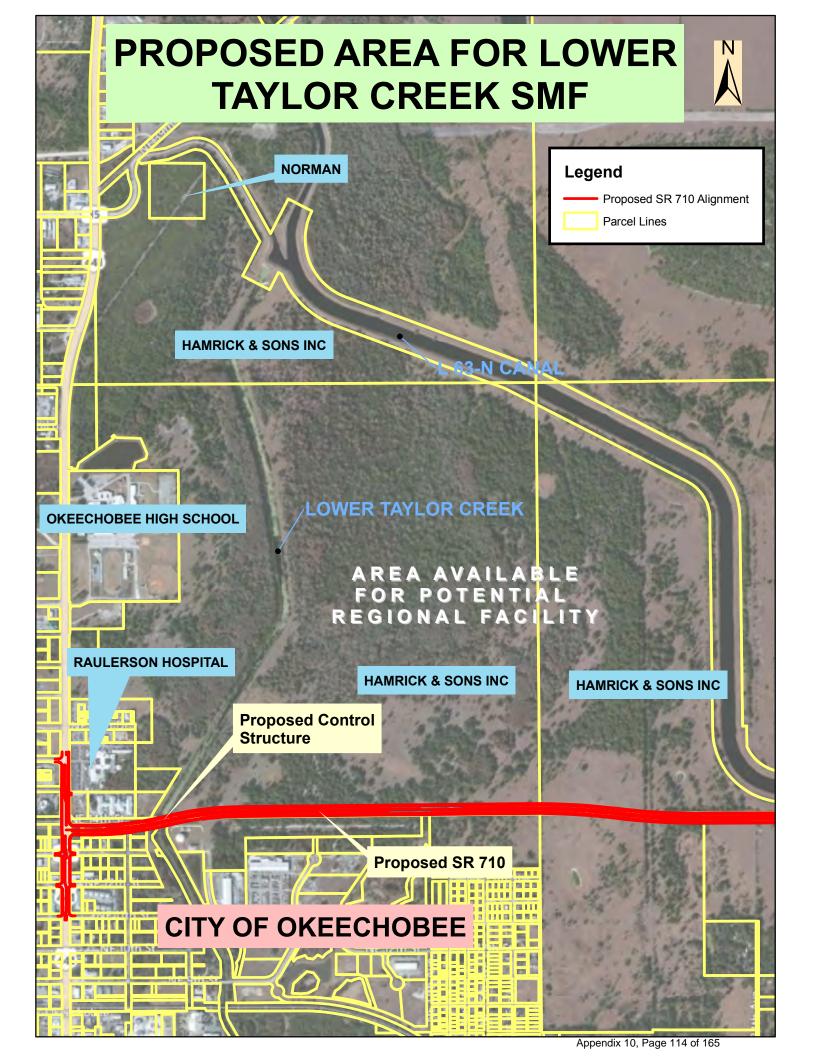
- 5. WatersQualitysdatasonsTaylorsCreek,sL-63N,sandsLakesOkeechobeeswouldsbes helpfuls ins determinings hows tos maximizes thes potentials benefits froms thiss concept.s
- 6. Its was snoted sthats Taylors Creeks used stoshaves as sands bottoms and siss nows covereds with sorganics silts and smuck.ss Thes southerns portions of sthesbasins contains shomes son septic stank.s
- 7. The smeeting sendeds with sansagreements to srevisits and solic uss smore sins details when sthesd rafts Ponds Sitings Reports is scompleted swhich swills be sins November. so Atsthis stime, sthes FDOTs will sknow smore sabout sponds izes, slocations sand scosts. so Thes FDOTs will scontact sthe sparticipants stoss chedules the smeeting sats as laters date. s

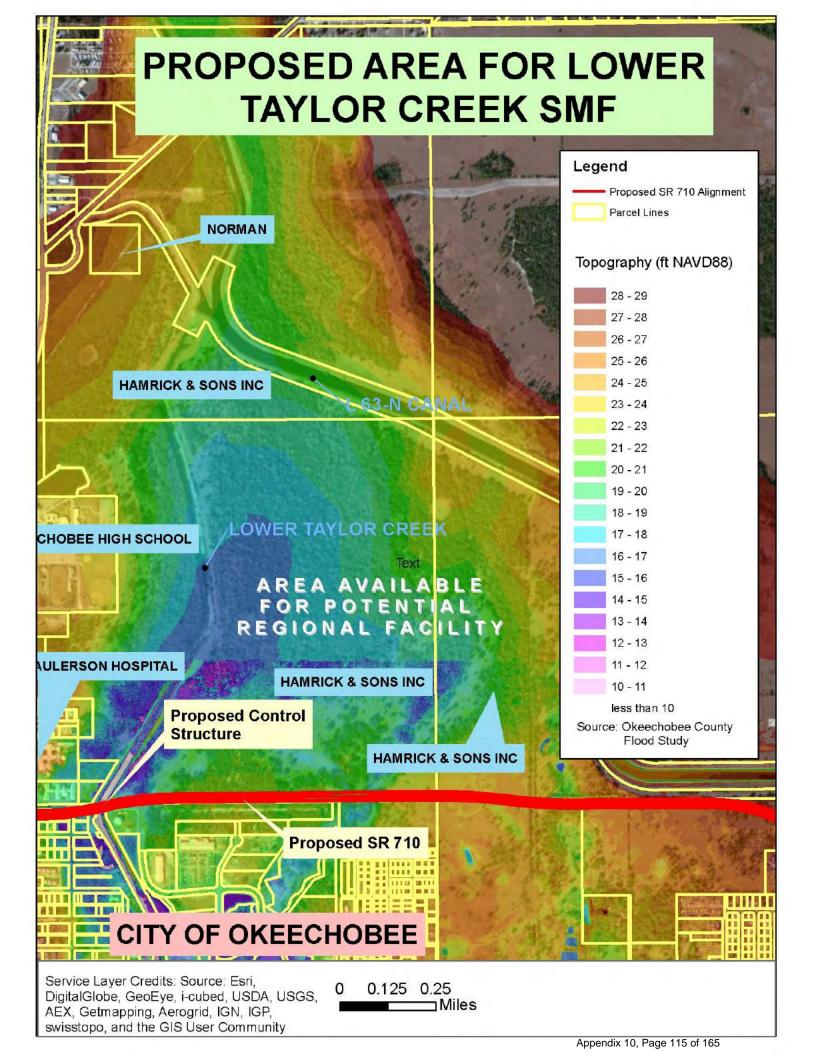
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Memo

To: Gregory Seidel, P.E.

From: Lori Stanfill, P.E.

CC:

Date: September 11, 2013

Re: SR 710 - Pump Information for Taylor Creek (Structures S-192 & S-133)

According to the System Operation Manual for Lake Okeechobee, Structure S-192 is located at the junction of L-63N Canal and Taylor Creek (North of the City of Okeechobee). This structure is a single 48" culvert with a gate and a pump. When the gate is open, it allows passage of water from L-63N to Taylor Creek (gravity flow), however, the gate is typically closed. The structure also permits back pumping from Taylor Creek to L-63N (See References).

The purpose of S-192 is to prevent stagnation in the lower reaches of Taylor Creek. The S-192 gate is normally closed, except for the following reasons: 1) Maintenance purposes, where it is needed to divert flows from L-63N Canal; 2) When the water quality in Taylor Creek is degraded (i.e. by discharge of the sewage treatment plant) and Lake Okeechobee is sufficiently low to allow gravity flow to the south into the lake (below elevation 14.0 ft, NGVD).

Similarly, the S-192 pump is only activated when the water quality in lower Taylor Creek is degraded (i.e. from discharge from the sewage treatment plant), and Lake Okeechobee is too high to allow flow into the lake (above elevation 14.0 ft, NGVD). When this occurs, structure S-193 (located at south end of Taylor Creek, at entry into Lake Okeechobee) is also open to discharge the same flow into Taylor Creek from Lake Okeechobee as is being pumped out to the north (into L-63N Canal).

S-192 is not designed to pass flood flows. Flood flows are routed to Lake Okeechobee via L-63N Canal, L-59 Canal, and structure S-191 (See Reference).

Stage and discharge Information for S-192 was obtained from the SFWMD website, and is shown below:

Location	Stage (ft NGVD)	Discharge	Date
S-192		Unavailable	11-15-2012
S-192 (US at L-63N)	19.42		3-12-2013
S-192 (DS at Taylor	13.67		3-12-2013
Creek)			

There is daily information for the stages and structures on Lake Okeechobee which can be accessed from the Army Corps of Engineers website (See References & Attachments). Structure S-133 is located at the southernmost end of Taylor Creek where it drains into Lake Okeechobee (at northeast bank of lake).

Structure S-133 includes 5 pumping units with a combined capacity of 625 cfs (or greater). It is designed to remove ¾ inch per day of runoff from the 16,190 acre drainage area. There are five – 48 inch steel pipes which convey pumped discharge into Lake Okeechobee. There are slidegates on the intake end (Taylor Creek side) and flapgates on the discharge end (Lake Okeechobee side).

Structure S-193 (mentioned above) is located 1200' to the east of S-133. It is a lock which can be opened to pass flows to the north or south depending on the stage in Lake Okeechobee (See Reference).

Information for the abovementioned structures can be obtained on the SFWMD website (See References). Stage and discharge Information for S-133 and S-193 was obtained from the SFWMD website, and is shown below:

Location	Stage (ft NGVD)	Discharge (cfs)	Date
S-133		282*	9-11-2013
S-133 (US at Taylor Creek)	13.67		9-11-2013
S-133 (DS at Lk. Okeechobee)	15.23		9-11-2013

Note: 2 pumps @ 1178.79 rpm discharging on 9-11-2013

According to the Army Corps of Engineers website, the pumps from Lake Okeechobee to the Caloosahatchee River were turned on in Feb. 2013, but turned off in late Aug. 2013 as the water level was sufficiently reduced and within the range the Corps likes to maintain. On September 10, 2013, the stage in Lake Okeechobee is 15.46 feet NGVD. The Corps acceptable range (Operational Management Band) for which no pumping is necessary is between 12.59 feet NGVD to 16.48 feet NGVD. The stage on the upstream side (Taylor Creek) of S-133 was 13.46 feet NGVD on Sept. 10, 2013. See attached chart for Lake Okeechobee stage information from January 2012 to September 2013 and Lake Okeechobee Vicinity Report.

References:

- Central and Southern Florida Project for Flood Control and Other Purposes
 <u>System Operating Manual, Lake Okeechobee & EAA Vol. 3, Version 1 Draft</u>
 <u>4</u>. Dept. of the Army Corps of Engineers, Jacksonville District, December 2005.
- 2. http://w3.saj.usace.army.mil/h2o/plots.htm. Army Corps of Engineers Website.
- 3. http://www.sfwmd.gov/portal/pls/portal/realtime.pkg rr.proc rr?p op=OKEECH

 OBEE&p wcs name=TAYLOR CK 1. SFWMD Website.

FIELD STATION AREAS OF RESPONSIBILITY

C0C03

CORK2 CORK3

CR31N CR31S CR951_ CR951_.

CYPRESS1

C18 C37WEIR

G208 G211 G212 G248A-D G249A-H G250S G251 G252H-J G254A-A1 G254B-B1 G254C-C1 G254D-D1

G304A-G305A-\ G306A-G307

G310 G311 G327A-C G328 G329A-E G330A-E G331A-C

G333A-E G334

G335 G336A-F G336G

G337 G337A

G367A-F G368 G370 G370S G371 G372 G372S G372HL G373 G375A-F

LUCKY_LA MERRI TT1

S59WEIF S60

S62 S63 S63A S65 S65A S65AX S65C S65CX S65CX

S65DX1

S65DX2

S65EW

S67X

S77

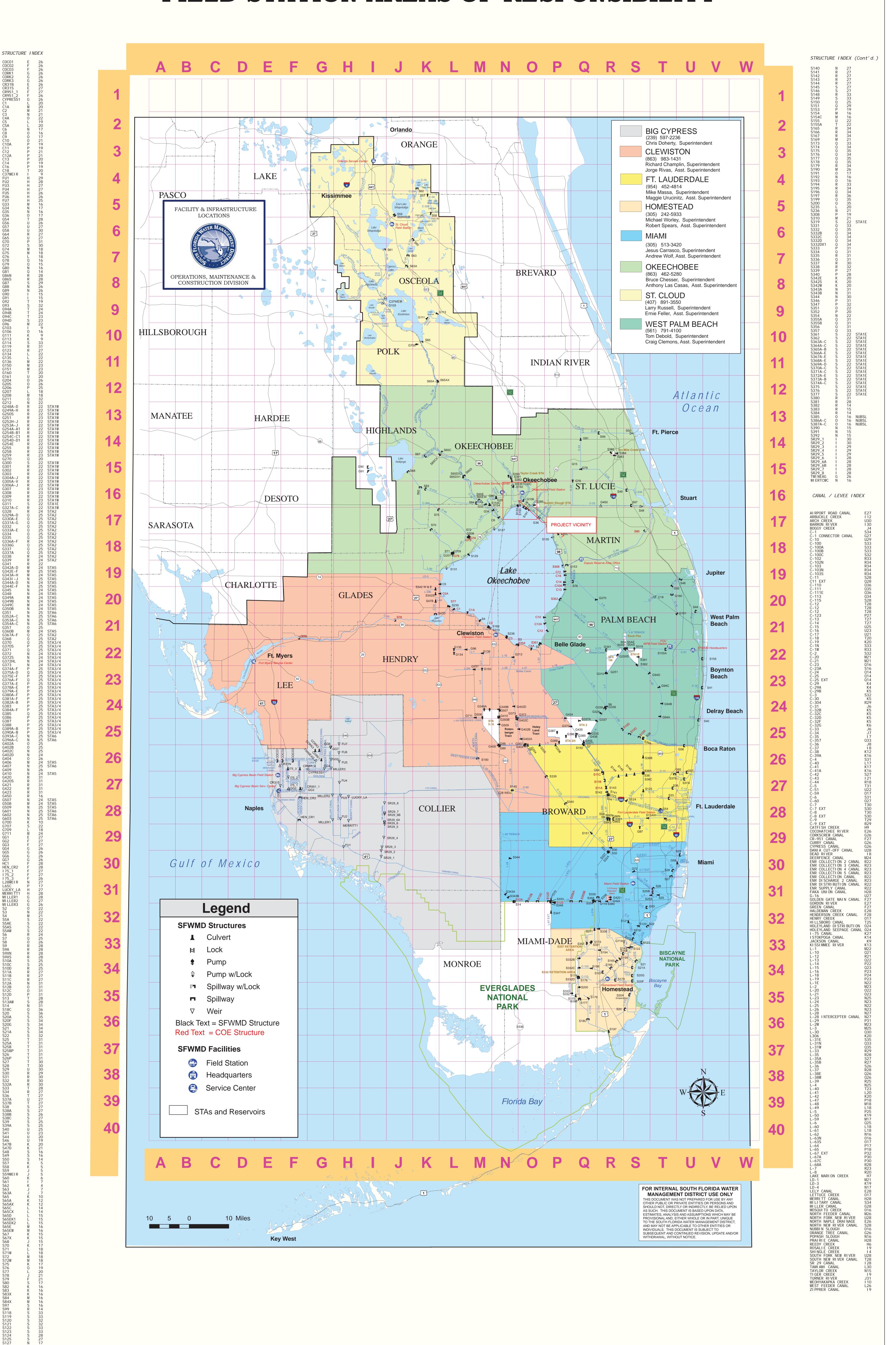
S78

S84 S84X

S123

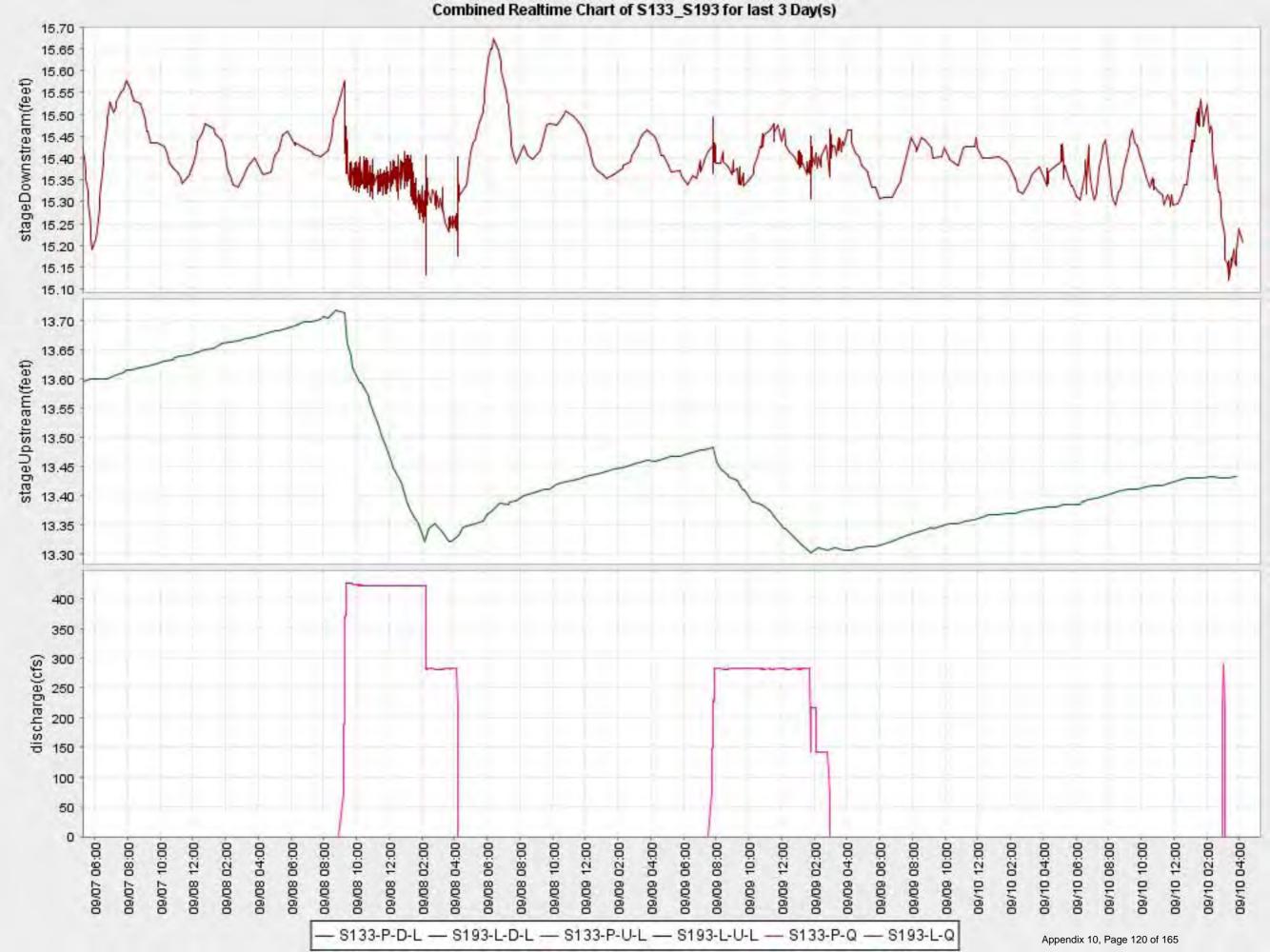
S133 S135 19 16

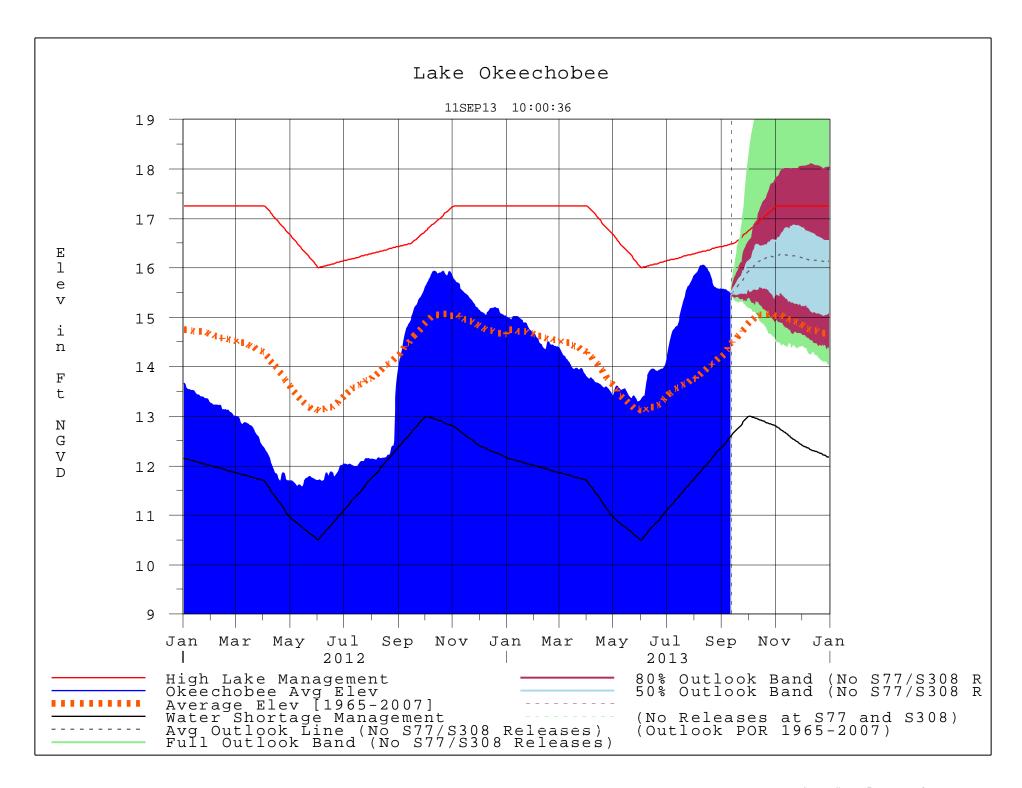
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Appendix 10, Page 119 of 165

05/07/2013





U. S. Army Corps of Engineers, Jacksonville District Lake Okeechobee and Vicinity Report ** Preliminary Data - Subject to Revision **

Data Ending 2400 hours 10 SEP 2013

```
Okeechobee Lake Regulation
                               Elevation Last Year 2YRS Ago
                                (ft-NGVD) (ft-NGVD) (ft-NGVD)
  *Okeechobee Lake Elevation
                                   15.46
                                             14.81 10.86 (Official Elv)
  Bottom of High Lake Mngmt= 16.48 Top of Water Short Mngmt= 12.59
  Currently in Operational Management Band
  Simulated Average LORS2008 [1965-2000]
                                             13.41
 Difference from Average LORS2008
                                             2.05
  10SEP (1965-2007) Period of Record Average
                                                14.47
 Difference from POR Average
  Today Lake Okeechobee elevation is determined from the 4 Int & 4 Edge stations
  ++Navigation Depth (Based on 2007 Channel Condition Survey) Route 1 ÷ 9.40'
  ++Navigation Depth (Based on 2008 Channel Condition Survey) Route 2 ÷ 7.60'
  Bridge Clearance = 49.24'
4 Interior and 4 Edge Okeechobee Lake Average (Avg-Daily values):
 L001
       L005 L006 LZ40
                              S4
                                      S352 S308 S133
  15.24 15.47 15.49 15.56 15.61 15.59 15.32 15.37
 *Combination Okeechobee Avg-Daily Lake Average = 15.46
                                                    (*See Note)
Okeechobee Inflows (cfs):
                                            162 Fisheating Cr 600
0 S135 Pumps 0
                3077
                          S191
  S65E
                         S133 Pumps
                                            0
  S154
                 152

      S127 Pumps
      0
      S2 Pumps

      S129 Pumps
      0
      S3 Pumps

      S131 Pumps
      0
      S4 Pumps

 S84
                  4
                                                                       0
 S71
                  156
                                                                       0
 S72
                  166
Total Inflows: 4317
Okeechobee Outflows (cfs):
 S135 Culverts 0 S354
                                              0
                                                     S77
                                                                     4001 (Used)
 S127 Culverts 0
S129 Culverts 0
S131 Culverts
                          S351
                                             0
                                                     S77Below
                                                                     4449 (NOT USED)
                          S352
                                            250
                                                     S308
                                                                     1300 (Used)
                           L8 Canal Pt 352
                                                     S308Below 1212 (NOT USED)
 C5
                    0
Total Outflows: 5903
****S77 Structure outflow is being used to compute Total Outflow.
****S308 Structure outflow is being used to compute Total Outflow.
Okeechobee Pan Evaporation (inches):
                 0.41
                        S308
                                           0.39
 Average Pan Evap x 0.75 Pan Coefficient = 0.30" = 0.02'
Lake Average Precipitation using NEXRAD: = 0.03" = 0.00'
```

Note: Headwater, tailwater, and stage values below are instantaneous values unless otherwise specified.

	Headwater	Tailwater				- Gat	te Pos	sition	ns		
	Elevation	Elevation	Disch	#1	#2	#3	#4	#5	#6	#7	#8
	(ft-msl)	(ft-msl)	(cfs)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)
		(I) see r	note at	bott	om					
North East Sh	nore										
S133 Pumps	: 13.46	15.52	0	0	0	0	0	0	(cf:	3)	
S193:											
S191:		15.50	162	0.0		0.5					
S135 Pumps		15.35	0	0		0	0		(cf:	3)	
S135 Culve	rts:		0	0.0	0.0						
_											
North West Sh		4									
S65E:		15.71	3077	2.0	1.5		1.5				
S127 Pumps		15.40	0	0	0	0	0	0	(cf:	3)	
S127 Culve	rt:		0	0.0							
G1 20 Dr	. 10 07	15 56	0	0	0	0			/ ~ F .	~ \	
S129 Pumps: S129 Culver		15.56	0 0	0 0.1	0	0			(cf:	3)	
S129 Culver			U	0.1							
S131 Pumps:	12 93	15.68	0	0	0				(cf:	=)	
S131 Culve		13.00	O	O	J				(С1)	<i>J</i> ,	
DIST CUIVE											
Fisheating	Creek										
nr Palmda		32.33	600								
nr Lakepo		16.02									
C5:	16.71	15.46	0	0.0 0	.0 0	.0					
South Shore											
S4 Pumps:	10.88	15.58	0	0	0	0			(cf:	s)	
S169:	14.41	10.90	0	0.0	0.0	0.0					
s310:	15.55		2								
S3 Pumps:	10.59	15.60	0	0	0	0			(cf:	s)	
S354:	15.60	10.59	0	0.0	0.0						
S2 Pumps:	9.87	15.52	0	0	0	0	0		(cf:	s)	
S351:	15.52	9.87	0	0.0	0.0	0.0					
S352:	15.49	11.48	250	0.8	0.8						
C10A:	-NR-	-NR-		10.0	10.0	8.	.0 10	0.0	10.0		
L8 Canal Pi	Γ	15.35	352								
	S35	1 and S352	Tempora	ary Pum	ps/S3	54 Sr	pillwa	яy			
S351:	9.87	15.52	0	-NRN	RNR	NR-	NR	-NR-			
S352:	11.48	15.49		-NRN							
S354:	10.59	15.60	0								

```
Caloosahatchee River (S77, S78, S79)
 S47B:
       13.04
                    12.03
                                       0.0 0.5
 S47D:
             12.03
                      10.71
                                -NR-
                                       0.0
 S77:
   Spillway and Sector Flow:
             15.26
                    10.86
                                4000
                                      -NR- 3.7 3.7 3.7
   Flow Due to Lockages+:
                                  1
 S77 Below USGS Flow Gage
                                4449
 S78:
   Spillway and Sector Flow:
              10.32
                    3.16
                                5255
                                       4.0 4.0 4.5 4.0
   Flow Due to Lockages+:
                                  4
 S79:
   Spillway and Sector Flow:
                                7862
                                       3.0 3.0 3.0 4.0 4.0 3.0 3.0 3.0
               2.92
                    1.40
   Flow Due to Lockages+:
                                  2.
   Percent of flow from S77
                                  51%
   Chloride
                      (mqq)
                                48
St. Lucie Canal (S308, S80)
 S308:
   Spillway and Sector Flow:
              15.30
                                1298
                                       0.0 3.0 3.5 0.0
                      14.26
   Flow Due to Lockages+:
                                  2.
 S308 Below USGS Flow Gage
                                1212
 S153:
             18.95 14.14
                                       0.5 0.0
                                84
 S80:
   Spillway and Sector Flow:
              14.08
                    0.85
                                1808
                                       0.0 1.0 1.0 0.0 1.0 1.0 0.0
   Flow Due to Lockages+:
                                  13
   Percent of flow from S308
                                  72%
 Steele Point Top Salinity (mg/ml) ****
 Steele Point Bottom Salinity (mg/ml) ****
 Speedy Point Top Salinity
                           (mg/ml) 7089
 Speedy Point Bottom Salinity (mg/ml) 7723
```

+ Flow Due to lockages is computed utilizing average daily headwater and tailwater along with total number of lockages for the day to calculate a volume which is then converted to an average discharge in cfs.

				Wi	nd
Daily Precipitation Totals	1-Day	3-Day	7-Day	Directio	n Speed
	(inches)	(inches)	(inches)	(Degø)	(mph)
S133 Pump Station:	-NR-	0.13	1.38		
S193:	-NR-	0.00	0.00	-NR-	-NR-
Okeechobee Field Station:	-NR-	0.00	0.00		
S135 Pump Station:	-NR-	0.98	2.15		
S127 Pump Station:	-NR-	0.00	0.08		
S129 Pump Station:	-NR-	0.70	1.62		
S131 Pump Station:	-NR-	0.00	0.07		
S77:	0.00	0.00	0.33	114	2
S78:	0.00	0.00	1.57	25	1
S79:	0.15	0.16	1.40	36	2

```
      S4 Pump Station:
      -NR-
      0.00
      0.00

      Clewiston Field Station:
      -NR-
      0.17
      1.30

      S3 Pump Station:
      -NR-
      0.01
      0.87

      S2 Pump Station:
      -NR-
      0.02
      0.35

      S308:
      0.18
      0.18
      0.24

      S80:
      0.57
      0.77
      0.78

      Okeechobee Average
      0.09
      0.17
      0.65

                                                                                                                   270
                                                                                                                                        0
                                                                                                                    90
                                                                                                                                         0
              (Sites S78, S79 and S80 not included)
    _____
    Oke Nexrad Basin Avg 0.03 0.06 0.67
Okeechobee Lake Elevations 10 SEP 2013 15.46 Difference from 10SEP13 10SEP13 -1 Day = 09 SEP 2013 15.49 0.03 10SEP13 -2 Days = 08 SEP 2013 15.51 0.05 10SEP13 -3 Days = 07 SEP 2013 15.52 0.06 10SEP13 -4 Days = 06 SEP 2013 15.51 0.05 10SEP13 -5 Days = 05 SEP 2013 15.53 0.07 10SEP13 -6 Days = 04 SEP 2013 15.54 0.08 10SEP13 -7 Days = 03 SEP 2013 15.55 0.09 10SEP13 -30 Days = 11 AUG 2013 16.03 0.57 10SEP13 -1 Year = 10 SEP 2012 14.81 -0.65 10SEP13 -2 Year = 10 SEP 2011 10.86 -4.60
Long Term Mean 30day Avearge ET for Lake Alfred (Inches) = 4.21
                                            Lake Okeechobee Net Inflow (LONIN)
                                  Average Flow over the previous 14 days | Avg-Daily Flow
     S65E
                                        Average Flow over previous 14 days | Avg-Daily Flow
```

	-13 Days =		AUG 2013	3278 THU	.	3496
Lake Okeecho	bee Outle	ts Last 14	Days			
		Discharge	Below S-77 Discharge (ALL-DAY) (AC-FT)	S-78 Discharge (0700-2100) (AC-FT)		
10 SEP 2013 09 SEP 2013 08 SEP 2013 07 SEP 2013 06 SEP 2013 05 SEP 2013	4738 4626 4554 4692 4782 5029	7934 7771 7673 7895 8158 8434	8822 8697 8528 8778 9020 9256	6192 6240 5960 5889 6229 6521	10429 10466 9945 9977 10457 10981	15595 17759 17447 14918 16324 16496
04 SEP 2013 03 SEP 2013 02 SEP 2013 01 SEP 2013 31 AUG 2013 30 AUG 2013	4866 4713 4878 4020 3853 3820	8168 7952 8225 8386 8386 8326	9168 8694 8778 8845 8850 8759	6620 6532 6024 4812 4618 4686	11170 10854 10130 10098 10162 10251	17692 18873 19373 15902 16993 18255
29 AUG 2013 28 AUG 2013	3880	8366 8438	8851 8769	4610 4459	10025 9759	18838 19453
	S-310 Discharge (ALL DAY) (AC-FT)	S-351 Discharge (ALL DAY) (AC-FT)		S-354 Discharge (ALL DAY) (AC-FT)		?t
10 SEP 2013 09 SEP 2013 08 SEP 2013 07 SEP 2013 06 SEP 2013 05 SEP 2013 04 SEP 2013	3 8 -0 10 2 12 18	0 0 0 0 0 0	496 333 621 682 1130 851 944	0 0 0 0 0 0	698 718 724 779 808 796 784	
03 SEP 2013 02 SEP 2013 01 SEP 2013 31 AUG 2013 30 AUG 2013 29 AUG 2013 28 AUG 2013	2 -5 2 60 29 -2 93	0 0 0 0 0	758 258 389 1251 1384 325 1222	0 0 0 0 0	804 743 782 797 808 718 753	
I (S-308 Discharge (ALL DAY)	Below S-30 Discharge (ALL-DAY)	08 S-80 e Discharg (ALL-DAY	7)		
DATE 10 SEP 2013 09 SEP 2013 08 SEP 2013 07 SEP 2013	(AC-FT) 2578 2419 2276 2781	(AC-FT) 2404 2236 2163 2741	(AC-FT) 3611 3596 3640 3600			
06 SEP 2013 05 SEP 2013 04 SEP 2013 03 SEP 2013 02 SEP 2013	2831 2722 2507 2560 2432	2814 2751 2431 2320 2114	3573 3596 3624 3620 3640			
01 SEP 2013 31 AUG 2013 30 AUG 2013 29 AUG 2013	2636 2920 2951 2820	2491 2712 2672 2650	3628 3604 3600 3580			

10SEP13 -12 Days = 29 AUG 2013 3197 FRI | 3501

28 AUG 2013 2344 2517 3620

- *** NOTE: 1) Discharge from (0700-2100) is computed using Spillway and Sector Gate Discharges from 0700 hrs to 2100 hrs.
 - 2) Discharge (ALL DAY) is computed using Spillway, Sector Gate and Lockages Discharges from 0015 hrs to 2400 hrs.

(I) - Flows preceded by "I" signify an instantaneous flow computed from the single value reported for the day

* On 11 May 1999, Lake Okeechobee Elevation was switched from Instantaneous 2400 value to an average-daily lake average. On 14 Mar 2001, due to the isolation of various gages within the standard 10 stations, the average of the interior 4 station gages was used as the Lake Okeechobee Elevation.

On 05 November 2010, Lake Okeechobee Elevation was switched to a 9 gage mix of interior and edge gages to obtain a more reliable representation of the lake level.

On 09 May 2011, Lake Okeechobee Elevation was switched to a 8 gage mix of interior and edge gages to obtain a more reliable representation of the lake level due to isolation of $\rm S135$ from low lake levels.

- Today Lake Okechobee elevation is determined from the 4 Int & 4 Edge stations ++ For more information see the Jacksonville District Navigation website at http://www.saj.usace.army.mil/
- \$ For information regarding Lake Okeechobee Service Area water restrictions please refer to www.sfwmd.gov

Report Generated 11SEP2013 @ 09:46 ** Preliminary Data - Subject to Revision **

MEETING MINUTES

SR 710 Possible Regional Pond Brainstorming Meeting 2 SR 710 from US 441 to the L-63N Canal FPID No. 419344-3-52-01

April 4, 2014, 2:00 pm; GoToMeetingsss

Attendaes:s

Attendees:s			
Names		E-mails	Office Phone s Numbers
FDOTb	S	S	S
RicksRennas	StatesDrainagesEngineers	rick.renna@dot.state.fl.uss	850-414-5351s
Brents Setchells	District £ nvironmentals Permitting £ ngineers	brent.setchell@dot.state.fl.uss	863-519-2557s
Nicoles Moniess	District £nvironmentals Permitting & pecialists	nicole.monies@dot.state.fl.uss	863-519-2359s
Amys Setchells	Senior Projects Managers	amy.setchell@dot.state.fl.uss	863-519-2609s
SFWMDb	S	S	S
Lesleys Bertolottis	Principal Scientists (Northerns Everglades Programs Managers)s	lbertolo@sfwmd.gov	(561)s682-6415s
KevinsCarters	LeadScientists(TMDLs Coordinator)ss	kecarter@sfwmd.gov	(561):682-6949s
Orlandos Diazs	SeniorsEnvironmentalsCcientists (WatersQualitysTreatments Technologies)s	odiaz@sfwmd.gov	(561):682-6534s
Erics Gonzalezs	ProjectsManagerPrincipals (Northern&verglades)s	ergonzal@sfwmd.gov	(561)s682-6391s
Jesses Markles	OkeechobeesRegulatorysServices CentersAdministratorss	jmarkle@sfwmd.gov	(863)\$462-5260\$3005\$
Damons Meierss	Principal £ ngineer (Disperseds Waters Management)s	dmeiers@sfwmd.govs	(561)s682-6876s
Garystitters	Intergovernmentals Representative: ① keechobee,s Glades, and Highlands Counties a	gritter@sfwmd.gov	(863)\$462-5260\$3017\$
Steves Sentess	RegulatoryProfessionaldeads (WestCoastanddocalProjects)s	ssentes@sfwmd.gov	(239)\$38-2929\$7754s
Tonys Waterhouses	AssistantsDirectorsRegulations Divisionss	twaterho@sfwmd.gov	(561)s682-6867s

S

Name		Email	Phone
FDEP			
Kim Dinkins	Environmental Consultant	Kimberleigh.Dinkins@dep.state.fl.us	850-245-8825
Katie Hallas	Environmental Consultant	Katie.Hallas@dep.state.fl.us	850-245-8432
Beth Alvi	Program Administrator	Elizabeth. Alvi@dep. state.fl. us	850-245-8559
Trina Veilhauer	Deputy Director	Trina.Vielhauer@dep.state.fl.us	850-245-8338
Wantman Group			
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Eric Lanning	Project Engineer	Eric.Lanning@WantmanGroup.com	407-581-1221
Kasey Carrere	Environmental Scientist	Kasey.Carrere@WantmanGroup.com	407-581-1221
Balmoral Group			
Greg Seidel	Project Drainage Engineer	gseidel@balmoralgroup.us	407-629-2185
Jennifer Nunn	Asst. Project Drainage Engineer	JNunn@Balmoralgroup.us	407-629-2185
Lori Stanfill	Asst. Project Drainage Engineer	LStanfill@balmoralgroup.us	407-629-2185
ATM			
Janet Hearn	Senior Engineer	JHearn@AppliedTM.com	386-256-1018

Purpose: The purpose of the meeting is for the FDOT to present the results of draft Pond Siting Report and continue discussion. Below are highlights of the meeting -

- 1. Greg Seidel began the meeting with introduction of the lead contacts for each agency and a brief description of the roles.
- 2. Brent Setchell reiterated from the previous meeting the FDOT's interest in providing as much nutrient loading reduction as possible based on the FDOT budget for "typical postage stamp ponds" on a project. He added that the FDOT is very interested in partnering in regional treatment. Rick Renna affirmed the FDOT position.
- 3. Mr. Setchell summarized the current SR 710 status the pond costs for the project are estimated at the summarized. The FDOT has not completed its review and this number is subject to change. The SR 710 project has ROW funding beginning in FY 2016 (July 2015). The goal for completing a partnering agreement for regional treatment would be April 2015 prior to finalizing our ROW maps. The project is not currently funded for construction, but the earliest construction could be funded would be FY 2019 (July 2018). Mr. Seidel provided a brief review of the SR 710 project utilizing the meeting exhibits (See

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Attachments) and google maps. The project will be a four-lane curb and gutter typical section. The roadway begins at US 441 at the Airport Ditch and runs east along a new alignment across Taylor Creek then turns south tying into the existing SR 710 before crossing the L-63N Canal and ending at Mosquito Creek. The project length is approximately 3.85 miles.

- 4. Mr. Seidel gave a review of the Taylor Creek and L-63N Canal Bridge Hydraulics Reports (BHR) at SR 710 noting that the reports were completed in NAVD datum. The Taylor Creek BHR indicated that the Lower Taylor Creek basin is comprised of a 3.26 square mile Airport Ditch Basin and a 2.20 square mile Lower Taylor Creek Basin for a total drainage basin of 5.46 square miles. From the BHR for the L-63N Canal, the drainage basin upstream of the SR 710 crossing is 111.89 square miles.
- 5. Mr. Seidel provided the control elevations within Taylor Creek as 12.83 NAVD and within the L-63 as 17.83 NAVD.
- 6. Mr. Seidel gave a review of the pond siting report for the project and focused on the different elements reviewed such as drainage patterns, wetlands, cultural resources, utilities, geotechnical data and contamination screenings and estimated costs. For each of the areas, Mr. Seidel highlighted the evaluations for Pond Site 2C which would be within the location of the regional facility. He noted the study area did not include the entire regional pond area shown in the first meeting.
- 7. Mr. Renna made a comment that the 2C site would likely contain wetlands which could be used for wetland enhancement and nutrient uptake.
- 8. Mr. Seidel commented that the regional pond would reduce pollutants at a much higher concentration than the smaller SR 710 ponds. Specifically, the PSR estimated a reduction of 12 kg/yr for the post stamp ponds vs an estimated 2-3 MT/yr for a regional facility depending on the size.
- 9. Mr. Seidel went over the preliminary stormwater management concept for SR 710 utilizing the regional pond. This concept includes 3 drainage basins: the first basin will discharge to the regional pond; the second basin will discharge for pre-treatment to an existing (SR 70) pond without meeting pre/post requirements prior to discharging to L-63N Canal; and the third basin will discharge directly to the L-63N Canal. Mr. Renna commented that the existing permitting rules allow for compensatory treatment, and that approval of discharge

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- into the L-63N Canal would not be difficult. There was no objection from either SFWMD or FDEP participants.
- 10. Several local projects were noted including the Nubbin Slough STA, the Upper Taylor Creek STA, Treasure Island and Oak Park.
- 11. Gary Ritter commented that there is water demand from the L-63N Canal. If S-192 is utilized, project needs to be cognizant of water supply needs.
- 12. Concerns were expressed with the proximity of the Okeechobee airport to the proposed regional treatment facility and need to be at least 10,000 feet away to reduce the risk of bird strikes.
- 13. Mr. Renna indicated that he was meeting with Tom Frick from FDEP on Thursday to discuss this project among others.
- 14. Trina Veilhauer indicated the FDEP is quite interested and asked how we best move forward from this point. Brent Setchell offered that FDOT could fund The Balmoral Group through their District 1 Districtwide Drainage contract to perform a feasibility study for the regional treatment. It was agreed that the feasibility study would analyze two options a project option funded and constructed entirely by the FDOT to meet permit requirements and a Stormwater Treatment Area (STA) option that investigated partnering and a much larger facility. Mr. Seidel indicated that a scope of services would be prepared to investigate the two options, which would include meetings and coordination with stakeholders. A draft report will be submitted to FDOT, SFWMD and FDEP for review prior to finalizing the report.
- 15. Brent Setchell noted that FDOT staff is not "experts" in the design of STAs and would look for either SFWMD or FDEP to take the lead in the design and construction of a larger STA.
- 16. Brent Setchell noted that FDOT would like to utilize suitable excavated material from the regional pond for use as fill on its SR 710 project.
- 17. It was noted that the project is not within the Central Florida Water Initiative (CFWI) boundaries.

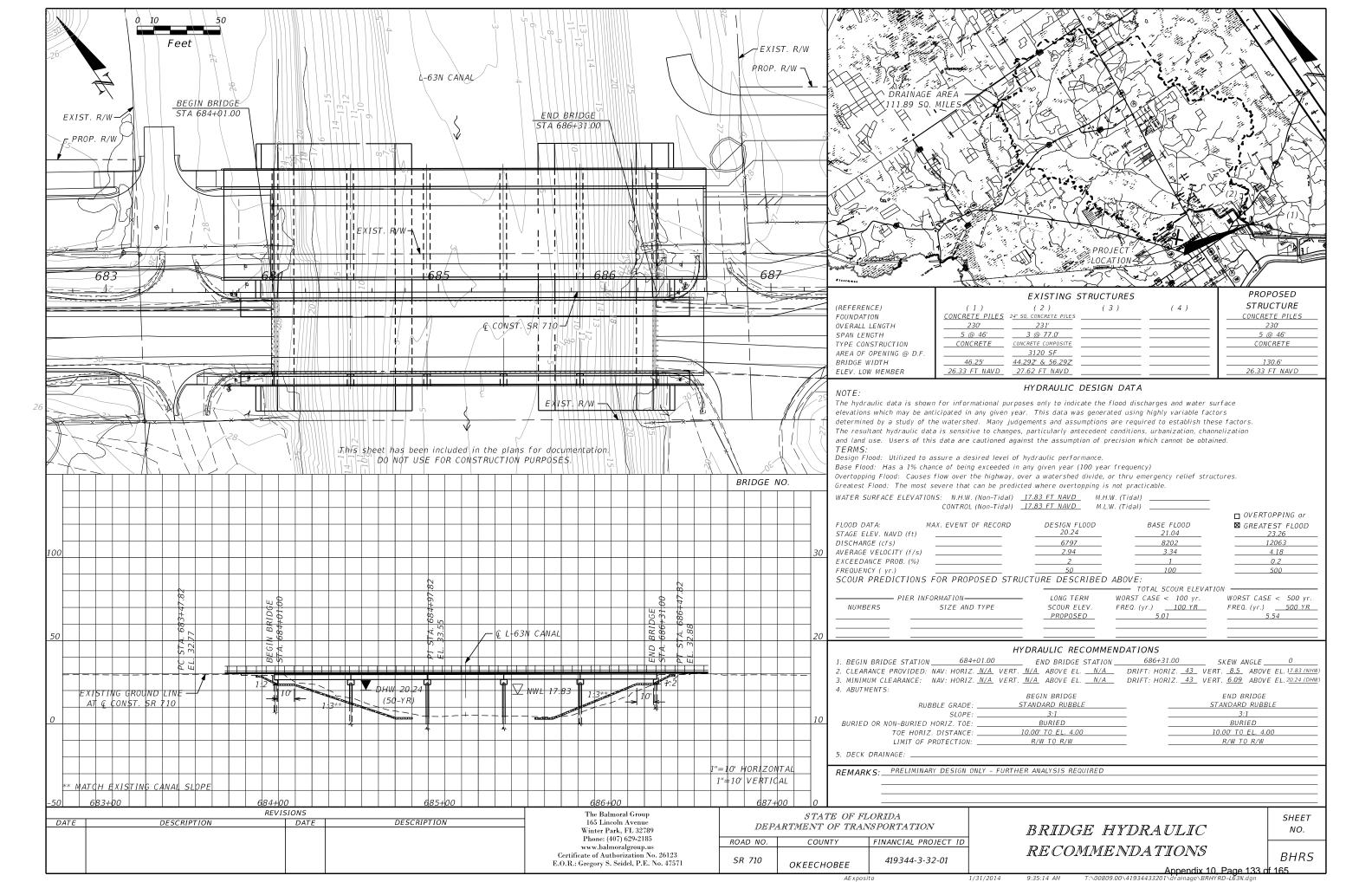
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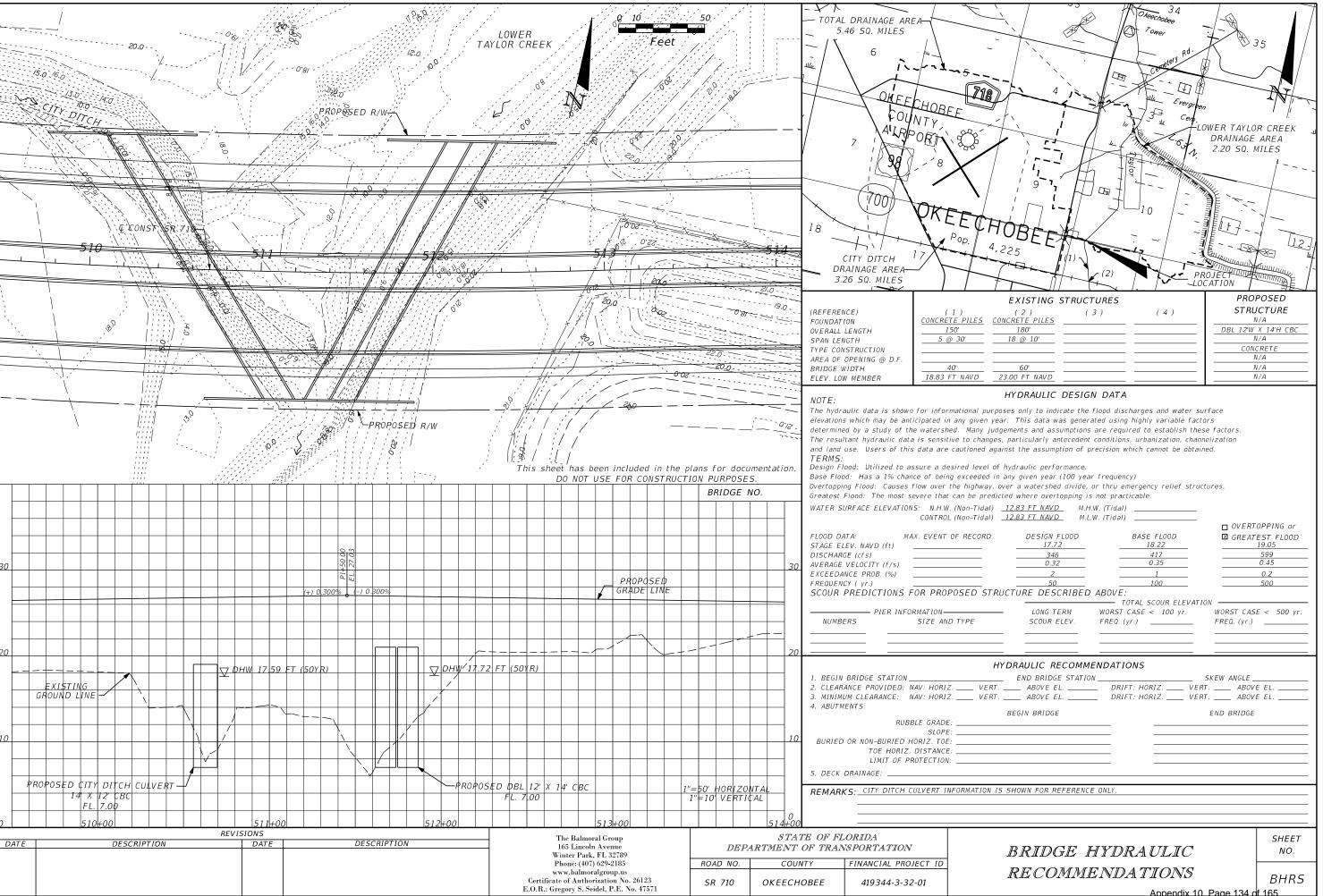
Action Items

- 1. FDOT shall negotiate a Task Work Order with the Balmoral Group to prepare the feasibility study for the regional treatment options. The draft report is expected to be sent to FDEP & SFWMD for review by August 15, 2014.
- 2. FDEP and SFWMD to explore funding participation options and be prepared to make a funding commitment no later December 31, 2014 so that we may move forward with preparing an agreement.
- c. Attendees (Via Email)

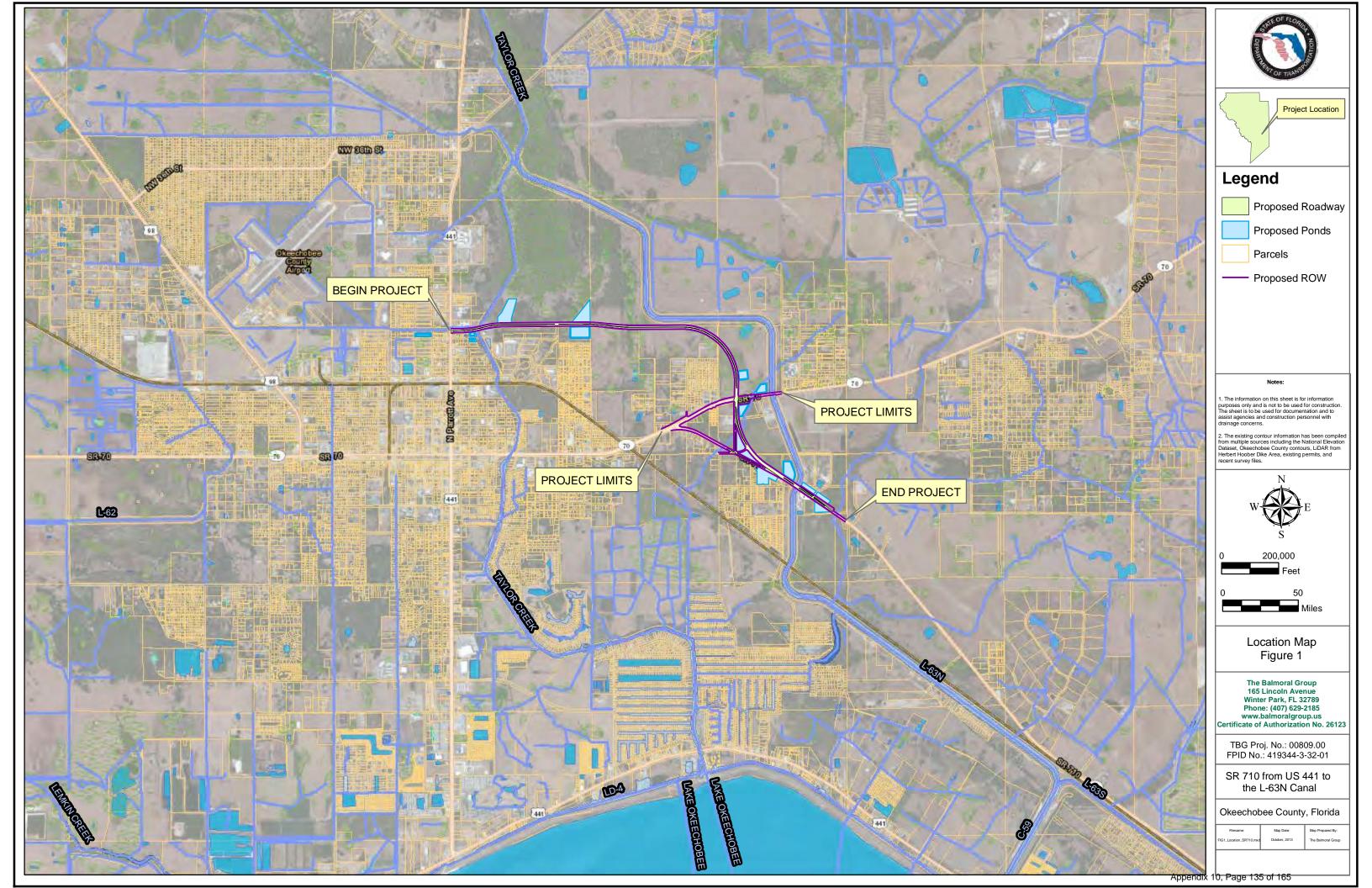
Attachment - Agenda Exhibitss

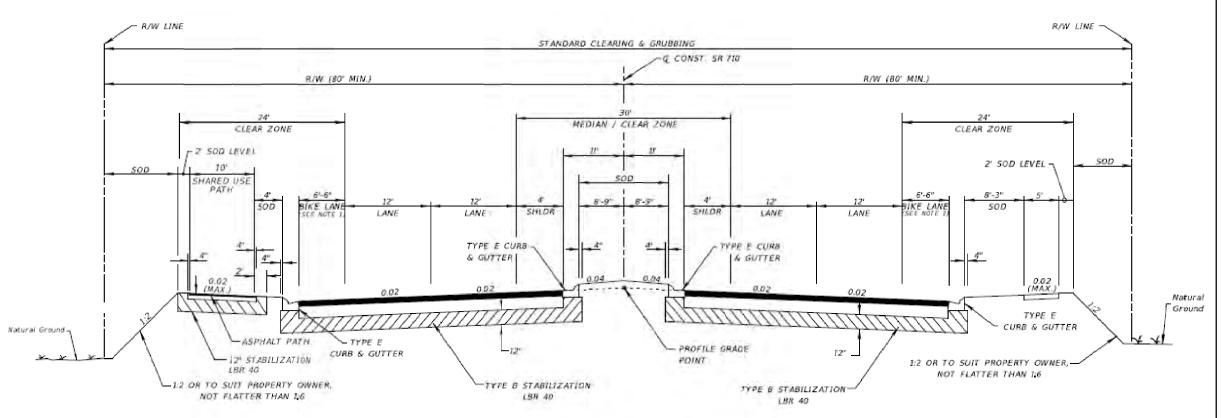
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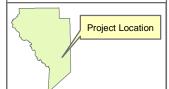


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TYPICAL SECTION NO. 1 SR 710 STA. 500+00.00 TO STA. 703+50.00

TYPICAL SECTION NOTES:

1. PROVIDES FOR 8' USABLE SHOULDER.

NEW CONSTRUCTION

OPTIONAL BASE GROUP 11 WITH

TYPE SP STRUCTURAL COURSE (TRAFFIC C) (4")

AND FRICTION COURSE FC-5 (¾") (RUBBER)

PATH

OPTIONAL BASE GROUP I WITH TYPE SP STRUCTURAL COURSE (TRAFFIC A) (1")

TRAFFIC DATA

CURRENT YEAR = 2013 AADT = 7,100 ESTIMATED OPENING YEAR = 2015 AADT = 11,400 ESTIMATED DESIGN YEAR = 2035 AADT = 14,190 K = 9.0% D = 56.2% T = 20.9% (24 HOUR) DESIGN HOUR T = 10.5% DESIGN SPEED = 50 MPH cccTypical Section cccccFigure 2

The Balmoral Group 165 Lincoln Avenue Winter Park, FL 32789 Phone: (407) 629-2185 www.balmoralgroup.us Certificate of Authorization No. 26123

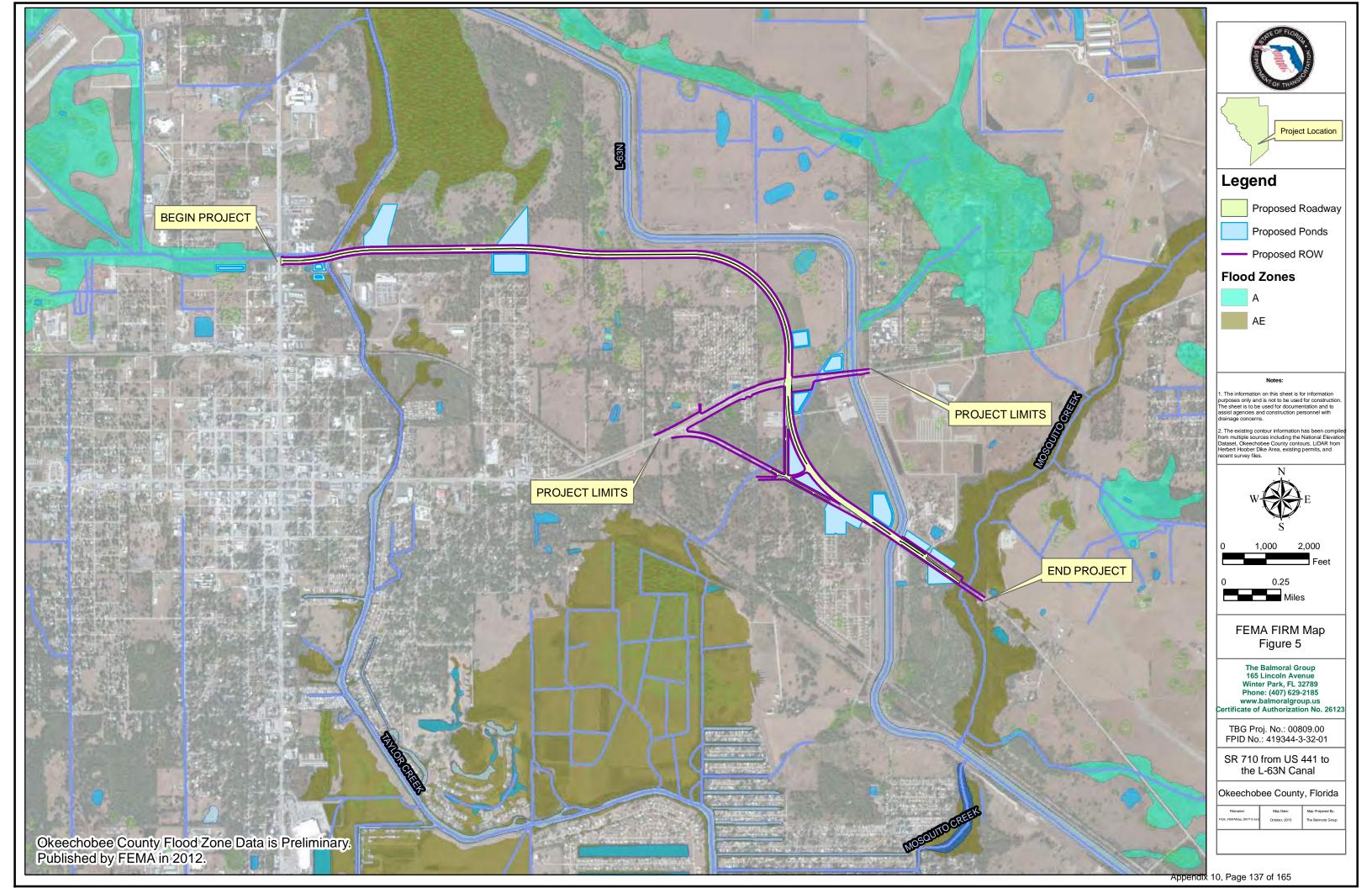
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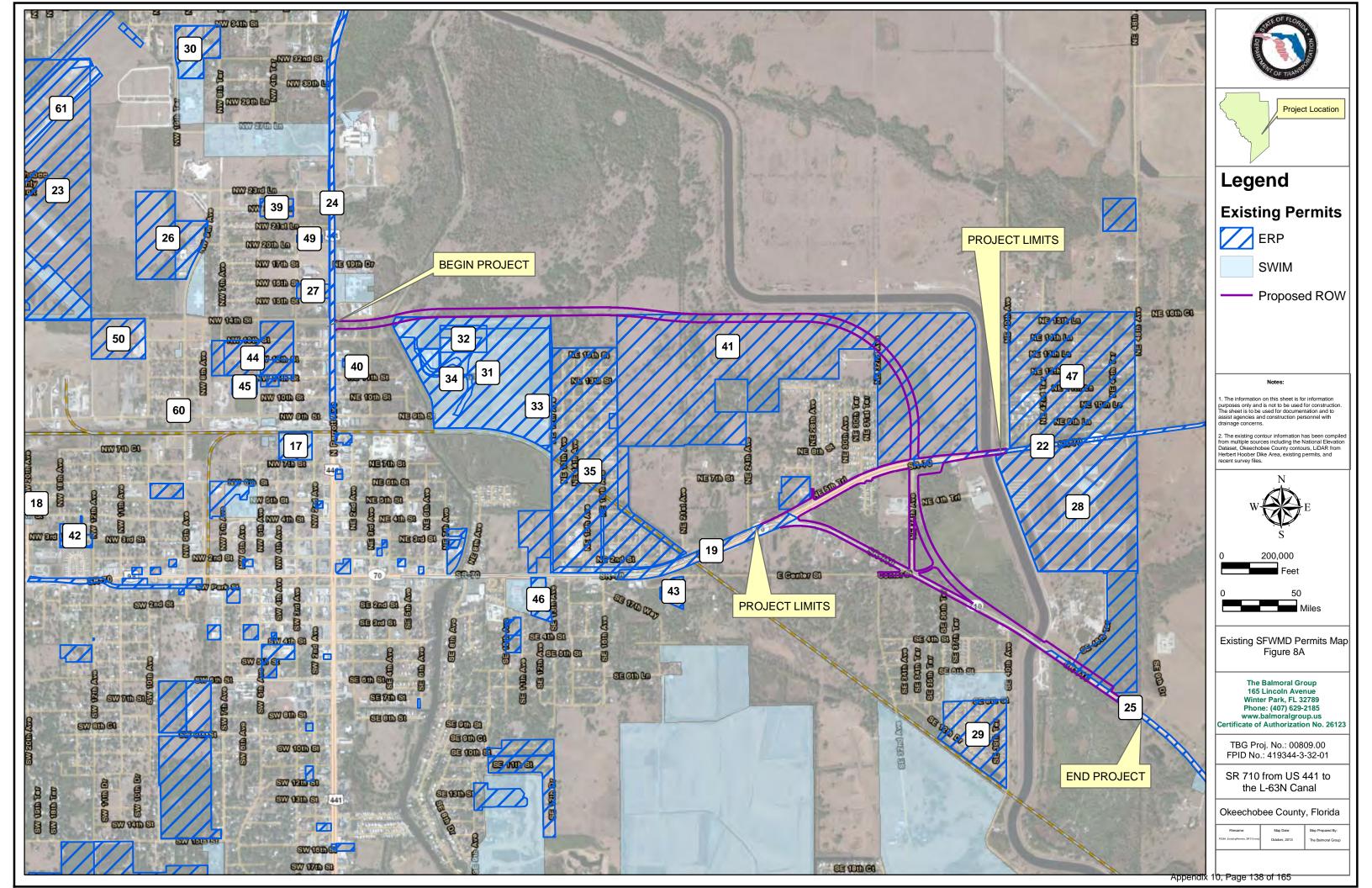
SR 710 from US 441 to the L-63N Canal

Okeechobee County, Florida

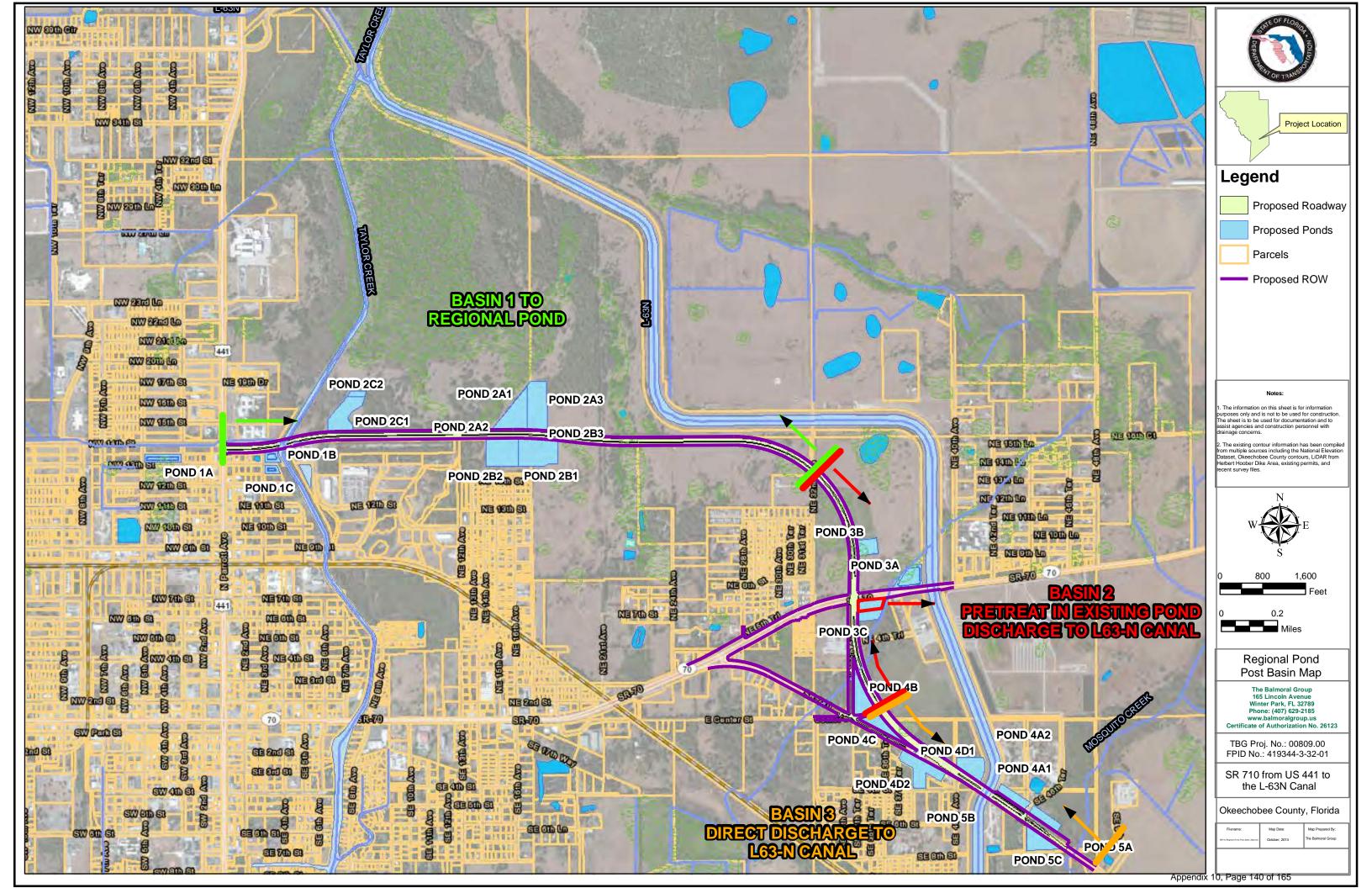
Filename:	Map Date:	Map Prepared By:
ypicalSection_SR710.mxd	October, 2013	The Balmoral Group

Appendix 10, Page 136 of 165









SR 710 Stormwater Treatment Area/Regional Pond Feasibility Study Initial Meeting with Hamrick Property Owner **Meeting Minutes**

FPID No. 432644-1-32-01 - D1 DW Drainage

Location: District One, Bartow

Date: July 11, 2014 Time 11:00 am

The purpose of the meeting is to introduce the SR 710 Stormwater Treatment Area/Regional Pond Feasibility Study as an investigation being undertaken by the FDOT District One as a part of the SR 710 new alignment project in Okeechobee.

Attendees: See attached Sign-In Sheet

- 1. Mr. Brent Setchell gave an introduction and project background on the SR 710 Feasibility Study to the property owners, Mr. Michael and Ms. Maryann Hamrick and their consultant, Morris Crady.
- 2. Mr. Greg Seidel introduced the regional pond alternative that is to be constructed by the FDOT for the SR 710. This option would incorporate offsite areas associated with Lower Taylor Creek.
 - Ms. Janet Hearn introduced the Stormwater Treatment Area (STA) alternative which would require interagency cooperation and be hydraulically connected to the L63-N canal and Upper Taylor Creek. Ms. Hearn said that the amount of nutrient reduction achieved by the STA would depend in part on the area of the STA but that a minimum size of 100 acres is desirable. This is comparable to the Taylor Creek STA which has a treatment area of 118 acres.
- 3. Ms. Amy Setchell gave a brief update on the SR 710 new alignment project from L-63N to US-41.
- 4. Mr. Hamrick reiterated that maintaining the integrity of the property is important to them.
- 5. As part of the study, a portion of the property will be surveyed to verify design assumptions. Access to the site will be coordinated with the ranch manager. Contact information to be provided by The Wantman Group. Survey will need to get started as soon as possible.
- 6. The next step is to set-up a Stakeholder Meeting in Okeechobee. This will be scheduled in the next two weeks. The Balmoral Group will be contacting the Hamricks regarding availability.

Fnd of Minutes

SIGN IN SHEET

SR 710 Stormwater Treatment Area/Regional Pond Feasibility Study Initial Meeting with Hamrick Property Owner Meeting Agenda FPID No. 432644-1-32-01 - D1 DW Drainage

Location: District One, Bartow

Date: July 11, 2014 Time 11:00 am

NAME	FIRM/AGENCY	OFFICE / RESPONSIBILITY	EMAIL ADDRESS	Initials
Carlton Spirio	FDOT	Drainage	Carlton.Spirio@dot.state.fl.us	
Brent Setchell	FDOT	Drainage	Brent.Setchell@dot.state.fl.us	BS
Amy Setchell	FDOT	PM	Amy.Setchell@dot.state.fl.us	aes
Michael Hamrick	Property Owner		MHamrick@manateelegal.com	my
Morris Crady				Moz
Gregory Seidel	The Balmoral Group	Consultant	gseidel@balmoralgroup.us	MM
Jennifer Nunn	The Balmoral Group	Consultant	jnunn@balmoralgroup.us	Sin
Janet Hearn	ATM	Consultant	jhearn@appliedtm.com	John
Henri Belrose	Wantman Group	Consultant	Henri.belrose@wantmangroup.com	HB
Alfredo Rodriguez	Wantman Group	Consultant	Alfredo.rodriguez@wantmangroup.com	AR
Gregory Bowne	FDOT	Right-of-way	Gregory.Bowne@dot.state.fl.us	greg
Jennie Richard	FDOT	Right-of-way	Jennie.Richard@dot.state.fl.us	Dre
Morris Crac	y Lucidos Ass		Mcrady Clucidodesign. com	yme
	AMRICK HAMRI	ciktisons	ANNIE HUF@ACI,com	MNM
Nicole Monit	es FOOT	Permits	nicole. Monies @ dot. state fl.us	tital

SR 710 Stormwater Treatment Area/Regional Pond Feasibility Study Stakeholder Meeting Minutes FPID No. 432644-1-32-01 - D1 DW Drainage

Location: SFWMD Okeechobee Service Center, Okeechobee

Date: July 31, 2014 Time 10:30 am

The purpose of the meeting is to introduce the SR 710 Stormwater Treatment Area/Regional Pond Feasibility Study as an investigation being undertaken by the FDOT District One as a part of the SR 710 new alignment project in Okeechobee.

Attendees: See attached Sign-In Sheet

- 1. Mr. Brent Setchell gave an introduction on the SR 710 Feasibility Study.
- 2. Mr. Greg Seidel gave a brief project history explaining how the SR 710 Feasibility Study has progressed to this point.
- 3. Mr. Greg Seidel introduced the regional pond alternative that is to be constructed by the FDOT for the SR 710. This option would incorporate offsite areas associated with Lower Taylor Creek.
 - a. Representatives from Okeechobee County confirmed the airport ditch is owned by the County from Taylor Creek up to airport property.
 - b. Mr. Setchell voiced his concern about conveying water from the airport ditch to the regional pond. He mentioned the preferred option on behalf of the FDOT would be to provide the required 1-inch of treatment for the SR 710 roadway and demonstrate that the nutrient removal shows a net benefit to the community.
 - c. Mr. Seidel mentioned that a lower treatment depth could be provided. He also indicated that a control structure could be located at Taylor Creek and securing flood rights from the property owners could be an option.
 - d. Mr. Setchell explained the SR 710 Regional Pond approach in that Basins 1 and 2 would be treated by the Regional Pond, Basin 3 and a portion of Basin 4 would pre-treat via the existing pond and that the remaining runoff would discharge directly to the L-63N Canal.
- 4. Ms. Janet Hearn introduced the Stormwater Treatment Area (STA) alternatives which would require interagency cooperation and be hydraulically connected to the L63-N canal and Upper Taylor Creek.
 - a. Ms. Hearn said that for planning purposes a 100-acre STA is being evaluated. This is comparable to the Taylor Creek STA which has a treatment area of 118 acres. A 100 acre STA could remove about 1,500 to 1,600 kg of TP per year. An overview of three potential locations for a 100 acre STA within the Hamrick property was presented. These three sites were selected to avoid wetlands.

- b. The Lake Okeechobee TMDL requires an in-lake concentration of 40 parts per billion (ppb) TP.
- FDEP added that the existing Taylor Creek STA provides approximately 1520 kg of removal.
- d. The STA 2 option would require some rehabilitation of the existing wetland in order to retain runoff from the surrounding property. This would provide additional storage and remove approximately 180 kg TP per year without additional flow from the L-63N Canal or Upper Taylor Creek.
- e. The STA 2 option could provide up to 1000 kg of removal if inflow was augmented with flow from L-63N Canal.
- f. Mr. Morris Crady asked if a combination of STA 1 and STA 2 would be possible in order to still use the property (i.e. for walking trails) in the winter. Mr. Seidel responded by saying the final STA choice is not part of the feasibility study and would be coordinated under final design.
- g. Mr. Setchell liked the fact that the STA 2 option would provide some treatment and attenuation. However, he expressed some concern for the STA 2 option since the restored wetlands would be limited on the treatment volume depth (storage) provided. Would this option still require a control structure and how would the western bank of Lower Taylor Creek be affected?
- h. If an STA option is chosen, FDOT would still need to obtain fill for the SR 710 project and this could be coordinated through agreements.
- i. Mr. Hamrick asked if an STA option would impact ranch operations. Ms. Bonnie Wolff Pelaez confirmed that the BMAP manual does not restrict cattle from the wetlands.
- j. Mr. Hamrick mentioned that the wetland portion of his property is the emotional piece, and the upland portion of his property is the economic piece.
- 5. Mr. Seidel mentioned that if an STA option was selected, FDOT would not be taking the lead on this design and this would most likely fall to the FDEP or SFWMD.
- 6. Mr. Jim Threewits reiterated his concerns with ponds adjacent to the right-of-way. The County has requested from FDOT that the new SR 710 alignment be a main corridor to attract development. The County wants this gateway to be pretty and attractive for development and does not want unattractive ponds or ponds along the roadway frontage. Mr. Threewits feels this is a chance to do something good and doesn't want to miss out and added that this is a very valuable piece of the land to the county.
 - a. Mr. Setchell responded by saying that FDOT is evaluating the need for pond fencing. FDOT is open to providing drainage easements for property owners to provide pond maintenance.
 - b. Mr. Setchell stated that FDOT does not want to move ponds away from the right-of-way due to the hydraulics and increase in cost.
- 7. Mr. Seidel commented that the current schedule calls for a decision to be reached by the end of the year.
 - a. Ms. Amy Setchell responded that the draft Feasibility report is due Sept. 22nd with the final report due Oct. 22nd.

- b. The next step is to review the information presented today individually with the stakeholders and obtain feedback as necessary.
- c. Final calculations need to be performed.

End of Minutes

c. Attendees Carl Spirio, P.E., FDOT Drainage Alfredo Rodriguez, P.E., Wantman

SR 710 Stormwater Treatment Area/Regional Pond Feasibility Study Stakeholder Meeting Sign-In Sheet FPID No. 432644-1-32-01 - D1 DW Drainage

Location:

SFWMD Okeechobee Service Center Auditorium

3800 NW 16th Boulevard, Suite A, Okeechobee, FL 34972

Date:

July 31, 2014

Time

10:30 am

NAME	FIRM/AGENCY	OFFICE / RESPONSIBILITY	EMAIL ADDRESS	Initials
Carlton Spirio	FDOT	Drainage	Carlton.Spirio@dot.state.fl.us	
Brent Setchell	FDOT	Permitting	Brent.Setchell@dot.state.fl.us	GES
Amy Setchell	FDOT	PM	Amy.Setchell@dot.state.fl.us	
Kevin Inlge	FDOT		Kevin.lngle@dot.state.fl.us	K51
Jeffrey Mednick	FDOT		Jeffrey. Mednick@dot.state.fl.us	JLM
Michael Hamrick	Property Owner	Hamrick & Sons	MHamrick@manateelegal.com	My
Morris Crady	Lucido & Assoc.	Hamrick & Sons	mcrady@lucidodesign.com	MRC
Maryann Hamrick	Property Owner	Hamrick & Sons	Annie4UF@aol.com	mah
Regina Hamrick	Property Owner	Hamrick & Sons		
Gregory Seidel	The Balmoral Group	Project Drainage Engineer	gseidel@balmoralgroup.us	9M
Jennifer Nunn	The Balmoral Group	Project Drainage Engineer	jnunn@balmoralgroup.us	89
Janet Hearn	ATM	STA Designer	jhearn@appliedtm.com	jul
Henri Belrose	Wantman Group	Consultant PM	Henri.belrose@wantmangroup.com	
Alfredo Rodriguez	Wantman Group	Consultant Asst. PM	Alfredo.rodriguez@wantmangroup.com	AN
Kathy Scott	Okeechobee Co.	Kathy Airport TOC	kscott@co.okeechobee.fl.us	KS
Lee Evett	Okeechobee Co.	0	levett@co.okeechobee.fl.us	10
Jim Threewits	Okeechobee Co.	Adara	jthreewits@co.okeechobee.fl.us	CA
Kelly Baney	Okeechobee Co.		kbaney@co.okeechobee.fl.us	
Katie Hallas	FDEP	PHONE	Katie. Hallas@dep. state.fl.us	
Elizabeth Alvi	FDEP	PHONE	Elizabeth.Alvi@dep.state.fl.us	
Jim Jeffords	USACE		jim.w.jeffords@usace.army.mil	
David Allen	City of Okeechobee		dallen@cityofokeechobee.com	
Lesley Bertolotti	SFWMD		lbertolo@sfwmd.gov	
Duillet Bela	er FDACS		Bonie Wolff Pelage a freshfor	nflori
Regina Hamre	ch			

SR 710 Stormwater Treatment Area/Regional Pond Feasibility Study Stakeholder Meeting Sign-In Sheet

FPID No. 432644-1-32-01 - D1 DW Drainage

Location:

SFWMD Okeechobee Service Center Auditorium

3800 NW 16th Boulevard, Suite A, Okeechobee, FL 34972

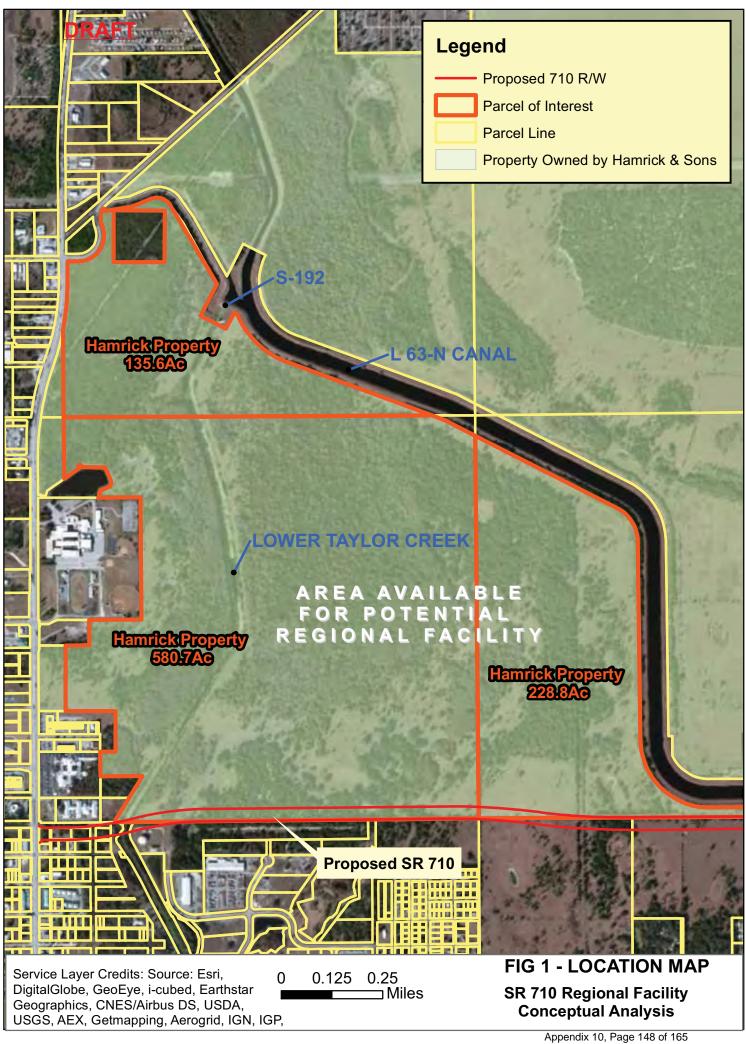
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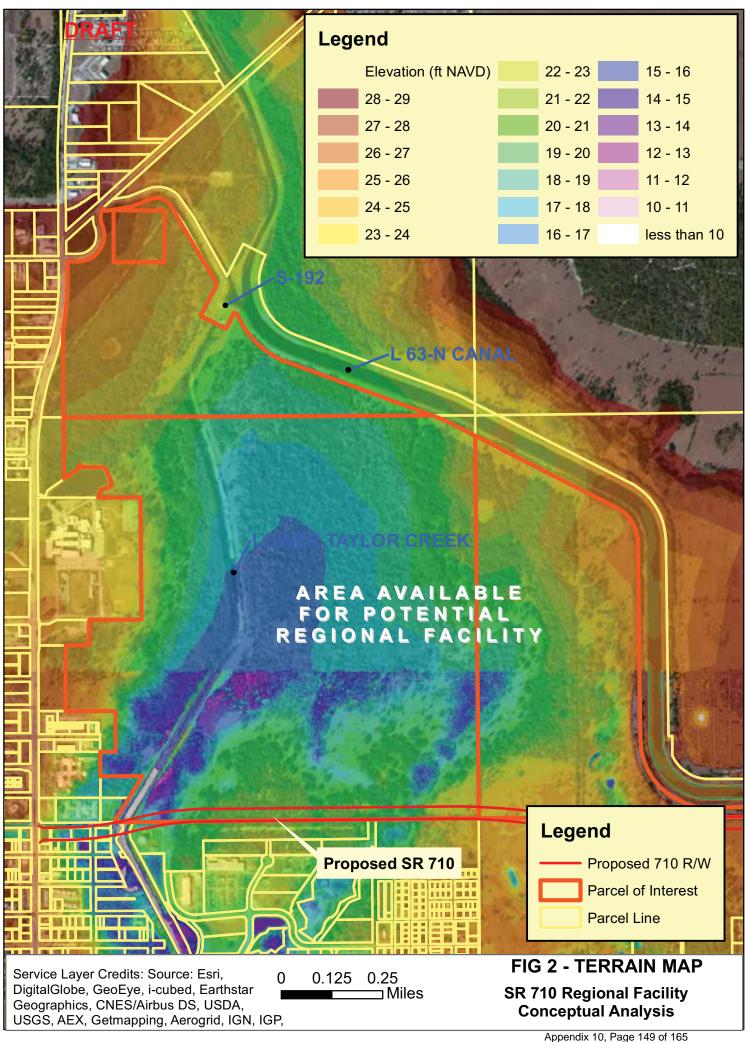
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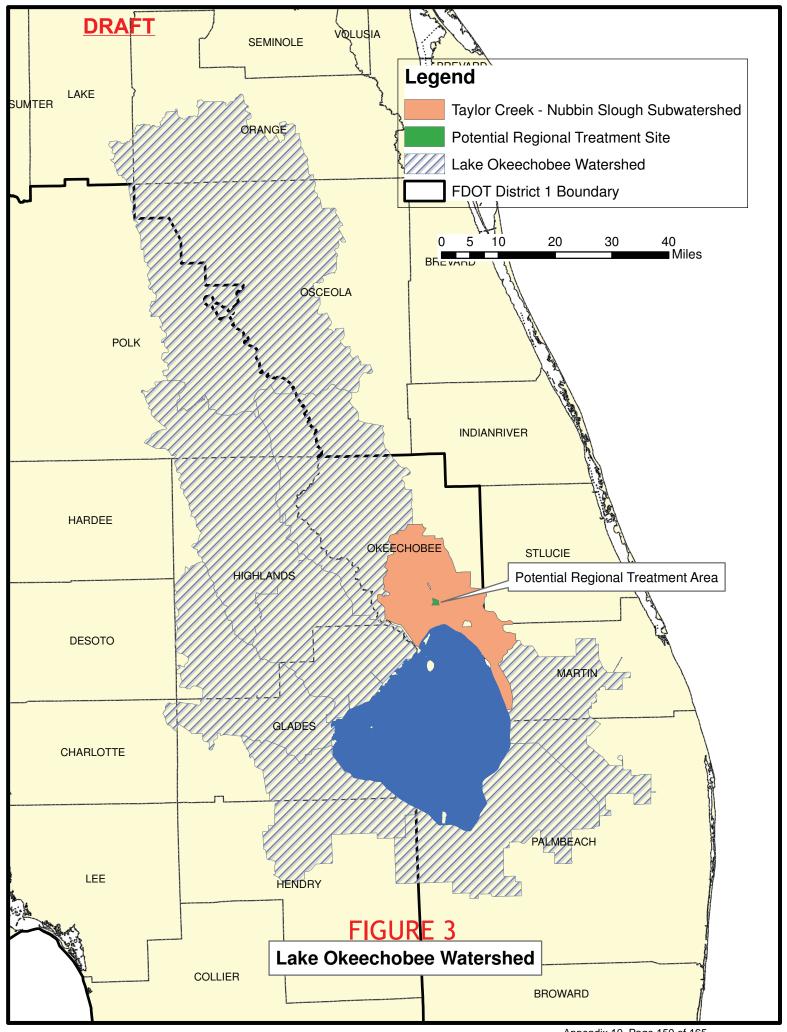
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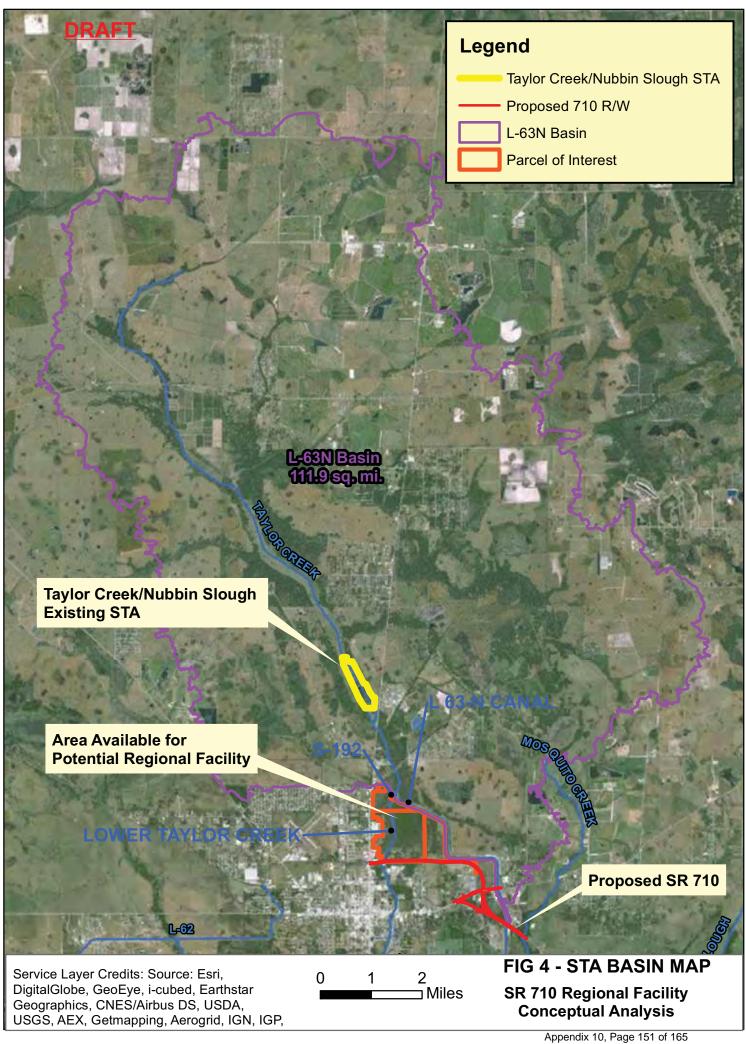
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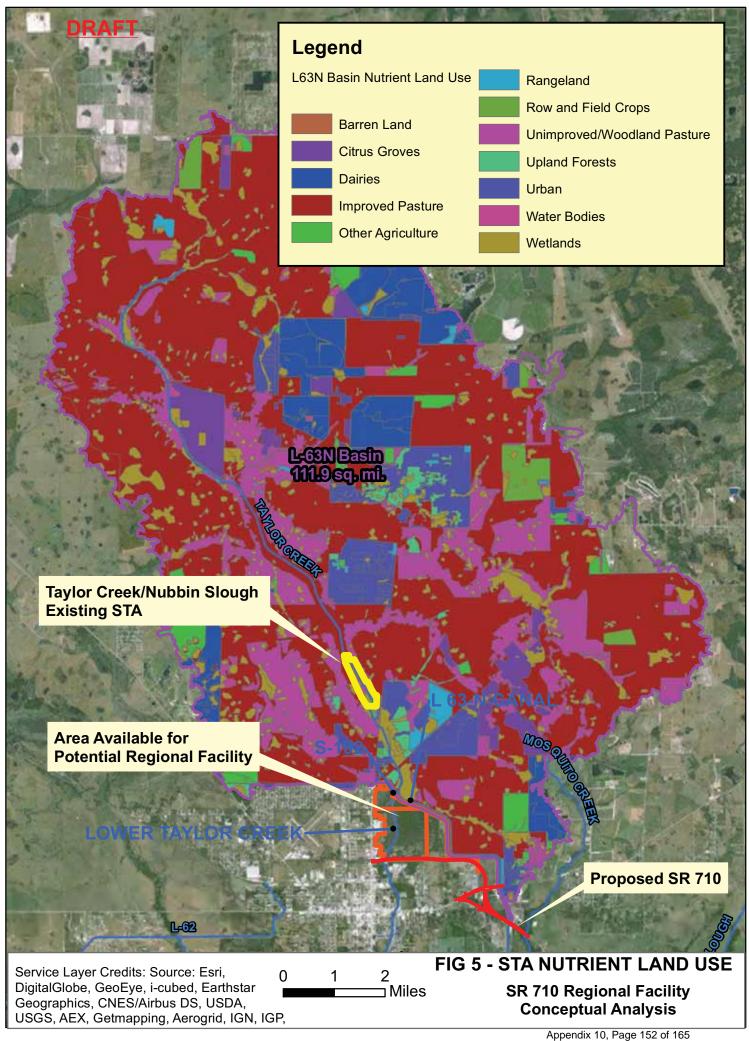
NAME	FIRM/AGENCY	OFFICE / RESPONSIBILITY	EMAIL ADDRESS	Initials
GARY RITTER	SFWMD	INTER GON	gritter @ Stwmd.gov	(4)
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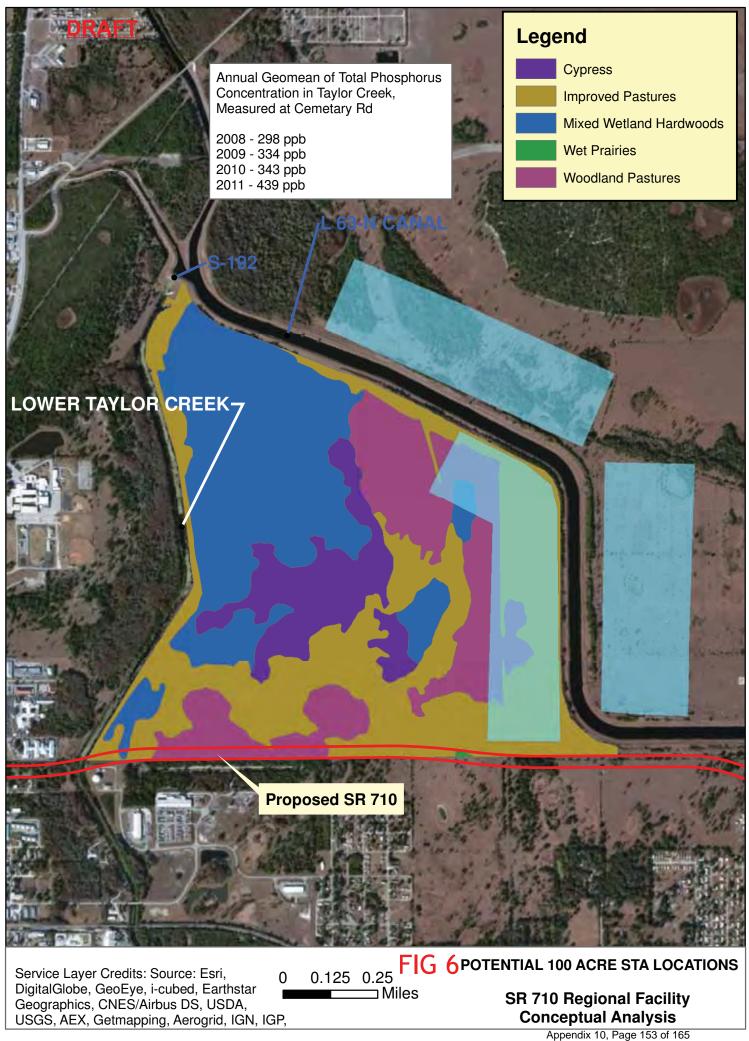


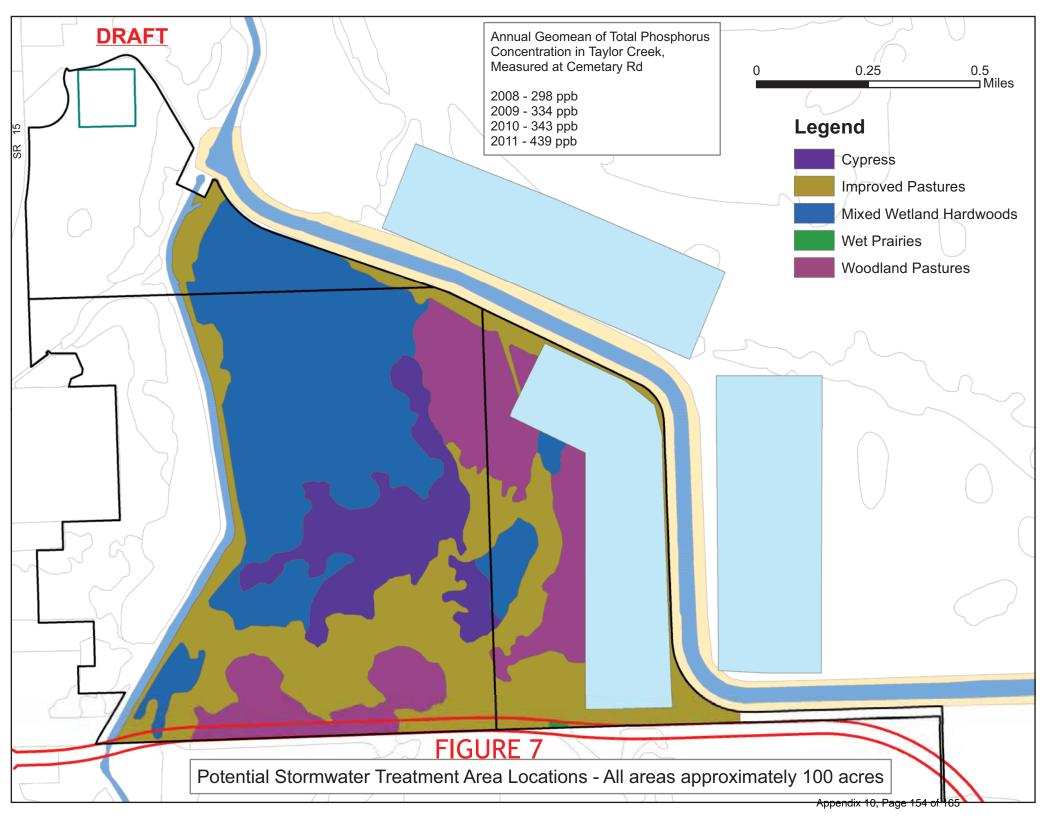


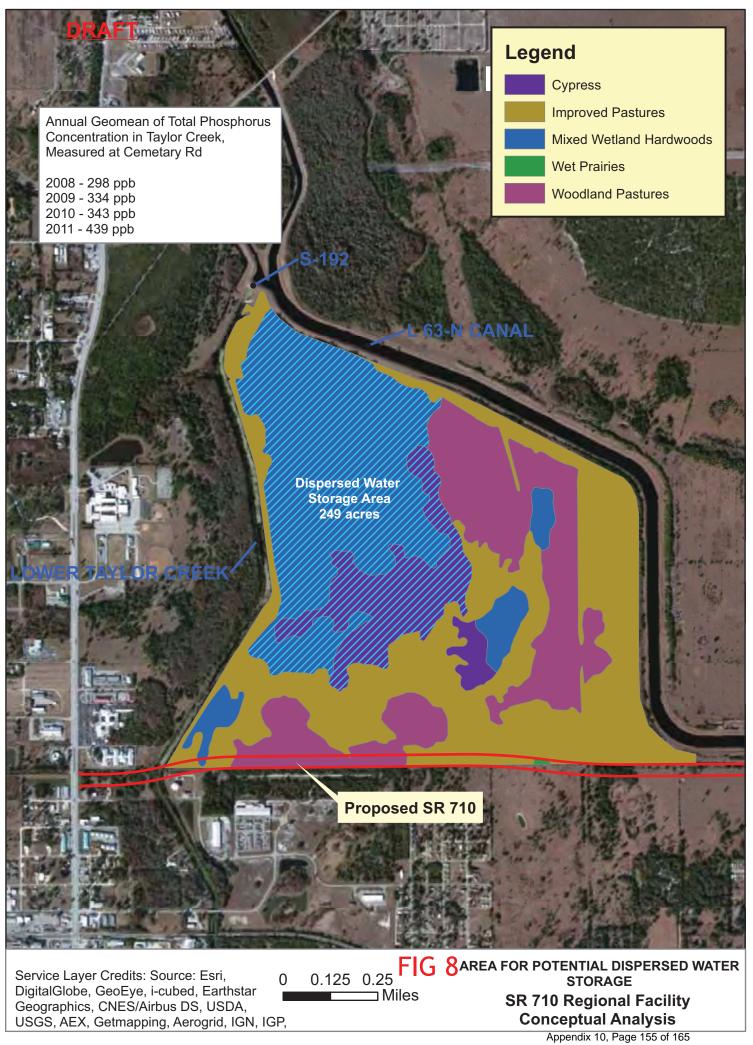


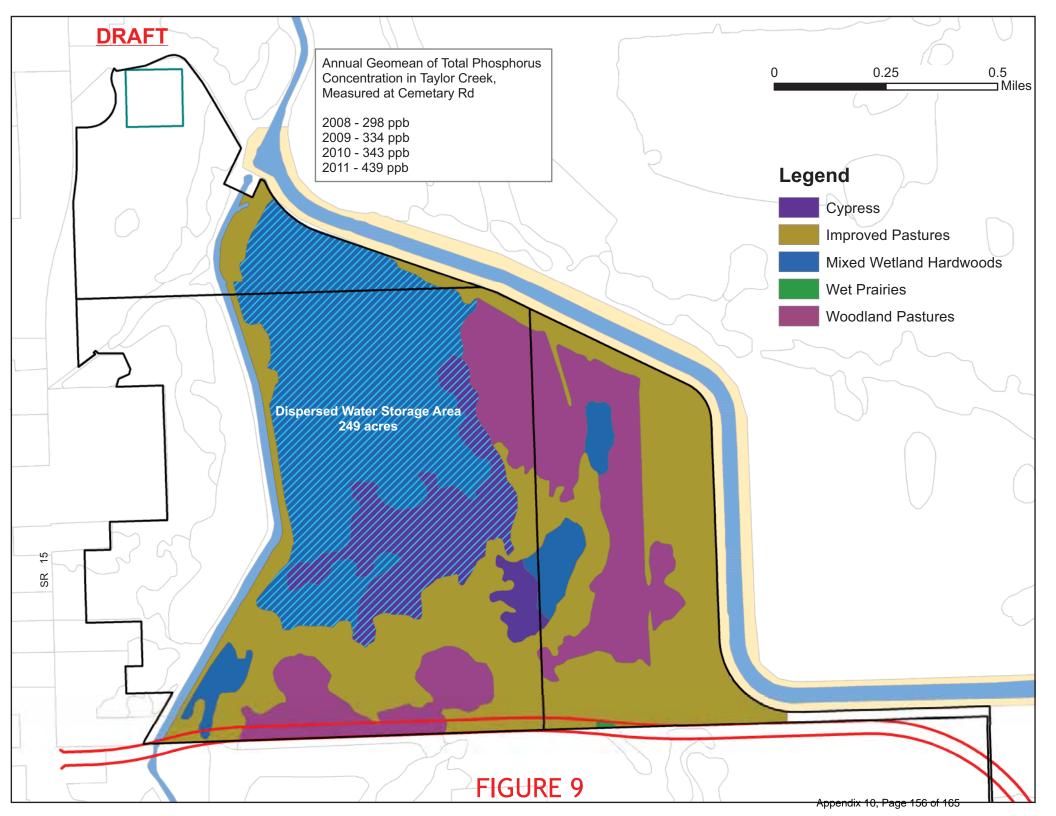


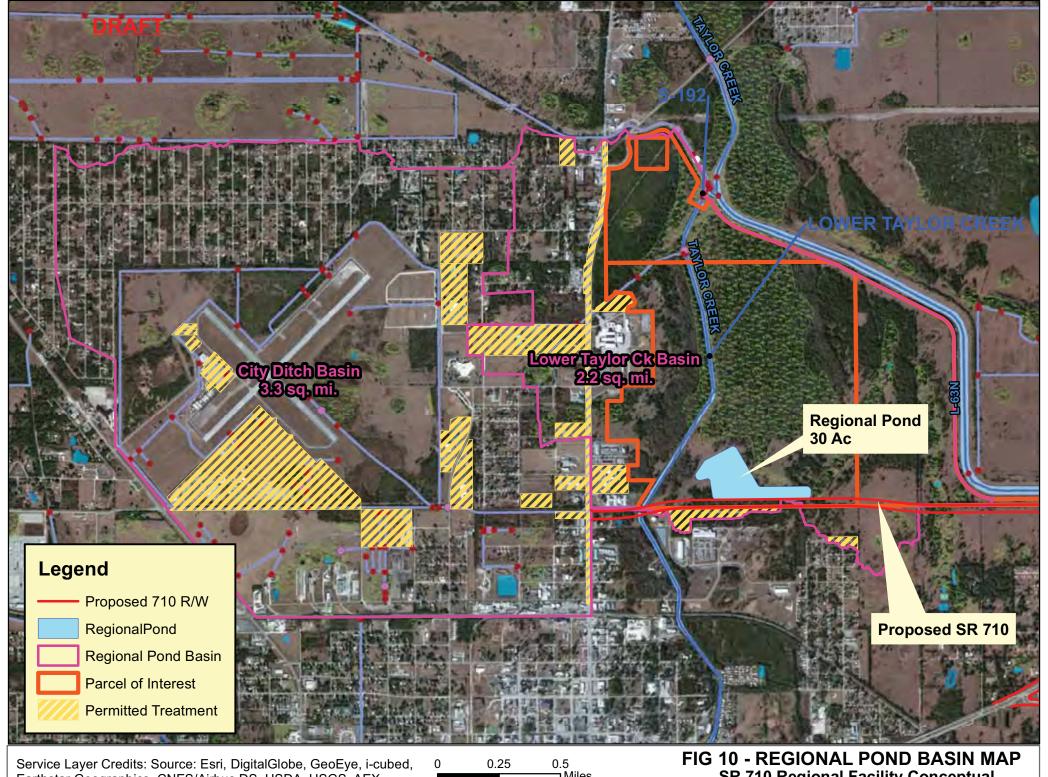










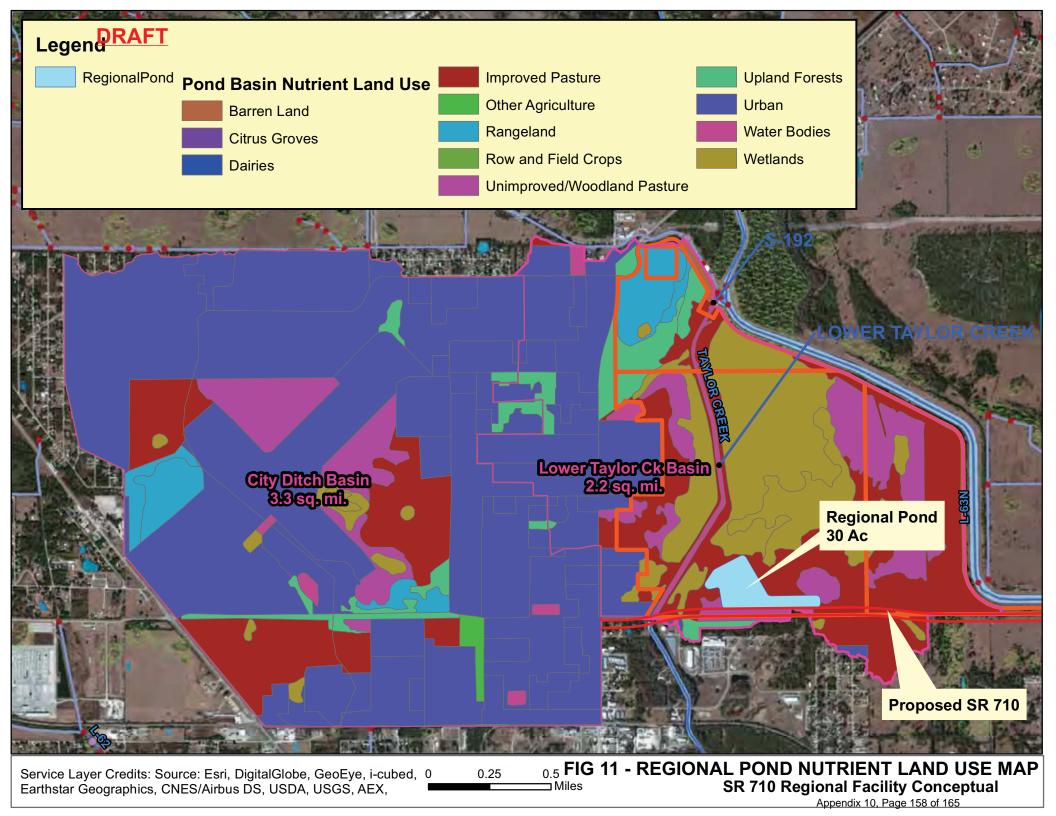


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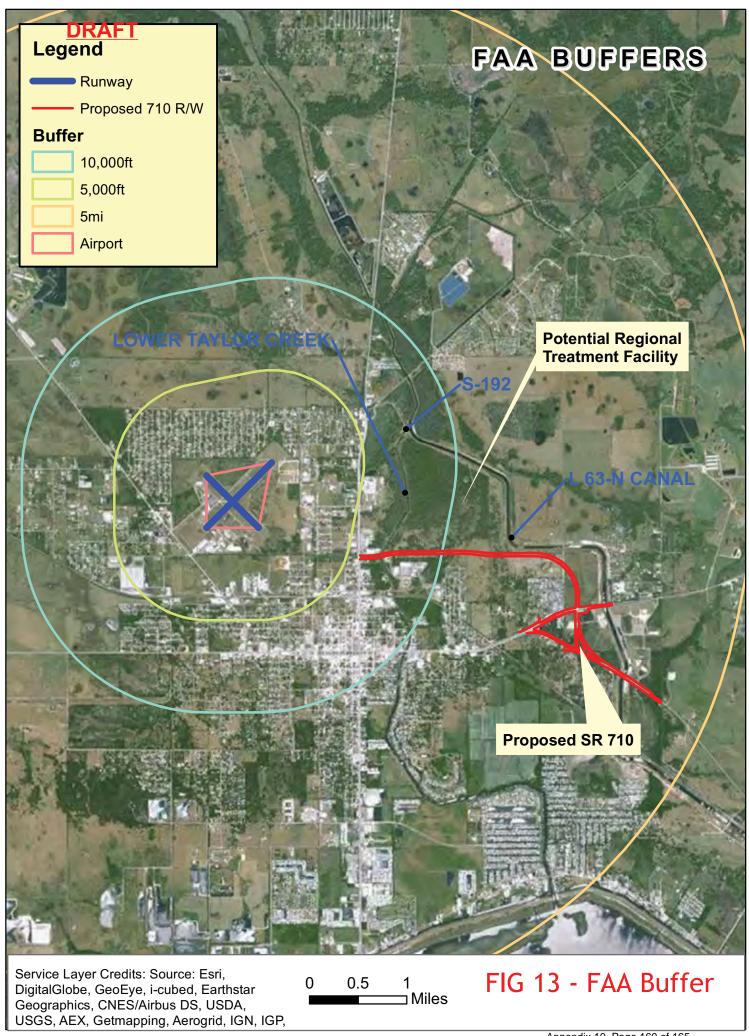
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SR 710 Regional Facility Conceptual

Appendix 10, Page 157 of 165







SR 710 Stormwater Treatment Area/Regional Pond Feasibility Study GOTO Meeting with Mike Hamrick, Property Owner Meeting Minutes FPID No. 432644-1-32-01 - D1 DW Drainage

Location: GotoMeeting
Date: August 12, 2014

Time 9:00 am

By: Greg Seidel Checked By: Janet Hearn

Attendees: Mike Hamrick, Tony Federico, Greg Seidel, Janet Hearn,

- 1. A Gotomeeting was held between Greg Seidel, Janet Hearn, Mr. Hamrick and Mr. Hamrick's consultant, Tony Federico, to advise him regarding pollutant loadings and discharges. Mr. Federico is a principal at Federico, Lamb and Associates and has worked extensively on water quality issues in the Lake Okeechobee basin.
- 2. Greg Seidel went through the Regional Pond/ STA options that are being reviewed by the FDOT and gave a brief project history of SR 710 and how we have gotten to this point. Mr. Federico asked multiple questions for clarification and inquired as to the preliminary loading rate calculations. Janet Hearn will provide preliminary rate calculations for his review.
- 3. Mr. Hamrick indicated that their preferred location for an STA would be in the triangle of land to the north of where Taylor Creek and the L-63 canal diverge but that they have not ruled out any of the other locations presented to date. Greg noted that putting something in the north triangle would be difficult because of the gas line that runs through that portion of the property. Mr. Hamrick said that the easement he negotiated for the gas line is more flexible than the standard easement language and may give FDOT more flexibility. The exhibit developed for the Hamricks that was shown at the stakeholder meeting was just an exhibit to demonstrate a size comparison; it was not a location exhibit.
- 4. Mr. Hamrick said that it is important to maintain the integrity of the property and the current level of use of the property.
- c. Attendees
 Brent Setchell, FDOT
 Carl Spirio, FDOT
 Amy Setchell, FDOT
 Jennifer Nunn, Balmoral Group

Greg Seidel

From: Setchell, Amy < Amy. Setchell@dot.state.fl.us> Sent: Thursday, September 04, 2014 1:25 PM

Mike Hamrick; Greg Seidel; federico@fla-inc.com; JHearn@AppliedTM.com To:

Cc: Setchell, Brent; Spirio, Carlton D; Jennifer Nunn

Subject: RE: SR 710 Regional Pond Hamrick Meeting Minutes.2014.08.12

Mr.sHamrick,s

The Department shase eceived your email and stawill be a coumented as spart of the SR710 Feasibility Study. Wes $appreciate syour participation {\tt mndsinterests} in {\tt shear} o ject {\tt mndso} o ks forward {\tt so} sharing {\tt shear} es ults {\tt so} f {\tt study} with {\tt syou}.$

Thanksyou,s

AmySetchell, P.E.s **Projects**Managers FDOTsDistricts1s 801sN.sBroadwaysAve.s Bartow, FLs33830s P:(863)519-2609s

Email:sAmy.Setchell@dot.state.fl.uss

S S

From: Mikes Hamrick mailto: MHamrick manateelegal.com s

Sent:sThursday, September 94, 2014 1:45 AMs

To:sGregSeidel;sfederico@fla-inc.com;slHearn@AppliedTM.coms Cc:Setchell, & rent; Spirio, Carlton D; Setchell, Amy; slennifer Nunns

Subject: RE: SRs710 Regional Ponds Hamricks Meeting Minutes. 2014.08.12s

S

Greg,ss

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President, sHamrick sons, slnc.ss

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601 12th Street West Bradenton, Florida 34205 mhamrick@manateelegal.com

Phone: (941) 747-1871 Facsimile: (941) 745-2866 www.manateelegal.com

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From: Greg Seidel [mailto:GSeidel@balmoralgroup.us]

Sent: Thursday, September 04, 2014 11:05 AM

To: Mike Hamrick; federico@fla-inc.com; JHearn@AppliedTM.com

Cc: Setchell, Brent (Brent.Setchell@dot.state.fl.us); CARLTON.SPIRIO@DOT.STATE.FL.US; Amy.Setchell@dot.state.fl.us;

Jennifer Nunn

Subject: SR 710 Regional Pond Hamrick Meeting Minutes.2014.08.12

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Regards,s Gregs

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Gregoryl . Seidel, P.E.s
The Balmoral Groups

165sLincolnsAve.s

Winter Park, \$L\$32789s

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Mobile: 407.739.4899 Fax: \$407.629.2183s

e-Mail:<u>gseidel@balmoralgroup.us</u>s Web:<u>shttp://www.balmoralgroup.us</u>s

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SR 710 Stormwater Treatment Area/Regional Pond Feasibility Study SR 710 Conceptual Regional Pond/STA Meeting with Avcon Representing Okeechobee Meeting Minutes

FPID No. 432644-1-32-01 - D1 DW Drainage

Location: AVCON, 5555 E. Michigan Street, Suite 200 Orlando, FL 32822-2779

Date: Thursday, August 14, 2014

Time 3:00pm

Attendees:

1. Greg Seidel - The Balmoral Group, Drainage

- 2. Jim Kriss-AVCON, Principal
- 3. Hilary Maull AVCON, Project Manager-Airports
- 4. Brent Setchell (by phone) FDOT, Project Manager

Purpose: The purpose of the meeting is for The Balmoral Group to present a brief recap of the stakeholder kickoff meeting to the Okeechobee Airport General Consultant and to share information to help determine if the airport may benefit from the project and be a contributing stakeholder should the project move forward.

- 1. Greg Seidel began the meeting by giving a project background to AVCON. Avcon is the general consultant for the Okeechobee County Airport and has developed their master stormwater plan.
- 2. Greg Seidel gave the background review.
- 3. Discussion was held regarding FAA requirements for a new pond within the FAA Wildlife Management Area. Mr. Seidel presented the map showing that the new proposed ponds would lie within this area. It was noted that if the airport got involved the requirements may be more stringent because the FAA dollars would be included in the project.
- 4. Mr. Kriss indicated that there was certainly some possibility for the group to work together and it all seemed very reasonable. The other issue the airport had was they were looking for mitigation credits for wetland impacts to their site. There was a previous worked out deal on the table with a mitigation bank, however that deal fell through and so this is an ongoing issue and the airport is pursuing possible mitigation options.
- 5. The meeting ended with the decision that AVCON would approach the FAA regarding non project specific questions and once those questions were answered they would return to discuss the responses with the FDOT. We would go forward from that point.
- c. Attendees
 Amy Setchell, FDOT
 Carl Spirio, FDOT
 Jim Threewits, Okeechobee County
 Kathy Scott, Okeechobee County
 Kelly Baney, Okeechobee County
 Jennifer Nunn, Balmoral Group

Greg Seidel

From: Jennifer Nunn

Sent: Friday, September 12, 2014 8:24 AM To: Jose Otero (jotero@sfwmd.gov)

Hearn, Janet; Greg Seidel; Ostrovsky, Moysey Cc:

Subject: SR 710 Regional Pond/STA Feasibility Study - SFWMD Operations

Attachments: Location.pdf

Jose,s

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Letsmesknowsfsyoushavesanysquestions.s

Thanks,s

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The Balmoral Group

165 Lincoln Avenue Winter Park, FL 32789 T: 407.629.2185 ext 108

F: 407.629.2183